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Drill Hole Coordinates Vulture Drilling to March 1987

Number	Northing	Easting	Elevation
84-1	26230.00	20673.00	2062.00
84-2	26382.00	20705.00	2052.50
84-3	26321.00	20685.00	2062.00
84-4	26690.62	20705.68	2061.50
84-5	26800.94	20702.63	2068.40
84-6	26710.13	20322.03	2083.80
84-7	26394.00	20242.00	2089.00
84-8	26201.00	20917.00	2051.50
84-9	26376.00	20897.00	2055.00
84-10	26346.16	20511.46	2078.80
84-11	26517.00	20495.00	2065.00
84-12	26391.66	21101.81	2066.00
84-13	26489.00	21462.00	2057.50
84-14	26525.00	21105.00	2066.00
84-15	26516.00	20900.00	2058.50
84-16	26678.84	20501.22	2067.00
84-17	26534.67	20291.90	2103.10
84-18	26240.00	20080.00	2046.50
H-1	26627.00	20755.00	2057.50
H-2	26620.79	21500.26	2062.80
H-3	26376.00	21454.00	2059.00
H-4	26350.00	21340.00	2065.00
H-5	26376.41	21190.68	2070.20
H-6	26421.32	21103.12	2064.80
H-7	26299.00	20899.00	2053.00
H-8	26421.00	20902.00	2055.00
H-9	26158.00	20699.00	2055.00
H-10	26444.00	20702.00	2058.00
H-11	26403.31	20510.54	2074.80
H-12	26304.00	20305.00	2065.80
H-13	26440.00	20820.00	2059.00
H-14	26132.00	21582.00	2071.00
H-15	26394.00	21535.00	2056.00
H-16	26400.58	21017.69	2061.00
H-17	26391.00	20964.00	2057.00
H-18	26324.00	20828.00	2051.00
H-19	26444.00	20823.00	2051.00
H-20	26306.00	20765.00	2051.00
H-21	26442.00	20759.00	2050.00
H-22	26415.10	20640.00	2062.60
H-23	26249.00	20177.00	2056.00
H-24	26333.07	20358.49	2081.30
H-25	26302.00	20435.00	2080.60
H-26	26429.20	20439.16	2080.30
H-27	26444.00	20362.00	2081.00
H-28	26566.48	20378.26	2085.30
H-29	26731.74	20516.51	2068.50
H-30	26664.80	20648.57	2064.50
H-31	26690.00	21815.00	2058.00
H-32	26381.94	21412.97	2060.30
H-33	26601.00	20979.00	2060.00

H-34	26659.00	20860.00	2053.50
H-35	26384.13	20558.89	2069.10
H-36			
H-37			
H-38			
H-39			
H-40	26335.00	22045.00	2050.40
H-41	26240.00	21420.00	2079.50
H-42	26235.00	21018.00	2061.40
H-43	26234.21	20559.46	2082.30
H-44	26524.26	20420.06	2074.70
H-45	26461.04	20595.10	2064.80
H-46	26516.49	20823.00	2054.50
H-47	26460.18	20979.87	2059.40
H-48	26507.36	21187.47	2063.40
H-49	26495.45	21546.02	2055.50
H-50	26100.00	21300.00	2087.70
H-51			
H-52			
H-53	26160.00	21730.00	2084.70
H-54	26195.00	21560.00	2080.00
H-55	26235.00	20760.00	2050.40
H-56	26180.00	20630.00	2056.40
H-57	26230.00	20240.00	2058.30
H-58	26515.00	21520.00	2056.80
H-59	26422.76	21590.27	2051.30
H-60	26554.95	21626.38	2056.50
H-61	26411.49	21670.85	2019.60
H-62	26424.10	21741.18	2018.30
H-63	26441.93	21809.58	2013.80
M-1	26382.18	21523.39	2058.00
M-2	26415.00	20621.00	2061.00
M-3	26130.00	21587.00	2072.90
DH-1	26119.00	21402.00	
DH-5	26377.00	20549.00	2067.00
DH-7	26581.00	21394.00	2056.50
DH-8	26708.00	21804.00	2058.00
DH-67	26474.00	20702.00	2062.00
DH-87	26277.00	20302.00	2071.00
DH-88	26317.00	20402.00	2076.00
DH-89	26386.00	20482.00	2081.00
DH-90	26260.00	20555.00	2084.00
DH-91	26356.00	20982.00	2060.00
DH-92	26430.00	21159.00	2066.00
DH-93	26439.00	21312.00	2060.00
DH-94	26464.00	21467.00	2057.00
DH-E	26692.00	21753.00	2058.50

HUGH M. HARRIS DRILLING COMPANY

Drilling Contractors Since 1956
11650 IBERIA PLACE, SUITE N-1 / SAN DIEGO, CALIFORNIA 92128-2479
Telephone (619) 487-5136

October 14, 1986

DMEA Ltd.,
7340 East Shoeman Lane
Suite 111 "B"
Scottsdale, Arizona 85251

DMEA LTD.
OCT 17 1986
RECEIVED

APPLICATION FOR PAYMENT

Re: Vulture Mines, Arizona
Our Number 86-33
Rig Number 1 - Anderson Driller

Services Rendered - September 27, 1986 thru October 7, 1986:

Angle Hole Number H-36:
Drilled 0-100TD = 100 ft.

Angle Hole Number H-37:
Drilled 0-100TD = 100 ft.

Angle Hole Number H-38:
Drilled 0-99TD = 99 ft.

Angle Hole Number H-39:
Drilled 0-80TD = 80 ft.

Angle Hole Number H-40:
Drilled 0-80TD = 80 ft.

Angle Hole Number H-41:
Drilled 0-90TD = 90 ft.

Angle Hole Number H-42:
Drilled 0-80TD = 80 ft.

Angle Hole Number H-43:
Drilled 0-90TD = 90 ft.

Angle Hole Number H-44:
Drilled 0-170TD = 170 ft.

Angle Hole Number H-45:
Drilled 0-120TD = 120 ft.

Angle Hole Number H-46:
Drilled 0-175TD = 175 ft.

Angle Hole Number H-47:
Drilled 0-150TD = 150 ft.

Angle Hole Number H-48:
Drilled 0-190TD = 190 ft.

Angle Hole Number H-49:
Drilled 0-140TD = 140 ft.

Vertical Hole Number H-50:
Drilled 0-60TD = 60 ft.

Angle Hole Number H-51:
Drilled 0-150TD = 150 ft.

Angle Hole Number H-52:
Drilled 0-80TD = 80 ft.

Vertical Hole Number S-1:
Drilled 0-60TD = 60 ft.

Vertical Hole Number S-2:
Drilled 0-78TD = 78 ft.

Vertical Hole Number S-3:
Drilled 0-80TD = 80 ft.

Core Hole Number M-1:
Drilled 0-25 = 25 ft.
Cored 25-34 = 9 ft.
Reamed 27-34 = 7 ft.
Cored 34-44 = 10 ft.
Reamed 34-44 = 10 ft.
Cored 44-46 = 2 ft.
Reamed 44-46= 2 ft.
Cored 46-54'5" = 5'5"
Reamed 46-54'5"
Cored 54'5"-85TD = 30'7"

Core Hole Number M-2:
Drilled 0-11 = 11 ft.
Cored 11-32 = 21 ft.
Reamed 11-32 = 21 ft.
Cored 32-40 = 8 ft.
Reamed 32-40 = 8 ft.
Cored 40-50 = 10 ft.
Reamed 40-50= 10 ft.
Cored 50-58 = 8 ft.
Reamed 50-58 = 8 ft.
Cored 58-60TD = 10 ft.

Core Hole Number M-3:
Drilled 0-14 = 14 ft.
Cored 14-31 = 17 ft.
Reamed 14-31= 17 ft.
Cored 31-40TD = 9 ft.

Vertical Hole Number H-53:
Drilled 0-60TD = 60 ft.

Vertical Hole Number H-54:
Drilled 0-60TD = 60 ft.

Vertical Hole Number H-55:
Drilled 0-60TD = 60 ft.

Vertical Hole Number H-56:
Drilled 0-60TD = 60 ft.

Vertical Hole Number H-57:
Drilled 0-60TD = 60 ft.

Vertical Hole Number H-58:
Drilled 0-160TD = 160 ft.

Vertical Hole Number S-4:
Drilled 0-50TD = 50 ft.

Vertical Hole Number S-5:
Drilled 0-35TD = 35 ft.

Vertical Hole Number S-6:
Drilled 0-50TD = 50 ft.

Footage Rates:		
Angle 0-400 = 1,894 ft. @ $6.50 per ft.	$12,311.00	
Vertical 0-400 = 873 ft. @ $5.50 per ft.	$ 4,801.50	
Total Footage Charges		$ 17,112.50
Core Holes - Hourly Rates:		
9-30-86 - 5 1/2 Hours		
10- 1-86 - 11 1/2 Hours		
10-2-86 - 12 Hours		
10-3-86 - 11 Hours		
10-4-86 - 11 1/2 Hours		
10-5-86 - 12 Hours		
10-6-86 - 2 1/2 Hours		
Total Hours - 66 @ $145.00 per hour		$ 9,570.00
Core Drill Bits and Accessories:		
1 - 8 x 5.875 Core Bit, Serial Number 6S4191 (Christensen Invoice Number 660149 - copy attached)	$ 2,745.00	
1 - Core Lifter and Shoe (Christensen Invoice No. 660131 & 660176 copies attached)	405.80	
1 - 8 5/8" Megabit, Serial No. V9673 (50% chargeable-Ross Equipment Invoice No. 13782-copy attached)	667.75	
Total Drill Bits and Accessories		$ 3,818.55
Core Muds and Chemicals:		
4 - Casting Plaster @ $17.81 per sk.	$ 71.24	
2 - Sks. Gel @ $8.08 per sk.	16.16	
35- Gals. Quik Foam @ $14.31 per gal.	500.85	
5 - Gals. Ez Mud @ $22.89 per gal.	114.45	
10- Gals. Polymer @ $26.40 per gal.	264.00	
10- Gals. Stafoam @ $14.30 per gal.	143.00	
2 - Car Wax for Core Barrel @ $10.79 ea.	21.58	
Total Core Muds and Chemicals		$ 1,131.28
TOTAL AMOUNT NOW DUE FOR RIG NUMBER ONE		$31,632.33

VULTURE Drill Hole Survey

10/15 + 10/21

BM 829
ELEV = 2050.09

STA	BS	∡ RT	FS	DIST	ELEV
CP 1	829	65°01'		410	2050.09 ✓
			CP2	425	2053.67 ✓
CP 2	CP1				
		198°18'	H-40	244	2050.38 ✓
		180°21	CP-3	404	2080.60 ✓
CP 3	CP2				
		175°51'	H-53	180	2084.65 ✓
H-53	CP3				
		186°58'	M-3	147	2072.90 ✓
		209°41'	H-54	172	2080.15 ✓
		212°24'	H-41	~~319~~ 219	2079.53 ✓
		188°26'	CP-4	~~620~~ 420	2088.77 ✓
CP-4	H-53				
		229°0'	H-50	135	2087.72 ✓
		359°19'	① LS5429	80	—
		196°05'	CP5	337	2053.86 ✓
CP-5	CP-4				
		283°14'	H 42	115	2061.38 ✓
		199°35'	H55	240	2050.37 ✓
		295°00'	CP6	189	2076.46 ✓
CP-6	CP5				
		44°07'	H56	460	~~2085.50~~ 2056.4 ✓
		52°14'	H43	~~425~~ 520	2081.06 ✓
		77°49'	H45	520	2063.67 ✓
		74°11'	M-2	470	2061.01 ✓
		117°35'	H-47	197	2058.21 ✓

Vulture Drill Hole Survey 10/15 + 10/21

STA	BS	∡ RT	FS	DIST	ELEV.
CP 6	CP5	0°00'			2076.46 ✓
		77°48'	H-45	516	2063.71 ✓
		78°04'	H-44	704	2073.70 ✓
		99°23'	H-46	340	2053.97 ✓
		64°15'	84-10	576	2077.97 ✓
		212°55'	CP-7	112	2075.79 ✓
CP 7	CP6	0°00'			2075.79 ✓
		118°08'	H48	166	2062.76 ✓
		199°15'	M-1	345	2057.57 ✓
		183°29'	H 49	400	2054.82 ✓
		178°40'	H58	386	2056.82 ✓
		186°51'	CP 8	560	2063.53 ✓
H43	CP6	0°00'			2081.06 ✓
		185°45'	H 57	310	2058.34 ✓
		223°56'	H-25	154	2080.66 ✓
		254°22'	84-10	122	
CP8	CP7	0°00'			
		218°21'	CP-2	610	2052.88 ✓
					(2053.67) Δ 0.79
CP2	CP3	0°00'			
		33°26'	CP 8		

7 ∡'s − 1 = 3

3 × 36 = 1080°00'

TOTAL ∡'s = 1079°57'

Δ = 0°03'

Vulture Hole Survey 10/21

STA	BS	∡ RT	FS	DIST		Δ ELEV	
CP6	CP5	0°00'					HI = CP6 + 5.55
		77°48'	H-45	11	13.58 (x2)	-13.58	-0°30' V∡
		78°04'	H-44	5.02	1.50 (x2)	-5.02	-0°15' V∡
		99°23'	H-46	14	12.3 (x2)	-14.0	-2°20' V∡
		64°15'	84-10	3.82	6.7 (x2)	-3.82	0°0' V∡
		212°55'	CP-7	5.44	6.56	-6.00	0°0' V∡
CP-7	CP6	0°00'					HI CP7 + 5.21
		118°08'	H48	11.62	13.28	-12.45	V∡ -2°0' .579
		199°15'	M-1	3.65	7.10	-5.37	V∡ -3°0'
		183°29'	H49	12.8	14.8 (x2)	-12.8	V∡ -1°55'
		178°40'	H-58	12.15	14.08 (x2)	-14.08	V∡ -1°30'
		186°51'	CP8	4.9	10.5	-7.7	V∡ -1°00'
H43	CP6	0°00'					HI H43 + 5.50
		185°45'	H57	3.9	5.45 (x2)	-3.9	-4°30' V∡
		223°56'	H25	5.13	6.67	-5.90	0°—
CP8	CP7	0°00'					HI = CP8 + 4.50
		218°21'	CP2	1.45	7.55	-4.50	-1°00' V∡
CP2	CP3	0°00'					
		33°26'	CP8				

	BS	∡	FS	DIST			
CP1	829	0°00'		8 8^{89}	10^{92}	12^{97}	N 2°30' W
		65°01'	CP2				
				5^{00}	7^{13}	9^{25}	=425
CP8	CP7	0°00'		4^{52}		5^{94}	7^{35} =283
		118° 33'	316				
CP2	CP1	0°00'					
		180°22'	CP3	1^{10}		3^{10}	5^{15} = 405'
H43	CP6	0°00'		6^{70}	9^{3}	11^{90}	= 520
		185°44'	H 51	11^{48}	13^{00}	14^{55}	= 307
		223°55'	H 25	4^{75}	5^{52}	6^{30}	= 155
		254°22'	84-10	10^{40}	11^{00}	11^{62}	= 122

STA	BS	∡ RT	FS	DIST	ELEV	
						HI = CP6 + 5.0
CP6	CP5	44°07'	H-56	5.7 10.3	-8	v ∡ 1°30'
		52°14'	H43	~~1.4 5.65~~ 8.20	-0.4	
		~~72°~~ 71°49'	H45	10.65 15.85 *	-13.25	v ∡ -0°30'
		74°11'	M-2	3.7 8.4	-6.1	v ∡ -1°45'
		117°35'	H47	5.09 7.07	-6.08	v ∡ -5°0'

∡
13.25
10.65
2.60

Vulture Drill holes 10/14 AIF AND JOSE ONTIVEROS

STA	BS	∡ RT	FS	DIST		Δ ELEV		
CP1	IP		~~CP2~~	13^{05}	8^{75}	$+11^{0}$		
		65°01'	CP2	9^{55}	5^{30}	-7^{42}		
CP2	CP1	-					HI	CP2 ELEV. $+5^{23}$
		198°18'	H-40 ~~CP3~~	9^{74}	7^{30}	-8^{52}		
		180°21'	CP3	8^{50}	4^{45}	-6^{48}	V ∡ 4°0'	
CP3	CP2	175°51'	H53	6^{05}	4^{25}	-1^{0}	HI	CP3 ELEV. $+5^{05}$
H 53	CP3	186°58'	M-3	14^{47}	13^{0}	-13^{73}	V ∡ −1°0'	H53 HI $+4^{55}$
		209°41'	H54	9^{92}	8^{20}	-9^{05}		
		212°24'	H41	7^{58}	10^{77}	-9^{67}		
		188°26'	CP4	0	6^{2}	-4^{10}	V ∡ +0°30'	
CP4	H53	229°0'	H50 ~~H53~~	$\boxed{13^{5}}$		-6^{05}		CP4 HI $+5^{0}$
		359°19'	1 ~~H55~~ 429	48^{8}	4^{08}			
	where is Hole 50?	196°05'	CP5	8^{85}	12^{23}	-10^{53}	V ∡ −5°	
CP5	CP4	283°14'	H42	1^{13}	2^{28}	-1^{70}	V ∡ +2°	CP5 HI $+5^{2}$
		199 35'	H55	1^{2}	3^{6}	-2^{41}	V ∡ −1°30'	
				~~5^{64}~~	~~-5^{44}~~			
		295°00	CP6	4^{68}	6^{58}	-5^{64}	V ∡ +7°0'	

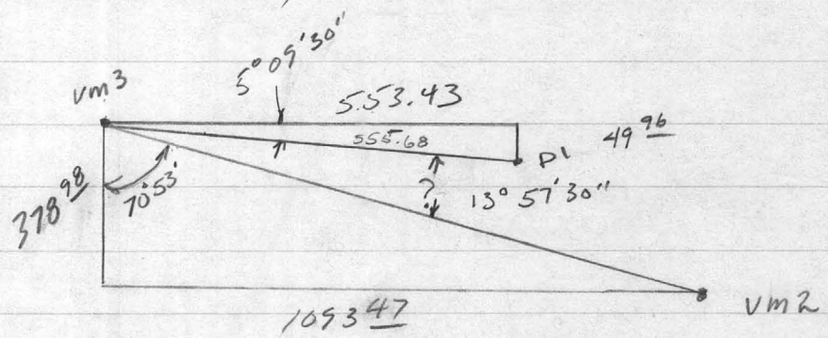
CP 3 – CP 4 ?

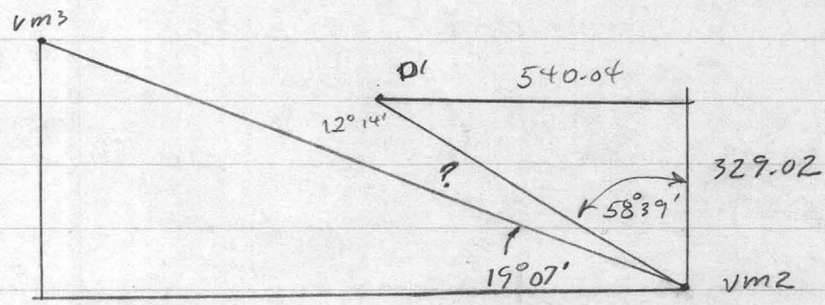
	BS	IS	∠ RT	FS
	VM 3			
D1 = 0+00 on ℄		D1	272° 40'	3+50
			206° 39'	VM2

	N	E	ELV
VM3	26 579.96	20 251.57	2109.8
	378 98	1093 47	
VM2	26, 200.98	21, 345.04	2098.2
D1	26 530 00	20 805 00	2054 05

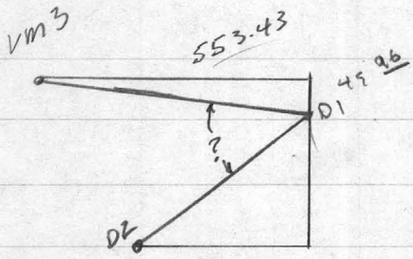
BS VM2, IS VM3, TURN 13° 57'30" LEFT TO 555.68 Feet TO STATION D1

BS VM3, I VM2, TURN 12° 14' RT, 632.37 FEET TO STATION D1





	N	E	ELEV
VM3	26,579.26	20251.57	2109.8
	49.96	553.43	
		650	
D1	26,530.00	20,~~805~~.00	2054.05
	430.00	155	
D2	26 100.00	20 650.00	

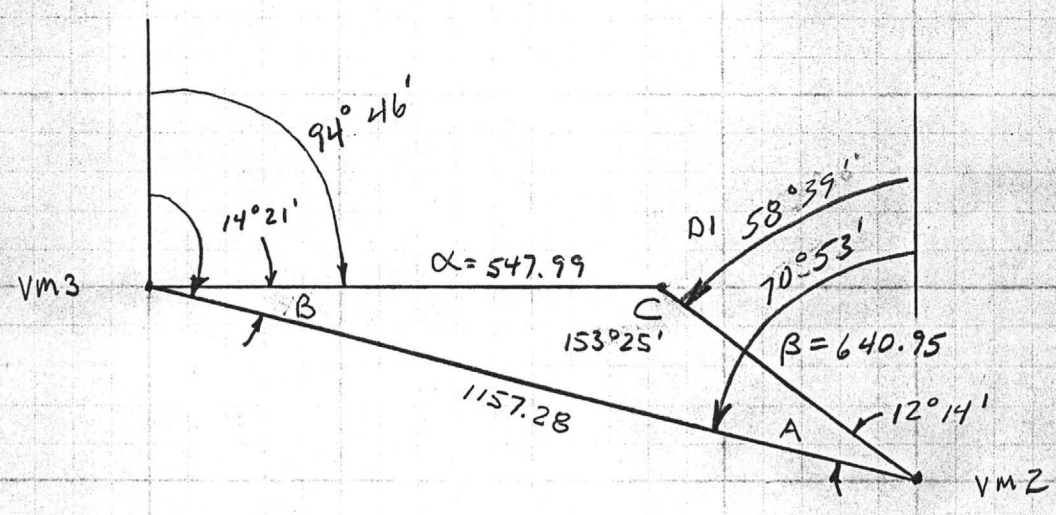


Vulture | Diversion Survey | 10/12/87

VM 2	26,200.98 N	21,345.04 E	2098.2
	-378.98	1093.47	
VM 3	26,579.96 N	20,251.57 E	2109.8

VM2 - VM3 - D1 < 14°21' N

VM3 - VM2 - D1 < 12°14' N



$$\frac{\sin 153°25'}{1157.28} = \frac{\sin 14°21'}{\beta}$$

$\beta = 640.95$

$$\frac{\sin 153°25'}{1157.28} = \frac{\sin 12°14'}{\alpha}$$

$\alpha = 547.99$

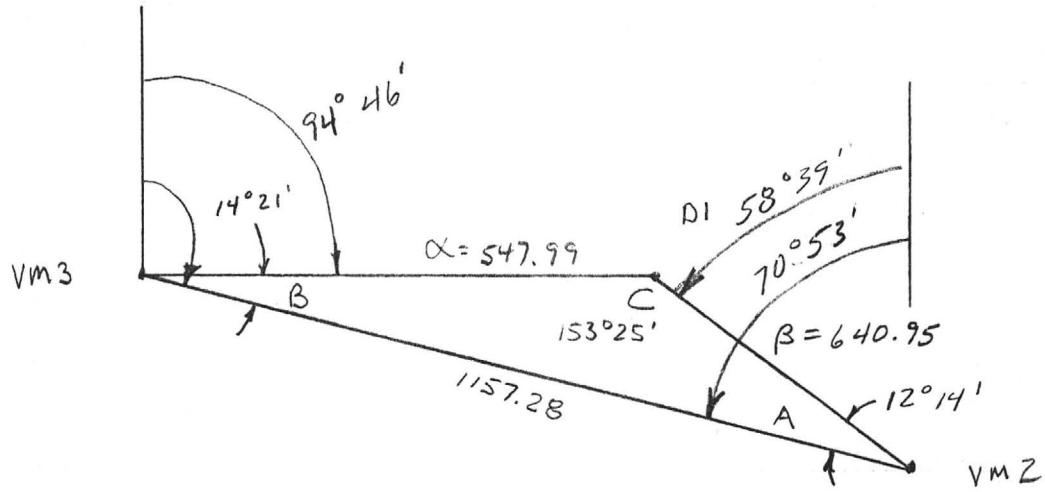
VM 3	26,579.96 N	20,251.57 E
	-45.53 N	+ 546.10 E
D1	26,534.43 N	20,797.67 E
VM2	26,200.98 N	21,345.04 E
	333.46	- 547.37 E
D1	26,534.44 N	20,797.67 E

CHECK

VM 2	26,200.98 N	21,345.04 E	2098.2
	-378.98	1093.47	
VM 3	26,579.96 N	20,251.57 E	2109.8

VM2 - VM3 - D1 < 14°21' N

VM3 - VM2 - D1 < 12°14' N



$$\frac{\sin 153°25'}{1157.28} = \frac{\sin 14°21'}{\beta}$$

$\beta = 640.95$

$$\frac{\sin 153°25'}{1157.28} = \frac{\sin 12°14'}{\alpha}$$

$\alpha = 547.99$

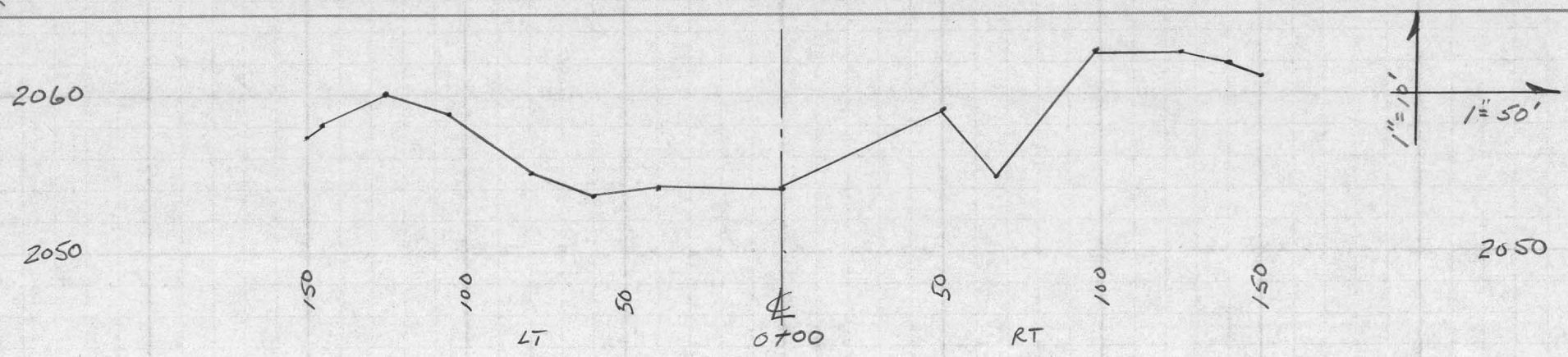
VM 3	26,579.96 N	20,251.57 E
	-45.53 N	+ 546.10 E
D1	26,534.43 N	20,797.67 E
VM 2	26,200.98 N	21,345.04 E
	333.46	- 547.37 E
D1	26,534.44 N	20,797.67 E

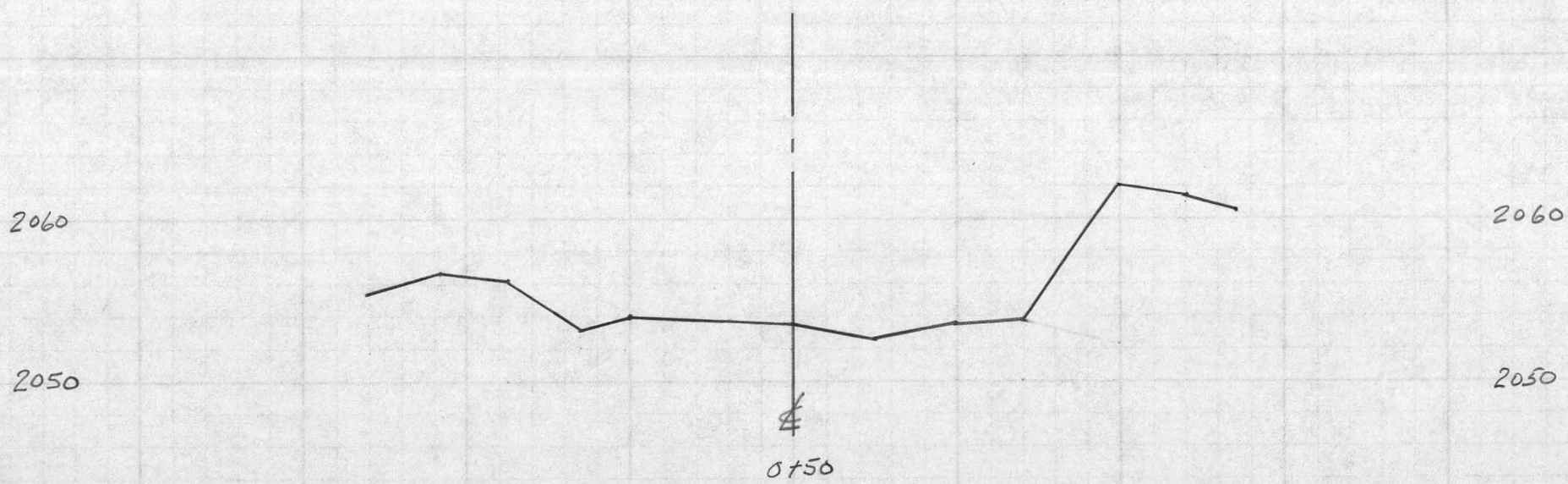
CHECK

1/14

10/23/87

DIVERSION X-SECTIONS





LOOKING UP STATION

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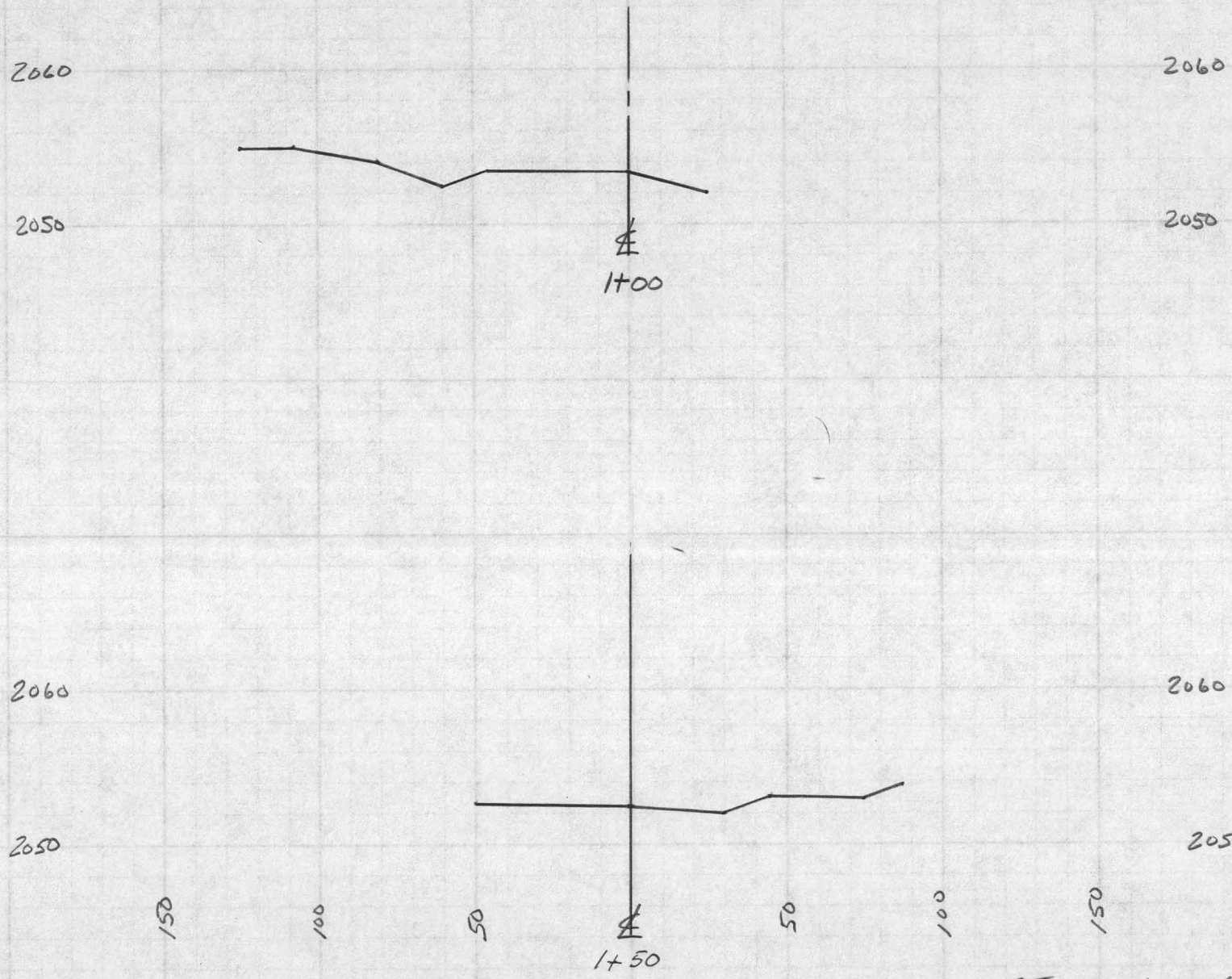
10/23/97

X-SECTIONS

Vulture - Diversion



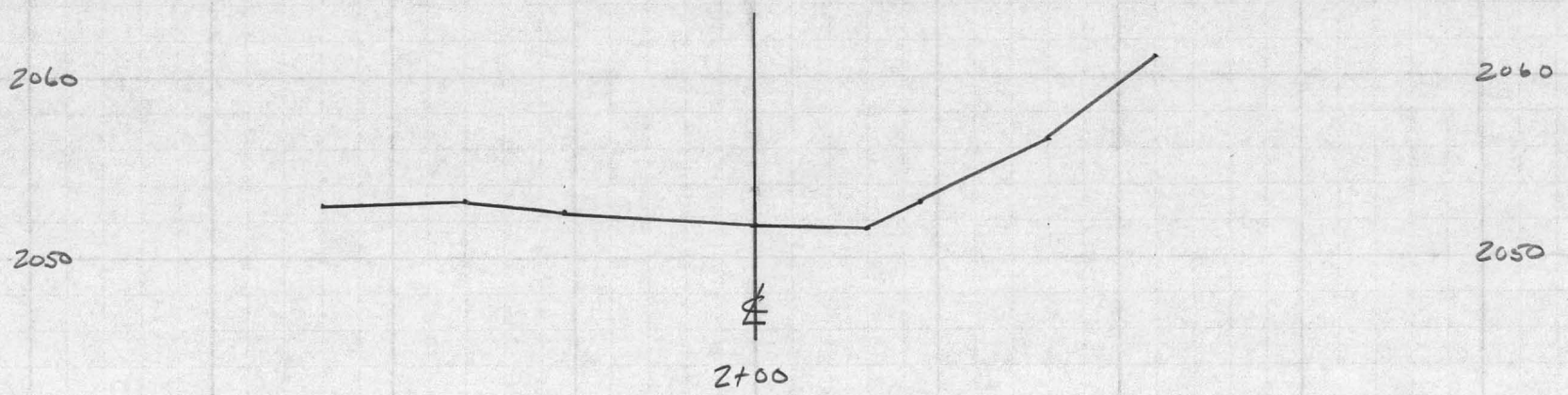
1" = 10' VERT.
1" = 50 HORZ.

3/14

10/23/87

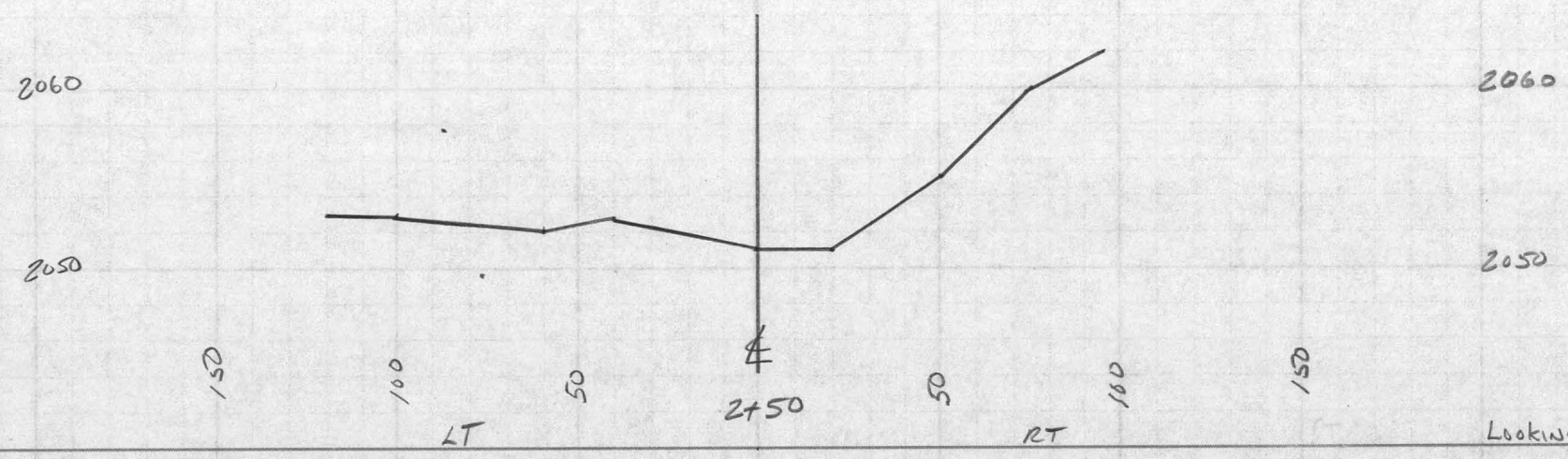
X-SECTIONS

VULTURE- DIVERSION



1" = 10' VERT

1" = 50' HORZ.



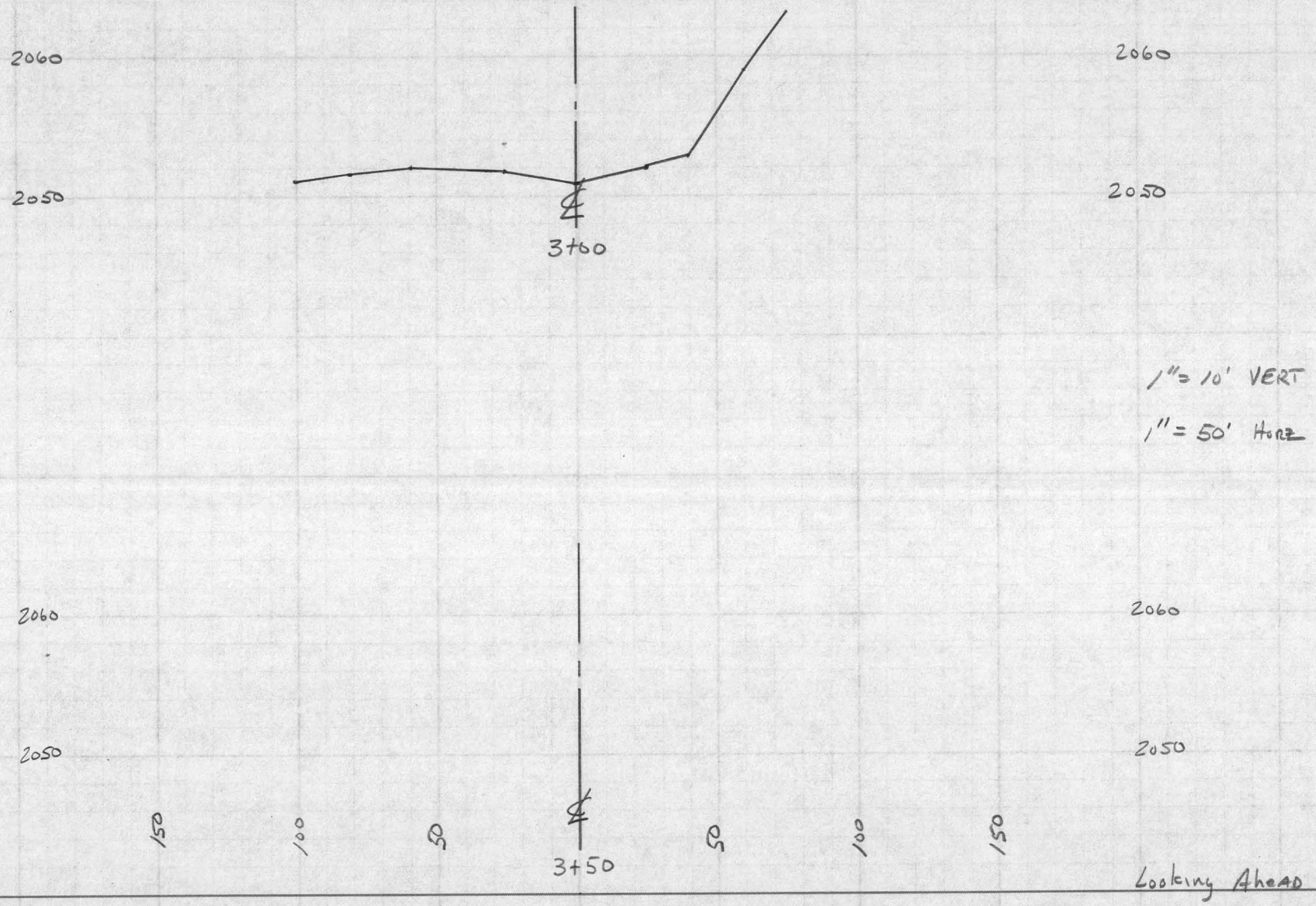
Looking AHEAD

4/14

10/23/87

X-SECTIONS

Vulture - Diversion



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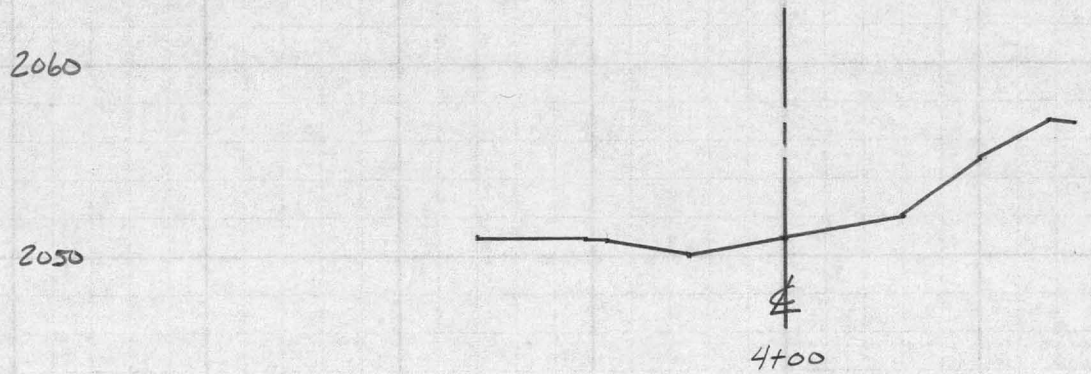
10/23/87

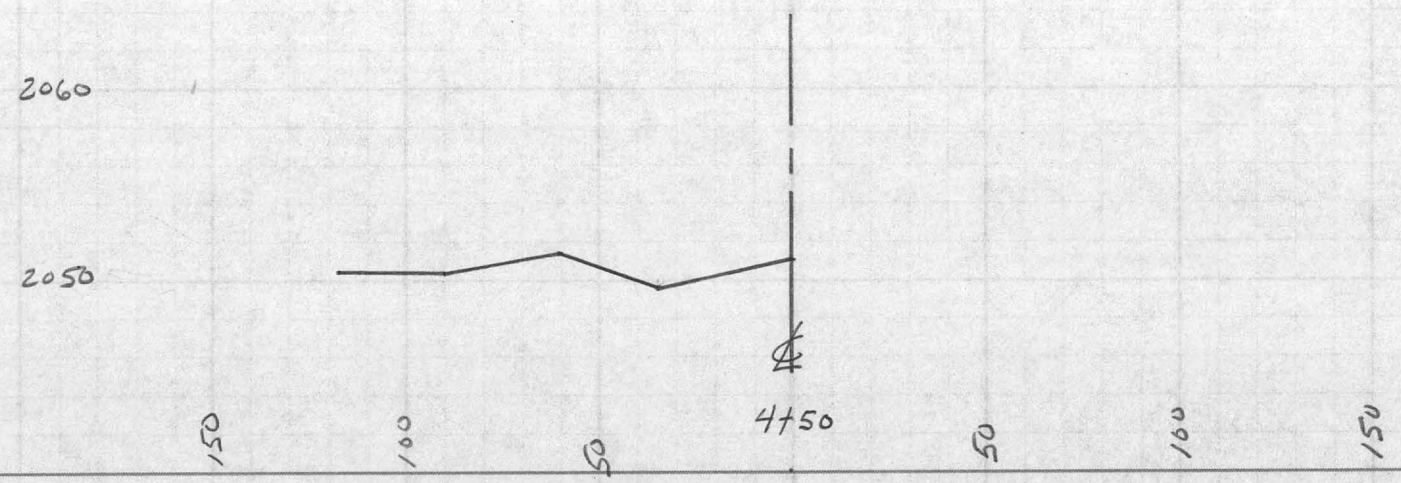
X-SECTIONS

Vulture-Diversion



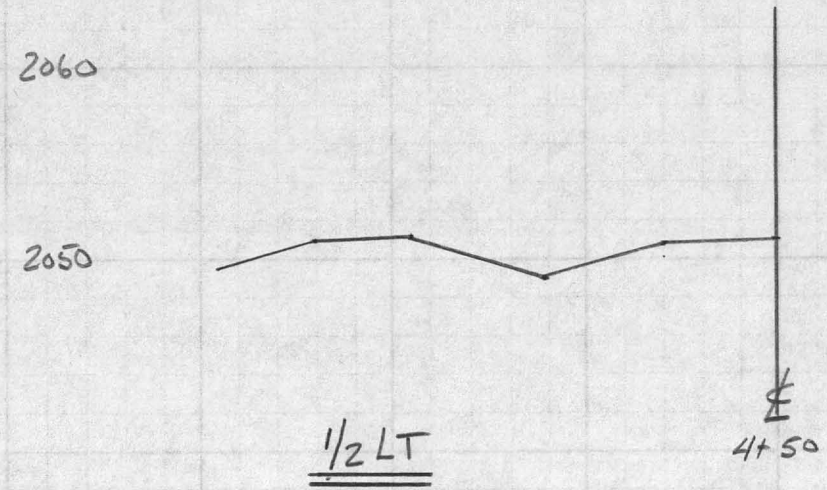
1" = 10' VERT

1" = 50' Horiz



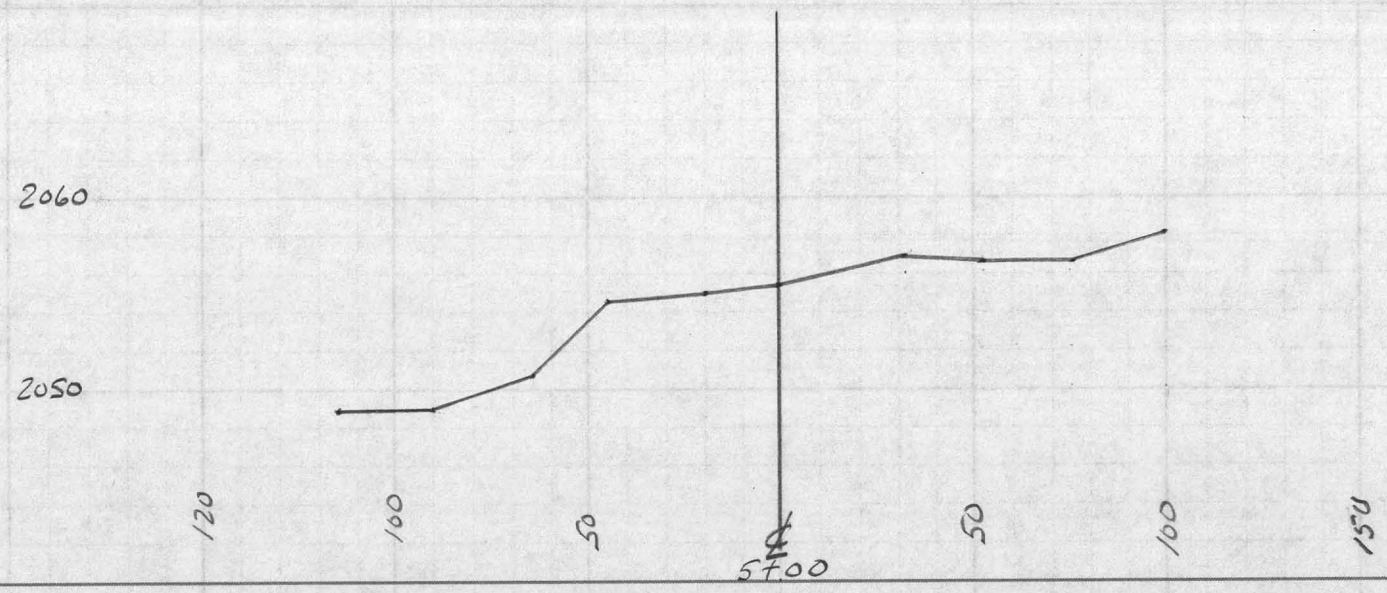
Looking Ahead

Vulture - Diversion | X-SECTIONS | 10/23/87 | 6/14

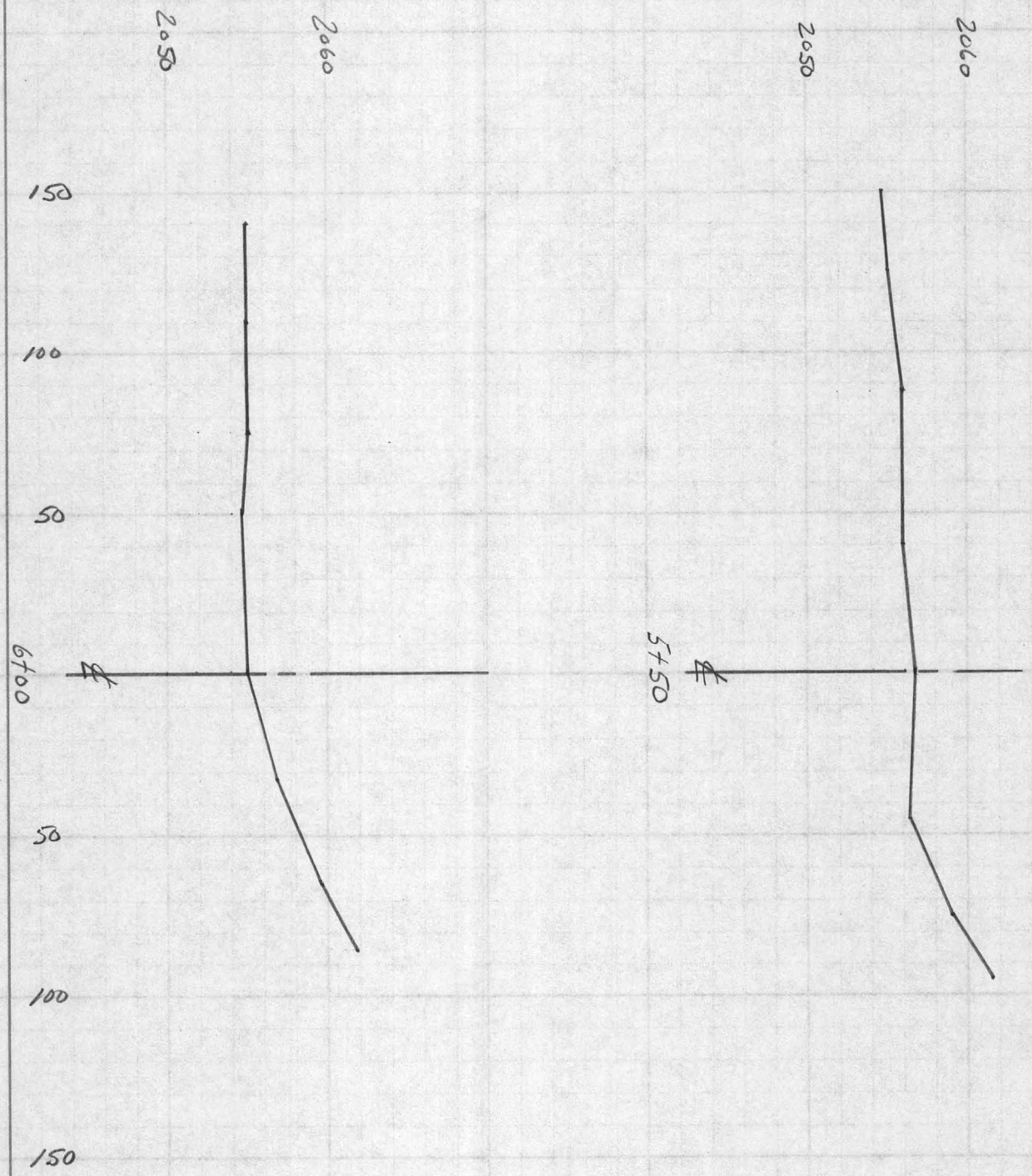


1" = 10' VERT

1" = 50' HORIZ



Looking Ahead



1" = 10' VERT

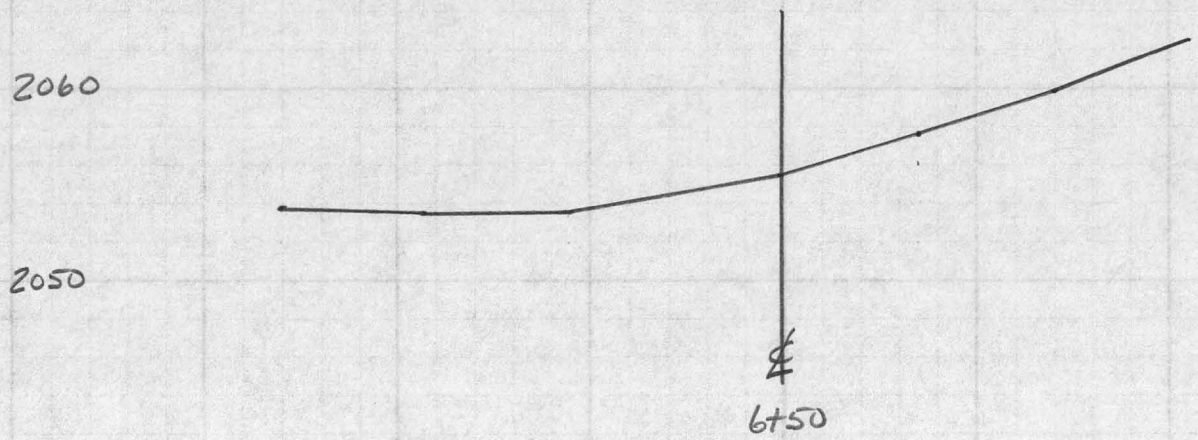
1" = 50' Horiz

8/14

10/23/87

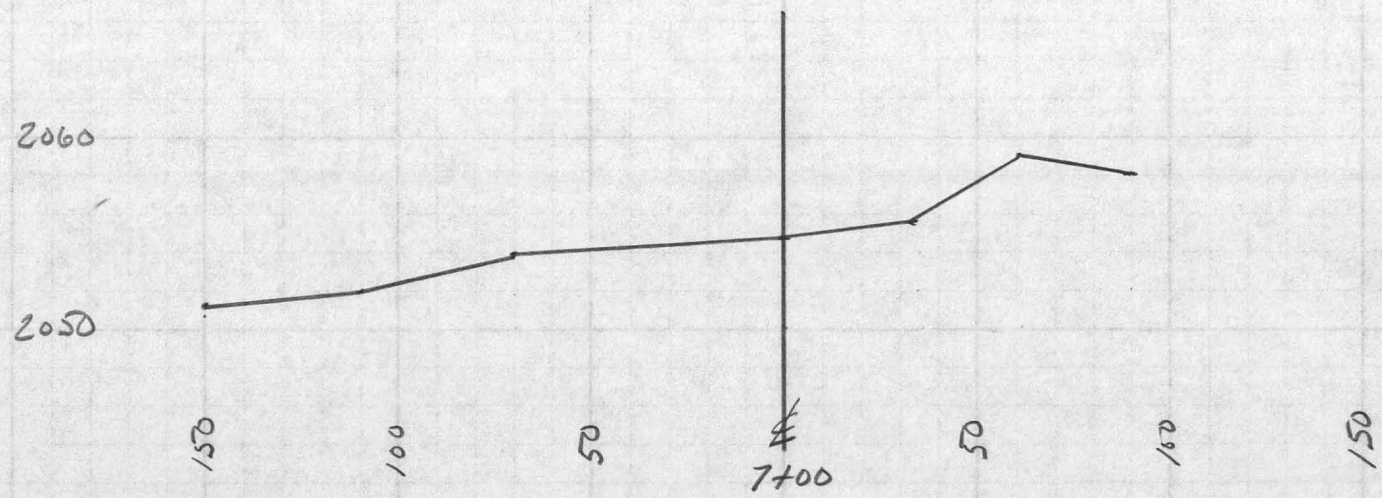
X-SECTIONS

Vulture- Diversions

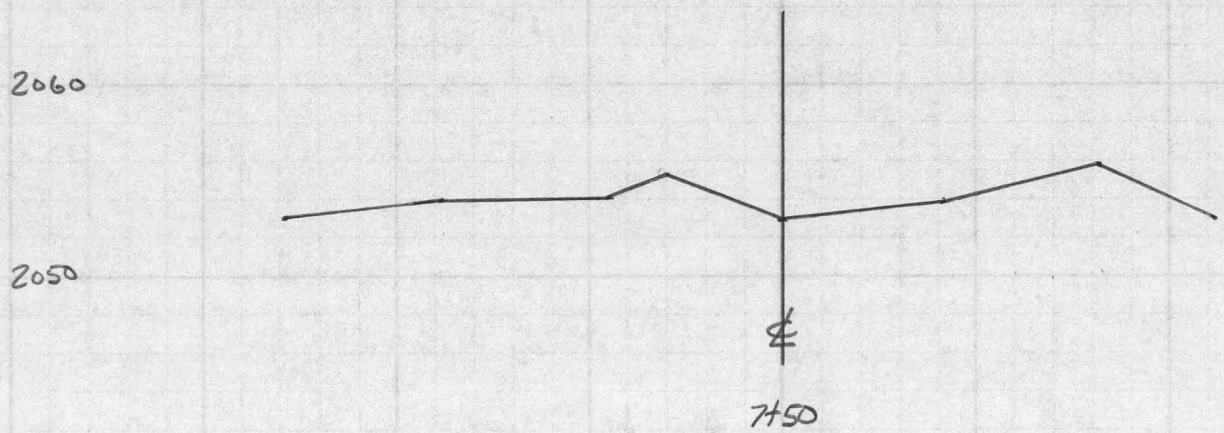


1" = 10' VERT

1" = 50' HORIZ

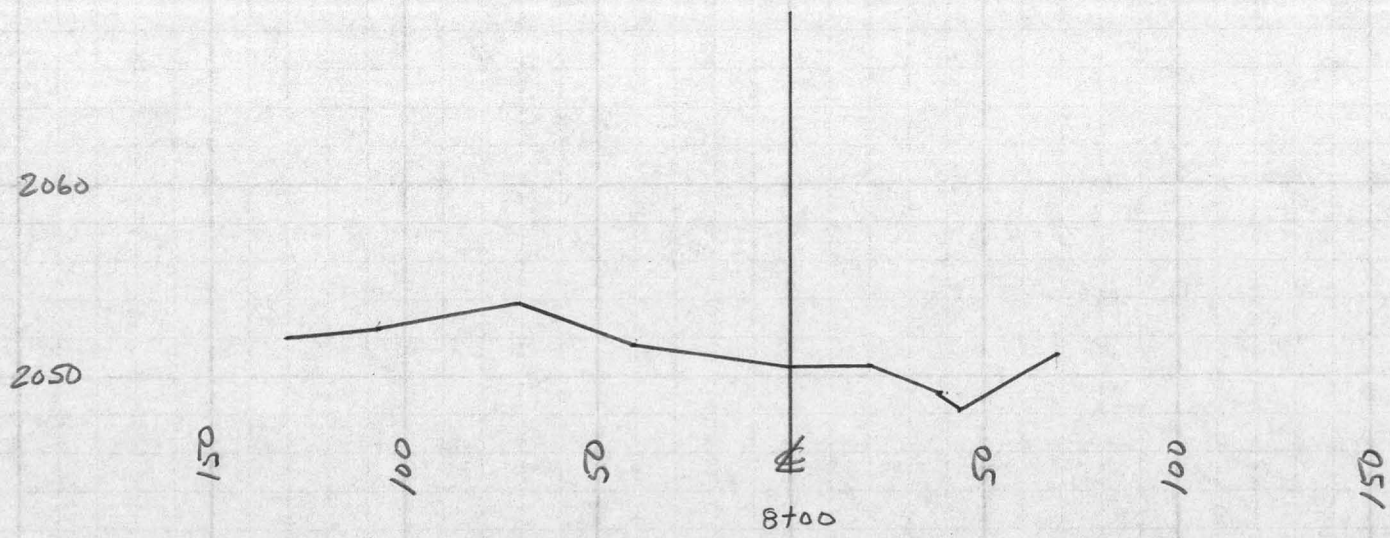


Valture - Diversion | X-SECTIONS | 10/23/87 | 9/14



1" = 10' VERT

1" = 50' HORIZ



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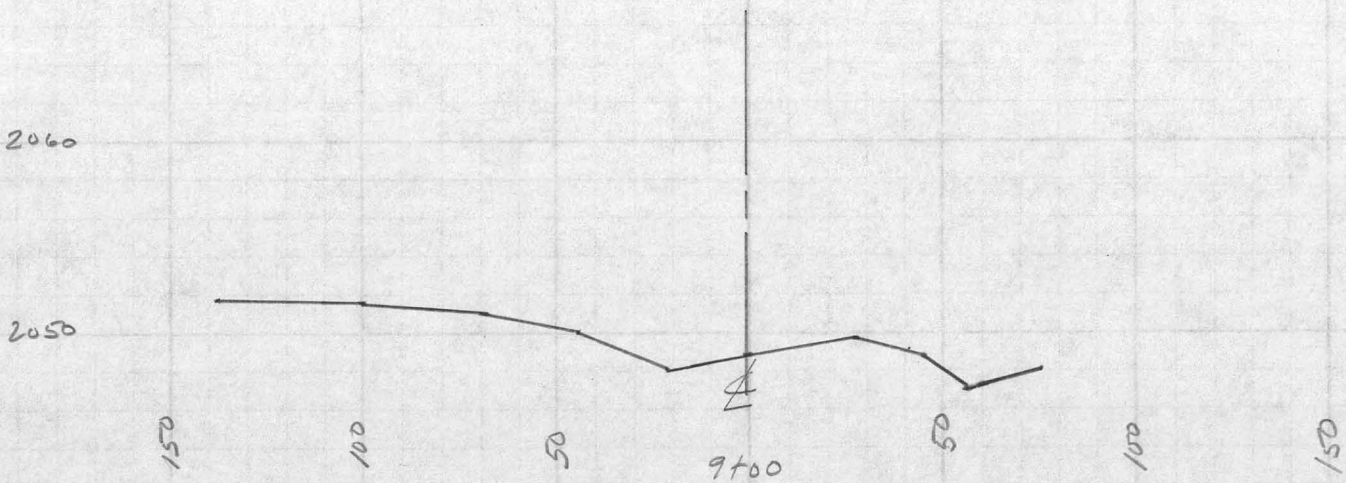
10/26/87

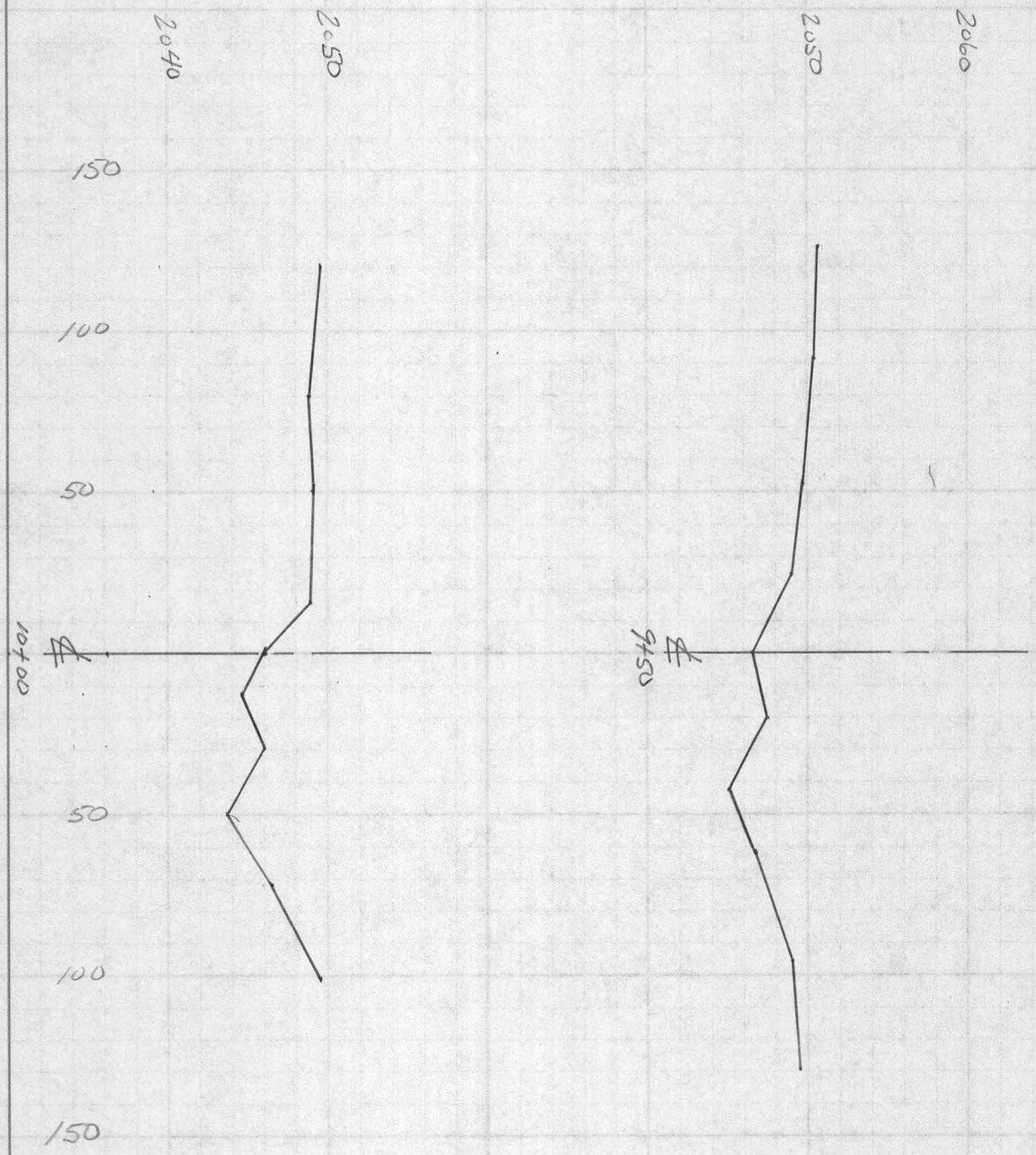
X-SECTIONS

Vulture - Diversion

1" = 10' VERT

1" = 50' HORIZ





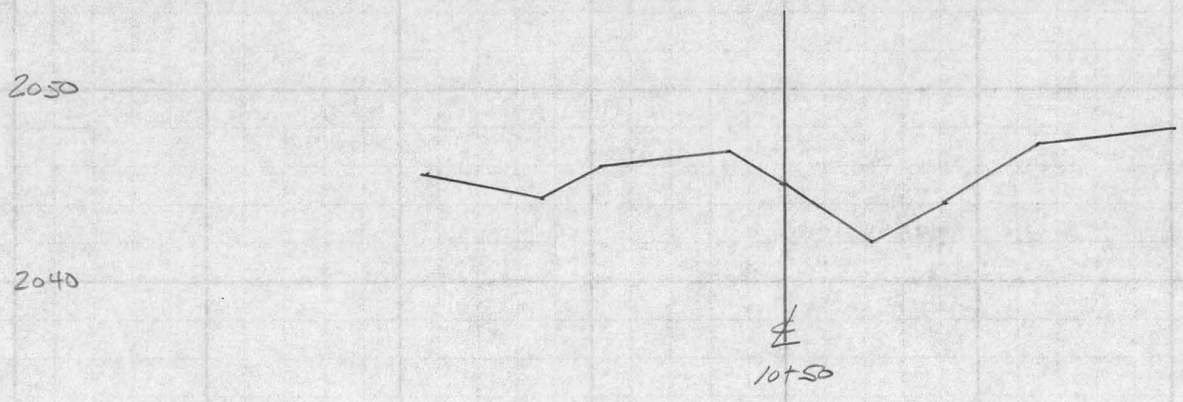
1" = 10' VERT
1" = 50' HORIZ

12/14

10/26/87

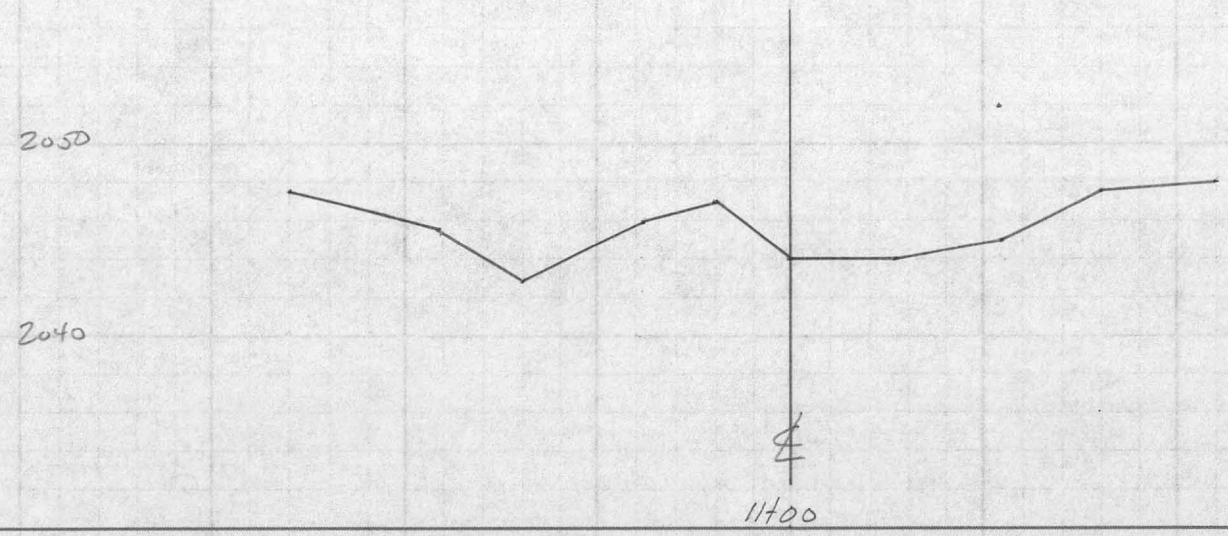
X-SECTIONS

Vulture - Diversion



1" = 10' VERT

1" = 50 HORZ



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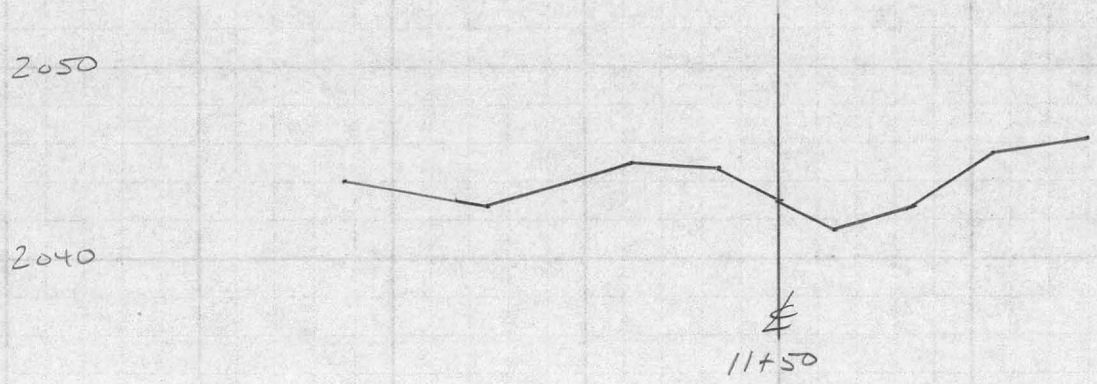
10/21/87

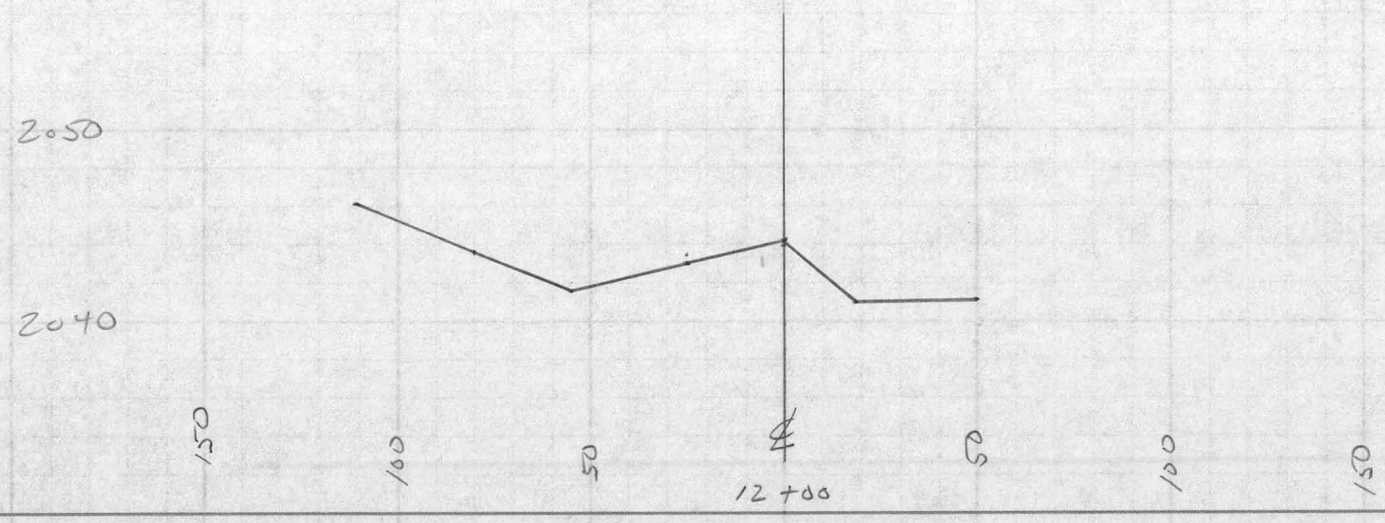
X-SECTIONS

Vulture Diversion



1" = 10' VERT

1" = 50' HORZ

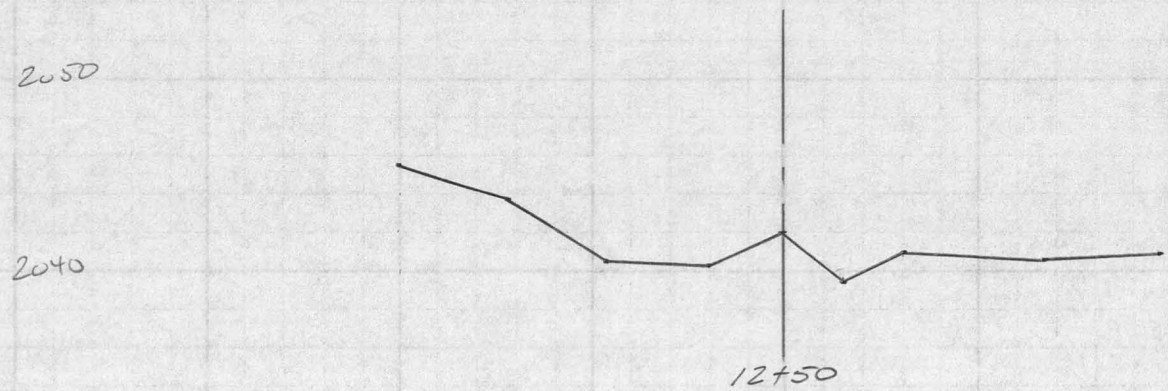


14/14

10/26/87

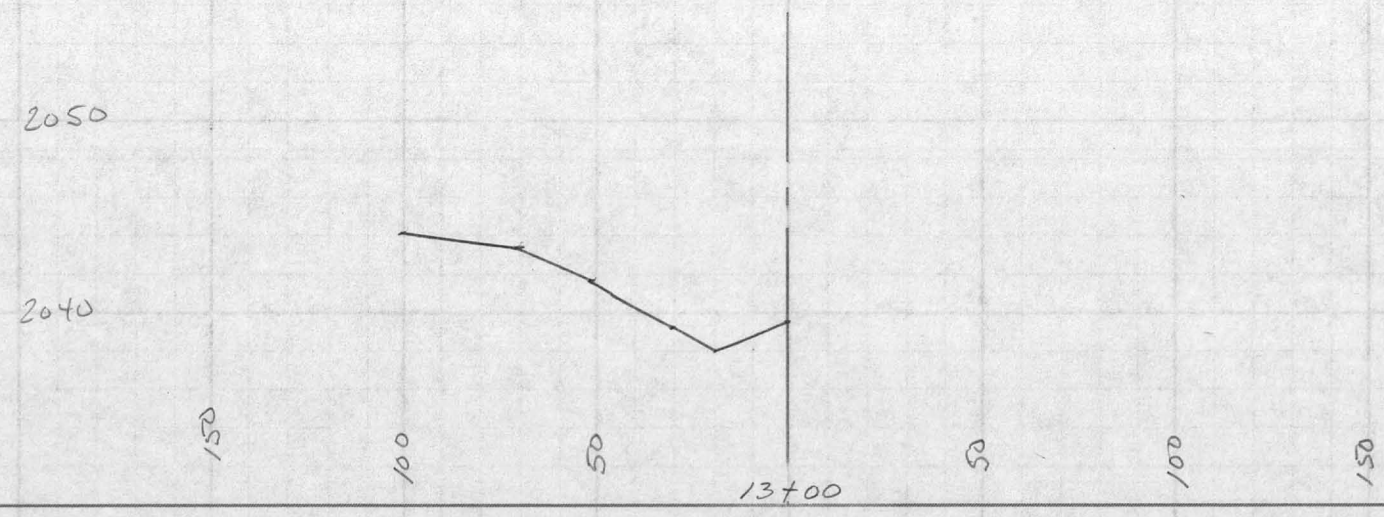
X-SECTIONS

Vulture - Diversion



1" = 10' VERT

1" = 50 HORIZ

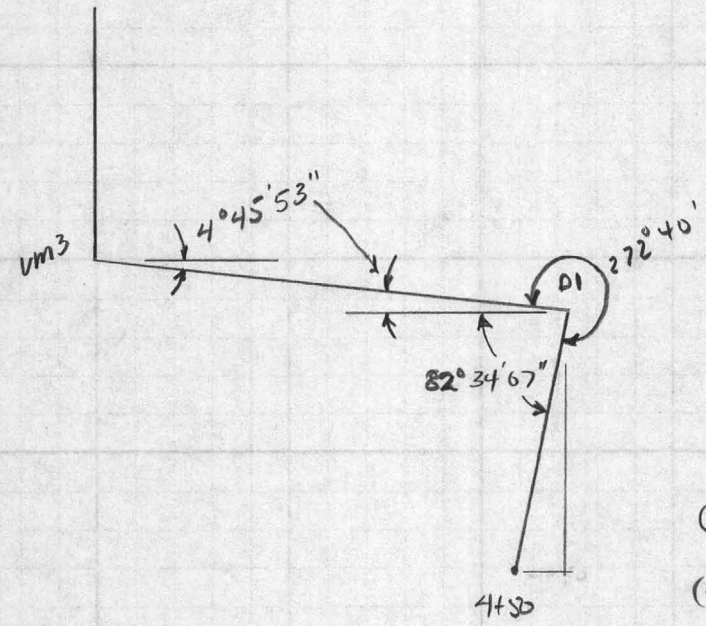


Vulture - Diversion | Survey Reduction | 10/26/87

D1 - coordinates 26 534.44 N 20 797.67 E
VM3 - Coordinates 26 579.96 N 20 251.57 E

BS	IS	∠ RT	FS
VM3	D1	272°40'	℄ 4+50

Coordinates of 4+50 ℄ sta.?



D1-VM3 Δ -45.52N 546.10 E

$\tan^{-1} \frac{45.52}{546.10} = 4°45'53''$

360°
- 4°45'53"
- 272°40'
82°34'07"

(450) Sin (82°34'07") = 446.22 N

(450) Cos (82°34'07") = 58.20 E

Both (-) (3rd Quadrant)

D1	26 534.44 N	20 797.67 E
	- 446.22	- 58.20
4+50	26 088.22	20 739.47

CROSS-SECTION ELEVATIONS (CONTINUED)

LT					RT			
				HI= 60.9				
53.0 / 120	52.8 / 80	52.6 / 52		+9.09	51.7 / 30	53.2 / 45	56.4 / 80	60.9 / 110
				2+ 00				
				2051.8				
				HI= 62.5				
52.6 / 120	52.8 / 100	52.2 / 60	52.6 / 40	+11.3	51.0 / 20	54.8 / 50	59.9 / 75	62.0 / 95
				2+ 50				
				2051.2				
				HI= 62.9				
				+12.3	52.3 / 26	53.4 / 40	59.3 / 61	62.9 / 75
				3+ 00				
				2050.6				
				HI= 56.6				
51.2 / 100	51.5 / 80	52.2 / 59	51.8 / 25	+6.0				
				3+ 00				
				2050.6				
50.6 / 120								

CROSS-SECTION ELEVATIONS (CONTINUED)

LT					RT			
				61.0 +10.3 3+ 50 2050.8	51.6 25	52.7 38	57.6 55	59.9 71
52.8 130	52.4 105	51.3 72	51.5 36	HI= 55.0 +4.2 3+ 50 2050.8				
50.7 80	50.7 51	50.7 37	50.0 25	HI= 60.3 +9.1 4+ 00 2051.2	52.0 31	55.3 51	57.3 68	57.1 75
50.5 118	50.3 90	51.6 60	49.5 35	HI= 56.4 +5.20 4+ 50 2051.2				
		½ LT		HI= 55.8 +4.6 4+ 50 2051.2				
50.7 120	50.9 95	49.3 62	50.7 30					
49.6 145								

CROSS-SECTION ELEVATIONS (CONTINUED)

LT					RT			
				HI = 61.6				
49.2 / 90	50.4 / 65	53.6 / 45	54.8 / 20	+6.0	57.1 / 32	56.5 / 52	56.6 / 75	58.1 / 100
				5+00				
				2055.6				
49.2 / 115								61.2 / 130
				HI = 61.6				
54.6 / 150	55.3 / 125	56.0 / 88	56.1 / 40	SAME AS FOR 5+00	56.3 / 45	58.7 / 75	61.5 / 95	
				5+50				
				2056.4				
				BS CAP #6 (+8.5)				
				HI = 62.5				
54.8 / 140	55.0 / 110	54.9 / 75	54.4 / 50	-7.2	56.7 / 32	59.5 / 65	61.7 / 85	
				6+00				
				55.3				
				SAME HI AS				
				6+00				
				HI = 62.5				
53.8 / 130	53.5 / 92	53.6 / 55		-6.9	57.5 / 35	59.8 / 70	62.5 / 105	
				6+50				
				55.6				
				SAME HI AS				
				6+00				
				HI = 62.5				
				-7.8				
51.2 / 150	52.0 / 110	54.1 / 70		7+00	55.7 / 36	59.0 / 61	58.2 / 91	
				54.7				

CROSS-SECTION ELEVATIONS (CONTINUED)

SAME HI AS 6+00

LT					RT			
				HI = 62^{5}				
52^{9} / 128	53^{8} / 88	53^{9} / 43		-9^{7}	53^{8} / 42	55^{8} / 82	53^{1} / 112	
			7+	50				
				2052^{8}				
				HI = 56^{6}				
52^{3} / 145	52^{9} / 116	53^{1} / 77	53^{5} / 45	$+4^{9}$	51^{4} / 43	52^{3} / 69	52^{8} / 106	
			8+	00				
				2051^{7}				
				HI = 55^{7}				
52^{1} / 130	52^{4} / 108	51^{9} / 72	51^{7} / 40	$+5^{3}$	50^{6} / 20	49^{1} / 37	48^{3} / 42	51^{1} / 68
			8+	50				
				2050^{4}				
				HI = 55^{7}				
51^{7} / 100	50^{8} / 68	50^{4} / 44	48^{2} / 23	$+6^{9}$	49^{8} / 27	48^{7} / 45	47^{1} / 57	48^{0} / 75
			9+	00				
				$2048.^{8}$				
51^{7} / 138								
				HI = 55^{4}				
50^{6} / 127	50^{4} / 92	49^{7} / 52	49^{1} / 25	$+8^{9}$	47^{5} / 20	45^{1} / 43	46^{6} / 62	49^{2} / 96
			9+	50				
				2046^{5}				
								48^{6} / 129

CROSS-SECTION ELEVATIONS (CONTINUED)

LT					RT			
$\frac{49^{7}}{120}$	$\frac{48^{7}}{80}$	$\frac{49^{2}}{50}$	$\frac{48^{7}}{17}$	HI = 53^{7} $+7^{5}$ 10+ 00 2046^{2}	$\frac{44^{6}}{13}$	$\frac{46^{0}}{29}$	$\frac{43^{8}}{50}$	$\frac{46^{5}}{73}$
								$\frac{48^{7}}{101}$
$\frac{45^{8}}{93}$	$\frac{44^{4}}{73}$	$\frac{46^{0}}{47}$	$\frac{46^{8}}{15}$	HI = 52^{6} $+7^{6}$ 10+ 50 2045^{0}	$\frac{41^{9}}{22}$	$\frac{44^{1}}{42}$	$\frac{47^{0}}{65}$	$\frac{47^{8}}{101}$
$\frac{42^{8}}{71}$	$\frac{45^{8}}{38}$	$\frac{46^{9}}{20}$		HI = 50^{3} $+6^{2}$ 11+ 00 2044^{1}	$\frac{42^{1}}{27}$	$\frac{45^{2}}{55}$	$\frac{47^{7}}{80}$	$\frac{48^{3}}{112}$
$\frac{45^{6}}{92}$	$\frac{47^{6}}{130}$							
$\frac{41^{4}}{76}$	$\frac{44^{9}}{37}$	$\frac{44^{5}}{15}$		HI = 49^{5} $+6^{7}$ 11+ 50 2042^{8}	$\frac{41^{6}}{15}$	$\frac{42^{6}}{36}$	$\frac{45^{5}}{56}$	$\frac{46^{3}}{81}$
$\frac{44^{1}}{113}$								

Cross-Section Elevations (Continued)

At 11+50 BS 4+50 Turn 138½° RT to 13+00

35 on 306 + 7.06 HI = 2049.8
- 5.6
12+00
44.20

42.8 / 80 | 41.4 / 55 | 43.1 / 24 | 40.9 / 18 | 41.0 / 50

46.2 / 111

HI = 49.8
- 7.8
12+50
42.0

43.8 / 72 | 40.5 / 47 | 40.3 / 20

45.6 / 100

HI = 45.4
+ 3.4
12+50
42.0

39.4 / 15 | 40.8 / 30 | 40.6 / 67 | 40.9 / 97

HI = 49.8
- 10.0
13+00
39.8

43.4 / 70 | 41.8 / 52 | 39.4 / 32

44.1 / 100

Cross-Section ELEVATIONS REDUCED FROM FIELD NOTES

LT					RT				
				HI = 65.2					
58.6 / 105	55.1 / 80	53.8 / 60	54.3 / 40	+11.15	54.9 / 50	54.5 / 67	62.5 / 98	62.5 / 125	61.9 / 140
				0+00					
				2054.05					
59.6 / 126	58.2 / 145	57.4 / 150							60.7 / 150
				HI = 63.4					
56.4 / 107	56.2 / 87	53.3 / 65	53.9 / 50	+ 9.83	52.6 / 25	53.9 / 50	53.9 / 69	62.3 / 100	
				0+50					
				2053.6					
55.6 / 130							60.4 / 135	61.4 / 120	
				HI = 58.1					
55 / 108	54.0 / 80	52.6 / 60	53.5 / 45	+4.7	52.1 / 26				
				1+00					
				2053.4					
54.8 / 125									
				HI = 61.1					
				+8.61					
obscured		52.6 / 50		1+50	51.8 / 30	52.8 / 45	52.7 / 75	53.9 / 88	
				2052.5					
								61.1 / 115	

obscured

ELEVATIONS OF ℄ STATIONS

STATION	ELEV.	
0+00 = D1	2054.05	by Bench Circuit from VM3
0+50	2053.57	
1+00	2053.43	
1+50	2052.50	
2+00	2051.82	
2+50	2051.24	
3+00	2050.59	
3+50	2050.79	
4+00	2051.24	
4+50	2051.17	
5+00	2055.59	CAP#6 ELEV. = 2054.00
5+50	2056.35	
6+00	2055.29	
6+50	2055.58	
7+00	2054.66	
7+50	2052.82	
8+00	2051.66	
8+50	2050.40	
9+00	2048.78	
9+50	2046.51	
10+00	2046.20	
10+50	2044.98	
11+00	2044.13	

ELEVATIONS OF ℄ STATIONS

STATION	ELEV	
11+50	2042.80	
12+00	2044.2	ELEV. 306 = 2042.72
12+50	2042.8	
13+00	2039.8	

10/19/87

AJF
+ J Ontiveros

BENCH CIRCUIT
D1 to NM3

	+BS	HI	-FS	ELEV.
D1	~~4.645~~ 13.42			2054.05
		2067.47		
B-007			4.43	
TP1			0.62	2066.85
	13.53	2080.38		
TP2			0.40	2079.98
	14.03	2094.01		
TP3			1.21	2092.80
	12.57	2105.37		
TP4			1.78	2103.59
	7.74	2111.33		
VM3			1.53	2109.8
	2.39	2112.19		
TP 5			14.72	2097.47
	0.36	2097.83		
TP 6			12.95	2084.88
	0.20	2085.08		
TP 7			13.60	2071.48
	0.02	2071.50		
TP 8			7.89	2063.61
	0.42	2064.03		
D1			9.95	2054.08
Σ	64.68		64.65	

D1 = 2054.05 ELEV.

Bench Circuit 10/19 + 10/20 ASF + J.O.
VM3 to CAP #6 LS 4529

	+BS	HI	−FS	ELEV
VM3	0.27			2109.8
		2110.07	11.92	
TP1	3.08			2098.15
		2101.23	14.44	
TP2	0.81			2086.79
		2087.60	14.36	
TP3	0.61			2073.24
		2073.85	14.13	
TP4	0.09			2059.72
		2059.81	5.80	
CAP #6 LS 4529	14.59			2054.01
		2068.60	0.47	
TP5	13.54			2068.13
		2081.67	1.05	
TP6	10.71			2080.62
		2091.33	1.34	
TP7	13.83			2089.99
		2103.82	0.78	
TP8	8.10			2103.04
		2111.14	1.32	
VM3				2109.82
	65.63		65.61	

CAP #6 ELEV. 2054.00

LT RT

HI=

$\frac{5^{4}}{11.3}$ $\frac{8^{1}}{76}$ $\frac{4^{6}}{37}$ $\frac{5^{0}}{15}$ $+6^{73}$ 11+50 $\frac{7^{9}}{15}$ $\frac{6^{9}}{36}$ $\frac{4^{0}}{56}$ $\frac{3^{2}}{81}$

11+50 TURN 138½° RT to 13+00

$+7^{06}$

BS on 306

HI=2049.78

WASH Bottom

$\frac{3^{6}}{111}$ $\frac{7^{0}}{80}$ $\frac{8^{4}}{55}$ $\frac{6^{7}}{24}$ -5^{6} 12+00 $\frac{8^{9}}{18}$ $\frac{8^{8}}{50}$

$\frac{4^{2}}{100}$ $\frac{6^{0}}{72}$ $\frac{9^{3}}{47}$ $\frac{9^{5}}{20}$ -7^{8} 12+50

WASH bottom

$\frac{5^{7}}{100}$ $\frac{6^{4}}{70}$ $\frac{8^{0}}{52}$ $\frac{10^{4}}{32}$ -10^{00} 13+00

Wash bottom

HI=1

$+3^{36}$ 12+50 $\frac{6^{0}}{15}$ $\frac{4^{6}}{30}$ $\frac{4^{8}}{67}$ $\frac{4^{5}}{97}$

LT RT

NOTE 0+00 - 2054.05 ELEV.

HI = 65.2

6.6 / 105	10.1 / 80	11.4 / 60	10.9 / 40	11.5 / 0+00	10.3 / 50	10.7 / 67	2.7 / 98	2.7 / 125	3.3 / 140	4.5 / 150
5.6 / 126	7.0 / 145	7.8 / 150								

HI =

7.0 / 107	7.2 / 87	10.1 / 65	9.5 / 50	+9.83 / 0+50	10.8 / 25	9.5 / 50	9.5 / 69	1.1 / 100	2.0 / 120	3.0 / 135
7.8 / 130										

HI =

3.1 / 108	4.1 / 80	5.5 / 60	4.6 / 45	+4.70 / 1+00	6.0 / 26
3.3 / 125					

HI =

8.5 / 50	+8.61 / 1+50	9.3 / 30	8.3 / 45	8.4 / 75	7.2 / 88	0.0 / 115

7.9 / 120	8.1 / 80	8.3 / 52	+9.09 / 2+00	9.2 / 30	7.7 / 45	4.5 / 80	0.0 / 110

9.9 / 120	9.2 / 100	10.3 / 60	9.9 / 40	11.26 / 2+50	11.5 / 20	7.7 / 50	2.6 / 75	0.5 / 95

LT

HI < 62^{9}
+ 12^{3}
3+00

RT

10^{6} / 26
9^{5} / 40
3^{6} / 61
0^{0} / 75

6^{0} / 120
5^{4} / 100
5^{1} / 80
4^{4} / 59
4^{8} / 25

HI =
+ 5^{95}
3+00

HI =
+ 10^{2}
3+50

9^{4} / 25
8^{3} / 38
3^{4} / 55
1^{1} / 71

2^{2} / 130
2^{6} / 105
3^{7} / 72
3^{5} / 36

HI =
+ 4^{22}
3+50

9^{6} / 80
9^{6} / 51
9^{6} / 37
10^{3} / 25

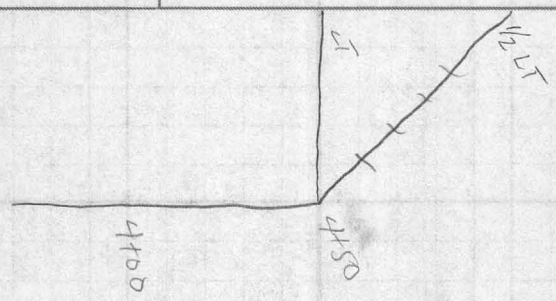
HI =
+9 ^{13}
4+00

8^{3} / 31
5^{0} / 51
3^{0} / 68
3^{2} / 75

4+00 + 4^{67} -4^{74}
4+50

HI =

5^{9} / 118
6^{1} / 90
4^{8} / 60
6^{9} / 35
+5^{20}
4+50



$\frac{5^{1}}{120}$ $\frac{4^{9}}{95}$ $\frac{6^{2}}{62}$ $\frac{5^{1}}{30}$ $+4^{64}$

4+50

$\frac{6^{2}}{145}$

LT						RT				
$\frac{12^{4}}{115}$	$\frac{12^{4}}{90}$	$\frac{11^{2}}{65}$	$\frac{8^{0}}{45}$	$\frac{6^{8}}{20}$	HI= +6^{02} 5+00	$\frac{4^{5}}{32}$	$\frac{5^{1}}{52}$	$\frac{5^{0}}{75}$	$\frac{3^{5}}{100}$	$\frac{0^{4}}{130}$
$\frac{7^{0}}{150}$	$\frac{6^{3}}{125}$	$\frac{5^{6}}{88}$	$\frac{5^{5}}{40}$	HI= 5+50		$\frac{5^{3}}{45}$	$\frac{2^{9}}{75}$	$\frac{0^{1}}{95}$		
				BS CAP#6 HI=	+8^{48}					
$\frac{7^{7}}{140}$	$\frac{7^{5}}{110}$	$\frac{7^{6}}{75}$	$\frac{8^{1}}{50}$	-7^{2} 6+00		$\frac{5^{8}}{32}$	$\frac{3^{0}}{65}$	$\frac{0^{8}}{85}$		
$\frac{8^{7}}{130}$	$\frac{9^{0}}{92}$	$\frac{8^{9}}{55}$	-6^{85} 6+50			$\frac{5^{0}}{35}$	$\frac{2^{7}}{70}$	$\frac{0^{0}}{105}$		
$\frac{11^{3}}{150}$	$\frac{10^{5}}{110}$	$\frac{8^{4}}{70}$	-7^{80} 7+00			$\frac{6^{8}}{36}$	$\frac{3^{5}}{61}$	$\frac{4^{3}}{91}$		
$\frac{9^{6}}{128}$	$\frac{8^{7}}{88}$	$\frac{8^{6}}{43}$	-9^{65} 7+50			$\frac{8^{7}}{42}$	$\frac{6^{7}}{82}$	$\frac{9^{4}}{112}$		
$\frac{4^{3}}{145}$	$\frac{3^{7}}{116}$	$\frac{3^{5}}{77}$	$\frac{3^{1}}{45}$	HI= +486 8+00		$\frac{5^{2}}{43}$	$\frac{4^{3}}{69}$	$\frac{3^{8}}{106}$		
$\frac{3^{6}}{130}$	$\frac{3^{3}}{108}$	$\frac{3^{8}}{72}$	$\frac{4^{6}}{40}$	HI= 8+50 +5^{25}		$\frac{5^{1}}{20}$	$\frac{6^{6}}{37}$	$\frac{7^{4}}{42}$	$\frac{4^{6}}{68}$	

$\frac{4^{6}}{138}$ $\frac{4^{0}}{100}$ $\frac{4^{9}}{68}$ $\frac{5^{3}}{44}$ $\frac{7^{5}}{23}$ 9

HI =
+ 189
+ 00

$\frac{5^{9}}{27}$ $\frac{7^{0}}{45}$ $\frac{8^{6}}{57}$ $\frac{7^{7}}{75}$

Bench Circuit
CAP #6 to 306

	+BS	HI	−FS	ELEV
CAP#6	2^{00}		$\cancel{13^{32}}$	2054^{00}
		2056^{00}	13^{28}	
306				2042.72

HI AS ABOVE $= 2056^{00}$

9+50	-9^{49}	2046.51
10+00	-9^{80}	2046.20
10+50	-11^{02}	2044.98
11+00	-11^{87}	2044.13
11+50	-13^{20}	2042.80

HI=

$\frac{4^{8}}{127}$ $\frac{5^{0}}{92}$ $\frac{5^{7}}{52}$ $\frac{6^{3}}{25}$ $+8^{93}$ 9+50 $\frac{7^{9}}{20}$ $\frac{10^{3}}{43}$ $\frac{8^{8}}{62}$ $\frac{6^{2}}{96}$ $\frac{6^{8}}{129}$

HI=

$\frac{4^{0}}{120}$ $\frac{5^{0}}{80}$ $\frac{4^{5}}{50}$ $\frac{5^{0}}{17}$ $+7^{47}$ 10+00 $\frac{9^{1}}{13^{4}}$ $\frac{7^{2}}{29}$ $\frac{9^{9}}{50}$ $\frac{7^{2}}{73}$ $\frac{5^{6}}{101}$

$\frac{6^{8}}{93}$ $\frac{8^{2}}{73}$ $\frac{6^{6}}{47}$ $\frac{5^{8}}{15}$ $+7^{60}$ 10+50 $\frac{10^{7}}{22}$ $\frac{8^{5}}{42}$ $\frac{5^{6}}{65}$ $\frac{4^{8}}{101}$

$\frac{2^{2}}{130}$ $\frac{4^{2}}{92}$ $\frac{7^{5}}{71}$ $\frac{4^{5}}{38}$ $\frac{3^{4}}{20}$ $+6^{16}$ 11+00 $\frac{8^{2}}{27}$ $\frac{5^{1}}{55}$ $\frac{2^{6}}{80}$ $\frac{2^{0}}{112}$

Vulture Mine Options (July 22, 1987)

Assumptions: Gold at $450.00/ounce

Tailings Reserve of 225,000 tons of 0.045 oz/t

High grade Reserves of 127,000 tons of 0.086 oz/t
with a Waste:Ore ratio of 3.6:1

Lower grade Reserves of 445,000 tons of 0.062 oz/t
with a Waste:Ore ratio of 2.9:1

	Heap Leach Tailings only	Heap Leach High Grade & Tailings	Heap Leach Lower Grade & Tailings	Heap Leach & C-I-L High Grade	Heap Leach & C-I-L Lower Grade
Gross Revenues	$3,189,375	$5,646,825	$9,397,125	$6,502,284	$10,515,105
Capital	$450,000	$650,000	$765,000	$1,615,000	$1,615,000
Operating Costs					
Mining (Rock)		$876,300	$2,603,250	$876,300	$2,603,250
Mining (Tailings)	$225,000	$225,000	$225,000	$225,000	$225,000
Processing	$1,237,500	$1,936,000	$3,685,000	$2,834,625	$4,861,875
Royalties & Bonus	$211,631	$334,758	$474,849	$331,736	$470,726
Operating Profit	$1,515,244	$2,274,767	$2,409,026	$2,234,623	$2,354,254
Recovery of Capital	($450,000)	($650,000)	($765,000)	($1,615,000)	($1,615,000)
Sunk Costs (6-15-87)	($632,000)	($632,000)	($632,000)	($632,000)	($632,000)
Net Profit	$433,244	$992,767	$1,012,026	($12,377)	$107,254

Assumptions and Parameters

gold	$450.00	per ounce
silver	$7.50	per ounce
tons of high grade	127000	tons
grade	0.086	oz/t
strip	3.6	3.6:1
tons of low grade	445000	tons
grade	0.062	oz/t
strip	2.9	2.9:1
tons of tailings	225000	tons
grade	0.045	oz/t
cost, mining rock	$1.50	per ton
cost, mining tails	$1.00	per ton
recovery, rock (heap)	0.5	50%
recovery, fines (CIL)	0.85	85%
recovery, tails (heap)	0.7	70%
recovery, tails (CIL)	0.85	85%
processing, heap leach	$5.50	per ton
processing, CIL	$9.00	per ton

STA	BS/FS	H-∠	V-∠	BEARING	SLOPE DIST	H-DIST	COORDINATES N	COORDINATES E	Δ-VERT	ELEV.
VM2							26 200.98	21 345.04		2098.2
	VM3	0°00'00"	89°23'53"	289°06'56"	1157 42	1157.36	26 579.96	20 251.57	+11 99/11 60	2109.8
	84-17	358°27'55"	89°44'20"	287°34'51"	1104 75	1104.74	26 534.67	20291.90	+4 86	2103.1
	H-26	355°01'30"	91°05'11"	284°08'26"	934 36	934.19	26,429.20	20,439.16	-	2080.3
	H-11	354°30'47"	91°33'02"	283°37'43"	858.98	858.67	26,403.31	20,510.54	-	2074.8
	84-10	350°45'51"	91°18'16"	279°52'47"	846.35	846.13	26,346.16	20,511.46	-	2078.8
	H 43	343°18'25"	91°08'59"	272°25'21"	786.44	786.28	26,234.21	20.559.46	-	2082.3
		348°30'37"	90°43'48"	277°37'33"	995.43	995.35	26 333.07	20 358.49	-	2081.3
		353°59'56"	91°46'03"	283°06'52"	807.58	807.20	26 384.13	20 558.89	-	2069.1
	H-45	0°06'34"	92°06'33"	289°07'30"	794.29	793.75	26 461.64	20595.10	-	2064.8
	H-22	357°46'40"	92°26'21"	286°53'36"	737.50	736.83	26,415.10	20640.00		2062.6
	H-44	0°08'56"	91°07'43"	289°15'52"	980.64	979.85	26,524.26	20420.66		2074.7
	84 16	10°24'28"	91°43'25"	299°31'24"	970.17	969.73	26,678.84	20501.22		2068.8
	84-6	7°20'38"	90°42'47"	296°27'34"	1142.80	1142.71	26,710.13	20 322.03		2083.8
		8°42'15"	90°61'09"	297°49'15"	1280.80	1280.80	26798.74	20212.29		2093.6
		19°38'54"	91°35'55"	308°45'50"	1030.00	1029.60	26 845.63	20 542.23		2065.3

STA	BS/FS	H-∠	V-∠	BEARING	SLOPE DIST.	H-DIST	COORDINATES N	COORDINATES E	ELEV	
VM2		23°55'38"	91°55'57"	313°02'34"	879.50	879.00	26800.94	20702.63	2068.4	
		18°19'49"	92°18'59"	307°26'45"	805.97	805.31	26690.62	20705.68	2061.5	
		14°32'46"	92°01'16"	303°35'42"	837.30	836.78	26664.80	20648.57	2064.5	
		12°04'33"	93°20'29"	301°11'29"	610.25	609.21	26516.49	20823.90	2054.5	
	H59	118°45'34"	97°21'21"	47°52'30"	333.38	330.64	26422.76	21590.27	2051.3	
	H60	109°21'46"	95°45'08"	38°28'42"	454.45	452.16	26554.95	21626.38	2056.5	
	H49	105°11'56"	96°10'01"	34°18'52"	358.60	356.52	26495.45	21546.02	2055.5	
		91°10'31"	93°59'11"	20°17'27"	448.68	447.59	26620.79	21500.26	2062.8	
		115°25'46"	98°03'52"	44°32'42"	256.79	254.25	26382.18	21523.39	2058.0	
		91°27'34"	99°54'43"	20°34'30"	196.22	193.29	26381.94	21412.97	2060.3	
		43°40'03"	94°45'23"	332°46'59"	345.72	344.53	26507.36	21187.47	2063.4	
	RP1	162°48'39"	95°18'57"	91°55'35"	233.80	232.79	26193.15	21577.70	2080.4	
RP1	VM2	0°00'00"		268°04'25"					2080.4	HI = 2085.15
	H63	134°54'46"	101°51'03"	42°59'11"	347.50	340.09	26441.93	21809.58	2013.8	
	H65	127°13'09"	103°17'15"	35°17'34"	290.73	282.95	26424.10	21741.18	2018.3	
	H61	115°01'51"	105°25'36"	23°06'16"	246.25	237.38	26411.49	21670.85	2019.6	

STA	BS/FS	H-∠	V-∠	BEARING	SL DIST	H-DIST	COORDINATES N	COORDINATES E	ELEV	
RP1	VM2	0°00'00'		268°04'25"			26193.15	21 577.70	2080.4	HI = 2085.15
LATH ON TC LINE							25 644.24	21 237.55	2079.0	HI = 2082.4
	NW VCT	0°00'00"	91°14'16"	280°47'41"	899.90	899.69	25 812.74	20 353.78	2051.0	
	RP2	271°50'14"	92°10'01"	192°37'55"	1191.89	1190.63	24 482.43	20 977.17	2019.7	
RP2	LATH ON TC LINE	0°00'00"		12°37'55"			24 482.43	20 977.17	2019.7	HI = 2024.45
	VS8	241°30'24"	89°41'09"	254°08'19"	384.60	384.59	24 377.32	20 607.22	2018.6	
	VS2N	213°15'36"	90°14'13"	225°53'31"	513.83	513.83	24 124.80	20 608.23	2014.3	
	VS7	192°50'39"	90°08'55"	205°28'34"	745.03	745.03	23 809.84	20 656.71	2010.5	
VS7	RP2	0°00'00"		25°28'34'			23 809.84	20656.71	2010.5	HI = 2015.7
	VS6	134°39'27"	90°32'02"	160°08'01"	309.57	309.56	23 518.70	20761.91	2004.8	
	VS10	139°23'46"	90°42'43"	164°52'20"	594.50	594.45	23 235.99	20 811.85	2000.3	

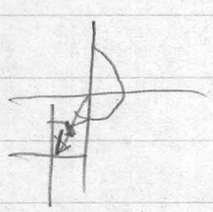
3/11/87

T A.J.F
P Jose O.

BS	STA	FS	H∠	V∠	S-DIST	HI	ROD Length
VM3	VM2		0°00'00"	89°23'53"	1157.42	3.83	4°
	DH		358°27'55"	89°44'20"	1104.75		4°
	H26		355°01'30"	91°05'11"	934.36		4°
	H-11		354°30'47"	91°33'02"	858.98		4°
	84-10		350°45'51"	91°18'16"	846.35		4°
	H 43		343°18'25"	91°09'59"	786.44		4°
			348°30'37"	90°43'48"	995.43		8°
			353°59'56"	91°46'03"	807.58		8°
	H-45		0°00'34"	92°06'33"	794.29		8°
			357°46'40"	92°26'21"	737.50		8°
	H-44		0°08'56"	91°07'43"	980.04		8°
			10°24'28"	91°43'25"	970.17		4°
	84-5		7°20'38"	90°42'47"	1142.80		4°
			8°42'19"	90°01'09"	1280.80		8°
			19°38'54"	91°35'55"	1030.00		8°
			23°55'38"	91°55'57"	879.50		4°

BS	STA	FS	HZ	VZ	S-DIST	HI	Rod length
VM3			0°00'00"				
	VM2		18°19'49"	92°18'59"	805.97	3.83'	8°
			14°32'46"	92°01'16"	837.30		8°
			12°04'33"	93°20'29"	610.25		12°
		H59	118°45'34"	97°21'21"	333.38		8°
		H60	109°21'46"	95°45'08"	454.45		0°
		H49	105°11'56"	96°10'01"	358.60		8°
			91°10'31"	93°59'11"	448.68		8°
			115°25'46"	98°03'52"	256.79		8°
			91°27'34"	99°54'43"	196.22		8°
			43°40'03"	94°45'23"	345.72		10°
		RP1	162°48'39"	95°18'57"	233.80		0°
		H54	160°06'41"	94°48'42"	211.35		4°
			153°32'39"	96°00'39"	172.03		4°
VM2	RP1	H63	134°54'46"	101°51'03"	347.50	4.75	0°
		H65	127°13'09"	103°17'15"	250.73		0°
		H61	115°01'51"	105°25'36"	246.25		0°

BS	STA	FS	HL	VL	S-DIST	HI	ROD LT.
NW corner VCT	LATH on N Line T.S.		0°00'00"	91°14'16"	899.80	3.46	12°
		RP2	271°50'14"	92°10'01"	1191.89		8°
LATH on N Line VCT	RP2		0°00'00"			4.75	
	✓	VS8	241°30'24"	89°41'09"	384.60		8°
		VS2N	213°15'36"	90°14'13"	513.83		8°
		VS7	192°50'39"	90°08'55"	745.03		12 ~~8~~°
RP2	VS7	~~VS7~~	0°00'00"			5.17	
		VS6	134°39'27"	90°32'02"	309.57		8°
		VS10	135°23'46"	90°42'43"	594.50		8°



5/14/84

Carole:

Here is copy of drill hole map along w/ pits 3 & 4. These have been shot in using drill holes 6 & 1 as a base line (direction only w/ DH#6 as starting station)

There is a problem between DH's 1-10 and the other holes. My survey gives proper location of holes to each other but don't know about a tie to coord system. etc.

NOT SCANNED