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MEMO TO: File

FROM: RFLucht/

Urangesellschaft Equilibrium Numbers

Equilibrium numbers for all of the Urangesellschaft core holes drilled in their last drilling program have been calculated using exactly the same techniques that were used to calculate equilibrium numbers on the rest of the property.

Based on those calculations, a revision was made to the REF contours map to reflect this new data. This revision entailted determining new REFs for the following Anderson Mine holes.

HOLE NUMBER		$\underline{R.E.F}$.
AM-689		1.30
AM-15	· ·	1.15
AM-449		1.22
AM-146		1.20
AM-439		1.20
AM-450		1.30

The following Urangesellschaft core holes were calculated:

HOLE NUMB	ER	R.E.F.
DC 126C DC 165C DC 171C		.845 1.039 .914
DC 161C DC 177C		1.108 1.131
DC 169C DC 158C		1.052
DC 145C DC 146C		.912 .850
Tonto 8C DC 28C		.897 1.012
DC 155C DC 176C		.841 1.105
DC 175C		1.153

The changes to the contours on the equilibrium factors map reflect a continuation of the same pattern observed on Minerals Exploration property. A copy of this revised map is enclosed. Also enclosed are copies of the raw data supplied by Urangesellschaft for their chemical assays and copies of the calculations done on this data.

The calculations done are in Appendix I $\,$ and the raw data is in Appendix II.

As soon as the Urangesellschaft data is input to the computer, additional REFs will be determined for all of their holes.

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APPENDIX I

DC HOLE NO. 28C

	DC HOLE NO	28C	U ₃ O ₈		
	DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
	485	1443.5	.004	.001	
	486	1442.5	.005	.001	
	487	1441.5	.074	.004	.054
	488	1440.5	.028	.003	.107
	489	1439.5	.201	.004	.020
	490	1438.5	.201	.007	.035
	491	1437.5	.026	.138	5.308
	492	1436.5	.016	.380	23.750
	493	1435.5	.008	.024	3.000
^	494	1434.5	.012	.014	1.167
	495	1433.5	.049	.014	.286
	496	1432.5	.037	.009	.243
	497	1431.5	.006	.012	2.000
	498	1430.5	.006	.045	7.500
	499	1429.5	.005	.005	
	500	1428.5	.005	.007	
	501	1427.5	.017	.005	.294
175	502	1426.5	.014	.004	.286
	503	1425.5	.010	.012	1.200
	504	1424.5	.009	.016	1.778
	505	1423.5	.024	.012	.500
	506	1422.5	.032	.013	.406
	507	1421.5	.013	.010	.769
	508	1420.5	.010	.019	1.900
	509	1419.5	.013	.047	3.615
	510	1418.5	.008	.011	1.375

DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
511	1417.5	.009	.010	
512	1416.5	.010	.010	× *
513	1415.5	.014	.008	.571 .
514	1414.5	.016	.008	.500
515	1413.5	.046	.008	.174
516	1412.5	.032	.012*	.375
517	1411.5	.015	.013*	.867
518	1410.5	.009	.019*	2.111
519	1409.5	.009	.058*	6.444
520	1408.5	.007	.041*	5.857
521	1407.5	.007	.010*	
522	1406.5	.007	.006*	
523	1405.5	.009	.006*	
524	1404.5	.011	.006*	.545
525	1403.5	.009	.006*	
526	1402.5	.011	.007*	.636
527	1401.5	.007	.007*	
528	1400.5	.006	.010*	
529	1399.5	.009	.011*	1.222
530	1398.5	.009	.012*	1.333
531	1397.5	.010	.009*	
532	1396.5	.009	.006*	
*These	assays composited	to even footag	ges	

CUTOFF GRADE	R.E.F
.01	1.004
.02	1.012
.03	1.041

DC HOLE NO.	,	U ₃ 0	_	
DEPT	ELEVATION	GAMMA	8 CHEMICAL	R.E.F.
646	1304.5		.001	
647	1303.5		.001	
648	1302.5		.002	,
650	1300.5		.001	
651	1299.5		.001	
652	1298.5	.007	.001	
653	1297.5	.011	.002	.182
654	1296.5	.008	.001	
655	1295.5	.006	.001	
656	1294.5	.005	.001	
657	1293.5	.008	.003	
658	1292.5	.009	.002	
659	1291.5	.013	.027	2.077
660	1290.5	.031	.020	.645
661	1289.5	.017	.028	1.647
662	1288.5	.035	.007	.200
663	1287.5	.031	.005	.161
664	1286.5	.058	.002	.034
665	1285.5	.080	.001	.013
666	1284.5	.079	.001	.013
667	1283.5	.043	.001	.023
668	1282.5	.065	.018	.277
669	1281.5	.080	.029	.363
670	1280.5	.152	.091	.599
671	1279.5	.212	.027	.127
672	1278.5	.065	.300	4.615

DC HOLE NO. 126C U_3O_8 R.E.F. CHEMICAL GAMMA DEPTH ELEVATION 9.273 .102 1277.5 .011 673 1.000 .010 1276.5 .010 674 .727 .008 .011 1275.5 675 .154 .006 .039 1274.5 676 1.095 .023 .021 1273.5 677 5.368 .102 .019 1272.5 678 .875 .028 1271.5 .032 679 2.909 .032 .011 1270.5 680 1.125 .018 .016 681 1269.5 .600 .009 1268.5 .015 682 .371 .013 .035 1267.5 683 1.056 .038 1266.5 .036 684 1.200 .018 1265.5 .015 685 1.417 .017 1264.5 .012 686 1.333 .016 .012 1263.5 687 .007 .010 1262.5 688 .267 .004 1261.5 .015 689 .600 .012 1260.5 .020 690 .684 .013 .019 1259.5 691 3.500 .063 .018 1258.5 692 1.074 .029 .027 1257.5 693 .118 .006 .051 1256.5 694 .514 .019 1255.5 .037 695 1.606 .053 .033 1254.5 696 2.000 .038 1253.5 .019 697

.030

1252.5

698

.467

.014

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$\overline{D}^{_{1},,_{L}}H$	ELEVATION	GAMMA	CHEMICAL	R.E.F.
699	1251.5	.028	.009	.321
700	1250.5	.025	.008	.320
701	1249.5	.037	.015	.405
702	1248.5	.057	.005	.088
703	1247.5	.045	.017	.378
704	12465	.028	.021	.750
705	1245.5	.016	.020	1.250
706	1244.5	.007	.009	
707	1243.5	.004	.082	20.500
708	1242.5	.004	.048	12.000
709	1241.5	.004	.034	8.500
710	1240.5	.004	.019	4.750
711	1239.5	.004	.007	
712	1238.5		.001	
713	1237.5		.001	
713'7"	1237.1		.001	
	CUTOFF GRAI)E	R.E.F.	
	.01		. 854	
	.02		.845	
	.03		.845	

HOLE # I	OC 145 C	U ₃ 0	8	
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
477	1418.5	.018	.002	.111
478	1417.5	.018	.003	.167
479	1416.5	.019	.004	.211
480	1415.5	.028	.003	.107
481	1414.5	.101	.005	
482	1413.5	.007	.009	
483	1412.5	.010	.007	
484	1411.5	.008	.012	1.500
485	1410.5	.012	.008	.667
486	1409.5	.013	.008	.615
487	1408.5	.016	.012	.750
488	1407.5	.015	.014	.933
489	1406.5	.013	.015	1.154
490	1405.5	.020	.020	1.000
491	1404.5	.016	.019	1.188
492	1403.5	.016	.012	.750
493	1402.5	.018	.010	.556
494	1401.5	.015	.012	.800
495	1400.5	.026	.029	1.115
496	1399.5	.033	.044	1.333
497	1398.5	.021	.017	.810
498	1397.5	.009	.011	1.222
499	1396.5	.009	.007	
500	1395.5	.013	.008	.615
501	1394.5	.009	.008	
502	1393.5	.012	.007	.583
503	1392.5	.017	.040	2.353
504	1391.5	.029	.140	4.828

.013

.010

.008

.007

1364.5

1363.5

531

532

.615

HOLE # DC	145C	U ₃ 0 ₈		
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
533	1362.5	.017	.009	.529
534	1361.5	.009	.013	1.444
535	1360.5	.010	.009	
536	1359.5	.009	.009	
537	1358.5	.012	.032	2.667
538	1357.5	.018	.043	2.389
539	1356.5	.025	.121	4.840
540	1355.5	.033	.087	2.636
541	1354.5	.134	.010	.075
542	1353.5	.108	.005	.046
543	1353.5	.023	.004	.174
544	1351.5	.011	.004	.364
545	1350.5	.008	.004	
557	1338.5	.015	.029	1.933
558	1337.5	.018	.056	3.111
559	1336.5	.034	.012	.353
560	1335.5	.030	.008	.267
561	1334.5	.012	.002	.167
562	1333.5	.007	.001	
568	1327.5	.010	.005	
569	1326.5	.010	.005	
570	1325.5	.009	.007	***
571	1324.5	.017	.036	2.118
572	1323.5	.036	.048	1.333
573	1322.5	.031	.026	.839
574	1321.5	.028	.014	.500
575	1320.5	.017	.011	.647
576	1319.5	.012	.008	.667

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CUTOFF GRADE	R.E.F.
.010	.848
.020	.912
.030	.960

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DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
576	1348	.006		
577	1347	. 0 ³ 0 7		
578	1346	.007		
579	1345	.007		
580	1344	.007		
581	1343	.007		
582	1342	.007		**
583	1341	.009		
584	1340	.007		
585	1339	.009		
586	1338	.015		
587	1337	.020		
588	1336	.014		
589	1335	.008		
590	1334	.009		
591	1333	.009	.013	1.444
592	1332	.003	.004	
600	1324	.007	.003	
601	1323	.006	.003	
602	1322	.003	.006	s
				# Y
605	1319	.007	.002	* 2
606	1318	.014	.003	.214
607	1317	.011	.003	.273
608	1316	.014	.001	.214

DC HOLE NO	146C	U ₃ O ₈		
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
609	1315	.017	.001	.059
610	1314	.007	.013	1.857
611	1313	.006	.006	
612	1312	.006	.009	
613	1311	.005	.017	3.400
614	1310	.006	.003	
615	1309	.034	.004	.118
616	1308	.012	.006	.500
617	1307	.012	.004	.333
618	1306	.016	.022	1.375
619	1305	.016	.014	.875
620	1304	.013	.005	.385
621	1303	.023	.014	.609
622	1302	.011	.009	.818
623	1301	.014	.011	.786
624	1300	.013	.012	.923
625	1299	.012	.017	1.417
626	1298	.012	.007	.583
627	1297	.011	.017	1.545
628	1296	.008	.008	
629	1295	.011	.014	1.273
630	1294	.015	.010	.667
631	1293	.015	.008	.533
632	1292	.032	.009	.281
633	1291	.142	.010	.070
634	1290	.182	.009	.049

		U ₃ 0 ₈		
DEPT	ELEVATION	GAMMA	CHEMICAL	R.E.F.
635	1289	.087	.012	.138
636	1288	.015	.025	1.667
637	1287	.009	.133	14.778
638	1286	.008	.192	24.000
639	1285	.013	.059	4.538
640	1284	.008	.007	
641	1283	.006	.006	
642	1282	.006	.013	2.167
				al.
645	1279	.007	.004	
646	1278	.009	.004	
647	1277	.011	.003	.273
648	1276	.010	.003	
649	1275	.011	.004	.364
650	1274	.003	.007	
651	1273	.003	.009	
652	1272	.007	.008	
653	1271	.007	.009	
654	1270	.009	.004	
655	1259	.017	.002	.118
656	1268	.013	.004	.308
657	1267	.015	.005	.333
658	1266	.010	.003	
659	1265	.013	.010	.769
660	1264	.032	.008	.250
661	1263	.047	.006	.128

DC HOLL NO.		U ₃ O ₈		
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
662	1262	.036	.013	.361
663	1261	.024	.005	.208
664	1260	.020	.005	.250
665	1259	.024		
666	1258	.028		
667	1257	.016		
668	1256	.012		
669	1255	.019		,
670	1254	.026		
671	1253	.022		
672	1252	.014		
673	1251	.011		
674	1250	.007		
675	1249	.007		
676	1248	.007		
677	1247	.007		
678	1246	.006		*
679	1245	.005		
680	1244	.005		
681	1243	.005		E
682	1242	.006		
683	1241	.003		Ī , , , , , , , , , , , , , , , , , , ,
		* * * * * * * * * * * * * * * * * * * *		
691	1233	.008		
692	1232	.008		
693	1231	.007		

DC HOLE NO. 146C U₃O₈

		$\frac{U_3U_8}{}$		
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
694	1230	.006		
695	1229	.007	*	
696	1228	.008		
711	1213	.011	.004	.364
712	1212	.015	.019	1.267
713	1211	.015	.011	.733
714	1210	.013	.012	.923
715	1209	.010	.011	1.100
716	1208	.008	.008	
717	1207	.009	.009	
718	1206	.011	.013	1.182
719	1205	.014	.016	1.143
720	1204	.013	.013	1.000
721	1203	.014	.006	.429
722	1202	.004	.002	
880	1044	.007		
881	1043	.008		
882	1042	.010		
883	1041	.010		
884	1040	.009		
885	1039	.009		
886	1038	.010		
887	1037	.011		
888	1036	.010		
				> "

DC HOLE NO. 146C U_3O_8 DEPTH ELEVATION **GAMMA** CHEMICAL R.E.F. 1035 889 .017 1034 890 .011 891 1033 .014 .003 .214 892 1032 .007 .015 2.143 900 1024 .008 .002 901 1023 .008 .005 902 1022 .013 .005 903 1021 .010 .010 1.000 904 1020 .013 .008 .615 905 1019 .022 .009 .409 906 1018 .060 .011 .183 907 1017 .036 .027 .750 908 1016 .058 .083 1.431 909 1015 .056 .982 .055 1014 910 .037 .072 1.946 911 1013 .036 .044 1.222 912 1012 .019 .040 2.105 913 1011 .074 .023 .311 914 1010 .057 .298 .017 915 1009 .022 .085 3.864 916 1008 .010 .021 2.100 917 1007 .049 .015 .306 918 1006 .037 .007 .189 919 1005 .017 .026 1.529

.052

.013

.250

920

1004

DC HOLE NO. 146C U308 CHEMICAL DEPT ELEVATION **GAMMA** R.E.F. 921 1003 .062 .030 .484 5.357 922 .075 1002 .014 923 1001 .013 .043 3.308 924 .011 .006 1000 .545 925 999 .010 .006 998 926 .007 .008 997 .006 927 .006 CUTOFF GRADE R.E.F.

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DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
514	1467.5	.004		
515	1466.5	.019		
516	1465.5	.016	.028	1.750
517	1464.5	.009	.013	1.444
519	1463.5	.011	.007	.636
520	1461.5	.010		
521	1460.5	.009		*
522	1459.5	.007		HE A R
523	1458.5	.010		
524	1457.5	.015		
525	1456.5	.015	a v	
526	1455.5	.020	.013	.650
527	1454.5	.026	.014	.538
528	1453.5	.030	.031	1.033
529	1452.5	.039	.023	.590
530	1451.5	.017	.048	2.824
531	1450.5	.015	.013	.867
532	1449.5	.012	.011	.917
533	1448.5	.009	.015	1.667
534	1447.5	.013	.012	.923
535	1446.5	.028	.008	.286
536	1445.5	.016		
537	1444.5	.009		
538	1443.5	.009		
539	1442.5	.018		
540	1441.5	.013		

DC HOLE NO. 155C

DC HOLE NO.	155C	U ₃ 0	8	
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
541	1440.5	.008		
542	1439.5	.012	.007*	.582
543-	1438.5	.009	.005*	·
544	1437.5	.007	.021*	3.000
545	1436.5	.023	.054*	2.348
546	1435.5	.068	.038*	.559
547	1434.5	.076	.006*	.079
548	1433.5	.014	.006*	.429
549	1432.5	.009		*
550	1431.5	.009		
551	1430.5	.019	* * .	
552	1429.5	.013		
553	1428.5	.010		
554	1427.5	.006		
555	1426.5	.009		
556	1425.5	.016		
557	1424.5	.013	.015*	1.154
558	1423.5	.015	.007*	.467
559	1422.5	.015	.030*	2.000
560	1421.5	.046	.041*	.891
561	1420.5	.043	.014*	.326
562	1419.5	.016	.011*	.688
563	1418.5	.015		
564	1417.5	.013		3
565	1416.5	.009		
566	1415.5	.008		

DC HOLE NO. 155C

DC HOLE NO.	·155C	U ₃ 0	0	
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
567	1414.5	.005		
568	1413.5	.006		
569	1412.5	.009		
570	1411.5	.013		
571	1410.5	.014		
572	1409.5	.012		
573	1408.5	.010		
574	1407.5	.006		
575	1406.5	.005		
576	1405.5	.005		
577	1404.5	.005		
578	1403.5	.006	.004	
579	1402.5	.015	.005	.333
580	1401.5	.024	.027	1.125
581	1400.5	.010	.013'	1.300
582	1399.5	.009	.006'	
583	1398.5	.009	.007'	
584	1397.5	.033	.022'	.667
585	1396.5	.045	.046'	1.022
586	1395.5	.013	.017'	1.308
587	1394.5	.006	.006'	
588	1393.5	.003		
596	1385.5	.003		
597 -	1384.5	.006		
598	1383.5	.038		
599 -	1382.5	.015		

DC HOLE NO. 155C

DC HOLE NO.	1330	Santa Santa de Carta	U ₃ O ₈	
<u>DEPTH</u>	ELEVATION	GAMMA	CHEMICAL	R.E.F.
600	1381.5	.017		
601	1380.5	.013	3	v 8
602	1379.5	.010		
603	1378.5	.013		
604	1377.5	.010		
	CUTOFF GRADE		R.E.F.	
	.01 .02 .03		.840 .841 .769	

Gamma 2' down Gamma 4' down

HOLE # DC 158	C	U ₃ 0 ₈	• • • • • • • • • • • • • • • • • • • •	
DEPTH E	LEVATION	GAMMA	CHEMICAL	R.E.F.
374	1472.5	.011		
375	1471.5	.022		
376	1470.5	.081		
377	1469.5	.098		
378	1468.5	.067		
379	1467.5	.051		
380	1466.5	.046		
381	1465.5	.033	.029	.879
382	1464.5	.029	.014	.483
383	1463.5	.037	.046	1.243
384	1462.5	.029	.052	1.793
385	1461.5	.035	.016	.457
386	1460.5	.032	.017	.531
387	1459.5	.023	.013	.565
388	1458.5	.024	.015	.625
389	1457.5	.020	.023	1.150
390	1456.5	.019	.028	1.474
391	1455.5	.034	.031	.912
392	1454.5	.025	.017	.680
393	1453.5	.039	.013	.333
394	1452.5	.026	.015	.577
395	1451.5	.010	.019	1.900
396	1450.5	.012	.014	1.167
397	1449.5	.025	.021	.840
398	1448.5	.023	.022	.957
399	1447.5	.024	.022	.917
400	1446.5	.023	.028	1.217
401	1445.5	.027	.023	.852

HOLE # DC 158 C		<u> </u>	-		
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.	
402	1444.5	.027	.029	1.074	
403	1443.5	.021	.034	1.619	
404	1442.5	.031	.026	.839	
405	1441.5	.039	.029	.744	
406	1440.5	.026	.011	.423	
407	1439.5	.023	.012	.522	
408	1438.5	.012	.009	.750	
409	1437.5	.011	.006	.545	
410	1436.5	.011	.006	.545	
440	1406.5	.013	.003	.231	
441	1405.5	.016	.003	.188	
442	1404.5	.010	.003		
443	1403.5	.009	.005		
444	1402.5	.007	.013	1.857	
445	1401.5	.007	.008		
446	1400.5	.006	.012	2.000	
447	1399.5	.006	.022	3.667	
448	1398.5	.006	.027	4.500	
449	1397.5	.007	.036	5.143	
450	1396.5	.010	.027	2.700	
451	1395.5	.013	.006	.462	
452	1394.5	.015	.006	.400	
453	1393.5	.016	.002	.125	
454	1392.5	.022	.001	.045	
455	1391.5	.038	.001	.026	
456	1390.5	.032	.001	.031	
457	1389.5	.012	.002	.167	
458	1388.5	.008	.003		

HOLE # DC	158 C	U ₃ 0 ₈		
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
459	1387.5	.006	.007	
460	1386.5	.006	.011	1.833
461	1385.5	.006	.053	8.833
462	1384.5	.006	.007	
463	1383.5	.006	.011	1.833
464	1382.5	.006	.012	2.000
465	1381.5	.017	.017	1.000
466	1380.5	.024	.024	1.000
467	1379.5	.014	.007	.500
468	1378.5	.012	.005	.417
469	1377.5	.010	.009	
470	1376.5	.018	.006	.333
471	1375.5	.016	.006	.375
472	1374.5	.013	.008	.615
473	1373.5	.010	.010	*
474	1372.5	.009	.009	
475	1371.5	.009	.033	3.667
476	1370.5	.007	.013	1.857
477	1369.5	.010	.010	
478	1368.5	.013		
479	1367.5	.019		
480	1366.5	.018		
481	1365.5	.017		
482	1364.5	.019		
483	1363.5	.021		
484	1362.5	.021		
485	1361.5	.023		
486	1360.5	.021		

HOLE # DC	158 C	U3(08	
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
487	1359.5	.014		
488	1358.5	.013		1
489	1357.5	.013	.033	2.538
490	1356.5	.034	.011	.324
491	1355.5	.101	.011	.109
492	1354.5	.220	.098	.445
493	1353.5	.108	.283	2.620
494	1352.5	.044	.068	1.545
495	1351.5	.041	.061	1.488
496	1350.5	.039	.081	2.077
497	1349.5	.052	.018	.346
498	1348.5	.025	.033	1.320
499	1347.5	.022	.009	.409
500	1346.5	.028	.012	.429
501	1345.5	.023	.009	.391
502	1344.5	.018	.008	. 444
503	1343.5	.013	.009	.692
504	1342.5	.014	.001	.071
505	1341.5	.014	.001	.071
506	1340.5	.012	.004	.333
507	1339.5	.007	.004	
	Cutoff Grad	<u>e</u>	R.E.F.	
	.01 .02 .03		.904 .959 1.014	

DC HO	LE NO.	161C	U ₃ O ₅	,		
DEPTH		ELEVATION	GAMMA	CHEMICAL		R.E.F.
511		1446.5		.003		
512		1445.5		.004		
513		1444.5		.003		
514		1443.5		.002		
515		1442.5		.001		
516		1441.5		.003		
517		1440.5		.001	* *	
518		1439.5	.002	.002		
519		1438.5	.006	.002		
520		1437.5	.032	.003	*	.094
521		1436.5	.016	.003		.188
522		1435.5	.016	.002		.125
523		1434.5	.013	.032		2.462
524		1433.5	.021	.014		.667
525		1432.5	.033	.023		.697
526		1431.5	.055	.014		.255
527	*.	1430.5	.045	.018		.400
528		1429.5	.012	.004		.333
529		1428.5	.017	.012		.706
530		1427.5	.023	.041		1.783
531		1426.5	.039	.012	•	.308
532		1425.5	.030	.010		.333
533		1424.5	.034	.012		.353
534		1423.5	.039	.010		.256
535		1422.5	.039	.041		1.051
536		1421.5	.028	.037		1.321

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DEPTH	ELEVATION .	GAMMA	CHEMICAL	R.E.F.
537	1420.5	.042	.017	.405
538	1419.5	.029	.027	.931
539	1418.5	.031	.121	3.903
540	1417.5	.018	.016	.889
541	1416.5	.021	.037	1.762
542	1415.5	.017	.031	1.824
543	1414.5	.022	.032	1.455
544	1413.5	.021	.025	1.190
545	1412.5	.026	.023	.885
546	1411.5	.022	.019	.864
547	1410.5	.015	.018	1.200
548	1409.5	.013	.020	1.538
549	1408.5	.016	.025	1.563
550	1407.5	.009	.021	2.333
551	1406.5	.007	.016	2.286
552	1405.5	.009	.014	1.556
553	1404.5	.008	.015	1.875
554	1403.5	.009	.011	1.222
555	1402.5	.006	.006	
556	1401.5	.009	.008	
557	1400.5	.009	.006	
558	1399.5	.008	.007	
559	1398.5	.008	.007	
560	1397.5	.007	.005	
561	1396.5	.008	.009	
562	1395.5	.013	.009	.692

DC HOLE NO	161C	U ₃ O ₈		g- 1
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
561	1396.5	.008	.009	
562	1395.5	.013	.009	.692
563	1394.5	.010	.008	, , , , , , , , , , , , , , , , , , , ,
564	1393.5	.008	.007	
565	1392.5	.007	.007	
566	1391.5	.007	.009	
567	1390.5	.006	.011	1.833
568	1389.5	.013	.006	.462
569	1388.5	.034	.006	.176
570	1387.5	.053	.004	.075
571	1386.5	.020	.005	.250
572	1385.5	.018	.005	.278
573	1384.5	.014	.009	.643
574	1383.5	.019	. 044	2.316
575	1382.5	.010	.041	4.100
576	1381.5	.009	.009	
577	1380.5	.006	.010	
578	1379.5	.008	.016	2.000
579	1378.5	.009	.015	1.667
580	1377.5	.010	.010	
581	1376.5	.011	.006	.545
582	1375.5	.011	.005	.455
583	1374.5	.009	.009	
584	1373.5	.006	.009	
585	1372.5	.008	.012	1.500
586	1371.5	.010	.010	

DC HOLE NO.	1010	U ₃ O ₈		
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
587	1370.5	.009	.010	
588	1369.5	.002	.007	
589	1368.5		.006	
590	1367.5		.012	
591	1366.5		.010	
592	1365.5	.006	.003	
593	1364.5	.010	.003	
594	1363.5	.016	.002	.125
595	1362.5	.037	.001	.027
596	1361.5	.039	.004	.103
597	1360.5	.016	.004	.250
598	1359.5	.016	.007	.438
599	1358.5	.066	.046	.697
500	1357.5	.068	.044	.647
601	1356.5	.023	.035	1.522
602	1355.5	.017	.008	.471
603	1354.5	.026	.018	.692
604	1353.5	.027	.124	4.593
605	1352.5	.015	.038	2.533
606	1351.5	.006	.014	2.333
607	1350.5	.006	.036	6.000
608	1349.5	.006	.035	5.833
609	1348.5	.006	.016	2.667
610	1347.5		.003	
611	1346.5		.002	
612	1345.5		.002	
613	1344.5		.001	

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DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
614	1343.5		.001	4
615	1342.5	.008	.001	
616	1341.5	.011	.001	.091
617	1340.5	.014	.002	.0143
618	1339.5	.007	.002	
619	1338.5	.005	.012	2.400
620	1337.5	.007	.011	1.571
621	1336.5	.013	.012	.923
622	1335.5	.007	.006	
623	1334.5	.006	.003	
624	1333.5	.007	.013	1.857
625	1332.5	.005	.011	2.200
626	1331.5	.009	.007	
627	1330.5	.015	.004	.267
628	1329.5	.018	.006	.333
629	1328.5	.035	.004	.114
630	1327.5	.009	.006	
631	1326.5	.015	.020	1.333
632	1325.5	.018	.017	.944
633	1324.5	.034	.015	.441
634	1323.5	.032	.012	.375
635	1322.5	.020	.021	1.050
636	1321.5	.034	.014	.412
637	1320.5	.015	.045	3.000
638	1319.5	.013	.015	1.154
639	1318.5	.057	.122	2.140
640	1317.5	.035	.014	.400

DC	HOLE	NO.	161C
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be note no.	1610	U ₃ 0	8	_
DEPTH	ELEVATION	GAMMA	CHEMICAL	<u>R.E.F.</u>
641	1316.5	.023	.009	.391
642	1315.5	.020	.160	8.000
643	1314.5	.017	.012	.706
644	1313.5	.033	.011	.333
645	1312.5	.028	.013	.464
646	1311.5	.014	.034	2.429
647	1310.5	.009	.046	5.111
648	1309.5	.009	.036	4.000
649	1308.5	.005	.005	
650	1307.5	.005	.004	
651	1306.5		.003	
652	1305.5		.003	
653	1304.5		.001	
654	1303.5		.001	
655	1302.5	*	.001	
656	1301.5		.001	
657	1300.5		.001	
658	1399.5		.001	
659	1298.5		.001	
660	1297.5		.001	r z ×
661	1296.5		.001	
662	1295.5		.001	
663	1294.5		.001	
	CUTOFF GRADE		R.E.F.	
•	.01		1.037	
	.02		1.108	

1.168

DC HOLE NO.		U ₃ O ₈		
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
546	1408.5	.006	.005	
547	1407.5	.007	.004	
548	1406.5	.008	.007	
549	1405.5	.007	.008	
550	1404.5	.008	.006	
551	1403.5	.013	.005	.385
552	1402.5	.015	.013	.867
553	1401.5	.026	.010	.385
554	1400.5	.011	.033	3.000
555	1399.5	.003	.004	
556	1398.5		.004	
557	1397.5		.002	*
558	1396.5		.002	
559	1395.5	.006	.002	
560	1394.5	.009	.002	
561	1393.5	.008	.002	
562	1392.5	.003	.007	
563	1391.5		.002	
564	1390.5		.002	
565	1389.5	· · · · · · · · · · · · · · · · · · ·	.002	
566	1388.5		.002	
567	1387.5		.002	
568	1386.5		.002	
569	1385.5		.002	
570	1384.5		.001	
571	1383.5		.002	

		U ₃ O ₈	}	
<u>DEPTH</u>	ELEVATION	GAMMA	CHEMICAL	R.E.F.
572	1382.5		.002	
573	1381.5	3	.003	à
574	1380.5	.005	.003	
575	1379.5	.017	.003	.176
576	1378.5	.021	.002	.095
577	1377.5	.171	.036	.211
578	1376.5	.046	.211	4.587
579	1375.5	.088	.048	. 545
580	1374.5	.019	.027	1.421
581	1373.5	.021	.019	.905
582	1372.5	.007	.006	
583	1371.5	.008	.006	
584	1370.5	.005	.005	
585	1369.5	.006	.007	
586	1368.5	.008	.005	
587	1367.5	.026	.008	.308
588	1366.5	.012	.010	.833
589	1365.5	.013	.028	2.154
590	1364.5	.016	.013	.813
591	1363.5	.017	.013	.765
592	1362.5	.024	.017	1.417
593	1361.5	.022	.022	1.000
594	1360.5	.014	.032	2.286
595	1359.5	.016	.020	1.250
596	1358.5	.019	.013	.684
597	1357.5	.014	.018	1.286

DC HOLE NO. 165C

		U ₃ 0 ₈	·	
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
598	1356.5	.013	.012	.923
599	1355.5	.007	.015	2.143
600	1354.5	.007	.008	
601	1353.5	.006	.008	
602	1352.5	.007	.005	
603	1351.5	.008	.007	
604	1350.5	.009	.020	2.222
605	1349.5	.010	.010	1.000
606	1348.5	.005	.011	2.200
607	1347.5	.005	.020	4.000
608	1346.5	.007	.003	
609	1345.5	.007	.005	A
610	1344.5	.006	.007	
611	1343.5	.006	.006	,
612	1343.5	.010	.004	
613	1341.5	.011	.007	.636
614	1340.4	.010	.009	
615	1339.5	.010	.009	
616	1338.5	.012	.007	.583
617	1337.5	91013	.009	.692
618	1336.5	.018	.010	.556
619	1335.5	.026	.012	.462
620	1334.5	.023	.011	.478
621	1333.5	.010	.033	3.300
622	1332.5	.010	.026	2.600
623	1331.5	.010	.007	
624	1330.5	.016	.009	.563

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DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
625	1329.5	.029	.007	.241
626	1328.5	.029	.010	. 345
627	1327.5	.018	.057	3.167
628	1326.5	.010	.026	2.600
629	1325.5	.007	.012	1.714
	CUTOFF GRADE		R.E.F.	
	.010		1.017	
k.	.020		1.039	
	.030		1.257	

DC HOLE NO.	169C	U ₃ O ₈	9	
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
606	1315		.004	
607	1314		.005	
608	1313	.003	.006	
609	1312	.009	.007	
610	1311	.012	.016	1.333
611	1310	.024	.016	.667
612	1309	.018	.016	.889
613	1308	.022	.016	.727
614	1307	.019	.015	.789
615	1306	.019	.010	.526
616	1305	.018	.052	2.889
617	1304	.019	.015	.789
618	1303	.018	.014	.778
619	1302	.016	.010	.625
620	1301	.011	.008	.727
621	1300	.015	.010	.667
622	1299	.021	.021	1.000
623	1298	.025	.010	.400
624	1297	.026	.014	.538
625	1296	.015	.010	.667
626	1295	.020	.012	.600
627	1294	.016	.012	.750
628	1293	.020	.012	.600
629	1292	.036	.011	.306
630	1291	.048	.030	.625
631	1290	.030	.045	1.500

DC HOLE NO. 169C

DC HOLE NO.	169C	II. O		
DEDTH	DI DIAMANA	U ₃ 0 ₈		
DEPTH	ELEVATION		CHEMICAL	R.E.F.
632	1289	.027	.030	1.111
633	1288	4.016	.014	.875
634	1287	.021	.026	1.238
635	1286	.015	.014	.933
636	1285	.018	.030	1.667
637	1284	.021	.022	1.048
638	1283	.022	.028	1.273
639	1282	.026	.030	1.154
640	1281	.031	.035	1.129
641	1280	.028	.039	1.393
642	1279	.062	.035	.565
643	1278	.027	.028	1.037
644	1277	.013	.019	1.462
645	1276	.008	.009	
646	1275	.010	.009	
647	1274	.011	.009	.818
648	1273	.019	.017	.895
649	1272	.020	.020	1.000
650	1271	.016	.018	1.125
651	1270	.015	.008	.533
652	1269	.014	.017	1.214
653	1268	.007	.010	
654	1267	.007	.005	* * *
655	1266	.007	.006	

DC HOLE NO. 169C

DC HOLE NO	169C	. 11.0		
DEPTH	ELEVATION	U ₃ O ₈	CUEMICAL	D E E
	ELEVATION	GAMMA	CHEMICAL	R.E.F.
666	1255	.006	.007	
667	1254		.007	3
668	1253		.004	
669	1252		.003	
670	1251		.002	
671	1250		.002	
672	1249	.008	.001	
673	1248	.011	.013	1.182
674	1247	.007	.007	
675	1246	.003	.002	
676	1245		.002	* * * * * * * * * * * * * * * * * * *
677	1244		.002	
678	1243		.002	
679	1242	* * * * * * * * * * * * * * * * * * * *	.001	
680	1241		.002	
681	1240		.001	
682	1239		.002	
683	1238	.007	.013	1.857
684	1237	.011	.008	.727
685	1236	.011	.007	.636
686	1235	.008	.006	*
687	1234		.004	
688	1233		.001	
689	1232		.001	
690	1231		.002	
691	1230		.002	

DC HOLE NO. 169C

		3-8		
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
692	1229		.002	
693	1228		.001	
694	1227		.001	
695	1226		.001	
696	1225		.001	
697	1224		.001	
698	1223		.001	
699	1222	Y A S	.001	
700	1221		.001	
701	1220		.001	
702	1219	.008	.003	
703	1218	.020	.007	.350
704	1217	.012	.021	1.750
705	1216	.003	.004	
706	1215		.004	
707	1214	.003	.004	
708	1213	.009	.004	
709	1212	.007	.008	
710	1211	.010	.006	
711	1210	.011	.005	.455
712	1209	.013	.008	.615
713	1208	.009	.009	
714	1207	.008	.006	
715	1206	.009	.007	
716	1205	.010	.008	
717	1204	.015	.005	.333

U308

DEPTH

169C			
	U	308	
ELEVATION	GAMMA	CHEMICAL	R.E.F
1203	.020	.010	.500
1202	.024	.022	.917
1201	.026	.025	.962
1200	.034	.017	.500
1199	.013	.045	3.462
1198	.007	.035	5.000
1197	.007	.006	
1196	.007	.003	
1195	,	.002	
1194		.001	
1193		.001	E 1 4
1192		.001	
1191		.001	
1190		.001	
1189		.001	
1188		.001	
1187		.001	
1186		.001	
1105	8 P S S X R		

1188					.001
1187					.001
1186					.001
1185					.001
1184					.001
1183				* .	.001
CUTOFF	GRADE				R.E.F.
.01		\			.938
.02					1.052
.03					1.121
					2.4

DC HOLE NO. ___171C

		U ₃ O ₈	77. The state of t		
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.	
661	1320		.002		
662	1319		.002		
663	1318		.003		
664	1317		.001		
665	1316		.001	* *	
666	1315		.001		
667	1314		.001		
668	1313		.002		
669	1312		.003		
670	1311		.003		
671	1310		.002		
672	1309	.004	.003		
673	1308	.009	.001		
674	1307	.008	.007		
675	1306	.010	.004		
676	1305	.014	.001	.071	
677	1304	.014	.016	1.143	
678	1303	.009	.021	2.333	
679	1302	.010	.011	1.100	
680	1301	.012	.005	.417	
681	1300	.007	.012	1.714	
682	1299	.007	.007		
683	1298	.005	.003		
684	1297	.007	.001		
685	1296	.013	.001	.077	
686	1295	.013	.004	.308	
687	1294	.039	.001	.026	

DC HOLE NO. 171C

			1308	
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
688	1293	.055	.040	.727
689	1292	.031	.034	11.097
690	1291	.036	.035	.972
691	1290	.155	.016	.103
692	1289	.228	.017	.075
693	1288	.054	.214	3.963
694	1287	.061	.172	2.820
695	1286	.034	.030	.882
696	1285	.016	.101	6.313
697	1284	.022	.017	.773
698	1283	.033	.009	.273
699	1282	.031	.010	.323
700	1281	.027	.038	1.407
701	1280	.024	.028	1.167
702	1279	.028	.017	.607
703	1278	.029	.028	.966
704	1277	.031	.017	.548
705	1276	.015	.017	1.133
706	1275	.016	.016	1.000
707	1274	.022	.013	.591
708	1273	.021	.012	.571
709	1272	.025	.018	.720
710	1271	.046	.022	.478
711	1270	.019	.019	1.000
712	1269	.014	.046	3.286
713	1268	.012	.015	1.250

DC HOLE NO. 171C

U₃0₈

<u>DEPTH</u>	ELEVATION	GAMMA	CHEMICAL	R.E.F.		
714	1267	.014	.009	.643		
715	1266	.020	.010	.500		
716	1265	.026	.011	3		
717	1264	.029	.009	.423		
718	1263	.013	.049	.310		
719	1262	.009	.015	3.769		
720	1261	.007	.014	1.667		
721	1260	.008	.008	2.000		
722	1259	.006	.008			
723	1258	.011				
724	1257	.012	.005	.455		
725	1256	.012		. 41.7		
726	1255	.014	.007	.583		
727	1254	.024	.011	.786		
728	1253	.016	.010	.417		
729	1252	.016	.026	1.625		
730	1251	.007	.020	1.250		
731	1250	.007	.011	1.571		
732	1249	.007	.003			
733	1248	.007	.003			
734	1247	r	.005			
735	1246	.009	.004			
736	1245	.018	.007	.389		
737	1244	.016	.031	1.938		
738	1243	.010	.018	1.800		
739	1243	.004	.003			
	1444		.001			

171C DC HOLE NO. _ U₃0₈ **DEPTH** ELEVATION **GAMMA** CHEMICAL 740 1241 .002 1240.5 740.5 .001 CUTOFF GRADE R.E.F. .01 .900 .02 .914

.959

.03

R.E.F.

DC HOLE NO. 175C

DC HOLE NO.	175C	UzOg		
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
560	1516.5	.006	:	4
561	1515.5	.013	.006	.462
563	1514.5	.022	.004	.182
563	1513.5	.012	.004	.333
564	1512.5	.007	.006	
565	1511.5	.008	.037	4.625
566	1510.5	.016	.008	.500
567	1509.5	.015	.005	.333
568	1508.5	.022	.004	.182
569	1507.5	.022	.007	.318
570	1506.6	.004	.018	4.500
571	1505.5		.018	
572	1504.5		.026	
573	1503.5	* .	.011	
574	1502.5		.002	
575	1501.5		.001	
576	1500.5	.008	.002	
577	1499.5	.011	.001	.091
578	1498.5	.003	.001	
579	1497.5	.004	.001	
580	1496.5	.013	.002	.154
581	1495.5	.009	.012	1.333
582	1494.5	.003	.007	
583	1493.5	.007	.003	
584	1492.5	.010	.004	
585	1491.5	.015	.011	.733

DC HOLE NO.		U ₃ O ₅	,	
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
586	1490.5	.057	.054	.947
587	1489.5	.064	.021	.328
588	1488.5	.031	.085	2.742
589	1487.5	.007	.018	2.571
590	1486.5	.003		
591	1485.5			
592	1484.5		.006	
593	1483.5		.004	
594	1482.5		.004	
595	1481.5		.002	
596	1480.5	.006	.001	1
597	1479.5	.007	.001	
598	1478.5	.003	.001	
599	1477.5		.001	1
600	1476.5		.002	
601	1475.5		.001	
602	1474.5		.008	** *** *** *** *** *** *** *** *** ***
603	1473.5		.016	
604	1472.5	.007	.099	14.143
605	1471.5	.023	.033	1.435
606	1470.5	.065	.026	.400
607	1469.5	.016	.009	.563
608	1468.5	.012	.004	.333
609	1467.5	.007	.003	
610	1466.5	.003	.002	

CHEMICAL DOWN 5'

CUTOFF	GRADE		R.E.F.
.010			1.009
.020			1.153
.030			1.392

DC HOLE NO. 176C

		U_	308	
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
531	1556.5		.002	
532	1555.5	.003	.002	
533	1554.5	.010	.002	s
534	1553.5	.009	.009	
535	1552.5	.007	.010	**
536	1551.5	.007	.005	
537	1550.5	.007	.004	
538	1549.5	.007	.004	*
539	1548.5	.008	.002	
540	1547.5	.011	.004	.364
541	1546.5	.004	.017	4.250
542	1545.5	E	.005	
543	1544.5		.002	* * * * * * * * * * * * * * * * * * *
544	1543.5		.005	
545	1542.5		.002	
546	1541.5	.003	.002	
547	1540.5	.008	.002	
548	1539.5	.014	.004	.286
549	1538.5	.015	.010	.667
550	1537.5	.010	.014	1.400
551	1536.5	.010	.015	1.500
552	1535.5	.009	.006	
553	1534.5	.010	.007	.636
554	1533.5	.010	.007	
555	1532.5	.013	.769	
556	1531.5	.061	.006	.098

		U ₃ O ₈		
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
556	1531.5	.061	.006	.098
557	1530.5	.066	.012	.182
558	1529.5	.008	.210	26.250
559	1528.5	.007	.012	1.714
560	1527.5	.009	.006	
561	1526.5	.012	.009	.750
562	1525.5	.013	.013	1.000
563	1524.5	.005	.014	2.800
564	1523.5	.005	.003	
565	1522.5	.005	.004	
566	1521.5	.008	.005	8 · 8
567	1520.5	.021	.005	.286
568	1519.5	.052	.002	.038
569	1518.5	.056	.005	.089
570	1517.5	.085	.105	1.235
571	1516.5	.070	.012	.171
572	1515.5	.032	.240	7.500
573	1514.5	.022	.012	.545
574	1513.5	.019	.006	.316
575	1512.5	.006	.005	
576	1511.5	.006	.003	
577	1510.5	.008	.006	
578	1509.5	.015	.009	.600
579	1508.5	.023	.004	.174
580	1507.5	.028	.002	.071
581	1506.5	.020	.023	1.150

DC HOLE NO. 176C UzOg R.E.F. CHEMICAL **GAMMA** ELEVATION DEPTH .519 .014 .027 1505.5 582 1.533 .023 .015 1504.5 583 3.400 .017 .005 1503.5 584 6.200 .031 .005 1502.5 585 .005 .005 1501.5 586 .002 .005 1500.5 587 .002 1499.5 588 .002 1498.5 589 .001 1497.5 590 .001 1496.5 591 .004 1495.5 592 .003 1494.5 593 .004 .005 1493.5 594 2.357 .033 .014 1492.5 595 .826 .019 .023 1491.5 596 .972 .035 .036 1490.5 597 1.000 .019 .019 1489.5 598 .139 .005 .036 1488.5 599 .148 .004 .027 1487.5 600 .250 .004 .016 1486.5 601 .004 .006 1485.5 602 .006 .007 1484.5 603 .005 .006 1483.5 604 .004 .006 1482.5 605 .004 1481.5 606 .005 1480.5

607

DC HOLE NO. 176C

DC HOLL NO.					
		U ₃ O ₈			
<u>DEPTH</u>	ELEVATION	GAMMA	CHEMICAL		R.E.F.
608	1479.5		.006		
609	1478.5		.010	,	
610	1477.5		.033		
	CUTOFF GRADE		R.E.F.	,	
	.01		1.066		Y. al
	.02	•	1.105		
	.03		1.336		

DC HOLE NO. 177C

DC HOLE NO.	1//0	U ₃ O ₈		
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
541	1365.5	.028	.018	.643
542	1364.5	.025	.023	.920
543	1363.5	.030	.044	1.467
544	1362.5	.025	.022	.880
545	1361.5	.020	.017	.850
546	1360.5	.019	.012	.632
547	1359.5	.017	.015	.882
548	1358.5	.018	.013	.722
549	1357.5	.023	.028	1.217
550	1356.5	.027	.016	.593
551	1355.5	.020	.028	1.400
552	1354.5	.014	.010	.714
553	1353.5	.014	.014	1.000
554	1352.5	.014	.010	.714
555	1351.5	.014	.009	.643
556	1305.5	.014	.008	.571
557	1349.5	.008	.006	
558	1348.5	.008	.014	1.750
559	1347.5	.008	.007	
560	1346.5	.013	.007	.538
561	1345.5	.011	.022	2.000
562	1344.5	.011	.020	1.818
563	1343.5	.029	.006	.207
564	1342.5	.022	.004	.182
565	1341.5	.009	.003	Tw.
566	1340.5	.005	.003	

DC HOLE NO. 177C

		U ₃ O ₈		
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
567	1339.5	.005	.004	9
568	1338.5	.005	.015	3.000
569	1337.5	.007	.007	
570	1336.5	.014	.010	.714
571	1335.5	.010	.004	
572	1334.5	.007	.007	
573	1333.5	.007	.004	
574	1332.5	.007	.004	
575	1331.5	.011	.006	.545
576	1330.5	.012	.009	.750
577	1329.5	.018	.040	2.222
578	1328.5	.033	.040	1.212
579	1327.5	.033	.009	.273
584	1322.5	.008	.006	
585	1321.5	.013	.007	.538
586	1320.5	.022	.007	.318
587	1319.5	.018	.007	.389
588	1318.5	.011	.010	.909
589	1317.5	.009	.113	12.556
590	1316.5	.006	.010	
591	1315.5	.006	.006	
592	1314.5	.005	.007	
593	1313.5	.007	.003	
594	1312.5	.008	.003	
595	1311.5	.007	.004	

DC HOLE NO. 177C

DC HOLE NO	177C	U ₃ O ₈		
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
596	1310.5	.006	.008	*
597	1309.5	.006	.006	•
598	1308.5	.006	.005	
599	1307.5	.009	.005	
600	1306.5	.008	.004	
601	1305.5	.007	.005	
602	1304.5	.016	.006	.375
603	1303.5	.012	.005	.417
604	1302.5	.017	.011	.647
605	1301.5	.026	.013	.500
606	1300.5	.018	.008	. 444
607	1299.5	.014	.033	2.357
608	1298.5	.010	.016	1.600
609	1297.5	.003	.012	4.000
610	1296.5		.009	
611	1295.5		.004	
612	1294.5		.002	
613	1293.5	Gamma up 2'	.001	
614	1292.5	to core	.001	
615	1291.5	As a second	.001	
616	1290.5	Gamma	.001	
617	1289.5	Flat to core	.001	
618	1288.5		.001	
619	1287.5	.008	.003	
620	1286.5	.016	.026	1.625
621	1285.5	.011	.008	.727

DC HOLE NO. ____177C

¥		U ₃ O ₈	}	
<u>DEPTH</u>	ELEVATION	GAMMA	CHEMICAL	R.E.F.
622	1284.5		.002	
623	1283.5		.003	
624	1282.5	.003	.004	
625	1281.5	.006	.004	
626	1280.5	.006	.004	
627	1279.5	.008	.010	
628	1278.5	.009	.006	
629	1277.5	.006	.006	
630	1276.5	.007	.005	
631	1275.5	.010	.010	
632	1274.5	.009	.007	
633	1273.5	.010	.009	
634	1272.5	.017	.010	.588
635	1271.5	.021	.014	.667
636	1270.5	.038	.051	1.342
637	1269.5	.028	.016	.571
638	1268.5	.021	.014	.667
639	1267.5	.012	.012	1.000
640	1266.5	.009	.006	
641	1265.5	.010	.008	
642	1264.5	.014	.017	1.214
643	1263.5	.011	.005	.455
644	1262.5	.005	.003	
645	1261.5	.005	.002	
646	1260.5		.002	
647	1259.5		.002	

×	U ₃ O ₈				
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.	
648	1258.5		.002		
649	1257.5		.002		
650	1256.5		.002		
651	1255.5		.003		
652	1254.5	*	.002	W.	
653	1253.5	e N	.002		
654	1252.5		.002		
655	1251.5		.001		
556	1250.5		.001		
657	1249.5		.001		
658	1248.5		.001		
659	1247.5		.001	***	
660	1246.5		.001		
661	1245.5		.001		
662	1244.5		.001		
663	1243.5		.001		
	CUTOFF GRADE		R.E.F.		
	.01		.989		
	.02	8 × 1	1.131		
	.03		1.886 - <u>Note</u> :	based on only 7 samples	

^{*} Gamma up 2' to core in to 1/2 of this hole

DC HOLE NO. Tonto 8C

DC HOLE NO	Tonto 8C	U_3(0,8	
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
539	1378.5	.016		
540	1377.5	.015	*	
541	1376.5	.013	.063	4.846
542	1375.5	.019	.005	.263
543	1374.5	.026	.015	.577
544	1373.5	.047	.026	.553
545	1372.5	.055	.035	.636
546	1371.5	.028	.036	1.286
547	1370.5	.013	.012	.923
548	1369.5	.015	.013	.867
549	1368.5	.021	.015	.714
550	1367.5	.030	.020	.667
551	1366.5	.058	.036	.621
552	1365.5	.032	.047	1.469
553	1364.5	.065	.016	.246
554	1363.5	.131	.092	.702
555	1362.5	.032	.064	2.000
556	1361.5	.023	.010	.435
557	1360.5	.020	.010	.500
558	1359.5	.017	.021	1.235
559	1358.5	.028	.013	.464
560	1357.5	.007	.025	3.571
561	1356.5	.012	.007	.583
562	1355.5	.008		
563	1354.5	.014		
564	1353.5	.019		

DC HOLE NO.	Tonto 8C	U ₃ 0 ₈		
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
565	1352.5	.018	.018	1.000
566	1351.5	.3017	.016	.941
567	1350.5	.015	.016	1.067
568	1349.5	.012	.013	1.083
569	1348.5	.011	.010	.090
570	1347.5	.013	.009	.692
571	1346.5	.010		***
572	1345.5	.006		
573	1344.5	.007		
574	1343.5	.006		
575	1342.5	.010		
576	1341.5	.027	.006	.222
577	1340.5	.012	.026	2.167
578	1339.5	.013	.009	.692
579	1338.5	.016	.008	.500
580	1337.5	.030	.011	.367
581	1336.5	.016	.021	1.313
582	1335.5	.016	.027	1.688
583	1334.5	.013	.015	1.154
584	1333.5	.070	.011	.550
585	1332.5	.030	.006	.200
586	1331.5	.035	.022	.629
587 -	1330.5	.062	.018	.290
588	1329.5	.071	.052	.732
589	1328.5	.027	.058	2.148
590	1327.5	.009	.052	5.778

DC HOLE NO.	Tonto 8C	U ₃ 0	8	
<u>DEPTH</u>	ELEVATION	GAMMA	CHEMICAL	R.E.F.
591	1326.5	.006	.009	
592	1325.5	.006	.004	
593	1324.5	.006		
594	1323.5	.006		* *
595	1322.5	.006		
601	1316.5	.005		
602	1315.5	.009	.0041	
603	1314.5	.017	.035	2.059
604	1313.5	.023	.015	.652
605	1312.5	.016		
606	1311.5	.043		**
607	1310.5	.061	.0041	.066
608	1309.5	.027	.0061	.222
609	1308.5	.013	.033	2.538
610	1307.5	.007	.047	6.714
611	1306.5	.003	.037	12.333
612	1305.5		.012	
614	1707 5	0.06		
614	1303.5	.006		
615	1302.5	.009		
616	1301.5	.009		
617	1300.5	.000		
618	1299.5	.006		
619.	1298.5	.009	1	
620	1297.5	.015	.011	.733
* *	8,	9	**	

DC HOLE NO	Tonto 8C	U ₃ (),	,
DEPTH	ELEVATION	GAMMA	CHEMICAL	R.E.F.
621	1296.5	.021	.0251	1.190
622	1295.5	.011	.016	1.455
623	1294.5	.008		
628	1289.5	.006		
629	1288.5	.011		
630	1287.5	.009		
631	1286.5	.010		
632	1285.5	.018	.1252	1.389
633	1284.5	.016	.0322	2.000
634	1283.5	.011	.0322	2.909
635	1282.5	.022	.0032	.136
636	1281.5	.050	.0122	.240
637	1280.5	.077	.0142	.182
638	1279.5	.181	.0592	.326
639	1278.5	.117	.0882	.752
640	1277.5	.102	.1282	1.255
641	1276.5	.058	.1612	2.776
642	1275.5	.008	.0042	
643	1274.5	.011	.0012	.091
644	1273.5	.010		
	CUTOFF GRADI	3	R.E.F.	
	.01 .02 .03		.879 .897 .943	
•		cal up 3'		

APPENDIX I

HAZEN RESEARCH, INC.



WET OR DRY DENSITY? CUTOFF FOR Equil 4601 INDIANA STREET GOLDEN, COLORADO 80401 TELEPHONE 303/279-4501

HRI Project 4603
Copy No. _/

ANALYTICAL RESULTS
OF DATE CREEK DRILL CORES

for

Urangesellschaft U.S.A., Inc. 6000 E. Evans Avenue Building 3, Suite 200 Denver, Colorado 80222

February 6, 1979

Prepared by:

Dennis M. Johnson Research Engineer Approved by:

P. N. Thomas Vice President

4603 - Date Cree

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		202	- 1																												
		Gamma	Equiv							3 .																					
		Beta	Equiv																												
	8	Beta/	Gamma																												
	TraCo	4	ruorimetric		8				0.002										0 003											0.020	
		Fluorimetric	1	0.002	2000	0.003	0.002		0.00	0.003	0.002	100.0	0.001	0.002	0.00	0.002	1000	0.002			0.003	0.005	0.009	0.00	0.008		800.0	0.014	0.015		0.019
		H2O		10.5	19.6	14.4	13.2	13.6	11,4	9.5	ອ ແ ຜ		ο · ·	15.4	20.8	17.5	17.7	15.1	33.7	8.8	16.54	15.4	10.7	20.1	19.9		200				8.42/ 14.22/
		Dry 1/ Grams		858	209	871	963	1105	1098	1080	1006	1146	1115	842	795	624	952	686	1159	895	2 2	1305		791		,	1105		1105		1135 908 1
	į	HRI No.	14220-1	-2-	e-	4-	5.	9	-1	φ.	î -	-	-12	-13	-14	-15	-16	-17	-18	-19	3 . 5	-22	-53	-24	-25	-26	-27	-28	-30	: :	-37
		Footage	460-461	-462	-463	-464	-465	-466	-467	-468	-470	-471	-472	-473	-474	-475	-476	-477	-4/8	-480	-481	-482	-483	-484	-485	-486	-487	-488	-490	107	-492
	2	Hole	145-C 4																											×	v

One-half core before removing assay pulps (2 pulps from Samples 1-204, I pulp thereafter). Each pulp weights approximately 150 g.

CI = Composite interval.

3/ Reblended.

House Hous							van one						7 20 2)	(2 or 4/ pages)	
Pootage No. Check Beta Beta Corganic Fl-7 Ann Check Beta Corganic Fl-7 Ann Check Corganic Check Check Corganic Check	2			,			U3OB								ī
492-493 14329-33 1128 17.92 ² 0.010 -494 -34 1032 16.92 ² 0.0012 -495 -35 1089 12.62 ² 0.002 -496 -36 1089 12.62 ² 0.0014 -498 -38 1138 12.22 ² 0.017 -498 -38 1138 12.22 0.011 -499 -38 1135 15.52 ² 0.001 -40 1182 11.52 ² 0.007 -40 1182 11.52 ² 0.007 -500 -40 1182 11.52 ² 0.007 -501 -41 1182 11.52 ² 0.007 -503 -43 1069 11.52 ² 0.007 -503 -44 1231 11.52 ² 0.007 -504 -44 1231 11.52 ² 0.019 -505 -45 10.008 -506 -46 11.51 15.62 -507 -47 10.008 -508 -48 10.008 -509 -49 11.44 12.51 15.62 -509 -40 11.40 0.11 -50 10.40 0.003 0.003 0.003 0.003 0.003 0.004 -50 11.40 0.103 0.003 0.003 0.003 0.003 0.008 -50 11.40 0.103 0.003 0.003 0.003 0.003 0.003 0.003 0.003 -50 11.40 11.52 ² 0.013 -50 11.40 0.103 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 -50 11.40 0.103 0.003	Hole	Footage	No.	Grams	H20	Fluorimetric	Check Fluorimetric		Beta	Gamma	% CO CO	C Organic	Ft3/ton	6	
-494 -394 1032 16.32 0.000 -495 -39 1032 16.32 0.000 -498 -39 1133 12.32 0.001 -498 -39 1133 12.32 0.001 -409 -39 1133 12.32 0.001 -40 1132 12.32 0.001 -40 1132 12.32 0.001 -40 1132 12.32 0.001 -40 1132 12.32 0.001 -40 1132 12.32 0.000 -40 1140 12.30 0.000 -40 1140 12.30 0.000 -40 1140 12.30 0.000 -40 1140 12.30 0.000 -40 1140 12.30 0.000 -40	45-C	492-493	14329-33	1128	17.02/								Delistry	50.00	.,
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1120 5.5 0.009 1245 6.9 0.009 11245 6.9 0.0009 11245 6.9 0.0009 11245 6.9 0.0009 11245 6.9 0.0009 1139 9.4 0.007 1139 9.4 0.007 1139 9.4 0.007 1132 0.0009 1132 0.0009 0.01 0.008 0.004 0.1 0.1 1.1 17.0 2.26 11.32 0.009 0.01 0.008 0.004 0.1 0.1 1.1 17.0 2.26 11.32 0.009 0.02 0.009 0.01 0.00 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0		89-	831	10.2	0.007	0.005								
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1153 4.2 0.008 1154 6.5 0.008 1154 6.5 0.009 1154 6.5 0.009 1155 1.2 0.009 1151 1.2 0.009 1152 1.3 0.009 1153 1.3 0.009 1154 1.3 0.009 1155 1.3 0.009 1062 1.0 0.002 0.0 1072 1.0 0.009 1072 1.0 0.009 1072 1.0 0.009 1073 1.0 0.003 1074 1.0 0.003 1075 1.0 0.003 1075 1.0 0.003 1075 1.0 0.003 1075 1.0 0.003 1075 1.0 0.004 1075 1.0 0.004 1075 1.0 0.004 1075 1.0 0.004 1075 1.0 0.005 1075 1.0 0.005 1075 1.0 0.005 1075 1.0 0.005 1075 1.0 0.005 1075 1.0 0.005 1075 1.0 0.005 1075 1.0 0.005 1075 1.0 0.005 1075 1.0 0.005 1075 1.0 0.005 1075 1.0 0.005 1075 1.0 0.005 1075 1.0 0.005 1075 1.0 0.005 1075 1.0 0.005 1075 1.0 0.005 1075 0.005 1075 0.005 1075 0.005 1075 0.005 1075 0.005 1075 0.005 1075 0.005 1075 0.005 1075 0.005 1077 0.005 1077 0.011 0.01 1071 1.0 15.1 1071 1.0 15.1 1071 1.0 15.1 1071 1.0 1071 1.0 1.0 1		-20	1245	6.9	600.0									
1153 9.4 0.007 1174 8.5 0.009 1174 8.5 0.009 1174 8.5 0.009 1175 8.5 0.009 1175 1.1 1.1 1.1 1170 1.2 1183 7.1 0.009 1183 7.1 0.009 1183 7.1 0.009 1192 11.32 0.003 1102 16.42 0.013 0.01 0.005 1102 16.42 0.013 0.11 1102 16.42 0.013 0.12 0.005 1102 16.42 0.010 0.010 0.005 0.005 1103 14.92 0.004 0.11 0.006 0.005 1104 1.4 0.005 0.001 0.006 0.000 1105 11.8 0.003 0.001 1106 11.4 0.000 0.001 1118 11.7 0.002 0.001 1118 11.7 0.002 0.001 1118 11.7 0.002 0.001 1118 11.7 0.002 0.001 1118 11.7 0.002 0.003 1118 11.7 0.002 0.003 1118 11.7 0.002 0.003 1118 11.7 0.002 0.003 1118 11.7 0.002 0.003 1118 11.7 0.002 0.003 1118 11.7 0.002 0.003 1118 11.7 0.002 0.003 1118 11.7 0.002 0.003 1118 11.7 0.002 0.003 1118 11.7 0.002 0.003 1118 11.7 0.002 0.003 1118 11.7 0.002 0.003 1118 11.7 0.002 0.003 1118 11.7 0.002 0.003 1118 11.7 0.002 0.003 1118 11.7 0.002 0.003 1118 11.7 0.002 0.003 1118 11.7 0.003 0.017 0.011 0.11 0.11 15.1 11.4 11.7 0.002 0.003 11.4 11.7 0.003 0.003 11.5 11.4 0.011 0.011 0.011 0.011 0.011 0.011 0.011 11.5 11.4 0.003 0.003 11.5 0.005 0.005 0.005 0.005 0.005 0.005 0.005 11.5 11.4 0.005		-71	1071	4.2	0.008	3								
1121 8.5 0.009		-72	1159	4.6	0.007		,							
1121 8.5 0.013 0.02 0.012 0.005 0.01 1.1 17.0 2.26 1.2 1.32 0.009 0.01 0.009 0.02 0.004 0.1 0.1 0.3 15.9 2.43 1.05 0.009 0.004 0.002 0.2 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.03		-73	1174	6.5	0.00									
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		-74	1121	8.5	0.013		0.02	0.012	0.005	<0.1	1.1	17.0	2 26	50
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		-75	1153	7.1	600.0			0	700				3 .	, , ,
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		-76		11.32/	0.00		0.0	000	****		n .	15.9	2.43	000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		-77	•	15.02/	0.032		0.02	0.00	70.002	7.0	7.0	15.8 0.1	2.46	
102 16.42 0.121 CI 0.1823 0.137 0.032 21.5 0.01 14.6 2.51 2.55 0.005		-78		14.02/			90.0	0.00	0.00	7.6		12.0	2.54	0000
1102 16.42 0.087 CI		-79	879	15.42/			0.19	0.137	0.092	23.5	70.1	14.6	2.61	06.70
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		-80		16 42/			:					2.0	00.7	2
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		-81		17.92/			100	780.0	0.060	21.3	7.0	21.6	/2.50	25.84
1105 14.92		-82		17.52/	0.005		70.0		0.011	⊃ (5.0	16.5	2.53	20.10
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		-83		14.92/	000		7.0		×0.002	æ (0.5	16.0	2.59	19.39
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		-84		9.2	0.004		0.01	0.00	<0.00	9.0	0.2	15.6	2.62	•
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		-85	430	9.9	0.004									
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		98-	460	11.4	0.003									
998 12.9 0.002 1023 11.8 0.001 1126 12.4 <0.001 1178 11.7 0.002 1037 20.0 0.002 903 19.02/ 867 20.62/ 87 20.62/ 8826 17.42/ 811 20.72/ 811 20.72/ 812 20.55 CI 828 0.003 0.017 0.011 829 12.9 820 17.6 0.029 820 0.03 0.017 0.011 820 1.5 1 15.1 21.4 2.14 820 20.3 2.11		-87	1037	13.8	0.003									
1023 11.8 0.001 1126 12.4 <0.001 1178 11.7 0.002 1037 20.0 0.002 903 19.02/ 867 20.62/ 87 20.62/ 8826 17.42/ 811 20.72/ 803 0.017 0.017 0.017 0.017 15.1 21.4 2.14 811 20.72/ 813 20.72/ 814 20.05 CI 815 20.05/ 816 0.05/ 817 0.05/ 818 0.05/ 819 0.0		-88		12.9	0.002									
1126 12.4 <0.001 1178 11.7 0.002 <0.001 1037 20.0 0.002 903 19.02/ 0.009 867 20.62/ 0.009 811 20.72/ 0.056 CI 0.06 0.033 0.017 0.11 16.0 20.3 2.11		-89		11.8	0.001									
1178 11.7 0.002 < 0.001 1037 20.0 0.002 > 0.002 903 19.02/ 0.009 0.01 0.012 0.011 < 0.1 17.5 21.3 2.04 867 20.62/ 0.009 0.03 0.017 0.011 0.1 15.1 21.4 2.14 826 17.42/ 0.056 GI 0.06 0.033 0.017 0.1 16.0 20.3 2.11		06-	1126	12.4	<0.001									
1037 20.0 0.002 903 19.02/ 0.009 0.01 0.012 0.011 <0.1 17.5 21.3 2.04 867 20.62/ 0.009 0.03 0.017 0.011 0.1 15.1 21.4 2.14 811 20.72 / 0.056 GI 0.05 GI 0.033 0.017 0.017 0.01 16.0 20.3 2.11		-91	. ,	11.7	0.002	<0.001					ē.			
903 19.02/ 0.009 867 20.62/ 0.009 0.01 0.012 0.011 <0.1 17.5 21.3 2.04 826 17.42/ 0.029 0.03 0.017 0.011 0.1 15.1 21.4 2.14 811 20.72 / 0.056 GI 0.06 0.033 0.017 0.1 16.0 20.3 2.11		-92		20.0	0.002									
867 20.62 / 826 17.42 / 811 20.72 / 80.056 CI 0.010 0.012 0.017 0.011 0.1 15.1 21.4 2.14		-93		19.02/	00.00						(3)			
826 17.42/ 811 20.72/ 0.056 GI 0.06 0.033 0.017 0.1 15.1 21.4 2.14 820 20.33 0.017 0.1 16.0 20.3 2.11		-94		20.62/			0.01	0.012	0.011	<0.1	17.5	21.3	6	20.00
811 20.72/ 0.056 GI 0.06 0.033 0.017 0.1 16.0 20.3 2.11		- 9.5		17 42/							•	2		
611 20./2 0.056 C1 0.06 0.033 0.017 0.1 16.0 20.3 2.11		90		17.00	670.0		0.03	0.017	0.011	0.1	15.1	21,4	2,14	12.52
		061		70°/07	0.056		90.0	0.033	0.017	0.1	16.0	20.3	2.11	25.60

						Coll	8				,			
Hole Hole	Footage	HRI No.	Dry1/ Grams	H2O	Fluorimetric	Check	Beta/	Beta	Gamma	200	C Organic	Ft3/ton		
						2	Callinia	rdary	rdniv	8	%	Density	Sp. Gr.	
145-C	558 -559	14329 -97	1139	13.42/	0.012		0.02	0.011	0.004	7.8	6	7 51	,	37.51
•	-561	2 0	893	15.2%	0.008			are a					۲۰3) : :
	-562	-100	988	11.9	<0.002									
	-563	-101	726	24.4	<0.001									
	-564	-102	1013	6.8	0.001									
	-565	-103	1107	10.0	0.002		,							
	-266	-104	009	14.1	0.004									X
	-567	-105	722	17.3	0.013									
	25.0	103			200									
	1520	100-	456	13.8	0.005									
	1570	907-	848	14.76	0.007		<0.01			<0.1	5.4	19.2	0 30	17.51
	-572	110	700	25.25			0.05		0.022	0.1	22.5	21.2	20.1	28.34
	3	277	0	73.53	0.048 CI	0.045	0.05		0.016	0.1	15.6	18.4	2.18	14.05
	-573	-111	888	18.12/	0.026		0.04		0.014				9	1016
	-574	-112	1170	13.52/	0.014		0.02	0.012	<0.00	. 4	10.0	1.6.1	2.11	1000
	10/0	-113	1035	13.24/	0.011					:		1001	77.7	14.51
	-577	-114	983	13,66/	0.008	0.008								
		CTT-	1054	10.9	0.005									
	-578	-116	1108	11.9	0.005									
	1580	-117	982	10.0	0.006									
	-581	-119	1032	p 0	0.006									
	-582	-120	1132	13.72/	0.008									
	-583	-121	1140	16.42/	010	8								
	-584	-122	1053	8.12/	0.016				,	*				
	-585	-123	962	8.82/	0.022									
	-586	-124	1155	14.92/	0.033									
	-587	-125	1109	15,42/	0.021									
	-588	-126	1259	14.32/	0.013	0.013								
	-589	-127	1117	15.02/										
	-590	-128	1189	15.54	0.044 CI	91	0.02	0.026	0.008	0.1	<0.1	15.3	2.66	12.11

4603 - Date Creek

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	Ft ³ /ton Density										115 -91'02 =		Samores		020%25	0.1.50
	CO ₂ C Organic					3					13	<	Ú	4	•	ī
	% CO %															
	Gamma		* 1													
	Beta															
%	Beta/ Gamma								i.							
U3O8, %	Check Fluorimetric		•								0.001		* * * * * * * * * * * * * * * * * * * *			
	Fluorimetric	0.006	0.008	0.009	0.00	0.002	0.002	0.001	0.001	0.001	0.001	0,002	0.001			
	H20	14.52/	18.92/	12,3	13.7	10.9	10.7	10.2	10.6	8.7	6.2	10.0	12.0			
	Grams	1112	410	831	914	1170	1063	1079	852	934	822	931	827			
	HRI No.	14329 -129	-130	-131	-132	-133	-134	-135	-136	-137	-138	-139	-140			
	Footage	590 -591	-592	-593	-594	-595	-596	-597	-598	-599	-600	-601	-602	2-S		
Č	Hole	145-C												End of 145_C	7 10 2112	v.

	(6 of 47 pages)		Sp. Gr																															
	(6 of 4	P43 A.	Density			ø																												
		C Organic	%													e i				*														
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	8	Beta/	Dillion																															
4603 - Date Creek	U ₃ O ₈ .	Check Fluorimetric		0.014													2				,			0.018				0.023						
460		Fluorimetric	0.013	0.004	0.003	0.004	200	<0.001	0.001	0.002	0.003	000	0.003	9000	0.003	0.002	200	0.003	0.001	0.001	0.013	0.006	0.009	0.003	0.004	0.006	0.004	0.022	0.014	0.003	0.014	0.009	012	0.017
		H20	8.2	10.3	10.7	17.8		12.3	16.5	12.5	11.8	15.2	21.5	27.2	21.0	8.9	9.4	10.2	11.7	12.7		24.2	11.5	13.0	14.1		12.5							. , .
	Drv1	Grams	1273	1136	1120	881	024	1239	872	1148	1190	1000	688	664	987	1241	096	1187		1083		206					1166 1					950 11		
	HRI	No.	14329 - 141	-142	-144	-145	-146	-147	-148	-149	-130	-151	-152	-153	-154	561-	-156	-157	150	-160	-161	-162	-163	-164		165	-169	-169	-170				-174	
			590 -591	-593	-594	-595	-596	-597	298	- 600		-601	209-	-603	-605		-606	-608	609-	-610	-611	-612	-613	-615	-616	-617	-618	-619	-620	-621	-622	-623	-625	· · · · · · · · · · · · · · · · · · ·
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(8 of 47 pages)		Ft3/ton Density																																
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	0	Beta/ Gamma		4																									¥:					
4603 - Date Creek	U308,	Check Fluorimetric	0.008												<0.001				2.0							0.014								
4603		Fluorimetric	0.008	0.008	0.005	0.005	<0.001	<0.001	<0.001			×0.001	70.00	×0.001	<0.001	0.002	0.002	0.004	0.019	0.011	0.012	0.011	0.008	0.009	0.016	0,013	900.0	0.002	0.003	0.003	0.003	0.003	0.002	>
		H20	4.6	15.2	9.6	10.1	10.4	9.6	8.8	8' 2'		10.1	12.6	11.8	14.9	16.1	15.5	17.9	23.1	15.7	15.8	16.2	7.6	10.8	6.6	14.3	11.4	12.0	16.52/	14.42/	13.9	12.3	15.4	
	/Ind	Grams	824	1211	1060	932	1294	1222	790		946	1208	1276	934	1147	1074	828	987	861	266	1280	741	1490	1037	815	1621	1429						1047	
	HRI	No.	14438 -6	φ •		.010	-11	-12	-13	-15	-14	-13	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	97-	-28	-29	-30	-31	-35	-33	-34	-35	130	-38	
		Footage	-661	-662	-663	-663-10"	-701	-702	-/03	-705	-704	-705	-706	-707	-708	-709	-710	-711	-712	-713	-714	-715	2712	-718	-719	-720	-721	-722	-723	-724	-725	-727	-728	
		F	629				200				703																							
	8	Hole	146-C												V.																			

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- Date
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(9 of 47 pages)		ני ני	9																						;	25.7	2.36	2,43	2.35	2.30		2.51	2.41	2.35	2.12
(9 of 4		Ft3/ton Density	- Company																						, ,,	4.0	17.6	7.67	15.4	23.7	1 2	14.2	16.5	18.2	1/.6
		C Organic %			*					·												,					4.1	7.6		0.6	2 6	9.0	0.4	0.3	?
		% 00 00 00 00 00 00 00 00 00 00 00 00 00																							٠							•			
		Gamma Equiv																							0.008						0.017		٧	0.021 <0.1	
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	8	Gamma	e L																			ja S			0.01	<0.01				0.08				0.08	
4603 - Date Creek	U308,	Fluorimetric				<0.001										× ×	000	200.0							•		×		0.055		4				
460		Fluorimetric	0.002	0.001	< 0.001 0.001	× 0.001	100.00	< 0.001	< 0.001 0.001	< 0.001		200.0	0.006	0.002	0.001	0.002	0.002	0.002	0.003	0.002	0.005	0.005	0.010	0.008	600.0			0.083 CI				0.040 CI	0.023	0.085 CI	
		H20	18.0	11.7	13,3	13.3	0 0	13.9	12.2	12.7	16.3	13.2		18.4	7.7	6.3	0.9	5.7	7.5	5.1	9.7	9.1	7.9	11.62/	13.84/	13.82/	8.74/	10.72/	18.12/	, ,	17.62/	12.7	12.12/	2.05/	
	Dry1/	Grams	891	1032	1182	1278	1933	1233	1076	1293	1019	866	1326	849	1414	1358	1375	1403	1225	1411	1001	1417				1104			1067		1307				
	HRI	No.	14438-39	-40	-41	-43	-44	7	46		-48	-49	-20	-51	-52	-53	-54	-55	-26	-57	-58	-59	9-	19-	70-	-63	50-	99-	-67		2 0	- 20	-71	-72	
		Footage	-729	-730	-732	-733	-734	-735	-736	-736-9"		-892	-893	-894	-895	968-	-897	-898	668-	006-	-901	-902	-903	100		906-	808	606-	-910	1.0-	-912	-913	-914	-915	
	8	Hole	146-C 728								890			* .											٠										

4603 - Date Creek

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8			TOT	1			U308. %	%							
Hole	낊	Footage	No.	Grams	H	Flance	Check	Beta/	Beta	Gamma	င်	2	7,5		
7 37					1	Dinaminati	Fluorimetric	Gamma	Equiv	Equiv	%	% %	Density		
01071	915	-916	14438-73	957	15.82/	0.021	•						Constry	op. Gr.	
	,	-917	-74	935	13.52/			0.01	0.017		<0.1	6.4	. 01		2
		816-	-75	1224	14.12/		•	0.02	0.015	-	<0.1	3.2	19.3	2.20	77.4
		-920	-77	1101	10.52/	0.026		<0.07 <0.01	0.024	0.032	e .	3,5	18.0	2.28	20.92
	920	-921	-78	080	20.02	0.013		0.01	0.015	(8)		٠.٧	14.3	2,33	15.98
		-922	-79	950	13.02/	0.030	0.029	0.02	0.021				1.12	2.29	26.57
		-923	-80	1153	18.02	0.075 CI		0.07	0.063		7.0	15.6	19.0	2.10	223
		-924	-81	896	10 02/	0.043 CI		0.03	0.028			11.1	17.8	2.07	20165
		-925	-82	1171	14.72/	9000		<0.01	0.007			4	19.4	2.25	23.75
		-926	-83	1452	11 42/	900.0		< 0.01	0.007		<0.1	1.0	17.9	2,39	1,22
		-927	-84	1182	17.02/	0.007								60.7	5
		-928	-85	1351	8.92/	0.00									
,		-929	-86	1354	8.02/	0.004									
		-930-4"	-87	1291	10.62/	0.003									
				172	10.4 =	0.002					٠				
nd of 146-C	46-C										×				

X = 20.28 ± 3.04 SAMPLES = 31 AUS 680 = .059 ±.04

(11 of 47 pages) ູ້ບໍ 2.54 2.56 2.55 2.44 2.36 2.31 2.18 1.98 2.14 2.38 2.39 2.37 Sp. 2.33 2.27 2.29 2.14 2.62 2.41 Ft³/ton Density 15.9 16.0 17.3 17.9 16.2 17.5 19.8 23.8 16.6 15.7 17.8 16.3 16.1 16.6 16.2 17.5 15.6 C Organic % <0.1 0.1 3.0 5.2 0.2 0.7 1.1 % CQ % 4.8 11.5 1.2 60.1 60.1 60.1 0.1 60.1 17.1 9.2 2.9 2.9 4.2 0.1 0.1 0.1 Gamma Equiv 0.027 0.019 0.008 0.012 0.011 0.006 0.007 0.006 0.014 0.017 0.013 0.020 0.020 0.024 0.011 0.011 0.013 0.009 0.011 0.019 0.013 0.007 0.009 0.010 0.017 0:046 0.020 0.012 0.008 0.017 0.014 0.027 0.015 0.008 0.010 0.008 Beta Equiv 0.009 0.008 0.006 0.014 0.013 0.011 0.024 0.025 0.037 0.012 0.009 0.013 0.021 0.009 0.009 0.006 0.009 0.007 0.006 0.016 0.049 Beta/ Gamma 0.03 <0.01 <0.01 <0.01 <0.01 0.01 <0.01 0.01 0.02 0.01 4603 - Date Creek Check Fluorimetric 0.030 0.035 Fluorimetric ដ ប ប 0.028 0.013 0.007 \overline{G} 0.048 0.013 0.011 0.015 0.012 0.013 0.014 0.031 0.023 0.008 0.007 0.005 0.021 0.054 0.006 15.82 16.72 20.02 18.32 18.22 17.62/ 17.62/ 18.52/ 11.82/ 18.22/ H20 18.02 17.42 18.02 19.42 14.92 4.82 13.72 11.22 3.12 8.12 6.62 11.82 10.62 11.32/ 14.12/ 14.72/ 12.12/ 14.12/ Dry1/ Grams 1013 1210 1037 1184 1140 1239 1165 950 1015 1121 1022 1046 1135 1113 957 1080 1109 1147 1048 1070 1383 1331 1167 1512 HRI No. 14445-1 -20 -21 -23 -23 -516 -517 -518 -519 -521 -522 -523 -524 -525 -527 -528 -529 -526 Footage -530 -531 -532 -533 -535 -536 -537 -538 -538 -540 -541 -542 -543 -544 -545 -546 -547 -548 -549 515 529 Hole 155-C

33.81

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4603 - Date Creek

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2			:	,,			U308,	%						
Hole	Footage	. Je	No.	Dry-L/ Grams	H20	Fluorimetric	Check	Beta/	Beta	Gamma	202 CO2	C Organic	Ft3/ton	
								Dilling	ATRIBOT	rdniv	%	%	Density	Sp. Gr.
155-C	581	-582 144	14445-67	1171	12 32/			;						
	Í		-68	1213	12 02/	10.0		0.01	0.012	0.010	9,3	4.2	15.	09 6
	Ī	703	2 0	1 6	10.01	0.000		<0.0V	0.005	0.007	c			00.3
	1 1		201	1230	15.25			< 0.01	0.005	0000		1.0	14.1	3.02
	•	282	-70	1209	16.54	*			200	000				
	í	286	-71	1226	16.92/			100	0.004	0.002				
			í	:	,		***	70.07	0.003	0.003				
	í	/80	-72	1040	19.06			100	000					
	ĩ	588	-73	910	18.72/					200.0				
	ĩ	-589	-74	973	14.5					< 0.002				
	ĭ	290	77.	2 6				<0.01		< 0.002				
			21	304	15.3			< 0.01	0.005	0 00				
	í	160	9/-	922	16.3			Ī						
	51	265	-77	1903	6				200.0	0.003				
				503	0.0			<0.01	0.003	2000				
	í		8/-	879	18.5			V 0 01		700				
	593 -5	94	-79	676	22.0					*00.0				
	-5	-595	-80	0 0	27.0			<0.01	0.004	0.003				
		90	8 6	100	0.71			< 0.01	0.007	0.005				
	,	0 1	19-	1023	13,3			0	0.10					
	ָרָי רַי	16.	-82	1218	10.0				200	0.013				
	-5	86	-83	1084	14.7			100	0.011	0.011				
	ו	. 00		:				10.0	0.012	600.0				
	7	0 0	1	1111	12.4			<0.01	0.007	0 005				
	•	3	-82	1298	2.6			200						
	9-	01	-86	968	16.4			100	0.012	0.013		j		
	9-	02	-87	666	16.1			10.02	0.002	0.002				
	9	-603.2"	-88	1510	9.7			<0.01	0.003	20.002				
Pad of 166_0										500.0				
10 011	2													

ı		Ģ	1																																			
		Sp. G		2.64	2.52	2.64	2.52	2.61		2.60	2.72	2.75	2.76	6/07	2.66	2.67	2.65	5.66	2.57	2.52	2.44	2.44	2.38	2.33	20				2.47	2,47	2.49	2,39	2,32	2.29				
	F+3 /+0n	Density		16.9	16.8	13.7	16.6	14.9		13.0	14.8	14°0	12.3	0.01	17.6	14.2	12.8	13.6	17.9	17.0	19.2	17.0	17.7	17.9	18.7				17.1	18.4	18,4	15.6	15.8	16.7				
	C Organic	% ************************************		<0.1	0.3	<0.1	6.0	0.8		2 0	2 0	0.4	2.0	:	6.0	0.5	9.0	<0.1	<0.1	<0.1	<0.1	0.2	o.s	1.7	1.5				4.	0.7	0.3							
	ç			5.77	1.8	19.7	14.3	16.2	30.3	10.1	20.02	25.9	40.1		80.00	35.6	9.00	28.4	ο. Ο.	8.0	0.2	1.0	.0.1	٥.	<0.1			10.6		14.6	16.4	8.7	7.6	7.2				
ľ	Gamma	Equiv		0.013	600.0	7000	0.027	0.046	0.034	0.017	0.011	0.020	0.027					0.100	0.030	0.017	0.011		20.0	610.0		0.005	900.0	0.012				900.0	0.014	0.014	0.019	0.016	0.010	0.011
	Beta	Equiv			0000	610.0	0.023	0.043	0.035	0.013	0.010	0.014	0.022	0.041	0.044	0.024	40.0	0.062		0.018	210.0	0.019	0.01	2	900.0	0.005	8000				0.010		0.013				700.	0.006
%		Gamma		10.00	0.0	200	200		0.04	0.01	0.01	<0.01	0.02	0.04	0.05	0.01	0.12	0.07		0.02	200	200	0.03	;	0.01	0.0	0.0	0.01		20.0	200	70.0	0.0		×0°01	0.07	100	<0.01
U3O8.	Check	Fluorimetric							0.036									*			0.022												×				5*	
		r tuorimetric	0.063 CI	0.005	0.015	0.026	0.035	000	0.036	210.0	0.013	0.013	0.050		0.047 CI	.016	0.092 CI	0.064 CI	0.010	0.010	0.021	0.013	0.025	0.007				0.018	0.016	0.016	0.013	0.010	0.00	- 5				
	Coff	2717	14.12/	18.42/	15.32/	14.24/	16.14/	10 22/	8 42/	12 42/	12 42/	14 82/		18.24/	16.94/	5.04/	10.64/	14.24	15.4	15.4	15,6	13.1	10.7	7.5	9.5	7.8	11.1	10.0	13.0	9.2	8.6	7.0	8.0	5.4	5.5	8.9	8.0	6.1
,,	Grams		1194	1188	1466	1039	1098	1031	1437	1067	1322	1280		1414	1249	1701	2511	1101	838	699	930	1060	11/5	888	1239				17132	988	1085	1277	983	1259	1428	1060	1042	1062
	No.		14453-1	v	77 4	4 " ('n	9	7	00	າ ຫ	10	:	11	12	2 7	* "	61	16	17	81 .	67 6	03	21	22	53	4. 2	67	26	17	87.0	67 6	30	31	32	33	80 C	
	Footage		540-541	25.0	244	272	2	-546	-547	-548	-549	-550	-551	-552	-553	-554	-555		-556	-557	000	-560		-261	-562	-563	-565		-567	100	286	1570		-571	-572	-573	107	
2	Hole	E	8-C																				9					500										•

(15 of 47 pages) 2.33 2.33 2.25 2.25 2.26 2.19 2.32 2.59 2.55 2.55 2.55 2.56 2.66 Sp. Gr. 2.45 2.00 2.03 2.51 2.54 2.42 Ft3/ton Density 15.1 14.7 13.8 15.6 16.0 16.3 15.8 15.8 17.1 15.5 15.0 16.0 15.9 16.6 16.6 16.0 C Organic % 0.2 0.2 0.8 0.7 0.7 0.7 1.0 0.2 0.2 0.2 0.3 1.3 1.0 0.5 % O 2.7 2.4 2.4 0.1 0.1 3.2 0.2 0.2 0.2 0.3 13.7 13.5 1.6 0.1 2.5 5.7 Gamma Equiv 0.012 0.025 0.018 0.013 0.025 0.018 0.017 0.020 0.015 0.019 0.031 0.048 0.058 0.023 0.013 0.008 0.010 0.009 0.009 0.009 0.008 0.011 0.006 0.015 0.009 0.011 0.012 0.017 0.007 0.026 0.013 0.010 0.021 0.022 0.017 0.014 0.009 0.022 0.030 0.055 0.061 0.017 0.006 0.006 Beta Equiv 0.003 0.008 0.006 0.005 0.005 0.006 0.006 0.023 0.015 0.006 0.004 0.007 0.009 <0.01
0.03
<0.01
<0.01
<0.01
<0.01</pre> 0.02 0.03 0.02 <0.01 0.03 0.06 0.06 0.06 0.01 0.01 0.01 0.01 Beta/ < 0.01
< 0.01
< 0.03
0.03
</pre> U3O8, % Check Fluorimetric 0.010 0.052 Fluorimetric 0.022 0.018 0.052 CI 0.058 CI 0.006 0.026 0.009 0.008 0.021 0.027 0.015 0.011 0.006 0.004 0.004 H20 7.3 10.9 8.4 10.0 9.0 112.8 11.6 7.4 15.2 11.8 12.9 10.4 9.4 14.3 11.8 16.0 13.1 15.2 13.4 19.5 Dry L/ Grams 1077 1068 1400 1248 998 987 1011 962 936 774 1085 877 814 992 1316 977 908 1313 975 944 907 977 724 679 920 920 954 1061 136 14453-36 HRI No. 51 53 54 55 55 57 57 58 59 60 61 62 63 -597 -597 -598'3" 600-601 575-576 -577 Footage -578 -579 -580 -581 -582 -583 -584 -586 -587 -588 -589 -590 -591 -592 -593 -594 -595 -596 -603 -604 -605 -606 -609 -610 -611 Tonto 8-C Hole Hole

4603 - Date Creek

pages)		Sp. Gr		2.08	2.04	.22	.37								, 1,	2.11	:																					
(16 of 47 pages)	2 2																			•										2.64	2.64	2.63	2.63	2.71	2.64	2,63	2.67	2.64
4-				18.0	61	9 :	15.							17.8	22.7	24.5														14.0	15.2	16.2	17.6	15.4	16.2	16.2	16.2	16.0
	O Comment	%	:	12.0	16.4	9 0	0.0							7.9	13.2	9.5	,														1.0	1.0	1.0	1.0	0.1	<0.1		0.1
	8	%	0		11.1	15.4								0.2	0.1	0.5													1 2									
	Gamma	Equiv	0.047	0.028	0.016	0.008	0.008	010	0.013	T 0 0	0.03	0.010		0.011	0.018	0.021	0.00		0.002	0.002	0.018	600.0	0.010	0.009	0.00	0.005	0.018	.014	0.038						0.018 <0.1	۸		0.157 <0.1
	Beta	Equiv	0.048	0.036	0.013	0.004	0.005	0.005	0.012	0.006	0.003	900.0		110.0	170.0						0.019							0 210.0					0.016 0	0 0 0				0.170 0.
ð		Gailling	0.05	0.04	<0.01	<0.01	<0.01	<0.01	0.01	<0.01	<0.01	<0.01	0	0.02	0.01	<0.01	<0.01	100		70.0							0.03	٠.					0.02 0		0.06			0.18 0.
i Gell	Check																								•	•								•				
										×													×							191				0.014				
	Fluorimetric		0.047 CI	0.012	0.001								=	52	16												v				-							
		. c		0	0								0.011	0.025	0.016									3				0.025	0.032	0.032	0.003	0.012		0.014	0.00	0.128	0.161	
	H20	12.6	Ξ			4.9	0	15.6	12.6	16.0	16.6	2.	7.7.0	0.0		0 6		13.9	1.87	16.7	10.1	10.1	10.3	12.0	9.4	6.4	8.74/	14.42/	17.32/	15.42/	16.12/	17.02/	14 02/	13 52/	14.92/	15.52/	15.12/	
	Grams	986	1162	1280	606	952	895	799	1076	968	724	736	714	776	965	991		1010	1100	1000	1080		1367	1311	1208	1586	1315	1518	1122	1231	928	1183	1285				1058	•
HRI	No.	14453-71	72	73	4 7	ç	92	77	78	79	80	81	82	83	84	82	98	8 2	ά	8 &	06		91	35		4 o	2	96	97	86	66	100	101	102	103	104	105	u V
	age		7 2	2 4				6	۰.	-	2		•														ř.		÷						· · · · · · · · · · · · · · · · · · ·			
	Footage	612-613	-614	1616	-617		-618	-619	-620	-621	-622	-623	-624	-625	-626	-627	-628	-629	-630	-631	-632	-633	1634	1634	-636	-637	-630	000	600	-641	-642	750	-643	-644	-645	-040	104/	
8	Hole	Tonto																																				

2						U3O8, %	%						
Hole	Footage	HRI No.	Dry±/ Grams	H20	Fluorimetric	Check	Beta/	Beta	Gamma	00%	C Organic	Ft3/ton	
							2	2400	ATRICA	٩	R	Censity	Sp. Gr.
Tonto	647-648	14453-106	1073	16.02/	0.004								
ပူ	-649	107	978	15.12/	0.001		<0.01	0.006	0.008	<0.1	<0.1	16.6	2,65
	-650	108	1170	12 52/			<0.01	0.004	0.008	0.1	0.1	15.3	2,65
	-651	001	000	12.51			<0.01	0.003	0.007				•
	-652	120	1190	14.4			<0.01	0.004	0.005				
				10.01			<0.01	0.004	0.005				
	-653	111	1240	17.02/									
	-654	112	1107	17 22/			10.07	0.003	0.005				
	-655	113	840	15 22/			<0.01	0.003	900.0				
	-656	114	130	10.2/			<0.01		<0.002				
	-657	211	1101	10.1			<0.01	0.003	<0.002				
		011	101	10.8=			<0.01		<0 U				

End of Tonto 8-C

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- 1						U3OB	%						
Hole	Footage	HRI No.	Dry L/ Grams	H2O	Fluorimetric	Check		Beta	Gamma	8	C Organic	Ft3/ton	
				221		or manufacture.	Gamina	rdniv	Equiv	86	%	Density	Sp. Gr.
158-C	380-381	14509-1	1228	8.54	0.029		0.04	0.026	0.017	21.7	6	2.0	2 60
	-382	2	966	12.4	0.014		0	100	610	30.0		. 91	
	-383	67	1337		0.046		5	1000	20.0		1.0,	7.07	20.0
	-384	V	1178		2000			0000	0.029	4.07	/	4.4	2.31
				3 1			000	0.030	0.014	27.3	<0.1	13.9	2.51
	-385	n	1263	9.7	0.016		0.03	0.017	0.010	28.9	1.9	13.6	2.60
	-386	9	1251	10.1	0.017	0.017							
	-387	7	1243	7.5	0.013)*S							
	-388	80	1065	14.1	0.015				18				
	-389	6	1368	11.7	0.023		0 04	0.033	710	28 4		3 21	70
	-390	10	869	11.0	0.028		0.04	0.00	1000	14.0		17.0	2.40
								6.0	000	2	1.01	7. /1	66.3
	-391	11	1305	13.0	0.031 CI		0.04	0.033	0.029	24.5	2.4	15.1	2.52
	-392	12	1278	7.0	0.017		0.03	0.013	0 003	25 A		15.3	2.58
	-393	13	928	16.5	0.013		0.02	0.008	200.00	23.7		14.7	
	-394	14	951	15.4	0.015			•			7.7		
	-395	15	908	15.4	0.019	i.							
	-396	16	1168	13,3	0.014					,			
*	-397	17	1125	13.2	0.021		0.03	0.016	800	30.4	,	8 71	2 65
	-398	18	995	13.1	0.022	0.021	0.04	0.020	800	17.7	2.4	74.0	20.0
	-399	19	1209	13.0	0.022		0.04	0.019	000	26.5	r c	12.0	19.0
	-400	20	1219	10.9	0.028		0.05	0.022	0.006	28.5	9.0	18.1	2.50
	-401	21	1154	16.4	0.023		0.03	0.016	0.005	0		15.7	2 42
	-402	22	1027	12.3	0.029		0.04	0.025	0.015	25.7	. 0>	14.2	7.0
	-403	23	1203	12.8	0.034 CI	21	0.05	0.027	2100	0		7.7.	7 .
	-404	24	1066	14.0	0.026		0.04	0.025	0.010	11.0		14.0	74.7
	-405	25	869	15.5	0.029		0.05	0.026	0.011	19.7	3 - 0	0 0 0	74.7
	2									•	4	•	

4/ No core individually wrapped with foil. Sheets of foil were laid over all cores in a box before the cover was closed.

						2021	2						
8		HRI	Dryl			Check I	Beta/	Beta	Gamma	ć	c) usual	F+3 /40m	
Hole	Footage	No.	Grams	H20	Fluorimetric	Fluorimetric	Gamma	Equiv	Equiv	3%	% Salite %	Density	Sp. Gr.
158-C	405 -406	14509 -26	503	23.2	0.011					,_			
	-407	-27	512	17.3	0.012								
	-408	-28	781	16.7	0.00								
3	-409	-29	986	14.5	900.0						3		
	-410	-30	278	17.0	900.0	900.0						*	
	-411	-31	988	15,8	0.008								
	-412	-32	1034	17,3	0.008								
	-413	-33	887	15.9	0.008		1						
	-414	-34	910	17.1	0.008				•				
	-415	-32	1022	14.3	0.009								
	-416	-36	800	16.0	600.0								
	-417	-37	842	17.6	0.007								
	-418	-38	823	16.0	0.007				c				
	-419	-39	866	16.6	9000								
	-420	-40	998	14.1	0.010								
	-421	-41	982	12.0	210.0								
	-422	-42	1042	11.7	0.012	0 012					٠		
	-423	-43	1284	12.9	0.008	•							
	-424	-44	1094	9.7	0,008							K	
	-425	-45	1180	12.7	0.000								
e:	-426	-46	1177	12,1	600.0								
)¥	-427	-47	729	16.7	0.008							,	
	-428	-48	692	19.2	0.015								
	429	-49	1284	16.2	0.007								
	00%	06-	914	15.0	0.007								
	-431	-51	1157	15.0	0.009			*	_				
	-432	-52	903	17.2	0.009								
	-433	-53	998	16.7	0.012							×	
	-434	-54	1141	16.8	0.020	0.021					٠		
	-435	-52	1226	15.5	0.010								
	-436	-56	1239	16.1	90000				547				
	-437	-57	1033	16,3	0.004								
A 30	-438	-58	979	13,9	0.007						*		
	-439	-29	1088	13.1	0.005								
	-440	09-	1035	12.2	0,003								

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						Tage Oree	, VI				8	(21 of	(21 of 47 pages)
8	*	HRI	1	1/		U3O8	84						(2)6-4
Hole	Footage	No.	Grams	s H ₂ O	Fluorimetric	Che		Beta	Gamma	005	C Organic	F+3.40n	
158-C		14509 -96	831	13.9			Dilling	rdana	Equiv	96	96	Density	Sp. Gr.
	488 -489	-97	1012		0.010		0.02	0.014	0.008	1 0 >			
		8 66 6 -	1079	17.9		5	0.03	0.013	<0.002	0.1	0.2	15.8	2.37
	-491	-100	1049	13.7	0.011		0.03		0.006	0.1 0.1	2.0	14.8	2.48
	-492	-101	1131	18,3	0.011		0.03	0.017	010		•	14.5	2,65
	-493	-102	947	18,1	0.283 0	1	0.11	0.073		1.0	7.07	17.0	2.64
	-495	-104	1247	17.6		OI	0.32	0.208	,	<0.1	0.1	16,9	2.64
	-496	201-		0.01	0.061 C		0.08	0.048	0.026	<0.1 0.1	0.1	15.3	2.65
161	-497	-106	931	20.0	0.081 CI		0.10	4		7.0	0.1	15.9	2.63
	-498	-107	1017	18.7	0.018			0.034		0.1	0.1	15,9	2 64
	-500	-108	1105	18.7	0.003				0.012 <	<0.1 <0.1	×0.1	16.3	2.76
		-109	1005	18,3	0.012		0.04				1.07	14.5	2.55
	-501	-110	773	14.9						•	7.0	16.5	2.62
	-502	-111	1093	16.4	0.00								
	-504	-112	1149	16.3	0.009								
	-505	-114	1157	15.4	0.001	<0.001				,			
	-506	-115	000	2	0.001		ŗ				,		
	-507	-116	806	15.3	0.004		÷					2 8	
	-508	-117	1151	15.9	0.004	*	¥						
	-510	-118	898	14.8	0.002			,					
è		611-	715	11.1	0.002								
	-511	-120	709	19.6	0.001								
	-513	-122	1054	20.8	<0.001					.:			
	-514	-123	694	17.6	<0.001						1) -		
	-515	-124	926	17.6	<0.001								
	-516	-125	167	18.5	<0.001								
	-518	-126	811 1058	17.4	<0.001	<0.001							
id of 158-C	U			?	<0.001	•							•

1		.1					
	į	15 de				2.58	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
	Ft3/ton	Ariginal		*		14.1	14.3 14.8 14.4 15.3 17.2 14.1
	C Organic		5			^ 0.1 ^ 0.1 ^ 0.1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	% CO					30.9 23.2 10.8	8.8 0.3 0.1 0.1 18.0 22.7 36.0
	Gamma		,		91 **	0.019 0.033 0.094	
	Beta					0.018 (0.029 (0.098 (0.	0.031 0.239 0.106 0.021 0.007 0.025 0.083 0.048
8	Beta/ Gamma					0.01	0.02 0.12 0.01 0.01 0.02 0.02 0.04 0.03
o o O o TI		gr. le	0.001		0.005		800.0
	Fluorimetric F		0.001 0.001 0.001 0.001	0.001 0.003 0.002 0.027	0.028 0.007 0.005 0.002	0.001 0.001 0.018 0.029 CI 0.091 CI	0.027 CI 0.300 CI 0.102 CI 0.008 0.006 0.023 0.102 CI 0.028 CI
	H ₂ O FI	13.0 8.1 11.0 11.8 6.1	9.6 10.5 17.3 20.1	19.6 17.4 12.8 7.7 9.8	11.0 11.3 8.4 13.3	13.2 12.6 7.3 11.12/ 10.62/	20.128.11. 10.128.22.22.22.22.22.22.22.22.22.22.22.22.2
	Dry 1/ Grams	1071 1245 1261 1188 1375	1027 1214 976 901 1065		875 1 1106 1 912 1064 1	856 921 1098 1263 1207	1200 1026 11230 1023 1048 1048 1176 1176 1176 1166 1409
	HRI No.	14556-1 -2 -3 -4	198811	-11 -12 -15 -15	-16 -17 -18 -19	-21 -22 -23 -25	26 27 23 23 23 23 23 23 23 23 23 23 23
	Footage	645 -646 -647 -648 -649 -650	6552 6552 6554 554 554	655 1 655 1 658 1 660	- 661 - 662 - 664 - 664	-666 -668 -669 -669	-671 -672 -673 -674 -675 -676 -678 -679
	DC	2 9 -0			•		

Part						4	4603 - Date Creek						(23 of	(23 of 47 pages)
Processee No. Gram's H2O Planetric Fluorimetric Gamma Paris Equit	S	,	T. C.	-			U3OE							
14.55 - 36 346 13.54 0.018 0.01 0.01 0.017 0.016 1.1 0.1 14.5 2.5	Hole	Footage		Grams		Fluorimetric		Beta/ Gamma		Gamma		C Organic	Ft3/ton	
14.6 1.1	26-0				•				1	-	9	R	Density	Sp. Gr.
-38 956 16.12 0.0138 CT			14556 - 36	846	15.86	0.018		0.01	0.017	0.016	1.1	-		
-39 789 13.62/ 0.038 CT 0.03 0.040 0.042 0.1 <0.1 15.9 -41 1075 11.3 0.017 -42 833 19.3 0.016 -43 878 18.0 0.017 -44 1079 18.6 0.007 -45 1120 11.6 0.003 -46 1120 11.6 0.003 -47 1150 11.6 0.003 -48 1028 13.6 0.003 -49 868 18.9 0.006 -50 396 12.4 0.019 -51 720 12.2 0.033 CT 0.014 -52 896 11.5 0.003 -53 846 11.5 0.003 -54 1092 11.5 0.003 -55 1149 13.9 0.005 -51 1149 13.9 0.005 -52 1150 11.6 0.003 -53 846 11.5 0.003 -54 1093 12.4 0.017 -55 1149 13.9 0.005 -56 1167 11.9 0.001 -57 1149 13.9 0.005 -58 1173 14.8 0.001 -59 1173 14.8 0.001 -50 1158 13.1 0.002 -50 1158 13.1 0.002 -51 1159 13.1 0.002 -52 1093 13.1 0.003 -53 1150 13.1 0.003 -54 1050 0.017 -55 1051 0.003 -57 1149 13.1 0.003 -58 1150 0.017 -59 1150 0.017 -60 1158 13.1 0.003 -60 1158 15.1 0.003 -60 1158 15.1 0.003 -60 1158 15.1 0.003 -60 1158 15.1 0.003 -60 1158 15.1 0.003 -60 1158 15.1 0.003 -60 1158 15.1 0.003 -60 1158 15.1 0.003 -60 1158 15.1 0.003 -60 1158 15.1 0.003 -60 1158 15.1 0.003 -60 1158 15.1 0.003 -60 1158 15.1 0.003 -60 1158 15.1		-683	-38	906	16.12	0.00						:	0.57	2.50
-40 1053 11.9 0.017 -41 1075 11.3 0.017 -42 833 19.9 0.016 -43 838 18.0 0.007 -44 1079 18.0 0.007 -45 1137 18.1 0.006 -46 1137 18.1 0.002 -47 1150 11.6 0.003 -48 1028 11.6 0.003 -49 1028 11.6 0.003 -40 1028 11.6 0.003 -40 1028 11.6 0.003 -50 10 10.003 -50 10 10.003 -50 10 10.003 -50 10 10.003 -50 10 10.003 -50 10 10.003 -50 10 10.003 -50 10 10.003 -50 10 10.003 -50 10 10.003 -50 11.5 0.003		-684	-39	789	13.62/	0.038 CI								
-41 1075 11.3 0.016 0.015		-685	-40	1053	11.9	0.018		0.03	0.040	0.042	0.1	<0.1	15.9	2.48
-42 873 19.9 0.016 0.015 -44 1079 18.6 0.0007 -45 1137 13.1 0.012 -46 1123 10.0 0.0013 -47 1150 11.6 0.003 -48 1137 13.1 0.012 -49 1150 11.6 0.003 CI 0.005 0.018 0.023 <0.01 (See note) -49 1150 11.6 0.003 CI 0.005 0.018 0.005 0.018 0.005 0.018 -50 356 15.9 0.005 CI 0.005 0.019 -51 720 12.2 0.005 CI 0.005 0.019 -52 909 11.6 0.038 CI 0.005 0.019 -53 886 11.5 0.014 -54 1092 11.6 0.003 CI 0.005 0.015 0.015 0.01 0.015 0.015 -54 1092 11.6 0.003 CI 0.003 0.004 -55 1041 10.8 0.003 -56 1049 0.015 0.015 0.005 -57 1149 13.9 0.015 -58 1150 13.9 0.003 -59 1150 13.9 0.003 -59 1150 0.003 0.005 -59 1150 13.9 0.003 -59 1150 0.003 0.005 -59 1150 13.9 0.003 -59 1150 0.003 0.005 -59 1150 0.003 0.005 -59 1150 0.003 0.005 -59 1150 0.003 0.005 -59 1150 0.003 0.005 -59 1150 0.003 0.005 -59 1150 0.003 0.005 -59 1150 0.003 0.005 -59 1150 0.003 0.005 -59 1150 0.003 0.005 -59 1150 0.003 0.005 -59 1150 0.003 0.000 -59 1150 0.003 0.000 -59 1150 0.001 -		989-	-41	1075	11.3	0.017		360	141					
-43 878 18.0 0.007 -45 11079 116.6 0.0004 -45 11079 116.6 0.0004 -45 11079 116.6 0.0004 -46 11233 10.0 0.013 -47 1150 11.6 0.0013 -48 1108 11.6 0.003 0.013 -49 868 116.9 0.005 -50 936 112.4 0.019 -51 909 116.6 0.018 0.009 -52 909 116.6 0.018 0.009 -53 846 115.9 0.003 -54 1092 11.5 0.003 -55 1107 11.9 0.015 -56 1107 11.9 0.015 -57 1109 12.2 0.009 -58 1109 12.2 0.009 -59 1109 0.015 -50 1109 0.01		-687	-42	833	19,9	0.016	210 0							
-44 1079 16.6 0.004 -45 1137 13.1 0.012 -46 1137 13.1 0.012 -47 1150 11.6 0.013 0.013 -48 1028 10.0 0.0131 -48 1028 10.0 0.0131 -48 1028 10.0 0.0131 -49 1028 10.0 0.0131 -40 1028 10.0 0.0131 -40 1028 10.0 0.0131 -40 1028 10.0 0.013 0.014 -40 11.5 0.0036 CI -51 720 12.2 0.033 CI -52 909 11.6 0.038 CI -53 846 11.5 0.003 -54 1032 11.5 0.003 -55 1041 10.8 0.003 -56 1167 11.9 0.003 -57 1148 0.021 -58 1173 14.8 0.021 -59 1173 14.8 0.032 -61 138 12.2 0.032 -61 138 12.2 0.032 -61 138 12.2 0.032 -61 138 13.1 0.032 -62 1033 13.1 0.032 -63 1173 14.8 0.034 -64 1024 15.9 0.034 -65 1037 13.8 0.007 -66 1037 13.8 0.007 -67 1219 11.2 0.009 -68 55 19.9 0.001 -69 398 12.2 0.001 -60 398 12.2 0.001 -60 398 12.2 0.001 -60 308 0.005 -60 308 0.		-688	-43	878	18.0	0.007	0.013							
-45 1137 13.1 0.012		-689	-44	1079	16.6	0.004								
-46 1233 10.0 0.013 0.013 0.015 0.01		069-	-45	1137	13,1	0.012		0	610		,			
-47 1150 11.6 0.063 CI 0.053 CI 0.018 0.023 <0.01 (See note) 16.4 -48 1028 13.6 0.053 CI 0.055 CI 0.005 CI 0.		-691	-46	1233	0 01				0.013	0.016	0.1	0.3	16.3	2.47
-48 1028 135 0.029 0.005 0.045 0.045 0.045 0.01 17.3 -49 868 16.9 0.006 0.005 0.009 0.009 0.005 0.011 15.7 -50 936 12.4 0.019 0.009 0.009 0.009 0.015 0.04 (See note) 16.5 -51 720 12.2 0.053 CI (See note) 1.6 (See note) 15.1 -52 909 11.5 0.003 0.009 0.016 0.016 0.01 0.01 0.01 0.01 -54 1092 11.5 0.009 0.009 0.016 0.01 0.016 0.01 0.01 0.01 -55 1149 13.9 0.005 -51 1159 13.4 0.021 0.002 0.01 0.021 0.022 0.9 0.2 -61 938 12.2 0.009 -62 1093 13.1 0.008 0.005 -64 1024 16.9 0.003 -65 1057 13.8 0.004 -67 1129 13.2 0.009 -68 949 17.1 0.0001		-692	-47	1150	11.6	0.013		0.01	0.018	0.023	<0.1	(See note)	16.4	6
-49 868 16.9 0.005		-693	-48	1028	13.6	0.000		0.05	0.049	0.045	<0.1	<0.1	17.3	6.03
-50 936 12.4 0.019		-694	-49	898	16.9	670.0		0.01	0.026	0.032	0.1	<0.1	15.7	10.2
-51 720 12.2 0.053 CI (See note) 1.6 (See note) 15.1 -52 909 11.6 0.038 CI (See note) 0.1 0.1 18.0 -53 846 11.5 0.014 0.009 0.015 (See note) 0.1 0.1 16.4 -54 1092 11.5 0.009 0.009 (See note) 0.016 (See note) 0.1 16.4 -55 1041 10.8 0.008 0.009 (See note) (See note) 0.1 (See note) 14.7 -56 1167 11.9 0.015 -59 1173 14.8 0.021 0.015 -60 1158 13.6 0.020 0.01 0.021 0.022 0.9 0.2 16.3 -61 138 12.2 0.009 0.056 0.035 0.05 0.06 (See note) 15.3 -62 1093 13.1 0.082 CI 0.09 0.056 0.035 3.1 1.3 16.1 -64 1024 16.9 0.019 0.017 0.01 0.017 0.016 0.1 (See note) 15.3 -65 1097 13.8 0.007 0.007 0.017 0.017 0.016 0.1 (See note) 16.7 2 -68 949 17.1 <0.001 0.007 0.007 0.007 0.017 0.016 0.1 (See note) 16.7 2 -69 398 16.5 <0.001		-695	-50	936	12.4	0000		<0.01	0.009	0.015		(See note)	16.5	
-51 720 12.2 0.053 CI -5.2 899 11.6 0.038 CI 0.038 CI 0.04 0.055 0.031 <0.1 10.1 15.4 -5.4 1092 11.5 0.004 0.009 0.016 0.016 0.016 0.016 0.01 0.1 16.4 -5.4 1092 11.5 0.009 0.009 0.01 0.016 0.016 0.016 <0.01 0.1 16.4 0.1 16.4 -5.5 1041 10.8 0.005 0.005 0.005 0.01 0.021 0.021 0.021 0.021 0.021 0.021 0.021 0.021 0.021 0.021 0.021 0.021 0.022 0.9 0.2 16.3 12.4 0.021 0.032 0.01 0.022 0.9 0.056 0.035 0.03 0.05 0.036		-606				610.0			(See not	(e.		See note)	15.1	2.39
-52 909 11.6 0.038 GI 0.038 GI 0.04 0.05 10.0 1 10.1 10.1 10.0 1 10.1 10.1		000	-51	720	12.2	0.053 CI			(Cop 200)	7		(200	1.01	6.70
-53 846 11.5 0.014 0.015 0.035 0.031 <0.0 -54 1092 11.5 0.009 0.009 0.01 (See note) 0.01 16.4 -55 1041 10.8 0.008 0.009 0.001 (See note) 0.01 14.7 -56 1167 11.9 0.015 -59 1173 14.8 0.021 -60 1158 13.6 0.020 -61 938 12.2 0.009 -62 1093 13.1 0.082 CI 0.09 -63 1073 13.8 0.007 -64 1024 16.9 0.019 -65 1097 13.8 0.007 -67 1219 15.2 0.001 -68 949 17.1 <0.001 -69 949 17.1 <0.001 -69 949 17.1 <0.001 -60 16.8 0.001 -60 16.8 0.001 -60 17.8 0.001 -60 17.8 0.001 -60 18.8 0.001 -60 1		769-	-52	606	11.6	0,038 CI		0	O OSE	(g)		0.1	18.0	2.62
-54 1092 11.5 0.009 0.009 (See note) 0.11 (See note) 14.7 -56 1167 11.9 0.015 -57 1149 13.9 0.005 -58 1093 12.4 0.017 -59 1173 14.8 0.021 -61 1938 12.2 0.009 -62 1093 12.4 0.0020 -61 1093 12.1 0.008 -62 1097 13.8 0.007 -63 1024 16.9 0.034 -65 855 19.9 0.019 -66 1097 13.8 0.007 -67 1219 15.2 0.001 -68 949 17.1 <0.001 -69 398 16.5 <0.001 -60 1097 13.8 0.007 -60 1097 13.8 0.007 -60 1097 15.2 0.001 -60 1097 15.2 0.001 -60 1097 15.2 0.001 -60 1097 15.2 0.001 -60 1097 15.2 0.001 -60 1097 15.2 0.001 -60 1097 15.2 0.001 -60 1097 15.2 0.001 -60 1097 15.2 0.001 -60 1097 15.2 0.001 -60 1097 15.2 0.001 -60 1097 15.2 0.001 -60 1097 15.2 0.001 -60 1097 15.2 0.001		869-	-53	846	11.5	0.014		5.0	0.03	0.031	1. 0	0.1	16.4	2.36
-55 1041 10.8 0.008 -56 1167 11.9 0.015 -57 1149 13.9 0.005 -58 1093 12.4 0.017 -59 1173 14.8 0.021 -60 1158 13.6 0.020 -61 938 12.2 0.009 -62 1093 13.1 0.082 CI -64 1024 16.9 0.003 -65 855 19.9 0.007 -66 1097 13.8 0.007 -69 398 15.2 0.001 -69 398 15.2 0.001 -69 398 15.2 0.001 -69 398 15.2 0.001 -69 398 15.2 0.001 -69 398 15.2 0.001 -69 398 15.2 0.001 -69 398 16.5 <0.001 -69 398 16.5 <0.001		669-	-54	1092	11.5	0.009	0.009	10.0	(600 201	0.016		0.1	16.4	2.34
-56 1167 11.9 0.015 -57 1149 13.9 0.005 -58 1093 12.4 0.017 -60 1158 13.6 0.020 -61 138 12.2 0.009 -62 1093 13.1 0.082 CI -64 1024 16.9 0.007 -65 1097 13.8 0.007 -66 1097 13.8 0.007 -69 398 15.2 0.001 -64 1024 16.9 0.034 -65 1097 13.8 0.007 -66 1097 13.8 0.007 -67 1219 15.2 0.001 -68 949 17.1 < 0.001 -69 398 16.5 <0.001		-700	-52	1041	10.8	0.008			10u aac)	(e)			14.7	2.52
-57 1149 13.9 0.005 -58 1093 12.4 0.017 -59 1173 14.8 0.021 -60 1158 13.6 0.020 -61 1938 12.2 0.009 -62 1093 13.1 0.082 CI -63 1126 14.5 0.048 CI -64 1024 16.9 0.007 -65 1097 13.8 0.007 -66 1097 13.8 0.007 -69 398 15.2 0.001 -69 0.056 0.035 3.1 1.3 16.1 -60 1097 13.8 0.007 -60 1097 13.8 0.007 -60 1097 13.8 0.007 -60 1097 13.8 0.007 -60 1097 0.016 0.11 (See note) 16.7 -60 1097 13.8 0.007 -60 1097 13.8 0.007 -60 1097 0.016 0.11 (See note) 16.7 -60 1097 15.2 0.001		-701	-56	1167	11.9	210.0								
-58 1093 12.4 0.017 -59 1173 14.8 0.021 -60 1158 13.6 0.020 -61 938 12.2 0.009 -62 1093 13.1 0.082 CI -63 1126 14.5 0.048 CI -64 1024 16.9 0.019 -65 855 19.9 0.009 -65 1097 13.8 0.007 -67 1219 15.2 0.001 -68 949 17.1 < 0.001 -69 398 16.5 <0.001		-702	-57	1149	13.9	0.005								
-59 1173 14.8 0.021 0.021 0.023 1.4 (See note) 16.6 -60 1158 13.6 0.020 0.001 0.021 0.022 0.9 0.2 16.3 -62 1093 12.2 0.009 0.082 CI 0.09 0.056 0.035 3.1 12.3 16.1 0.048 CI 0.048 CI 0.04 0.040 0.036 2.8 0.7 15.6 -64 1024 16.9 0.019 0.019 0.017 0.017 0.016 0.1 (See note) 16.7 -67 1219 15.2 0.001 0.007 0.017 0.017 0.016 0.1 (See note) 16.7 -68 949 17.1 <-0.001		-703	-58	1093	12.4	0.017								
-60 1158 13.6 0.020 0.01 0.021 0.023 1.4 (See note) 16.6 -61 938 12.2 0.009 0.01 0.021 0.022 0.9 0.2 16.3 -62 1093 13.1 0.082 CI 0.09 0.056 0.035 3.1 1.3 16.1 -64 1024 16.9 0.034 0.048 CI 0.044 0.040 0.036 2.8 0.7 15.6 -65 855 19.9 0.019 0.014 0.030 0.020 0.5 9.4 17.5 -66 1097 13.8 0.007 0.007 0.017 0.017 0.016 0.1 (See note) 16.7 -68 949 17.1 <0.001 0.001 0.017 0.016 0.1 (See note) 16.7 -69 398 16.5 <0.001		-704	-59	1173	14.8	0.021								
-61 938 12.2 0.009		-705	09-	1158	13.6	0.020	`	10.0	0.021	0.023		(See note)	16.6	2,57
-62 1093 13.1 0.082 CI 0.09 0.056 0.035 3.1 15.3 16.1 0.09 0.056 0.035 3.1 1.3 16.1 0.09 0.056 0.035 3.1 1.3 16.1 0.048 CI 0.04 0.040 0.036 2.8 0.7 15.6 0.04 0.030 0.020 0.5 9.4 17.5 0.019 0.007 0.017 0.017 0.016 0.1 (See note) 16.7 0.001 0.017 0.016 0.1 (See note) 16.7 0.001 0.001 0.017 0.016 0.1 (See note) 16.7 0.001 0.0		904-	-61	938	12.2	0		•	0.021	0.022	6.0	0.2	16.3	2.73
-63 1126 14.5 0.048 CI 0.09 0.056 0.035 3.1 1.3 16.1 0.04 10.24 16.9 0.034 0.04 0.040 0.036 2.8 0.7 15.6 0.04 10.24 16.9 0.034 0.014 0.036 2.8 0.7 15.6 0.04 0.030 0.020 0.5 9.4 17.5 0.01 10.07 13.8 0.007 0.007 0.017 0.016 0.1 (See note) 16.7 0.00 0.001 0.001 0.001 0.001 0.017 0.016 0.1 (See note) 16.7 0.001 0.0		-707	-62	1093	13.1	0.009	-	<0.01	0.015	0.020		See note)	15.3	03 6
-64 1024 16.9 0.034 0.04 0.040 0.036 2.8 0.7 15.6 0.04 855 19.9 0.0034 0.010 0.017 0.016 0.1 (See note) 16.7 0.01 0.017 0.016 0.1 (See note) 16.7 0.01 0.017 0.016 0.1 (See note) 16.7 0.01 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001		-708	-63	1126	14.5	10 200 C		0.09	0.056	0.035		1.3	16.1	2 64
-65 855 19.9 0.019 0.014 0.030 0.020 0.5 9.4 17.5 -66 1097 13.8 0.007 0.007 0.017 0.016 0.1 (See note) 16.7 -67 1219 15.2 0.001 -68 949 17.1 <0.001 -69 398 16.5 <0.001		-200	-64	1024	16.9	0.034		0.04		0.036	2.8	0.7	15.6	20.2
-66 1097 13.8 0.007 0.007 0.017 0.016 0.1 (See note) 16.7 -67 1219 15.2 0.001 -68 949 17.1 <0.001 -69 398 16.5 <0.001		-710	-65	855	19,9	0.019		0.04		0.020	0.5	9.4	17.5	2.75
-67 1219 15.2 0.001 -68 949 17.1 <0.001 -69 398 16.5 <0.001		-711	99-	1007	13 0			10.0		0.016		See note)	16.7	2,16
-68 949 17.1 c		-712	-67	1210	0.0	200.0	0.007			(re)		10.75		
-69 398 16.5		-713	9	677	7.01	0.001		*						
6.01 066		-713'7"	99-	000	1/1	<0.001						ř		
			3	000		700°0>						•		

End of 126-C Note: Insufficient sample.

2		HRI	Dryl/			U308,	~						
Iole F	Footage	No.		H20	Fluorimetric	Fluorimetric	Gamma	sera Equiv	Equiv	% 0	C Organic %	Ft3/ton Density	ני ני
5-C 530	-531	14585-1	1143	10 3									5
		-2	1065	10.5	1000						is in		
	-533	6	1125	14.3	0.00								
	-534	4-	1230	15.0	0.004								
	-535	-5	1098	19,9	0.004								
	-536	9-	863	23.2	0.004		,						
	-537	-1	1458	12.9	0.001								
	-538	8	1107	14.2	0.001								
	-539	ଟ	1009	14.4	0.001								
	-240	-10	1146	12.1	0.001								
	-541	-11	915	11.5	0.011								
	-542	-12	1060	15.0	0.003								
	-543	-13	604	16.2	900.0							,	
	-544	-14	897	16.8	0,005								
	-545	-15	843	16.7	0.004	*							
	-546	-16	1018	16.4	0.005				9				
	-547	-17	981	11,5	0.004			k e					
	-548	-18	1068	13,1	0.007	0.007							
	-549	-19	1132	11.0	0.008								
	-220	-20	1130	11.4	900.0								
	-551	-21	1305	6.0	0.005								
	-552	-22	1417	7.2	0.013		2.						
	-553	-23	1193	10.7	0.010								
	1554	-24	1130	12.9	0.033								
	000	67-	1204	10.4	0.004								
	-556	-26	1044	13.4	0.004								
•	-557	-27	1083	13.5	0.002								
	-558	-28	813	14.5	0.002								
•	-559	-29	1127	16.6	0.002				,				
•	-260	-30	825	22.1	0.002	0.002							
	-561	-31	832	23.6	0.002								
	-562	-32		17.3	0.002								
	-563	-33		12.2	0.002								
•	-564	-34	1176	9.7	0.002			340					
•	-565	-35	1157	11.6	0.002								

End of 165-C

						U3OB,	%,						
Hole For	Footage	HRI No.	Dry L/ Grams	H20	Fluorimetric	Check Fluorimetric	Beta/ Gamma	Beta Equiv	Gamma	80	C Organic	Ft ³ /ton Density	Sp. Gr.
												-	
161-0	510 -511	14579 -1	899	20.0	0.003								
	-512	-5	777	25.8	0.004								
	-513	۳-	786	25.8	0.003								
	-514	4-	1184	10.7	0.002								
	-515	S.	1107	11.5	0.001								
	-516	9-	1062	11.8	0.003	0.002	N.						
,	-517	-1	1344	12.1	0.001								
	-518	80	1127.	13.82/	0.002			3					
	-519	6	1013	$16.3\frac{2}{3}$	0.002								: 61
	-220	-10	883	15.64/	0.003			0.00					
	-521	-11	870	13.72/	0.003		ecv		æ				
	-522	-12	1162	14.02/	0.002								
	-523	-13	992	16.42/	0.032		0.05	0.043	0.037	1.2	6	18.0	2, 60
	-524	-14	1038	15.62/	0.014) ;	•	3
	-525	-15	1067	15.7	0.023			ě					
	-526	-16	794	15.32/	0.014								
	-527	-17	952	19.32/	0.018								
	-528	-18	394	23.82/	0.004	0.004	0.02	0.027	0.034	0		18 7	1 3 3
	-529	-19	1053	17.42/	0.012		0.03	0.030	0.056		1 10	16.3	2 2 2 2
	-530	-20	1056	13,32/	0.041 CI		0.08	0.071	0.061	0.1	. 6	16.4	2.28
	-531	-21	990	18.32/	0.012		0.02	0.022	0.026	1 0>		6	2 42
	-532	-22	763	16.12/	0.010		0.02	0.013	0.011	2 0.1	, ,	8 8	25.2
	-533	-23	943	8.82/	0.012		0.02	0.017	0.012	<0.1	4.0	14.8	2.28
	-534	-24	1032	17.32/			0.02	0.024	0.025	0.1	0.3	18,5	2,35
	-535	-25	1107	13.72/	0.041 CI		90.0	0.049	0.038	0.5	0.2	17.0	2,43
	-536	-26	1151	$12.1\frac{2}{2}$	0.037		0.05	0.042	0.037	4.7	0.3	15,3	2,44
	-537	-27	849	21.22/	0.017		0.03	0.029	0.028	1.9	0.2	16.8	2,41
	-538	-28	1200	12.87			0.05	0.040	0.032	0.2	8.0	16.0	2.40
	-539	-29	606	16.52/	0.121 CI		0.13	0.065	0.028	<0.1	0.4	18.6	2.41
	-540	-30	1021	18.5%	0.016	0.016	0.03	0.030	0.030	0.1	0.3	17.0	2.49
	-541	-31	1135	17.22/	0.037		0.05	0.050	0.045	5.3	0.5	15.7	2,62
	-542	-32	1097	15.34	0.031		0.05	0.039	0.032	17.6	0.7	16.4	2.56
	-543	-33	1151	14.92/	0.032		0.05	0.042	0.037	21.4	1.3	15.7	2.42
	-544	-34	1198	14.24/	0.025								
	-545	-32	1001	16.45	0.023								

580 -581 14579 71 917 14.72 -582 -72 838 15.5 -583 -73 1110 16.0 -584 -74 1086 12.2 -584 -74 1086 12.2 -584 -74 1086 12.2 -585 -75 1022 12.0 -586 -76 1095 11.0 -587 -77 1192 12.9 -589 -78 1021 10.7 -589 -80 873 16.3 -593 -80 873 11.8 -594 -84 1128 14.0 -595 -87 975 11.8 -595 -87 975 11.8 -595 -87 975 11.2 -595 -87 97 16.12 -596 -86 898 13.9 -597 -87 924 20.3 </th <th>-581 -582 -583 -584 -585</th> <th>No.</th> <th>Grams</th> <th></th> <th></th> <th>Check</th> <th>Beta/</th> <th>Rota</th> <th>Gamma</th> <th>S</th> <th>C Organic</th> <th>Ft3/ton</th> <th></th>	-581 -582 -583 -584 -585	No.	Grams			Check	Beta/	Rota	Gamma	S	C Organic	Ft3/ton	
-881 1479-71 917 14.72 0.006 -72 1818 15.5 0.009 -73 1110 16.0 0.009 -74 1106 12.2 0.009 -75 1102 12.2 0.009 -75 1102 12.2 0.0009 -76 1095 11.0 0.010 -88 -76 1095 11.0 0.010 -88 -77 1192 12.9 0.010 -89 173 16.3 0.0007 -89 173 16.3 0.0007 -89 189 13.9 0.0004 -80 189 13.9 0.0004 -80 189 13.9 0.0004 -80 189 13.9 0.0004 -80 180 180 180 180 180 180 180 180 180 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				Fluorimetric	Fluorimetric	Gamma	Equiv	Equiv	86	%	Density	Sp. Gr.
-588 -77 838 155 0.000 -588 -74 1000 -588 -74 1000 -588 -75 1022 12.0 0.000 -588 -75 1022 12.0 0.001 -588 -76 1022 12.0 0.001 -588 -76 1022 12.0 0.001 -589 -79 1022 12.0 0.001 -580 -79 1022 12.0 0.001 -580 -80 1021 12.0 0.002 -580 -80 1021 12.0 0.002 -580 -80 1021 12.0 0.002 -580 -80 1021 12.0 0.003 -580 -80 1021 12.0 0.003 -580 -80 1021 12.0 0.003 -580 -80 1021 12.0 0.004 -580 -80 1021 12.0 0.004 -580 -80 1021 12.0 0.004 -580 -80 1021 12.0 0.002 -580 -80 1021 12.0 0.004 -580 -80 1022 12.0 0	1 5 8 8 4 5 8 8 5 8 8 8 8 8 8 8 8 8 8 8 8	14579 -71	917	14 72/	900		*						
-73 1110 16.0 0.009 -74 1086 12.2 0.009 -75 1005 11.0 0.010 -77 1092 12.0 0.000 -78 947 10.3 0.000 -79 10.3 0.000 -70 10.3 0.000 -70 10.3 0.000 -70 10.3 0.000 -70 10.3 0.000 -70 10.3 0.000 -70 10.3 0.000 -70 10.3 0.000 -70 10.3 0.000 -70 10.3 0.000 -70 10.4 0.000 -70 10.5 0.0	1 1 1 8 8 8 8 8 8 8 8	-72	838	15.5	900.0								
-74 1086 12.2 0.009 -75 1082 12.0 0.010 -76 1095 11.0 0.010 -77 1192 12.9 0.000 -78 1092 12.9 0.000 -79 1021 10.3 0.0007 -79 1021 10.3 0.0007 -80 1021 10.3 0.0007 -80 1021 10.3 0.0007 -80 1022 12.6 6.5 0.0003 -81 1026 11.9 0.0004 -82 1026 6.5 0.0003 -83 16.7 0.0004 -84 1028 11.9 0.0004 -85 10.0007 -90 1001 10.0007 -90 1001 10.0007 -90 1001 10.0007 -90 1001 10.0007 -90 1001 10.0007 -90 1001 10.0007 -90 1001 10.0007 -90 1001 10.0007 -90 1001 10.0007 -90 1001 10.0007 -90 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-73	1110	16.0	0.009								
-75 1022 12.0 0.010 -77 1095 11.0 0.010 -78 1095 11.0 0.010 -79 1021 10.3 0.010 -79 1021 10.3 0.010 -70 1022 12.0 0.010 -70 1022 12.0 0.010 -70 1021 10.7 0.000 -80 873 16.3 0.000 -81 1226 6.5 0.000 -81 1226 6.5 0.000 -82 1128 14.0 0.000 -83 912 11.8 0.000 -84 1128 14.0 0.000 -85 975 11.8 0.000 -86 898 13.9 0.000 -87 51.4 0.001 -88 10.6 0.002 -89 11.5 0.000 -90 11.	2885	-74	1086	12.2	0.00								
-76 1195 11.0 0.010 -77 1192 12.9 0.010 -78 947 10.3 0.007 -79 1021 10.7 0.005 -70 0.005 -70 0.005 -70 0.005 -80 1134 10.3 0.001 -81 1184 11.0 0.001 -82 1226 6.5 0.003 -83 961 11.8 0.0001 -85 975 11.8 0.0004 -87 912 16.72 -90 0.005 0.0004 -91 911 21.42 -91 911 21.42 -91 911 21.42 -91 911 21.42 -91 911 21.42 -91 911 21.42 -91 911 21.42 -91 911 21.42 -91 911 21.42 -91 911 21.42 -91 911 21.42 -91 911 21.42 -91 911 21.42 -91 911 21.42 -91 911 21.42 -91 911 911 21.42 -91 911 91.23 -91 911 91.22 -91 911 91.23 -91 911 91.22 -91 911 91.23 -91 911 91.22 -91 911 91.23 -91 911 91.23 -91 911 91.23 -91 911 91.22 -91 911 91.23 -91 911 91.23 -91 911 91.23 -91 91 91 91.23 -91 91 91 91.23 -91 91 91 91.23 -91 91 91 91 91.23 -91 91 91 91 91 91 91 91 91 91 91 91 9	-586	-75	1022	12.0	0.012								
-77 1192 12.9 0.010 -78 973 16.3 0.007 -79 1021 10.7 0.006 -80 873 16.3 0.012 -81 1144 16.1 0.010 -82 1226 6.5 0.003 -83 956 113.6 -84 1128 14.0 0.000 -85 975 113.6 -87 975 113.6 -87 975 113.6 -87 975 113.6 -87 975 113.6 -87 975 113.6 -87 975 113.6 -87 975 113.6 -87 975 113.6 -87 975 113.6 -98 975 113.6 -99 975 119.2 -90 976 10.3 -90 976 976 976 976 976 976 976 976 976 976	***	-76	1095	11.0	0.010						×.		
-78 947 10.3 0.007 0.007 -78 11.0 10.00 0.007 0.007 0.007 0.007 0.006 0.007 0.006 0.007 0.006 0.007 0.006 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.001 0.007 0.007 0.007 0.007 0.007 0.007 0.007 0.007 0.007 0.007 0.009 0.01 0.0	-587	-77	1192	12,9	0.010								
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-82 1226 6.5 0.003 -84 1128 13.6 0.003 -84 1128 0.003 -85 1128 0.003 -87 1128 0.004 -88 13.9 0.004 -88 16.12 0.004 -90 608 24.72 0.044 CI 0.046 0.07 0.007 0.07 0.07 16.4 -91 911 21.42 0.035 -92 857 10.32 0.008 -93 857 10.32 0.008 -94 603 23.62 0.038 CI 0.044 0.044 0.042 0.01 17.4 16.5 -95 1030 18.12 0.038 CI 0.03 0.02 0.02 0.02 0.02 -97 921 19.12 0.038 CI 0.038 0.03 0.022 0.02 -98 845 15.52 0.038 CI 0.03 0.038 0.032 16.5 17.0 -99 752 14.82 0.036 CI 0.03 0.038 0.032 16.8 3.2 16.4 -90 103 10.4 0.002 0.003 0.003 0.003 0.003 0.003 0.003 -101 1093 10.4 0.0002 -102 1091 10.4 0.0001 -103 1091 10.4 0.0001	-591	-81	1144	16.1	010								•
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-86 898 13.9 0.004 -87 1912 16.72 0.004 -88 1063 16.12 -89 697 25.42 -90 608 24.72 0.044 CI 0.05 0.031 0.012 0.009 -91 121.42 0.044 CI 0.046 0.07 0.056 0.042 0.1 15.4 -92 24.72 0.044 CI 0.046 0.07 0.056 0.042 0.1 17.4 16.5 -93 857 19.22 0.018 -94 603 23.62 0.018 CI 0.04 0.012 0.012 0.1 7.7 15.2 -95 1030 18.12 0.018 CI 0.04 0.049 0.04 0.049 0.3 16.5 22.4 -95 1030 18.12 0.014 0.002 0.023 0.027 0.02 0.02 0.02 0.02 0.02 -97 921 19.12 0.014 0.003 0.022 0.023 0.7 0.4 17.6 -98 845 15.52 0.016 0.03 0.03 0.007 22.2 <0.1 15.0 -101 1093 10.9 0.002 0.002 -103 1091 10.4 0.002 -103 1091 10.4 0.001		;			100.0								
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	-596	-86	868	13.9	0.004								
-88 1063 16.1½ 0.007 0.01 0.012 0.009 0.1 1.0 14.7 14.7 14.7 15.2 0.046 CI 0.046 CI 0.05 0.036 0.021 <0.1 18.4 21.9 14.7 14.7 0.044 CI 0.046 CI 0.05 0.036 0.021 <0.1 17.4 16.5 15.2 0.03 0.035 0.035 0.037 0.017 0.0 1 17.4 16.5 0.03 0.03 0.017 0.0 1 17.4 16.5 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.	-297	-87	912	16.72/	0.004		0.01	0.007	0.007	0	7	16.4	61
-89 697 25.42 -89 608 24.72 -90 608 24.72 -91 911 21.42 -92 92.4 20.035 -92 92.4 20.32 -93 857 19.22 -93 857 19.22 -94 603 0.017 0.025 0.025 0.025 -95 1030 18.12 -96 1057 14.72 -97 921 19.12 -98 845 15.52 -99 752 14.82 -90 0.002 -101 1093 10.9 -102 951 10.4 -103 10.9 -104 1086 10.3 -105 0.003 -106 0.003 -107 0.014 0.	-298	-88	1063	16.12/	0.007		0.01	0.012	0.00			14.7	10.7
-90 608 24.7½ 0.044 CI 0.046 0.07 0.056 0.042 0.1 17.4 16.5 -91 911 21.4½ 0.035 -92 924 20.3½ 0.008 -93 857 19.2½ 0.008 -94 603 23.6½ 0.018 -95 1030 18.1½ 0.038 CI 0.04 0.049 0.03 16.5 -95 1030 18.1½ 0.038 CI 0.04 0.044 0.049 0.3 16.5 -96 1057 14.7½ 0.014 -97 921 19.1½ 0.036 CI 0.02 0.023 0.027 0.4 17.6 -98 845 15.5½ 0.036 CI 0.03 0.028 0.027 21.4 <0.1 15.0 -100 906 10.2 0.003 -101 1093 10.9 0.002 -102 951 10.4 0.001 -103 10.9 0.001 -104 1053 0.001	-299	-83	697	25.42/			0.05	0.036	0.021		18 4		00.0
-91 911 21.42 0.035 0.05 0.033 0.017 0.2 13.1 16.0 15.2 15.2 0.008 0.00 0.02 0.017 0.012 0.1 7.7 15.2 15.2 0.008 0.03 0.025 0.022 8.6 7.1 20.3 15.2 0.018 0.03 0.025 0.022 8.6 7.1 20.3 0.03 0.018 0.03 0.025 0.023 8.6 7.1 20.3 0.03 0.04 0.044 0.049 0.3 16.5 22.4 0.04 0.038 CI 0.038 CI 0.04 0.044 0.049 0.3 16.5 22.4 0.036 CI 0.036 CI 0.03 0.023 0.023 0.7 0.4 17.0 0.9 15.5 0.035 CI 0.035 CI 0.03 0.023 0.023 0.7 0.4 17.6 0.04 0.035 CI 0.03 0.035 0.03 0.035 0.03 0.03 0.03 0.	009-	-90	809	24.72/		0.046	0.07	0.056	0.042		17.4	16.13	30.7
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	-601	[0]		121								0.01	71.7
-32 857 19.22 0.018 0.02 0.017 0.012 0.1 7.7 15.2 19.3 16.5 19.22 0.018 0.3 16.5 0.025 8.6 7.1 20.3 16.5 19.22 0.018 0.3 16.5 0.025 8.6 7.1 20.3 16.5 19.22 0.018 0.3 16.5 0.024 0.088 0.3 16.5 0.234 0.044 0.049 0.3 16.5 0.234 0.044 0.049 0.3 16.5 0.234 0.044 0.049 0.3 16.5 0.034 0.035 0.0 0.028 0.027 21.4 <0.1 17.6 0.03 0.035 0.0 0.035 0.0 0.03 0.038 0.032 16.8 3.2 16.4 0.049 0.001 0.003	109-	161	116	20.22/	0.035		0.05	0.033	0.017	0.2	13.1	16.0	2,33
-94 603 23.62 0.018 CI 0.03 0.025 0.022 8.6 7.1 20.3 0.94 603 23.62 0.038 CI 0.038 CI 0.04 0.044 0.049 0.3 6.4 17.0 0.04 0.045 0.05 0.05 0.05 0.05 0.05 0	-603	300	170	25.05	800.0		0.02	0.017	0.012	0.1	7.7	15.2	2.34
-95 1030 18.12 0.038 CI 0.04 0.044 0.098 0.3 16.5 22.4 0.04 1030 18.12 0.038 CI 0.04 0.044 0.049 0.3 6.4 17.0 0.05 119.12 0.036 CI 0.02 0.023 0.027 21.4 17.0 0.03 0.035 CI 0.03 0.038 0.027 21.4 17.6 0.04 0.038 0.032 16.8 3.2 16.4 0.00 0.0	-604	86-	609	23.62/			0.03	0.025	0.022	8.0	7.1	20.3	2.10
-96 1057 14.72 0.014 0.04 0.044 0.049 0.3 6.4 17.0 -96 1057 14.72 0.014 -97 921 19.12 0.036 CI 0.02 0.023 0.027 21.4 <0.1 17.6 -98 845 15.52 0.035 CI 0.04 0.038 0.027 21.4 <0.1 15.0 -99 752 14.82 0.016 -100 906 10.2 0.002 -101 1093 10.9 0.002 -102 951 10.4 0.001 -104 1086 10.3 0.001 -105 1036 11.8 0.001	-605		200	12.01		100	0.16	0.123	0.088	0,3	16.5	22.4	1.90
-96 1057 14.72/2 0.014 0.02 0.023 0.07 0.4 17.6 -97 921 19.12/2 0.036 CI 0.03 0.028 0.027 21.4 <0.1		C F	1030	10.15			0.04	0.044	0.049	0.3	6.4	17.0	2.40
-97 921 19.12 -98 845 15.52 -98 845 15.52 -99 752 14.82 -100 906 10.2 0.003 -101 1093 10.9 0.002 -103 1091 10.4 0.001 -104 1086 10.3 0.001 -105 10.8 0.032 0.002 0.03 0.019 0.007 22.2 <0.1 17.1 17.1 -101 1093 10.9 0.002 -102 951 10.4 0.001 -104 1086 10.3 0.001	909-	96-	1057	14.72/	0.014		0.02	0.023	0.023	7	4	3 71	6
-98 845 15.52 0.035 CI 0.04 0.038 0.032 16.8 3.2 16.4 -99 752 14.82 0.016 0.03 0.019 0.007 22.2 <0.1 17.1 -101 1093 10.9 0.002 0.002 0.002	-607	-97	921	19.12/			0.03	0.028	0.027	21 A		0.0	70.7
-99 752 14.82 0.016 0.03 0.019 0.007 22.2 <0.1 17.1 100 906 10.2 0.002 0.002 0.002 17.1 17.1 17.1 17.1 17.1 17.1 17.1 17.	809-	86-	845	15.54		/A	0.04	0 038	0.030	16.0			00.0
-100 906 10.2 0.003 -101 1093 10.9 0.002 -102 951 10.4 0.002 -103 1091 10.4 0.001 -104 1086 10.3 0.001 -105 1036 11.8 0.001	-609	66-	752	14.82/				0000	9 0	0.00	7.0	10.4	2.60
-101 1093 10.9 0.002 -102 951 10.4 0.002 -103 1091 10.4 0.001 -104 1086 10.3 0.001 -105 1036 11.8	-610	-100	906	10.2	0.003		?	610.0	100.0	7.77	70.1	17.1	2.54
-102 951 10.4 0.002 -103 1091 10.4 0.001 -104 1086 10.3 0.001 -105 1036 11.8 0.001	-611	-101	1093	9.01	000								
-103 1091 10.4 0.001 -104 1086 10.3 0.001 -105 1036 11.8 0.001	-612	-102	951	10.4	0.00	600					*	×	
-104 1086 10.3 -105 1036 11.8	-613	-103	1091	10.4	0.001								
-105 1036 11.8	-614	-104	1086	10.3	100.0								
֡֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜	-615	-105	1036	11.8	0.001						F		

1		٠,																																							
	Sp. Gr.																							2 75		2.66	5.66	2.63	2.67	2.67	2,65	2.65	2.63	2.66	2 64		2.63	2.64	29.2	2.64	2.61
F+3 /40n	Density																							17.1	:	15.9	17.5	16.1	15.7	16.4	16.8	15.6	16.2	16.1	16.3		10.4	17.1	10.7	17.2	17.3
C Organic	%																							<0.1			1.		1.0	•	<0.1	0.1	0.1	i	0.1		•				
002																								0.1 <	0.1									٧	0.1					•	
١	-																							0.017 0			٧				V					29 <0.1			٧		
	-																								0.016			0.034			0.017	0.057	0.033	0.024	0.022	0.029	0.042	0.025	0.011	0.010	
	Equity																							0.019	0.017	0.035	0.024	0.062	0.015	2	0.015	0.00	0.025	0.019	0.020	0.030	0.045	0.028	0.011	0.008	
	Gamma																							20.0	0.02	0.03	0.02	0.11	0.01		11	200	20.0	20.0	20.0	0.04	90.0	0.04	0.01	<0.01	
Check	ruorimetric										0.014														0.014													0.035		V	
Fluorimetric	OT TOTAL	0.001	0,002	0.002	0.012	0.011		0.012	9000	0.003	0.013	0.011	.000	200	1000	0.00	0.004	0.006	0.020	0.017	2100	210	0.021			0.045 CI		0.122 CI	0.014	0.009	0.160 CI	0.012	0.011	0.013			0.040	9.030	0.003	0.004	
H20		20.7	18.2	21.2	20.2	12.2		1.11	1001	13.2	12.6	14.2	16.9	14.0	11.2	10.01	16.0	6.01	14.02/	20.52/	13.82/	11.82/	15,12/	12, 37	10.02/	18.02	10.01	10.40	19°,'e1	15.72/	15.32/	17.32/	7.42/	17.72/	7 02/	17.52/	7 72/	12/2	22/	17.6	,
Grams		930	832	908	685	1042	1101	802	200	500	865	942	857	826	1308	1115	1094						1128		200						1351					696		1019			
HRI No.		14579 - 106	-107	-108	-109	-110	-111	-112	113	711	777	c11-	-116	-117	-118	-119	-120		-121	-122	-123	-124	-125	-126	-127	-128	-129	-130		-131	-132	-133	-134	-135	-136	-137	-138	-139	-140		,
Footage		919- 619	170-	010	670	079-	-621	-622	-623	-624	-625		-626	-627	-628	-629	-630	į	-631	-632	-633	-634	-635	-636	-637	-638	-639	-640		1041	750-	540-	-044	-645	-646	-647	-648	-649	-650		
Hole Hole	. ()																														\									

												(31 06)	
8		Ē	-			ToO o	8					10 10	(of of 47 pages)
Hole	Footage	No.	Grams	H ₂		Check	Beta/	Beta					
				1	ruorimetric	Fluorimetric	Gamma	Equiv	Early	60°	C Organic	Ft3/ton	
2-101	650 -651	14579 -141	986	10 52/					an b	ę	88	Density Sp. Gr	Sp. Gr
	-652	-142	200	10.01	0.003								
	-653	-143	200	10.15	0.003								
	-654	25.	134	12.44/	0.001								
		551-	787	15.12/	100.00								
	669-	-145	1074	14.8	100.00								
	-656				100.0								
	200	-140	1116	16.6	<0.00								
	100	-147	997	16.0	100								
	-658	-148	648	13.7	1000						j		o
	-629	-149	1135	120	100.0								
	099-	-150	020	5.5	<0.00								
			0/6	14.6	<0.001	<0.001							
	199-	-151	912	14.6								•	
	-662	-152	803	13.0	1000								,
	-663	-153	1107	12.4	1000								
					100.0								
End of 161-C	익												

			•				U3O8, %	8, %						
Hole	Footage	HRI No.	Dry∐ Grams	H20	Fluori	Fluorimetric	Check Fluorimetric	Beta/ Gamma	Beta Equiv	Gamma	% 0	C Organic %	Ft ³ /ton Density	Sp. Gr.
	3													
169-C	909- 509	14643-1	1001	16.4	0.0	0.004	0.005							
	-607	-2	1057	13,5	0.0	0.005								
	-608	မှ	1021	13,1	0	90000	. · · · · · · · · · · · · · · · · · · ·							
	609-	4-	1055	13,1	0.0	0.007								
	-610	-5	1209	7.9	0.0	0.016								٠
	-611	9-	991	13.7	0.0	0.016								
	-612	-7	963	15.4	0	0.016								
	-613	œ.	965	15.3	0	0.016								
	-614	9	1130	15.8		0.015		000	0.00	2	9	-		
	-615	-10	932	14.1	0	0.010	0.011	×0.0	010	0.010	20.0	1.0	17.6	2.33
)			2	710.0			71.0	10.7
	-616	-11	1133	16.8	0.0	0,052 CI		90.0	0.038	0.023	20.3	1.0	16.0	2.59
	-617	-12	995	15,5	0.015	15		0.02	0.018	0.015	26.0	C 0 3	16.7	2 17
	-618	-13	1217	14.6	0.014	14		0 00	910	0.0	26.00		1001	71.7
	-619	-14	1265	12.4	0.0						0.07	1.07	13.0	4.30
	629		200	7 0 0 1		0.0								
	070-	cT-	4/6	7° C	•	0.008								
	-621	-16	1045	12,4	0.010	10								,
	-622	-17	857	14.9	0.021	121								
	-623	-13	944	10.4	0.00		17							
	-624	2 -	616		0.01	14								
9	-625	-20	202	15.0	0.0	1 0	0.013							
		2	2	0.01	•	2	710.0							
	-626	-21	647	12.9	0.012	12								
	-627	-22	1042	10.2	0.012	12								
	-628	-23	979	0.4	0.012	12								
	-629	-24	792	11.8	0.011	11		0.02	0.014	1100	2	1 0 2	3 31	000
	-630	-25	712	12.7	0.030	30		0.04	0.037	0.032	16.9	< 0.1	15.0	2.03
													•	1
	159-	97-	1003	17.6	0.045	45 CI		0.08	0.043	0.025	16.0	3.0	18,3	2.66
	-632	-27	880	20.0	0.030	30		0.04	0.029	0.022	10.9	8.0	17.7	2.57
	-633	-28	1165	13.2	0.014	14		0.02	0.016	0.014	40.5	<0.1	14.9	2.50
	-634	-29	1138	13.9	0.026	26		0.03	0.022	0.015	37.0	0.7	18.0	2.69
	-635	-30	1333	12.3	0.014	14	0.015	0.02	0.015	0.013	49.7	<0.1	16.5	2.66
		;		:										
	969-	-31	1220	11.4	0.030	30	•	0.03	0.025	0.020	40.8	<0.1	15,9	2.67
	100-	-35-	1728	11.4	0.022	7.7		0.02	0.020	0.017	43,3	40. 1	15,9	2.75
	-638	-33	980	10.0	0.028	28		0.03	0.022	0.019	23.9	4.2	15,3	2.64
	-639	-34	1080	10.6	0.030			0.02	0.022	0.023	46.4	< 0.1	16.7	2.63
	-640	-35	975	13,4	0.035	35 CI	•	0.03	0.027	0.025	34.3	1.0	14.9	2 20
								Ċ.			(F)	>

						TI3Os R	8						
N N	Pootage	HRI	Dry 1	. 6	District D	Check	Beta/	Beta	Gamma	000	C Organic	Ft3/ton	
	o financia		Citatio	2717	r and amenac	rinorimenic	Сашша	Equiv	Equiv	86	»e	Density	Sp. Gr.
169-C	640 -641	14643-36	827	10.9	0.039 CI		0.03	0.030	0.027	38.8	1.0	7.	
	-642	-37	1276	10.1	0.035 CI		0.03	0.028	0.027	35.9	< 0.1	2.5	2.30
	-643	-38	1160	13.9	0.028		0.02	0.041	0.050	25,3	< 0.1	16.6	2.00
	-644	-39	1134	10.8	0.019		0.02	0.016	0.013	33.9	1,2	15.2	000
	-645	-40	1260	10.7	0.009	0.00					•		
	-646	-41	1203	8,5	0.009		,						
	-647	-42	1270	0.6	0.00								
	-648	-43	997	16,5	0.017								
	-649	-44	1045	8.4	0.020			K			,	5	
	-650	-45	1098	13.9	0.018								
	-651	-46	808	16.0	0.008								
	-652	-47	1166	13.3	0 017								
	-653	-48	1130	12.1	010								
	-654	67-	1081	14.9	2000								
	-655	-20	916	15,3	0.006	0.006							
	939												
		10-	116	14.0	0.000								
	769-	-52	1882	2.5	0.003							*	
,	-658	-53	1042	14.1	0.004								
· ••	-629	-54	1128	11.7	0.004				•				
	099-	-55	959	15,9	0.004								
	-661	-56	1263	15.7	900.0								
	-662	-57	966	15.8	900.0								
	-663	-58	934	16.0	0.004		x 13						
	-664	-59	853	14.6	0.003	•							
	-665	-60	1119	15.7	0.004	0.007							
	999-	-61	1038	15,6	0.007				G.				
	-667	7-62	1005	16.0	0.007								
	899-	-63	788	17.1	0.004								
	699-	-64	817	26.6	0.003			*					
	-670	-65	794	16.5	0.002								
	-671	99-	1047	15.7	0.002				ė,				
	-672	-67	1245	11.8	0.001								9:
	-673	89-	1608	13.7	0.013								
	-674	69-	1097	13.7	0.007	ý							
	-675	-70	1269	13.9	0.002	<0.001							

(0.00		U3O8, %	*	5					
Hole	Footage	HRI No.	Dry⊥/ Grams	H20	Fluorimetric	Check Fluorimetric	Beta/ Gamma	Beta	Gamma	% 0	C Organic	Ft3/ton	ć
									ATRICA	8	9	Density	ob. 61.
169-C	675 -676	14643-71	1083	19,6	0,002								
	-677	-72	995	18,9	0.002								
	-678	-73	1019	17.5	0.002								
	629-	-74	1074	12.2	0.001					٠			
	-680	-75	888	16.8	0.002								
	-681	-76	890	17.4	0.001								
	-682	-77	1057	13.0	0.002								
	-683	-78	844	19.4	0.013								
	-684	-79	841	18.1	0.008		W.						
	-685	-80	863	17.0	0.007	0.010					ε		
	989-	-81	991	15.3	900.0			•		er.		ĸ	
	-687	-82	1339	8.6	0.004	•	2						
	-688	-83	1357	3.9	0.001								
	-689	-84	1111	5.3	0.001								
	069-	-85	1193	10.5	0.002								
	-691	-86	907	14.4	0.002								
	-692	-87	1020	14.3	0.002								
	-693	-88	1141	13.3	0.001								
	-694	-89	1295	12.6	0.001						×		
	-695	06-	1110	14.0	0.001	< 0.001							
	969-	-91	1000	11.8	0.001								
	-697	-92	1204	12,7	0.001								
	869-	-63	804	12.3	0.001								
	-700	# io	1222	13.2	0.001	* *							
	-701	96-	1006	10.8	0.001		19						
	-702	-97	746	15.7	0.003								
	-703	86-	1029	18,7	0.007								
	-704	66-	812	16.7	0.021	3							
	-/02	-100	823	36.1	0.004	0.005		ř					
	-706	-101	1137	11.9	0.004	2							
	-707	-102	1110	15,3	0.004								
	-708	-103	1026	19.3	0.004								
	60/-	-104	1089	10.3	0.008								
,	-/10	-103	8201	۸.۷	900.0	•							
									,				

					460	4603 - Date Creek						(35 of 47 pages)	pages)
2			-			U3OB,	86						
Hole	Footage	No.	Grams	H20	Fluorimetric	Check Fluorimetric	Beta/ Gamma	Beta	Gamma	°05	C Organic	Ft3/ton	
169-C	710 -711	14643-106	926	11 %					Amba	9	R	Density	Sp. Gr.
	-712	-107		10.2	0.00								
*	-713	-108		11.7	0000								
	-714	-109		30	0.00			3					
	-715	-110	1378	6.0	0.007	0.008							
	-716	-111		14.3	000		£°						
	-717	-112	1114	13.3	0.005				101				
	-718	-113		13,3	0.010								
	-719	-114		12.7	0.022		6						
	-720	-115	1186	3.6	0.025		20.0	0.020	0.013	40.0	<0.1	17.9	. 2.75
	-721	-116	942	a C.	6			0.050	0.020	19.1	0.2	15,5	2.55
	-722	-117	1373	8.0	0.045 CT		0.02	0.017		17.6	<0.1	17.0	2 53
	-723	-118		10.4	0.035 CT		90.0	0.035		0.3	<0.1	16.9	2 44
	-724	-119		13.9	0.006		0.04	0.026		0.1	< 0.1	15.0	2.54
	-725	-120		13.3	0.003	0.002	0.01	600.0	900.0	<0.1	0.1	17.0	2.56
	-726	-121	540	13.9	0 00						*		
	-727	-122	. 209	13.5	0.001				*				
	-728	-123	650	13,6	<0.001								
	-729	-124	624	13,4	0,001								
	-730	-125	296	13.9	0.001								
	-731	-126	948	13.6	0.001								
	-732	-127	901	3.2	0.001								
	-733	-128	277	13,7	0.001								
	-734	-129	857	14.1	0.001								
	-735	-130	629	14.6	0.001	<0.001							
	-736	-131	672	13.3	0.001								
	-737	-132	820	13.5	0.001								
		-133	642	14.0	0.001								
8	744 -/45	-134	957	12.3	0.001								
End of 169	End of 169-C						,				•		
Note: No 1	foil samples.											ä	

4603 - Date Creek

(36 of 47 pages)			Sp. Gr.																											2.58	2.54	2.61	2.67	80.7	2.52	2.51	2.52	2.54
(36 of 4		Ft3/ton	Density					Y																		ě			:	14.3	10.4	14.9	14.0		14.7	16.8	15.9	14.8
		C Organic	R																										,	4.0		8.0	1,1	,			0.2	0.7
	8	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	8																										. 9				0		٧			
	Gamma																										æ		1.6		~			0	-			20.9
			-															×				9							0.009	0.005	0.021	0.032	0.041	0.021	0.019	0.148	0.088	0.038
	Beta	-					2		140								25						ï						0.007	0.005	0.031	0.034	0.043	0.024	0.024	0.181	0.118	650.0
	% Beta/	Gamma																									ě	į	<0.01	<0.01	0.05	0.04	50.0	0.03	0.03	0.24	0.17	5 ,
	8 2 3 3 3 3	etric							_																	*			V	V					_	,		•
	Check	Fluorimetric							<0.001								,				0.021							i.				0.036						
	Pluodmodul	Transmetric	000	200.0	0.00		0.001		<0.001	0.001	0.002	0.003		0.002	0.003	100.0	0.007		0.001	0.016	0.021	0.005		0.012	0.00	0.001	0.001	0.004	0.001	0.040 CI	0.034 CI	0.035 CI	0.00	0.016	0.214 CT	0.172 CI	0.030 CI	
	HOO	l	18.3	10.3	7.6	9.1	8.6		7 0	0.0	30.0	15.8		r -	16.2	2 4	. 6	16.00	12 72/	16.62/	14.82/	12.52/	14 02/	11 52/	12.82/	15.72/	13,12/	11.52/	15.24	14.02/	12.12/	11.82/	12.02/	14.42/	11.92/	10.02/	14.05/	*
	Grams		825	1084	1339	1540	1371	1326	1207	1222	981	1283	1390	1274	819	1217	906	010	893	788	1055	1246	1157	1343	1170	1097	1243	1250	1147	1040			1382	867	1303	1358	1574	
	HRI No.	14	14661-1	-5	£-	-4	Ş	9-	-7	8	6-	-10	-11	-12	-13	-14	-15	116	-12	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30	-31	-32	ee-	-34	-32	
	Footage		660 -661	-662	-663	-004	-665	999-	-667	899-	699-	-670	-671	-672	-673	-674	-675	-676	-677	-678	-629	-680	-681	-682	-683	-684	6001	-686	1001	889-	600	0.60	-691	-692	5693	4 1	0 0 0 0 0	
2	Hole		1-C		·							×															(W)				٠							

		, ,				U3OB,	%						
Hole Hole	Footage	HRI No.	Dry.1/ Grams	H20	Fluorimetric	Check Fluorimetric	Beta/ Gamma	Beta Equiv	Gamma Equiv	% <mark>0</mark>	C Organic %	Ft ³ /ton Density	Sp. Gr.
7-121	303- 303	14661 - 36	1204	11 22/	5 101			000		:			
		1300	1176	11.02/	0.1010		0.12	0.080	0.056	12.0	4.0	13.9	2.57
	869	200	1231	10 22/			10.0	0.010	0.020			14.8	2.58
			101	12.01			10.07	0.011	0.013	2.0	0.0	14.7	2.58
	550	65-	1101	17.36	0.010		0.01	0.017	0.020	7.3	0.3	16.4	2.23
	-200	-40	1121	18.64	0.038 CI	•	0.05	0.034	0.027	15.7	<0.1	16.8	2.54
	-701	-41	1158	15.72/	0,028 CI		0,03	0.027	0.025	23.4	6.0	15.3	2 55
	-702	-42	1407	10.32/	0.017	0.019	0.02	0.022	0.021	27.0	5.0	13.0	2.5
	-703	-43	1161	14.92/	0.028		0.03	0.022	0.017	11.8	8.0	16.7	2 44
	-704	-44	1165	14.32/	0.017						•		,
	-705	-45	1227	8.82/	0.017								
	-206	-46	1104	12 12/	210.0							×	
	100	2 2	1000	12.12	0.00								
	1071	74.	1302	13.15	0.013			,			,		
	-708	-48	1254	9.66	0.012								
	-709	-49	953	9.36	0.018								
	-710	-20	1382	7.14/	0.022		0.02	0.019	0.016	18,1	0.7	14.0	2.44
*	-711	-51	1266	9.22/	0,019		0.02	0.017	0.016	15.7	<0.1	14 5	2 40
	-712	-52	1155	8.42/	0.046 CI		0.05	0.038	0.029	4	100	1 91	
	-713	-53	959	5.62/	0.015		0.01	0.011	0.011	4.7	4 0.1	19.5	26.0
	-714	-54	1369	10.12/	0.009	0,009	<0.01	0.009	0.010	2.8	9.0	17.0	38
	-715	-55	1127	16.02/	0.010		0.01	0.008	900.0	1.8	0.4	16,1	2,35
	-716	-56	1161	12.02/	0.011		10		110	0	ć	10.	,
	-717	-57	879	21.92/	0.00	196		410.0	0.0	, c	•	13.7	***
	-718	-58	1098	20.82/	0.049 CI		0.05	0.030	0.019		4 0.1	16.7	2.0
	-719	-59	1259	10,12/	0.015		0.01	0.017	0.018		V 0.1	8	
	-720	09-	1073	12,32/	0.014		0.01	0.011	0.010	0.3	0.4	16.6	2.63
	-721	-61	971	11,2	0.008				28				
	-722	-62	1206	12.1	0.008	i,							
	-723	-63	1079	7.5	0.005			•					
	-724	-64	1503	2.4	0.005						÷		
	-725	-65	1203	5.8	0.007								
	-726	99-	1076	9.5	0.011	0.011					ž		
	-727	-67	1270	10.7	0.010								
	-728	-68	1020	12.8	0.026							•	
	-729	69-	1144	15.1	0.020								
	-730	-70	976	15.1	0.011								

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		•			U3O8, %	%							
Footage	HRI No.	Dry I/ Grams	H20	Fluorimetric	Check Fluorimetric	Beta/ Gamma	Beta	Gamma	% 0 0 8	CO ₂ C Organic Ft ³ /ton % % Density	Ft3/ton Density	Sp	
730 -731	14001-71	1207	8.0	0.003									
-732	-72	1536	5.7	0.003									
-733	-73	1242	13.0	0.005									
-734	-74	1415	12.0	0.004									
-735	-75	1193	14.6	0.007									
-736		979	18.7	0.031 CI		0.02	0.012 0.009	0,009	0.1	12.5	16.3	2.28	
-737	-77	1100	17.0	0.018									
-738		1207	12.1	0.003	0.003				÷				
-739		1257	13,1	0.001									
-740		881	18.0	0.002									
740 -740'6"		432	16,3	0.001									

(23 of 47 pages)		ton	alto ca	1						74.7																				2.41	77.7	2,36	2.66	2.45	2.41		
60		Ft3/ton							16.3	•																			9	איני מיני	0 .01	21.1	15.5	13.0	2.6		
r		C Organic	%						1.5									,											4.1	10.9		8.7	9.0	7.7			
		O	%						3.8																				28.5	24.6		0.7	0.17			247	
		Gamma	Equiv						0.016	. 10							13											á			9000		0.054				
		Beta	Amba		ř				0.028																				0.005			0.038					
	86	Beta/	Dillilling						0.05																					0.01	0.07						
	U3OB,	Check Fluorimetric			0.00								9	0.020										0 003					•						0.005		
		Fluorimetric		900	0.00	500	00.0	0.037		0.008	0.005	0.004	0.007	970.0	0.018	0.026	0.011	0.002	100.0	0.002	0.001	<0.001	0.001	0.002		710.0	2000	200.0	0.011		0.054 CI	0.021	0.085 CI	010.0	900.0	0.004	0.004
		H20		13.9	15.0	13.2	14.8	16.1	1	8.71	12.4	12.2	2.1.2		19.6	24.5	13.0	12.7		16.7	16.0	18.1	18.1	16.4	19.5	2.6	4.3	7.7	16.4		6.02	0 0	2. 4.		17.2	1.01	
	7.2	Grams		520	299	786	1127	1026	000	1100	013							1264				1005							654 1				685	•	000		
	HRI	No.		14678-1	-2	۳	7	5-	9		e a	9 9	-10			112	71-	-15	:	97.	7.7	81-	-19	-20		-22				-26			-29	-30	-31		
		Footage		555 -556	-557	-558	-229	-260	-561	-562	-563	-564	-565	-566	-567	-568	-569	-570	122	-577	-572	575	7/0	-272	-576	-577	-278	-579	-580	-581	-582	-583	-584	1 -592	-593	-594	-595
	2	Hole		5																														591			

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						U3OR.	86						
DC	Footage	HRI No.	Dry 1/ Grams	H20	Fluorimetric	Check	Beta/ Gamma	Beta	Gamma	% CO %	C Organic	Ft3/ton Density	i S
											2	201102	5
175-C	295 -596	14678-34	1182	10.5	0.001								
	-297	-32	1089	10.6	0.001								
	-598	-36	1133	12.4	0.001						•		
	-599	-37	697	14.2	0.001								
	-600	-38	822	14.0	0.002								
	-601	-39	616	16.0	0.001								
	-602	-40	899	9.6	0.008	0.007	0.01	0.011	010	12.8	, ,	9	63
	-603	-41	1026	9.6	0.016		0.01	0.024	0.032	20.0	4.0	14.9	20.02
	-604	-42	602	12.9	0.099 CI		0.09	0.062	0.044	19,5		14.0	2.07
	-605	-43	1030	14.9	0.033 CI		0.04	0.028	0.022	6.8	< 0.1	15.6	2.69
	-606	-44	834	19.4	10 950 O		6	1		•			
	-607	-45	826	16.5	0000		500	0.01	0.01	1 C	0.0	15.3	2.55
	-608	-46	903	16.9	0.00		0.02	0.010	0.00	1.7	٥.	17.0	2.47
	-609	-47	606	12.6	0.003					140			
16	-610	-48	913	17.4	0.002						,		
	-611	-49	979	13,1	0.002						x		
	-612	-20	907	15.8	0.002	0.002							
	-613	-51	914	16.2	0.002								
	-614	-52	493	14.4	0.002								
	-615	-53	488	13,4	0.001			*					
	જો	-54	878	15.2	0.001	i							
	એ	-55	950	13.6	0.001								
	જો	-56	941	15.4	0.001							ŧ	
	ો	-57	645	12.6	0.001								
ě	ો	-58	1012	11.0	0.001								
						,			12				

End of 175-C

5/ Numbers 54-58 came from 615-630'. Very poor recovery. Only 5' of material in this box and samples taken in order, top to bottom, but no footages available.

						Tage	8						
Hole	Footage	HRI No.	Dry1/ Grams	H20	Fluorimetric	Check Fluorimetric	Beta/ Gamma	Beta	Gamma	%0	C Organic	Ft3/ton	, 5
				*								, and a second	
177-C	575 -576	14679-36	1241	15.0	0.009		0.02	0.017	0.012	2.5	0.2	1.91	2 53
	-577	-37	1142	14.9	0.040 CI		0.05	0.044	0.035	14.1	1.0	17.2	2.0
	-578	-38	1068	14.4	0.040 CI		0.05	0.044	0.036	13.6	<0.1	17.4	2. 5
		-39	900	14.5	0.00		0.02	0.017	0.018	7.1	<0.1	18.2	20.2
	583 -584	-40	1130	17.7	900.0	900.0					!		•
	-282	-41	1320	15.4	0.007								•
	-586	-42	1357	13.72/	0.007								
	-587	-43	853	18.22/	0.007		0.01	0.014	0.00	9 6		2 31	7
	-588	-44	1012	17.62/	0.010		0.02	0.018	0.016	4.0		7.01	20.2
	-589	-45	1002	18.32/	0.113 CI		0.12	0.078	0.035	8		16.3	2 53
	-290	-46	1219	17.92/	0.010	. 4	0.02	0.016	0.013	3,1	<0.1	16.4	2.60
	-591	-47	912	19.12/	900.0		0.02	0.012	0.006	P 0	~	7 91	6
	-592	-48	938	30.02/	0.007						2	r.01	60.3
	-593	-49	1231	7.12/	0.003								
	-594	-20	1118	12.62/	0.003	0.004							
	-595	-51	1130	17.52/	0.004								
	-596	-52	1252	16.52/	0.008			*					
	-597	-53	1275	15.62/	0.006								
	-598	-54	1081	16.32/	0.005								
	-599	-55	968	18.02/	0.005				*				
	-009	-56	963	16.62/	0.004	N.						9	
	-601	-57	1254	14.42/	0,005								
	-602	-58	1128	15.9	900.0								
	-603	-29	920	12.3	0.005								
	-604	-60	1093	16.6	0.011	<0.001							
	2001	10-	903	61.3	0.013				*			\	
	909-	-62	1266	14.5	0.008	,							
	-603	-63	939	14.5	0.033 CI		0.04	0.037	0.031	12.8	1.4	17.6	2.56
	000-	1 1 10 4	1128	12.0	0.016								
	-610	99-	1067	14.7	0,009								-
	-611	-67	949	13.9	0.004	,							
	-612	89-	1094	12.8	0.002								
	-613	69-	1123	11.9	0.001					*50			
	-614	-70	1096	12.0	<0.001	0.011			. •				
	-615	-71	1090	13.5	<0.001								
			i k										

						U3C	U3O8, %					. '	
8	٠	HRI	Dryl					Beta	Gamma	202	C Organic	Ft3/ton	,
Hole	Footage	No.	Grams	H20	Fluorimetric	c Fluorimetric	с Сатта	Equiv	Equiv	%	%	Density	Sp. Gr.
177-C	615 -616	14679-72	1079	13.6	<0.001								
	-617	-73	1132	12,4	<0.001					*			
	-618	-74	1133	16.2	0.001								
	-619	-75	985	18,6	0.003								
	-620	94-	813	22.2	0.026								
	-621	-77	837	19,0	0.008								
	-622	-78	1135	15,4	0.002								
	-623	-79	1326	11.3	0.003								
	-624	-80	1260	10.4	0.004	0.004		3					
	-625	-81	978	15.4	0.004								•
	363-	-82	1124	14.1	0.004		*						
	0701	300											
	179-	20.0	1100	10.0	0.00								×
	-628	40	9911		0000								
	-629	-82	1034	5.4	0.000				e la				
	-630	-86	1332	7.9	0.005	•							
	-631	-87	1080	4.8	0.010								
	-632	88-	1299	4.7	0.007								
	-633	-89	1079	7.7	0.009								
	-634	06-	1115	15.1	0.010	0.010	0.02	0.017	0.013	0.3	4.0	18.0	2.32
	-635	-91	793	20.6	0.014	:	0.03	0.023	0.018	9.0	<0.1	18.1	2,39
	-636	-92	1052	20.2	0.051	5	0.07	0.052	0.039	0.1	0.2	18.5	2.41
	-637	-93	1172	8.6	0.016		0.02	0.025	0.029	0.1	0.1	13.1	2.64
	-638	-94	1047	10.1	0.014		0.03	0.021	0.014	0.1	<0.1	14.8	2,38
	-639	-95	1240	13.6	0.012		,						
	-640	96-	1001	13.9	900.0								
	-641	-97	1104	14.1	0.008								
	-642	86-		14.9	0.017								
	-643	66-		14.6	0.005								
	-644	-100		15.1	0.003	٠							
	-645	-101		14.7	0.002								
	-646	-102		15.4	0,002								
	-647	-103		15,1	0.002	•							
	-648	-104		16.3	0.002					-			
	-649	-105	941	15.1	0.002								
	-650	-106		15.0	0.002								
												3	

			٠									,	
					460	4603 - Date Creek			180			(44 of 47 pages)	pages)
						U3O8, %	%						
8		HRI	Dryl			Check	Beta/	Beta	Gamma	C02	C Organic	Ft3/ton	
Hole	Footage	No.	Grams	H20	Fluorimetric	Fluorimetric	Gamma	Equiv	Equiv	86	»«	Density	Sp. Gr.
177-C	650 -651	14679-107	903	14.2	0.003								
	-652	-108	989	16.5	0.002								
	-653	-109	694	17.3	0.002								
	-654	-110	1075	15.5	0.002	0.002							
	-655	-111	993	16.4	0.001								
	-656	-112	1118	17.8	0.001								
	-657	-113	880	14.3	0.001				j				
	-658	-114	186	15.6	<0.001								
	-659	-115	951	16.6	<0.001								•
	099-	-116	878	13.7	<0.001	ar an							*
	-661	-117 10	1005	15,1	<0.001	9 2							
	-662	-118	961	16.3	0.001			191	٠			÷	
	-663	-119	920	16.0	<0.001			٠					
	-664	-120	1037	15.9	<0.001	<0.001							
	-665	-121	1042	15.8	<0.001								
	999-	-122	828	16.7	<0.001							H T	
	-667	-123	838	17.6	<0.001		ē	*		26			
	-668	-124	488	16.7	<0.001	•)							

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		Sp. Gr.				,					2.48 2.42 2.51 2.46	
	Ft3/ton	Density			•			*	300 1		16.5 15.0 17.5 13.6	
	C Organic	e									0.7 <0.1 1.5 <0.1 1.5	
	% CO %									4	3.4 7.6 < 12.1 28.5 < 14.9	
1	Gamma										0.006 0.009 0.152 0.012	
	Beta										0.007 0.012 0.167 0.010	
96	Beta/ Gamma										<pre>< 0.01 0.02 0.19 </pre>	
U3O8. %	Check Fluorimetric	*	·.		,				· ,		0.200	
	Fluorimetric	0.002	0.009	0.005	0.002	0.017	0.005	0.002	0.004	0.015 0.006 0.007 0.007	0.006 0.012 0.012 0.012	0.009 0.013 0.014 0.003
	H20	12.5	3.8	6.1 8.9 10.2	19.7	5.5 9.0 18.3	13.1	9.7	11.8 4.8 7.4	6 8 8 5 2 20 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	16.42 9.02 11.82 8.52 12.92	6.7 <u>2</u> / 8.9 18.2 10.6 6.9
/1 -	Grams	1160	1477	875 1045 1037	976	1150 990 953	1017	1326 1219	1161 1355 1094	1158 1096 1095 1224 1220		1292 1176 814 1193 1223
	No.	14783 -1 -2 -3	4 5	9118	-10	-11 -12 -13	-14 -15	-16 -17	-18 -19 -20	- 21 - 22 - 23 - 24 - 25	- 26 - 27 - 29 - 30 - 30	34 33 34 33 34 35 4 35 4 35 4 35 4 35 4
	Footage	530 -531 -532 -533	-534	-536 -537 -538	-539	-541 -542 -543	-544	-546	-548 -549 -550	1 5 5 5 1 1 1 1 5 5 5 5 5 5 5 5 5 5 5 5	1556 1557 1558 1559 1560	1562 1563 1564 1565
٤	Hole	176-C										

Creek	
Date	
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14783-36 1077 6.7 0.005 0.00			HR	Day			U308,	뗏						
14783-36 1077 6.7	11010	Footage	No.	Grams		Fluorimetric		Beta/ Gamma		Gamma	00°	C Organic	Ft3/ton	
-17 1068 13.5 0.000 -18 14 15. 0.000 -19 14 16.5 0.000 -19 15.0 0.	Q-9		14783 -36	1077	4					Ainba	86	%	Density	Sp. Gr.
		-267	-37	1068	13.5	500.0								
-39 847 147 0.005		-268	-38	1080	18.0	0000								
-40 684 13.7 0.100 CI 0.01 0.021 0.016 1.0 0.1 16.5 -41 910 16.2 0.012 CI 0.02 0.03 0.038 0.042 1.6 0.1 15.7 -43 969 16.3 0.012 CI 0.03 0.038 0.042 1.6 0.1 14.6 -44 863 18.8 0.005 0.005 0.020 0.026 0.026 1.6 0.1 15.9 -46 954 13.5 0.003 0.005 0.022 0.018 0.017 3.9 0.1 15.9 -48 1012 17.3 0.003 -49 1012 17.3 0.003 -51 84 22.9 0.023 -52 755 13.5 0.003 -52 758 13.5 0.003 -53 831 12.9 0.003 -54 823 22.6 0.017 -55 788 23.1 0.003 -60 975 14.4 0.001 -60 975 14.4 0.001 -60 975 14.4 0.001 -61 90 17.7 0.003 -62 0.018 0.023 1.5 16.5 0.1 15.9 -63 831 18.0 0.003 -64 0.003 0.003 -65 1129 7.2 0.003 -67 918 18.0 0.003 -68 910 18.5 0.003 -69 975 14.4 0.001 -60 975 14.4 0.001 -60 975 17.5 17.5 17.5 17.5 17.5 17.5 17.5 17	,	-269	-39	847	14.7	700.0		<0.01	0.010	0,00		,		
-41 910 16.2 0.100 01 0.12 0.098 0.098 1.6 0.1 15.7 0.100 01 0.1 0.100 01 0.1 0.1 0.1 0.1 0		-570	-40	684	13.7	0.005		0.01	0.021	910	0.0	0.1	16.5	2.70
-41 910 16.2 0.012 CT 0.03 0.036 1.6 0.3 17.0 14.6 0.3 17.0 14.6 0.3 17.0 14.6 0.3 16.3 0.005 16.3 0.005 0.0						0.105 CI		0.12	0.098	0.00	8.7	0.1	15.7	2.65
-42 997 14.9 0.24d CT 0.210 0.030 0.032 1.4 0.1 14.6 -43 989 16.3 0.005 0.005 0.002 0.007 1.4 0.1 14.6 -44 863 18.8 0.005 0.005 0.002 0.012 0.017 3.9 0.1 15.9 -46 954 13.5 0.003 0.0006 0.002 0.018 0.017 3.9 0.1 15.9 -48 1012 17.3 0.009 -50 917 11.9 0.002 -51 814 22.9 0.003 -52 755 18.5 0.003 -52 755 18.5 0.003 -53 891 22.9 0.003 -54 823 22.6 0.017 -56 1129 7.2 0.002 -57 998 14.9 0.002 -58 912 10.0 0.002 -59 913 18.0 0.003 -60 975 11.4 0.000 -60 975 11.4 0.000 -60 975 11.4 0.000 -60 975 11.4 0.000 -60 975 11.4 0.000 -60 975 11.5 0.003 -60 975 11.5 0.		176-	-41	910	16.2	0 012 CT				0.00	1.6	0.3	17.0	-
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-54 823 22.6 0.017 -55 758 23.1 0.031 CI 0.04 0.030 0.023 1.5 16.5 21.2 -56 1129 7.2 0.005 -57 998 14.9 0.002 -59 831 18.0 0.002 -60 975 14.4 0.001 -61 955 15.1 0.001 -62 1027 17.4 0.003 -64 1162 10.0 0.003 -65 710 22.3 0.003 CI 0.04 0.024 0.015 12.3 10.5 17.9 2 -65 840 17.7 0.019 CI 0.04 0.024 0.024 0.015 12.3 10.5 17.9 2 -65 866 16.8 0.003 -67 593 22.9 0.035 CI 0.04 0.024 0.026 0.001 0.05 -69 1233 7.8 0.003 -70 1139 16.1 0.004 -70 1139 16.1 0.004 -70 1139 16.1 0.004		-583	-53	591	22.9	0.014								
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-67 593 22.9 0.035 GI 0.03 0.019 0.010 0.3 15.0 17.9 -68 866 16.8 0.019 -69 1233 7.8 0.005 -70 1139 16.1 0.004 -69 0.005 -70 1139 16.1 0.004		-596	99-					0.04	0.024			10.5	15.9	2.50
-68 866 16.8 0.019 0.028 0.021 3.3 15.0 19.3 -68 1233 7.8 0.005 <0.01 0.006 0.006 0.004 15.3 0.8 -70 1139 16.1 0.004 0.005 0.006 0.006 15.3 0.8 14.4		-597			7.7			000			•	2.01	17.9	2.37
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-69 1233 7.8 0.005 -0.018 0.016 24.1 <0.1 17.1 -70 1139 16.1 0.004 0.004 15.3 0.8 14.4			80		8.9	0.019		* 6	870.0		3,3	3.7		
-70 1139 16.1 0.004 0.004 0.006 0.004 15.3 0.8 17.1		ממים ו	-69		7.8	0.005	,	20.0	0.018			<0.1		16.2
		000	-70		6.1	0.004		10.0	900.0			0.8		60.0
				*									r	70.

4603 - Date Creek

(47 of 47 pages)

		91	•			U3O8, %	8						
Hole	Footage	HRI No.	Grams	H20	Fluorimetric	Check Fluorimetric	Beta/ Gamma	Beta Equiv	Gamma	% 0 0 8	CO ₂ C Organic	Ft3/ton	5
176-C 60	600 -601	14783 -71	038	. 0								(Name)	1
	-602	-72	1050	17.9	0.004							ı	
	-603	-73	965	18.8	0.006								
	-604	-74	948	18.6	0,005								
	-605	-75	893	17.8	0.004								
	909-	97-	892	20.2	0.004								
	-607	-77	1089	14.9	0,005								
	-608	-78	1069	15,2	90000								
	-609	-79	1084	14.5	0.010				724		•		
End of 176-C		-80	1478	17.2	0.033 CI		0.04	0.027	0.018	9.1	9,1	16.4	. 15

Uranium Analyses of Core Number: DC-28-C HRI No. 13455-1 through 25

	Density	ft ³ /ton															×		17.1	•	16.9	17.1	3.4	17.0		1.01	7.00	•
	Specific	Gravity									X			1					1.87		-1.89	1.87	2.16	•	1 76		1 2 2	
	%	Moisture											¥		¥				6.0		8.6	13,5	4.5	15.6	7.1		10.1	
	%	Organic	000	0.10	0.03	0.58	0.12	0.08	0.04	0.03	0	0	0.05	0.04	90.0	0.23	0.02	0.28	0.03	0.03	90.0	90.0	0.13	0.23	90.0	0.16		
	% (200	19.2	0.25	4.	•	5.83	0.30	0.05	3,82	1.52	0.36	0.09	0.30	0.50	•	3,53	8.80	10.7	6,09	0°0	1.30	12.1	6.19	0.13	0.08	0.05	
	% Radon	2807																	0	ິ	7 6	000	7	9	22	44	54	
	Sealed Gamma	rday.																	0.009		2000	770.0	0.122	0.240	0.049	0.018	0.013	F
	Gamma																		600.0	0.005							900.0	•
775.0	Beta- Equiv.				*						8			• •			1		0.008	0.005			.133		.042		. 1	
	Beta- Gamma		* *- ,							•		•					•		10.0>	<0.01				0.52		0.02		
	Fluori- metric	,	0.002	0.001	0.00	<0.001	100.0>		0.002	200.0	900		<0.001 0.001	00.00	100.00	100.07			0.00				0.138	0.380	0.024	0.014	0.014	
	Interval ft		470-471	471-472	473-474		475-476	76-477		478-479	479-480			785-1987				485-486								\$05-50 0	494-495	
	HRI Sub No.		, , , ,	7 6) A	S	ဖ	^		တ	10	: :	11	77	14	15		1 2	18	19	0		1 2		2 4			

Attac ent to Letter Mr. David Hertzke

Uranium Analyses of Core Number: DC-28-C HRI No. 13455-26 through 50

	Density	ft³/ton	19.1	19.4	20.7	16.2				¥							300							18,3	-	18.5	ת	
	Specific	Gravity	1.68	1,65	1.55	1.97		•			ş												;	1.75	1.87	1.73	# 0 •	
	%	Moisture	13.0	8.9	14.6	6.7				*												•		7.8	2.0	2 6	•	
	%	Organic	0.39	0.70	9.01	0.64	50.00		0.14	0.22	0.54	0 47	0.26	0.27	1.02	1.83	0.73	0.62	0.72	0.38	0.19	000	. 0.39	. 07.7	54.0	12.09	•	
	% (2	0.05	90.0	90.0	0.05	7	, 0	0.08	5.91	4.10	2.15	1.65	6.01	28.1	2.71	1.49	1.24	11.9	0.11	0.09		2 0	000	200	0.03		
	% Radon	SSOT	64	33	11	44	•	•													0		33		7 0	31	j.	•
	Sealed Gamma	rdaily.	0.011	0.018	0.036	600.0	600				ý					e E					0.009		810.0	200	0.00	0.037		•
	Gamma	. 440.62	0.004	0.012	0.032	0.005	0.009											141			0.009		0.012		0.00	0.033	•	
% U3Og	Beta-	• • • • • • • • • • • • • • • • • • • •	0	0	0.039	o.	0.005														0.009		0.011	-		0.047		
	Beta- Gamma		0.01	0.01	0.05	<0.01	<0.01		•												<0.01		<0.01	0.0	0.02	0.07		
	Fluori- metric		0.009	0.012	0.045	0.002	0.005	0.004	0.012	0.016	0.012	0.013	0.010	0.019	0.047	0.011	•	0.010	0.008	0.008	800.0	0.012	0.012	0.014	0.023	0.082		
	Interval		495-496	מפ	2 2	498-499	500-501	501-502	502-503	-50	504-505			8 9	208-209	509-510	510-511	-51	512-513	-51	-51		516-516.4	4	4	4		
	Sub No.		. 26	17	200	30	31	32		4. 1	3	36	37	8 6	n (40	41	42	43	4	45	46	47		6			

Attachment to Letter Mr. David Hertzke

Uranium Analyses of Core Number: DC-28-C HRI No. 13455-51 through 63

Ų	ic Density y ft³/ton	18.7					
	Specific Gravity	1.72				¥.	
	% Moisture	15.5					* 1
i i	% Organic	0.75	0.21	0.22	0.07	0.14 0.13	0.13 0.18 0.49
٠,	CO %	90.0	0.02	0.75	0.73	1.52 5.40 9.65	14.3 12.1 0.40
%	Radon		0				/ *
Sealed	Gamma Equiv.	*	0.012	*,			•
	Gamma Equiv.	2	0.012				
% U3O8	Beta- Equiv.		0.009				
	Beta- Gamma		<0.01				
	Fluori- metric	0.013	0.008	900.0	0.006	0.007	0.013
	Interval ft	519.4-520.4	521.4-521.4	522.4-523.4 523.4-524.4	524.4-525.4 525.4-526.4	526.4-527.4 527.4-528.4 528.4-529.4	529.4-530.4 530.4-531.4 531.4-532.4
HRI	Sub No.	51	23	54 55	56	58 59 60	61



MEMO TO: G.C. Dohm

FROM:

R.F. Lucht

DATE: June 28, 1977

SUBJECT: Anderson Equilibrium

The attached tables are a summary of all equilibrium data on the Anderson Project. As you can see, Hazen is very consistant on both cuttings work and core data. Their work averages 1.08 for 424 net samples. Chemical Geological averaged .81 for 335 net samples. The difference observed between the first 12 pages of five foot cuttings data and the last 24 pages of five foot data can be explained because these groupings are not statistically significant by themselves.

Any bias present in the Hazen data caused by the sampling technique must be insignificant. The 50 high $\boldsymbol{\mathcal{S}}$ samples sent in have been included. Inclusion of this data changed the Hazen average from 1.10 to 1.07. The cuttings data is unbiased and it agrees at 1.09.

The 21 samples submitted to Hazen from the pulps done by Chemical Geological indicate wide divergence between the labs. Like you, I am of the opinion that Hazen is probably the more accurate lab. Hazen has done a number of checks and they were always able to verify reported data. These 21 samples will be submitted to another lab for comparison.

At this time, 1.00 seems a reasonable number to apply to reserves for equilibrium. If the conflict between labs can be settled, it may be possible to apply a factor of 1.08 (if Hazen is upheld).

RFL/pb Attachment

SUMMARY OF EQUILIBRIUM DATA BY LABORATORY

<u>Grade</u>	<u>Laboratory</u>	Source Sample	Number Samples	Total Equilibrium	Average Equilibrium
.015030	Chem. Geo.	Core	149	109.04	.73
	Hazen	Core	115	122.44	1.07
	Hazen	Cuttings	153	163.89	1.08
	All Labs	All Samples	417	395.37	.95
.030050	Chem. Geo.	Core	77	64.67	.84
	Hazen	Core	59	58.51	1.00
	Hazen	Cuttings	38	42.07	1.11
	All Labs	All Samples	174	165.25	.95
.050090	Chem. Geo.	Core	56	44.43	.79
	Hazen	Core	20	23.59	1.18
	Hazen	Cuttings	10	11.66	1.16
	All Labs	All Samples	86	79.68	.93
.090 →	Chem. Geo.	Core	53	50.91	.96
	Hazen	Core	25	28.58	1.14
	Hazen	Cuttings	4	4.48	1.12
	All Labs	All Samples	82	83.97	1.03
All Grades	Hazen	All Samples	424	455.22	1.08
	Chem. Geo.	All Samples	335	269.05	.81
	All Labs	All Samples	759	724.27	.96

Hazen Equilibrium	Factor	, 54	. 11	. 79	1.12	.27	. 22	.50	. 75	2.09	.26	. 87	1.27	1,18	.77	.51	. 28	99°	, 46	98.	.39	•71
Chem. Geo. Equilibrium	Factor	.04		34	°70	.29	.30	.22	.37	2,45	.03	. 54	. 78	5.84	2.18	.55	.33	99.	.41	• 10	, 44	.36
, Inc.	B-	.01	.03	.01	.14	,01	.02	.02	.03	.15	.01	.12	60.	.09	.01	.04	.05	.05	.04	.01	.32	.03
Hazen Research, Inc	$e^{0.8}$.011	.034	.014	. 098	.061	.049	.024	.028	.057	.031	.116	.055	.065	.009	.053	.133	.047	.045	.025	.616	.035
Hazen R	N ₃₀₈	900.	,014	.011	.110	.017	.011	.012	.021	.119	.008	.101	.070	.077	.007	.027	.037	.031	.021	600.	.242	.025
Minerals	B- & **		.01		And the state of t		-	900.	.024	.162	.011	.061	.147	.041	.007	1	.028	.024	.030	.010	.190	.017
Geo.	eU ₃ 0 ₈	.024	.034	.023	.147	.057	.054	.036	.030	.062	.036	.116	960.	.019	.011	.055	.135	.065	.061	.054	.626	.045
Chem.	U ₃ 0 ₈	< .001	.016	.008	.103	.017	.016	.008	.011	.152	.001	.063	.075		.024	.030	.044	.043	.025	.010	.273	.016
10	Depth	26-96	66-86	123-124	296 1_297 1	637-638	631-633	400-401	406-407	407-408	408-409	441-442	445-446	446-447	41-42	301-302	113.5-114	385-386	387-388	458-459	473-474	392-393
	Hole #	AM 7C		AM 13C			AM 49C	AM 51C		51C*	51C	510	51C	510	790	1130	1	135C	AM 135C			AM 149C

* Chemical Geological did chemical twice: .057% + .152% ** Missing Values due to poor quality copy.

Points of poor agreement between old and new data.



MEMO TO: G.C. Dohm, Jr.

DATE:

February 9, 1978

FROM:

R.F. Lucht

SUBJECT:

Anderson Equilibrium Preliminary

Numbers are in using a polygon model for determining pounds U₃0₈ by assay data and gamma log data. Maps have been made at .03% and .05% cutoffs. The area south of the red dashed line on the .05% cutoff could probably be averaged to yield one number. I am not certain whether this is the best way or not. Holes 51C, 396C and 412C can be averaged for another area. The "west pit" area can be averaged and the area hashered on the .03% map can be averaged. Areas not in any of the above are mostly in the tailings dam. They are very variable and present a problem.

A comparison of the two maps shows that, while individual holes become grade dependent (using this method), the overall map does not change much. The "west pit" seems to be an exception, possibly a .05 cutoff with a higher equilibrium factor would be more appropriate over there. The fact that the data is not overall grade dependent lends support to the validity of the numbers.

RFL/p

Attachments

Hole #	# Poun	ds U308	Equilibrium
	By Gamma	By Chemical	Factor
AM 1C	145,681	174,606	1.198
AM 2C	329,481	271,563	.824
AM 7C	282,302	308,112	1.091
AM 10C	247,583	270,369	1.092
AM 13C	73,693	19,031	.258
AM 16C	453,341	355,937	.785
AM 17C	188,665	145,808	.773
AM 18C	153,936	174,014	1.131
AM 22C	128,415	104,221	.811
AM 26C	424,253	519,131	1.224
AM 28C	30,987	45,072	1.454
AM 40C	78,613	24,803	.315
AM 49C	682,340	540,506	.792
AM 51C	1,016,323	1,037,427	1.021
AM 63C	302,900	317,449	1.048
AM 68C	340,524	281,227	.826
AM 71C	283,359	233,810	.826
AM 79C	34,474	29,429	.854
AM 88C	-	-	-
AM 106C	179,516	134,036	.747
AM 107C	108,837	121,571	1.117
AM 113C	133,282	97,756	.733
AM 119C	182,778	222,618	1.218
AM 127C	54,494**	8,278**	.152
AM 129C	343,150	320,183	.933
AM 135C	471,548	313,907	.666
AM 136C	546,590	431,799	.790
AM 149C	171,355	113,227	.661
AM 152C1	171,942	19,349	.113
AM 156C	399,406	290,712	.728
AM 171C	178,195	172,372	.967
AM 184C	-	-	-
AM 222C	254,583	199,538	.784
AM 229C	237,316**	318,123**	1.341
AM 244C	32,161*	17,657*	.549
AM 254C AM 258C AM 273C AM 274C AM 275C	296,555** 169,046 85,131 125,370 299,377	29,554** 133,700 107,707 20,680 409,103	.0997 .791 1.265 .165 1.367

Hole #	# Poun	ds U308	Equilibrium
	By Gamma	By Chemical	Factor
AM 281C	215,294	84,959	.395
AM 286C	117,407	93,096	.793
AM 289C	183,710	132,948	.724
AM 308C	35,640	15,888	.446
AM 323C	351,434	311,598	.887
AM 325C AM 336C AM 337C AM 338C AM 338C1	827,827 140,085 29,074 118,557	1,049,629 42,885 21,032 83,642	1.267 .299 .723 .705
AM 345C	255,650	409,468	1.602
AM 351C	103,369	85,157	.824
AM 371C	729,943	582,399	.798
AM 373C	61,153	57,787	.945
AM 384C	179,654	224,567	1.250
AM 388C	351,933	386,320	1.098
AM 390C	69,524	18,356	.264
AM 396C	309,071	584,672	1.892
AM 412C	443,690	573,999	1.294
AM 419C	605,604	497,696	.822
AM 422C	251,007*	423,095*	1.686
AM 427C	750,239	546,949	.729
AM 431C	-	-	-
AM 434C	29,084	41,281	1.419
AM 435C	124,755	133,914	1.074
AM 436C AM 443C AM 444C AM 486C	80,725 294,814 - -	48,650 272,513 - -	.603 .924 -

^{*} No reserves at .03% cutoff, used reserves at .02% cutoff. ** Used at .01% cutoff.

Hole #	# Pound By Gamma	ls U308 By Chemical	Equilibrium Factor
AM 1C AM 2C AM 7C AM 10C AM 13C	110,211 317,705 215,625 216,975 61,141	140,191 240,322 283,915 259,826	1.272 .756 1.317 1.197
AM 16C AM 17C AM 18C AM 22C AM 26C	383,565 77,795 124,451 93,519 334,774	282,935 95,031 146,339 88,467 414,611	.738 1.222 1.176 .950 1.238
AM 28C AM 40C AM 49C AM 51C AM 63C	59,275 469,588 822,076 279,091	35,494 24,803 371,837 980,352 292,318	- .418 .792 1.193 1.047
AM 68C AM 71C AM 79C AM 88C AM 106C	- 114,582 - - 135,480	267,203 149,680 - 34,635 103,715	- 1.306 - - .766
AM 107C AM 113C AM 119C AM 127C AM 129C	82,649 84,526 147,500 - 272,673	58,863 82,566 195,551 - 274,249	.712 .977 1.326 - 1.006
AM 135C AM 136C AM 149C AM 152C1 AM 156C	432,138 520,114 105,356 171,942 323,205	292,216 387,198 64,990 - 298,666	.676 .744 .617 -
AM 171C AM 184C AM 222C AM 229C AM 244C	32,611 200,482 202,978	111,226 354,493 162,841 156,510	3.411 1.768 .802
AM 254C AM 258C AM 273C AM 274C AM 275C	278,212 111,746 43,036 91,335 279,509	106,038 73,373 409,103	- .949 1.705 - 1.464

	# Pound	ls U308	Equilibrium
Hole #	By Gamma	By Chamical	Factor
AM 281C	135,162	58,570	.433
AM 286C	71,156	71,452	1.004
AM 289C	110,534	64,386	.583
AM 308C	-	-	-
AM 323C	337,592	311,598	.923
AM 325C AM 336C AM 337C AM 338C AM 338C1	827,827 121,255 19,589 100,565	49,629 35,021 11,753 76,445	.060 .289 .600 .760
AM 345C	190,135	401,397	2.111
AM 351C	25,596	68,913	2.692
AM 371C	701,173	582,399	.831
AM 373C	49,184	44,322	.901
AM 384C	150,026	202,865	1.352
AM 388C	277,641	323,702	1.166
AM 390C	69,524	18,356	.264
AM 396C	294,609	584,672	1.985
AM 412C	432,004	557,002	1.289
AM 419C	469,618	417,867	.890
AM 422C	60,286	105,774	1.755
AM 427C	551,098	520,673	.945
AM 431C	71,538	90,019	1.258
AM 434C	-	-	-
AM 435C	80,854	82,749	1.023
AM 436C	72,975	42,192	.578
AM 443C	227,466	193,123	.849
AM 444C	232,351	421,912	1.816
AM 486C	209,294	348,823	1.667

ANDERSON TOTAL RESOURCE

15, 055 885 # U308 CHEM 16 296 745 # U308 8

(924)

. 03 CUTOFF

Memorandum Union Oil Company of California

MEMO TO:

C.Z. Hill

DATE:

February 16, 1978

FROM:

R.F. Lucht

SUBJECT:

Correlation of Equilibrium

Factors to Other Parameters

at the Anderson Mine

The following observations have been made by me on this date.

They are not meant to be totally complete or even totally accurate.

They seem to exist to me. Look them over and comment. Maybe you can see additional correlations or reasons for these.

RFL/p Attachments

TO OTHER PARAMETERS AT THE ANDERSON MINE

- Thick basalt caps <u>seem</u> to correlate to small relative lows in equilibrium, i.e. AM-156C, AM-43, AM-419C, AM-135, AM-374 and AM-417.
- 2. Major fault in east side of property correlates very roughly to lows in equilibrium. AM-351C, AM-427C and AM-106C support this, but AM-107C, AM-119C and AM-275C do not. AM-119C is located near where fault dies out. AM-107 is a local high, possibly water movement along fault left some uranium enriched and some depleted.
- 3. <u>Major lows</u> in equilibrium are located <u>along outcrop line</u>. (AM-152C, AM-390C, AM-308C, AM-40C, AM-274C, AM-254C, AM-13C and AM-244C, etc.)

 There are exceptions along faults (local highs near outcrop near faults), AM-396C and AM-275C.
- 4. Total thickness of carbonaceous siltstone does not correlate to equilibrium in general. However, outside the O' countour on the isopach is an area of very low equilibrium, except AM-229C and core holes west of 83,500 East.
- 5. No correlation between thickness of overburden and equilibrium. Some of the highest equilibrium factors are in shallow ore and some of lowest equilibrium factors are deeply buried.

- 6. Local elevation highs on top of ore correspond to local relative highs in equilibrium factors, i.e. AM-28C, AM-289C, AM-229C, AM-351C AM-71C, AM-184C and AM-431C.
- 7. A relative high on grade thickness in the west central part of the property correlates to a low in equilibrium. A high in GT in the east central part correlates to a strong low in equilibrium at AM-336C. This same high also covers a low at AM-351C.

RFL/p c: GCD, file

PRELIMINARY DISEQUILIBRIUM STUDY FOR THE ANDERSON MINE SEPTEMBER, 1976

By

T. S. Hellinger

Plates prepared by

J. R. Ljung

T. S. Hellinger

INTRODUCTION

The coring program at the Anderson Mine was initiated to resolve the relationship between the recorded subsurface gamma ray mineralization (eU308) and the actual chemical uranium content (cU308). Core hole locations were chosen from pre-existing drill holes which exhibited favorable gamma mineralization. These drill holes were offset approximately five feet and the anomalous zones were cored. To date, 15 core holes have been completed, with 14 core holes containing significant equivalent (eU308) and chemical (cU308) uranium mineralization.

Two Reid Drilling Company and one Universal Drilling Company rotary rigs were contracted to pull 925 feet of core, of which 94-95% was recovered. Various size core bits and core barrels were tried with the best recovery attained by Russel Sharpe of Reid Drilling Company using a three inch diameter core barrel set up. The core from each core run (usually ten feet) was carefully measured, labeled and boxed. The core was next described by a geologist using a 10X to 45X binocular scope, and finally shipped to the Casper office.

Upon receipt of the cores in Casper, they were split longitudinally and half of the core was dried and pulverized. Pulverized core, representing one-half or one foot intervals, was analyzed on the Blake Beta-Gamma scaler. Each interval was analyzed three times and an average was taken. Initially all samples with an average indicated analysis greater than .02% eU308 were sent to Chemical and Geological Laboratories in Casper for chemical and

closed-can analyses. Subsequently, selected samples with an average beta-gamma analysis less than .02% U308 were sent out for chemical and closed-can analyses to fill in gaps in the assay intervals and to better delineate the ore zones (Table 1). A total of 448 core samples have been analyzed to date. In addition, 21 previously analyzed core samples, representing various grades of the mineralized lithologic units, were sent to Skyline Labs, Inc. in Wheat Ridge, Colorado for fluorimetric and closed-can uranium, chemical vanadium and spectrographic analyses (Table 4). Spectographic analyses were run to ascertain the presence of any element other than uranium which might constitute ore, or at least require consideration for secondary recovery during milling of the uranium ore (see Summary of Emission Spec. Results). Periodic cross check analyses were run on random samples throughout this study to verify the reproducibility of all the analyses.

DISEQUILIBRIUM AND CHEMICAL ASSAY RESULTS

Before a summary of the chemical analyses could be made and a subsequent disequilibrium factor computed, adjustments had to be made between the core assay footages and the digitized gamma log footage for each core hole. This adjustment was accomplished for each core hole by determining the best correlation between the closed-can gamma uranium assays and the digitized gamma log data. Plates 19 thru 33 graphically depict the relationship between eU308 and cU308. Only cored intervals with at least 2 feet of .03% eU308 from the gamma log, were considered in this disequilibrium study. The intervals in each core hole which met or exceeded

this cutoff have been summarized in Table 2 along with all other analyses of the respective interval. A weighted average for each core was computed for eU₃08, cU₃08, V₂05, CO₂, and total sulfur by dividing the total thickness of all the intervals into the respective total grade thickness (Table 2). Disequilibrium was then computed for each hole by dividing the weighted average cU₃08 by the weighted average eU₃08.

Two methods were used to determine the uranium disequilibrium for the Anderson Mine property. The first method involved totaling the weighted eU308 and cU308 (Table 3), and then dividing the total cU308 by the total eU308:

Total wt. cU₃08 = disequilibrium factor

Total wt. eU₃08 = .89

The first method yielded a disequilibrium factor of .89. The

second method simply entailed dividing the total mineralized thickness into the total weighted disequilibrium for all of the core

holes:

Total wt. disequilibrium = diseq. factor = .88

Total thickness = 201 ft.

This second method produced a disequilibrium factor of 0.88. The vanadium-uranium ratio (V2O5:cU3O8) of 1.39 was obtained by ratioing the appropriate weighted grade averages (Table 3). Average total CO2 and sulfur were determined by dividing the total thickness (160 ft.) into the total weighted analyses of each. The average weighted grades for CO2 and total sulfur were 6.38 wt. % and 0.57 wt. % respectively (Table 3).

SUMMARY OF EMISSION SPECTROGRAPH RESULTS

A rapid spectrographic scan of 21 uraniferous core samples was completed by Skyline Labs, Inc., Wheat Ridge, Colorado. The samples were selected to represent a cross section of the ore grades and mineralized lithologic units, recognized at the Anderson Mine. The spectrographic scan was run primarily for three reasons:

- 1. Identify elements other than uranium that might warrant consideration for secondary recovery during milling (i.e. V205).
- 2. Evaluate the concentration of those elements which might create milling problems (i.e. Mo).
- 3. Aid in geochemical exploration for similar uranium deposits in the Basin and Range area.

Before detailed evaluation of the data is made it should be pointed out that there were not enough samples analyzed to determine reasonable background values for all lithologic units. Therefore, average background values as tabulated by Turikian and Wedipohl (1961) were used when applicable.

The emission spectrographic scan provided semi-quantitative analysis of 31 elements. Elements which displayed the most interesting anomalies in at least one lithologic unit were: V, Mo, As, Co, Mn, and Sc (Table 4). Vanadium was the most pervasive anomally, present in all the mineralized units. Quantitative analyses (Table 1) indicate a high enough concentration of vanadium to at least warrant consideration for secondary recovery. The next most important anomalous element is molybdenum. Molybdenum was anomalous in seven

samples, with significant concentration (50 ppm to 300 ppm) in three samples (Table 4). The molybdenum appears to represent rare isolated accumulations within the carbonaceous marls. However, because molybdenum can adversely affect milling of the uranium if an acid leach is used, further molybdenum analyses should be initiated to determine the actual concentration and distribution. The remaining elements; As, Cr, Mn, and Sc are of only minor importance as anomalous trace elements. None of these elements are concentrated enough to warrant secondary recovery or pervasive enough to be used as a pathfinder for uranium mineralization in other areas. However, the overall effects of these trace element concentrations with respect to milling is presently unknown. The lithologic unit with the most trace element anomalies is the sandstone (Table 4).

RECOMMENDATIONS

The disequilibrium factor and the weighted grade averages computed from the 14 mineralized cores are good first approximations. However, the rather complex lithology requires a greater detailed and more comprehensive coring program so that a better statistical evaluation for each mineralized unit can be made. Several units were not cored as frequently as they probably should be in the future. Disequilibrium for each mineralized lithologic unit has also not been computed due to the unequal distribution of the lithologic units cored. Our past experience in other areas indicates that the disequilibrium factor will probably improve as more coring is completed. More coring should provide a better statistical

sampling of the area. Presently the disequilibrium factor neglects values with eU₃08 below the cutoff which also has correspondingly high cU₃08 (Example: Am-17c; 201 ft. - 202 ft., .076% cU₃08 vs. .011% eU₃08). Ranges of concentration for various elements via emission spectrograph should be determined for each lithologic unit. This may prove to be vital information for mill recovery. More quantitative work should be undertaken to better understand the concentration of at least U₃08, V₂05, CO₂, and Mo with respect to specific lithologies and areal distribution.

REFERENCES CITED:

Turekian, K. K. and Wedepohl, K. H., 1961, Distribution of the elements in some major units of the Earth's crust: G.S.A. Bull., v. 72, no. 2, pp. 175-191.

i			•				
-	Core Depth ft. 60.5-61 63-64 64.0-64.5 64.5-65	U ₃ 08 % by wt. 0.056 0.003 0.008 0.021 0.029	eU ₃ 08* % by wt. 0.071 0.010 0.023 0.015 0.037	V205 % by wt. 0.076 0.034 0.021 0.036 0.044	CO ₂ % by wt.	Total sulfur(s) % by wt.	Lithology sltstn. " calc.ls. & sltstns.
	65.5-66 66.5-67 67.5-68 67.5-68 68.5-69 94.5-95 95.5-96 96.5-97 97.5-98	0.017 0.019 0.102 0.021 0.051 0.012 0.020 0.004 0.084 0.031 0.054 0.043 0.005 0.015	0.013 0.024 0.109 0.018 0.043 0.021 0.025 0.002 0.084 0.118 0.077 0.022 0.011 0.056	0.043 0.025 0.061 0.020 0.030 0.009 0.014 0.029 0.025 0.037 0.068 0.008 0.005 0.021			sltstn. lignite " sltstn sltstn sltstn mdstn.
	98-98.5 98.5-99 99-99.5 99.5-100 100-100.5 101-101.5 101.5-100 103.5-100 104-104.5	0.121 0.012 0.009 4 0.016 5 0.098	0.011 0.014 0.054 0.075 0.170 0.121 0.038 0.015 0.030 0.096 0.028	0.005 0.020 0.021 0.036 0.133 0.110 0.050 0.049 0.125 0.168 0.023			sltstr " " sltstr " " ligni

^{*}Closed can gamma only assay for eU308.

Table 1. Summary of core analyses from the Anderson Mine Property, September, 1976.

					_
Core					Total
Depth	V308	eU308 *	V205	CO2	sulfur(s)
ft.	% by wt.	% by wt.	% by wt.	% by wt.	% by wt. Lithology
105-105.5	0.028	0.041	0.062	-	- lignite
105.5-106	0.051	0.049	0.169	, -	- mdstn & slts
106-106.5	0.015	0.020	0.026		- " "
	0.013	0.021	0.020	'	
106.5-107	0.008	0.025	0.009	_	- 11 11
109-109.5	0.000	0.021	0.026	· -	_ ";" "
109.5-110	0.023	0.033	0.025		_ 11 11
110-110.5	0.028	0.026	0.026	-	_ 11 11
110.5-111	0.028	0.044	0.071		_ 11 11
111-111.5	0.040	0.036	0.039	-	lignite
111.5-112	0.029	0.113	0.035	-	
112-112.5	0.106	0.110	0.041	_	п п
112.5-113	0.048	0.021	0.034	_	"
113-113.5	0.016	0.021	0.088	_	- sltstn
113.5-114	0.017	0.067	0.053	_	_ "
114-114.5	0.008		0.110	_	_ "
114.5-115	0.152	0.100	0.028		
115-115.5	0.129	0.117			_ "
115.5-116	0.060	0.078	0.020		
116-117	0.002	0.020	0.020		

*Closed can gamma only assay for eU308.

Table 1. (Continued)

AM - 7C Cored Intervals 15'-25'; 95'-118'

		•	*
Core Depth ft.	U308 eU308* % by wt. % by wt.	V ₂ O ₅ CO ₂ % by wt. % by wt.	Total sulfur(s) % by wt. Lithology
17-18 18-19 19-20 20-21 21-22 95-96 96-97 97-98 98-99 99-100 100-101 102-103 103-104 104-105	0.009 0.018 0.179 0.198 0.316 0.321 0.045 0.049 0.003 0.010 0.001 0.024 0.009 0.020 0.016 0.034 0.011 0.029 0.016 0.034 0.001 0.026 0.007 0.026 0.001 0.017 0.001 0.019	0.128 0.32 0.198 0.06 0.162 0 0.111 0 0.052 0.01 0.012 0 0.018 - 0.018 0 0.015 0 0.015 0 0.012 0 0.015 0 0.012 0	0.25 mdstn 0.26 " 0.33 mdstn-sltstn 0.30 " 0.29 " 0.29 mdstn 0.31 " 0.30 " 0.26 sltstn 0.19 " 0.03 sltstn
105-106 106-107	0.010 0.017 0.005 0.019		

*Closed can gamma only assay for eU308

		•				•
Core Depth ft.	U308 % by wt.	eU308* % by wt.	V ₂ 05 % by wt.	CO ₂ % by wt.	Total sulfur(s) % by wt.	Lithology
115-116 116-117 117-118 118-119 119-120 120-21 121-122 122-123 123-124 124-125 125-126 126-127 127-128 128-129 129-130 130-131 131-132 132-133 131-132 132-133 134-135 135-136 136-137 137-138 138-139 139-140 140-141	0.013 0.006 0.005 0.004 0.003 0.004 0.007 0.012 0.008 0.012 0.008 0.012 0.008 0.012 0.008 0.012 0.001 0.022 0.001 0.022 0.005 0.011 0.024 0.023 0.005 0.013	0.021 0.008 0.006 0.007 0.024 0.008 0.014 0.018 0.023 0.019 0.019 0.053 0.025 0.027 0.007 0.012 0.038 0.033 0.010 0.030 0.031 0.028 0.031 0.006 0.015	0.012 0.008 0.005 0.010 0.017 0.018 0.019 0.020 0.021 0.023 0.026 0.029 0.056 0.004 0.006 0.071 0.062 0.059 0.059 0.059 0.059 0.059	24.67 62 6.87 6.20 10.49 8.20 15.95 14.23 11.48 11.40 26.22 7.16 3.18 13.44 14.11 14.77 2.67 9.67 9.63 26.44 18.31	0.01 0.01 0.01 0.01 0.01 0.02 0.01 0.01 0.01	silty ls ss " " silty ls, cher silty ls " " " " " " " " " " " " " " " " " " "
			and the second second			

*Closed can gamma only assay for eU308.

AM - 16C Cored Interval 240'-335'

Core		•			Total	
	ΠοOo	0II-00 X	T 0	CO		*4
Depth	Ju ₃ 08	eu308*	V205	C02	sulfur(s)	T ! ! ! - 7
ft.	% by wt.	% by wt.	% by wt.	% by wt.	% by wt.	Lithology
olif r olir	0.003	0.014	0.067			0 waste
246.5-247	0.003			-	-	ss & mdstn
247-247.5	0.007	0.078	0.168	-		mdstn
247.5-248	0.014	0.058	0.048	-	-	
248-248.5	0.055	0.051	0.107	-		
248.5-249	0.078	0.103	0.099	-	-	11
249-249.5	0.425	0.444	0.257	-	-	mdstn & lignite
249.5-250	0.476	0.285	0.169	-	-	mdstn
250-250.5	0.447	0.416	0.159	_	-	ıı ;
250.5-251	0.181	0.122	0.278	_		mdstn & lignite
251-251.5	0.015	0.028	0.098	-	-	, "
251.5-252	0.003	0.008	0.115	-	-	sltstn
267.5-268	0.001	0.012	0.062	-	-	mdstn
268-268.5	0.004	0.014	0.030	-	-	n a
268.5-269	0.141	0.150	0.109		-	lignite
269-269.5	0.125	0.102	0.071		_	mdstn
269.5-270	0.046	0.061	0.070	-	-	
270-270.5	0.009	0.022	0.064	_	-	
270.5-271	0.005	0.021	0.089	_		
287.5-288	0.017	0.022	0.033	THE	ala da pala da da	및 보고수 교육 # 1. ~ 11일 (12)
288-288.5	0.062	0.048	0.015			mdstn '
288.5-289	0.033	0.053	0.031			n in
289-289.5	0.005	0.020	0.050	-		n .
207 207.7	0.00	0.020	0.000	and the second second		

Table 1. (Continued)

^{*}Closed can gamma only assay for eU308.

					* •	*
Core					Total	*
	JU308	eU308*	V ₂ 05	C02	sulfur(s)	
Depth	d by wt	% by wt.	% by wt.	% by wt.	% by wt.	Lithology
ft.	% by wt.	Dy WO.	70 D, Y WO.	70 5,7 110	<u> </u>	
	0.000	0.015	0.164			sltstn
292.5-293	0.007	0.015			_	11
293-293.5	0.009	0.015	0.112	~		aala mdata
293.5-294	0.004	0.014	0.082		-	calc. mdstn
294-294.5	0.060	0.045	0.102	-		mdstn
294.5-295	0.074	0.066	0.151	-		lignite & mdst
295-295.5	0.079	0.081	0.045		-	lignite
295.5-296	0.027	0.075	0.023	-	- '	u
295-206 5	0.060	0.090	0.179		-	. 11
296-296.5	0.067	0.095	0.049	-	-	11
296.5-297	0.007		0.265	-	-	11
297-297.5	0.045	0.077		-	_	mdstn ·
297.5-298	0.021	0.028	0.045		_	sltstn
298-298.5	0.027	0.035	0.023	-		SICSCII
298.5-299	0.045	0.050	0.034		-	Timber 0 maat
299-299.5	0.059	0.050	0.052		-	lignite & mdst
299.5-300	0.042	0.051	0.102	-		
300-300.5	0.034	0.037	0.062		-	lignitic sltst
300.5-301	0.025	0.025	0.031			lignitic sltst
301-301.5	0.233	0.218	0.218	-		lignite
301.5-302	0.125	0.141	0.134			lignite & mdst
302-302.5	0.022	0.025	0.023			calc mdstn
202 5 202	0.012	0.013	0.018			
302.5-303		0.014	0.015		-	и и
303-303.5	0.013	0.014	0.012		_	11 11
303.5-304	0.018	0.022				lignite
304.5-305	0.019	0.040	0.071			TIBILIO
305-305.5	0.071	0.054	0.054			
305.5-306	0.027	0.035	0.015			mdstn
306-306.5	0.038	0.038	0.018	•		
306.6-307	0.043	0.044	0.018			lignite
307-307.5	0.044	0.051	0.024	-	- 11 - 12 - 12 - 12 - 12 - 12 - 12 - 12	
307.5-308	0.035	0.050	0.036		-	
308-308.5	0.052	0.065	0.095			
308 5-300	0.013	0.011	0.018			mdstn
308.5-309	0.015	0.020	0.035			
309-309.5	0.015	0.014	0.033			
309.5-310	0.016			<u> </u>		
310-310.5	0.050	0.036	0.045		1000년	ø
310.5-311	0.039	0.045	0.033		사람이 집안된	u u
311-311.5	0.039	0.037	0.030			
311.5-312	0.038	0.031	0.042			11
312-312.5	0.012	0.011	0.052			

^{*}Closed can gamma only assay for eU308.

AM - 17C Cored Interval 100'-215'

÷						
Core Depth ft.	5 ^U 3 ^O 8 % by wt.	eU308* % by wt.	V205 % by wt.	CO2 % by wt.	Total sulfur(s) % by wt.	Lithology
			0.021	11.52	0.07	sltstn & Rs
104-105	0.009 0.004	0.017 0.014	0.070	0.40	0.02	sltstn
105-106 106-107	0.004	0.010	0.034	0.35	0.02	11
107-108	0.010	0.017	0.040	0.01	0.01	11
130-131	0.008	0.011	0.039	-	-	mdstn
131-132	0.040	0.037	0.046	0	0.02	11
132-133	0.012	0.007	0.034	0.07	0.02	11
133-134	0.030	0.026	0.035	11.49	0.02	. 11
134-135	0.008	0.013	0.016	-		
135-136	0.007	0.010	0.008	0.07	0.01	11
136-137	0.028	0.037	0.018	0.01		II.
137-138	0.006	0.008 0.025	0.015	0	0.01	
138-139	0.017	0.020	0.021	ŏ	0.02	u
139-140 140-141	0.009	0.013	0.061	Ö	0.02	sltstn
141-142	0.009	0.012	0.124	0	0.03	
143-144	0.003	0.010	0.098	0	0.02	H A
144-145	0.010	0.021	0.077	0	0.02	sltstn & mds
146-147	0.011	0.024	0.249	0	0.01	sltstn
147-148	0.023	0.022	0.159	0	0.02	
148-149	0.024	0.028	0.068	0	0.01	mdstn
149-150	0.039	0.039	0.092	0	0.01	mdstn
150-151	0.004	0.013	0.080	0	0.02	II .
154-155	0.009	0.013	0.102	0	0.01	п
162-163	0.004	0.002	0.205	0	0.01	mdstn
163-164	0.022 0.004	0.036	0.031	_		u
164-165 165-166	0.024	0.023	0.146	0	0.01	
166-167	0.005	0.005	0.026		• • • • • • • • • • • • • • • • • • •	
192-193	0.012	0.011	0,039		- i	
193-194	0.0I7	0.020	0.130	0	0.04	mdstn
199-200	0.076	0.090	0.133	0	0.21	
200-201	0.012	0.021	0.156	0	0.03	sltstn
202-203	0.003	0.008	0.049	0_	0.01	mdstn
203-204	0.059	0.064	0.159	0.15	0.04	ir .
204-205	0.059	0.068	0.127	0	0.01	mdstn & slts
205-206	0.001	0.011	0.076	•	0.02	
198-199	0.003	0.007	0.079		-	mdstn

^{*}Closed can gamma only assay for eU308.

AM - 18C Cored Interval 270'-320'

Core Depth ft.	U308 % by wt.	eU308*	V205 % by wt.	CO ₂ % by wt.	Total sulfur(s) % by wt.	Lithology
278-279 279-280 280-281 281-282 282-283 283-284 284-285 285-286 286-287 288-289 289-290 290-291 291-292 293-294 294-295 296-297 297-298 296-297 297-298 298-299 299-300 312-313 313-314 314-315	0.007 0.055 0.007 0.095 0.250 0.042 0.042 0.019 0.062 0.120 0.038 0.005 0.007 0.059 0.059 0.013 0.058 0.023 0.012 0.014 0.029 0.007	0.011 0.063 0.005 0.115 0.161 0.035 0.032 0.025 0.030 0.077 0.148 0.040 0.005 0.001 0.058 0.030 0.147 0.059 0.022 0.008 0.022 0.006	0.021 0.181 0.003 0.205 0.051 0.015 0.015 0.009 0.241 0.135 0.303 0.024 0.018 0.036 0.062 0.161 0.003 0.003 0.025 0.042 0.049	23.12 22.82 16.62 22.23 22.08 21.56 8.64 0.74 3.77 6.94 	0.56 0.73 1.00 0.88 0.84 0.77 0.75 0.50 0.62 0.75 - 0.89 0.86 0.52 0.44 0.87 - 0.63	silty ls """" """" lignite lignite & sltst sltstn & mdstn """ """ slstn & lignite "" marl & lignite "" sltstn """

*Closed can gamma only assay for eU308.

AM - 26c Cored Intervals 595'-649';705'-755'

Core Depth ft.	U308 % by wt.	eU308* % by wt.	V ₂ 05 % by wt.	CO2 % by wt.	Total sulfur(s % by wt.	
601-602 602-603 603-604 604-605 605-606 606-607 607-608 619-620 620-621	0.008 0.024 0.032 0.024 0.020 0.047 0.011 0.002 0.011	0.011 0.029 0.027 0.025 0.016 0.061 0.014 0.003 0.021	0.005 0.302 0.072 0.226 0.058 0.311 0.021 0.007 0.013	8.24 3.72 0.03 0.01 0.01 8.68	0.67 0.62 0.57 0.55 0.45 0.58	mdstn & sltst: slstn & lignite "lignite " lignite & sltst: " " lignite, sltstn
622-623 623-624 624-625 625-626 626-627 627-628 628-629 629-630 631-632 631-632 632-633 634-635 635-636	0.012 0.009 0.007 0.043 0.020 0.010 0.006 0.014 0.034 0.034 0.008 0.008 0.106 0.121 0.248	0.018 0.010 0.019 0.048 0.033 0.010 0.010 0.026 0.040 0.070 0.006 0.014 0.108 0.170	0.076 0.045 0.009 0.003 0.007 0.008 0.010 0.016 0.017 0.009 0.026 0.008 0.008 0.003	0.72 4.95 9.90 15.88 15.36 - 9.16 6.79 22.01 - 36.93 27.99 26.00	0.41 1.57 1.07 0.27 0.32 - 0.70 0.53 0.18 - 0.25 0.12 0.62	& mdstn lignitic sltstn sltstn silty ls lignitic sltstn """""""""""""""""""""""""""""""""""
637-638 638-639 639-640 640-641 718-719	0.017 0.012 0.052 0.008 0.004	0.057 0.018 0.048 0.015 0.005	0.001 0.010 0.010 0.010 0.012	29.91 27.32 18.09	0.27 0.09 0.50	ls % sltstn sltstn & mdstn

^{*}Closed can gamma only assay for eU308.

AM - 26C (Con't)

Core					Total	
Depth	JU308	,eu308 *	V205		sulfur(s)	4
ft.	% by wt.	% by wt.	% by wt.	% by wt. 9	by wt.	Lithology
719-720	0.008	0.019	0.015	-	***	mdstn
720-721	0.345	0.292	0.026	0.07	0.67	SS
721-721.3	0.067	0.081	0.071	0.71	0.08	11
722.5-723	0.007	0.009	0.071	0.17	0.00	11
723-724	0.022	0.038	0.054	0.68	0	ss & mdstn
725-726	0.006	0.012	0.013	-	2	sltstn
726-727	0.003	0.002	0.010		-	S S
733-734	0.003	0.003	0.010	_		. sltstn
734-735	0.007	0.016	0.018	- '	_	11 01 011
735-736 '	0.008	0.008	0.016		- 3	ignitic mdst
736-737	0.007	0.011	0.016	-	-	11 11
738-739	0.004	0.009	0.015	 ,	-	sltstn
740-741	0.003	0.002	0.008	-		marl
741-742	0.001	0.003	0.008		_ '1	. II
743-744	0.003	0.007	0.029	-	-	mdstn
737-738	0.034	0.037	0.086	0.09	1.74	11
739-740	0.045	0.029	0.089	30.06	0.19	slstn & mar
742-743	0.030	0.022	0.201	8.35		mdstn & lign:

Table 1. (Continued)

^{*}Closed can gamma only assay for eU308.

AM - 49 C Cored Interval 606'-650'

		,				
Core Depth ft.	U308 % by wt. 0.007	eU308* % by wt.	V ₂ 05 % by wt.	CO2 % by wt.	Total sulfur(s % by wt.) Lithology mdstn
610-611 611-612 612-613 613-614 614-615 615-616 616-617	0.020 0.010 0.034 0.008 0.033 0.058 0.061	0.019 0.017 0.034 0.027 0.054 0.051 0.058	0.076 0.079 0.120 0.155 0.005 0.039 0.026	0.01 1.99 30.72 26.51 25.33	- 0.32 0.36 0.05 0.01 0.04	chert mdstn&cherty : ls "
617-618 618-619 619-620 620-621 621-622 622-623 624-625	0.077 0.040 	0.091 0.051 0.030 0.036 0.026 0.020 0.024	0.026 0.048 0.042 0.196 0.014 0.007	25.63 6.65 5.98 0.22 11.89 33.60 2.73	0.01	ls&lignitic m lignite & mds mdstn mdstn & ls ls mdstn
625-626 629-630 630-631 631-632 632-633 633-634 634-635 635-636	0.019 0.004 0.019 0.114 0.016 0.020 0.013 0.011	0.025 0.008 0.027 0.089 0.054 0.027 0.019 0.024	0.014 0.021 0.053 0.336 0.039 0.049 0.046 0.146	0.06 0.09 0.22 0.65 0.99 9.01	0.63 0.73 1.38 0.94 1.19	lignitic mds lignite " mdstn lignite ls &
636-637 637-638	0.078 0.012	0.046 0.024	0.089 0.064	2.29 2.51	2.07 1.40	sltstn mdstn lignite & mds

Table 1. (Continued)

^{*}Closed can gamma only assay for eU308.

AM - 51C Cored Interval 377'-418';430-475'

	Core Depth ft.	U308 % by wt.	eU308* % by wt.	V205 % by wt.	CO2 % by wt.	Total sulfur(s) % by wt.	Lithology
	394-395 396-396 396-397 396-398 397-398 398-401 401-402 403-404 405-406 406-407 408-410 411-412 412-413 439-441 441-443 444-445 445-463 461-46	0.001 0.004 0.040 0.013 0.021 0.008 0.009 0.005 0.012 0.023 0.011 0.011 0.05 0.001 0.005 0.001 0.007 0.001 0.004 0.227 0.063 0.020 0.011 0.024 0.075 0.111 0.001 0.008 0.007 0.011 0.259 0.263 0.063 0.002	0.017 0.016 0.036 0.020 0.024 0.023 0.036 0.035 0.025 0.025 0.025 0.031 0.030 0.062 0.036 0.017 0.036 0.017 0.026 0.011 0.028 0.026 0.019 0.023	0.035 0.038 0.064 0.016 0.013 0.013 0.012 0.025 0.020 0.025	0 0 0 0 0.02 0.04 0.02 0.04 0 0 0 0.01 0 0 0 0.10 0 0 0.10 0 0.17 0.19 0.19 0.11 0.01 0.01 0.01 0.01 0.02 0.01 0.02 0.01 0.02	0.063 0.037 0.426 0.376 0.363 0.409 0.374 0.374 0.374 0.374 0.3846 0.384	sltstn "" sltstn & ss "" "" mdstn sltstn & ss slstn sltstn & mdstlignitic slt "" "" sandy sltstn mdstn lignitic mds mdstn ls & mdstn ls & mdstn lignitic md "" sltstn lignitic md "" sltstn lignitic slt "" sltstn "" sltstn "" sltstn "" sltstn
1							

^{*}closed can gamma only assay for eU308.

AM - 79C Cored Interval 25'-70'

40-41	Core Depth ft.	U308 % by wt. 2	eU308* % by wt.	V205 % by wt.	CO ₂ % by wt.	Total sulfur(s) % by wt.	Lithology
$6E_{-}66$ 0 010 0 012 0 011 - 1c & clicty	41-42 42-43 43-44 44-45 45-46 45-49 47-48 49-51 48-59 58-61 61-63 63-64 57	0.001 0.024 0.005 0.009 0.001 0.022 0.035 0.021 0.001 0.001 0.001 0.001 0.001 0.020 0.004 0.011 0.021	0.007 0.011 0.008 0.013 0.021 0.026 0.037 0.024 0.021 0.006 0.002 0.010 0.013 0.021 0.009 0.018 0.030 0.014	0.010 0.038 0.030 0.008 0.004 0.012 0.008 0.005 0.003 0.018 0.034 0.060 0.018 0.145 0.074 0.021	9.17 12.10 	0.33 0.32 0.11 0.32 0.08 - - 0.13	mdstn & ls """ """ silty ls "" sltstn "" sltstn

^{*}Closed can gamma only assay for eU308.

AM - 113C Cored Interval 270'-345'

Core Depth ft.	U308 % by wt.	eU308* % by wt.	V2 ⁰ 5 % by wt.	CO ₂ % bỳ wt.	Total sulfur(s) % by wt.	Lithology
272-273 273-274 274-275 275-276 276-277 277-278 278-279	0.013 0.028 0.005 0.007 0.013 0.007 0.020	0.012 0.022 0.015 0.010 0.013 0.011 0.024	0.036 0.030 0.026 0.029 0.026 0.030	7.75 0.44 - - - 11.15	1.75 2.17 - - - 1.44	lignite " mdstn lignite " lignite, mdstn ls
279-280 280-281 285-286 295-296 296-297 297-298 298-299 299-300 300-301 301-302 302-303 303-304 316-317 317-318 318-319 319-320 340-341 341-342 342-343 343-344	0.016 0.015 0.014 0.004 0.005 0.008 0.022 0.054 0.030 0.032 0.004 0.004 0.070 0.020 0.012 0.007 0.156 0.006 0.008 0.0057 0.001	0.016 0.025 0.022 0.018 0.012 0.009 0.016 0.045 0.062 0.055 0.040 0.016 0.011 0.036 0.019 0.017 0.035 0.017 0.016 0.022 0.076 0.004	0.014 0.014 0.077 0.065 0.132 0.138 0.150 0.223 0.148 0.195 0.095 0.024 0.029 0.036 0.016 0.021 0.022 0.036 0.017 0.021 0.028 0.032	14.84 7.39 0 0 0 0 0 0 0 0 0	1.92 1 2.13 0.90 0.63 0.47 0.49 0.69 0.15 0.85 - 1.46 2.78 0.47 0.13 1.42	ignite, mdstn & lignite lignitic slt " sltstn lignitic sltst " lignitic sltst " lignitic mdst ss

^{*}Closed can gamma only assay for eU308.

Table 1. (Continued)

AM - 119C Cored Interval 26'-41';105'-135'

30-31 31-32 34-35	0.001 0.076 0.007	eU ₃ 08* % by wt. 0.005 0.076 0.022	0.055 0.102 0.036	% by wt. %	Total sulfur(s) by wt.	Lithology mdstn "" calc mdstn
113.5-114 114-115 116-117 118-119 119-120 120-121 121-122 122-123 123-124 124-125 130-131 131-132 132-133 133-134	0.044 0.017 0.014 0.016 0.090 0.045 0.007 0.007 0.011 0.007 0.288 0.194 0.011	0.135 0.029 0.015 0.017 0.083 0.040 0.008 0.008 0.058 0.019 0.012 0.251 0.118	0.101 0.011 0.006 0.012 0.030 0.065 0.021 0.024 0.083 0.026 0.029 0.170 0.077 0.027	10.63 20.86 35.45 26.81 27.03 31.24 - 12.26 - 24.52 0.37	0.52 0.99 0.58 0.45 0.93 0.63 - 1.53	calc mdstn ls & lignite marl " marl & lignite ls & lignite silicified ls & lignite marl marl & lignite lignite lignite

*Closed can gamma only assay for eU308.

AM - 135C Cored Interval 373'-399';452'-484'

		(5)						**			-
•	Core Depth ft.	U308 % by wt.	eU308* % by wt.	<u>.</u> .	V ₂ 05 % by wt.	605 % ph m	Total sulfur(s % by wt.	,	Lithol	.og y	
	377-378 378-379 382-383 383-384-386 383-386-388 385-388 386-389 459-461 462-463 463-464 467-468 4667-468 467-468 469-471 471-472 471-472 471-473 471-475 471-4	0.008 0.027 0.020 0.024 0.028 0.043 0.035 0.035 0.006 0.010 0.033 0.171 0.176 0.090 0.090 0.098 0.090 0.058 0.058 0.058 0.058 0.058 0.059 0.059 0.011 0.059 0.012	0.008 0.027 0.017 0.025 0.038 0.065 0.065 0.061 0.051 0.051 0.122 0.014 0.054 0.		0.065 0.095 0.077 0.030 0.027 0.032 0.062 0.062 0.047 0.064 0.064 0.056 0.056 0.051 0.051 0.071 0.071 0.051	0 0 0.34 0 0 0.01 0.01 0.10 1.43 4.61 0.16 8.99 0.37 28.06 22.01 16.84 15.58 4.71 0.22 0.01 0.06	0.47 0.96 1.00 1.10 0.21 2.22 0.56 0.67 0.16 0.33 1.57 0.51 0.75 2.42 2.24 2.24 0.21 0.33 0.33 0.33 0.21 0.83 1.10 2.09 1.70	ma ma	mdst "" "" "" "" "" "" "" "" "" "" "" "" "	mdst	str """ "" "" te te

^{*}Closed can gamma only assay for eU308

AM - 149C Cored Interval(s) 340'-355';380-420'

Core Depth		Մ ₃ 08	е Մ ვ0 8*	.V205	CO2	Total sulfur(s)	2
ft.		% by wt.	% by wt.		% by wt.	% by wt.	Lithology
10.		70 -					
350-3	51	0.008	0.015	0.015	3.07	0.017	sltstn
351-3		0.005	0.013	0.022	3.38	0.133	11
352-3		0.001	0.004	0.076	0.17	0.007	. 11
380-38		0.008	0.008	0.064	0.07	0.498	11
381-38		0.014	0.022	0.016	0.20	0.534	11
382-3		0.061	0.076	0.012	0.14	0.658	5000
383-3	84	0.072	0.081	0.014	0.13	0.215	. "
384-3	85	0.032	0.048	0.011	0.38	0.075	11
385-3	86	0.022	0.028	0.013	0.26	0.316	11
386-3	87	0.012	0.027	0.015	0.06	0.848	11
387-3		0.003	0.015	0.017	0.04	1.216	11
388-3		0.011	_ 0.013	0.021	0.04	1.009	11
389-3		0.012	0.012	0.024	0.01	0.852	11
390-3		0.009	0.011	0.041	0.01	0.892	11
391-3	92	0.003	0.013	0.070	0	1.169	n n
392-3		0.016	0.045	0.099	0 .	1.921 0.159	lignite sltstr
393-3		0.050	0.050	0.209 0.143	0.02	0.077	11 11
394-3		0.039	0.028	0.143	3.45	0.317	sltstn
395-3		0.001	0.008	0.163	0.10	0.094	11
396-3	97	0.001	0.033	0.571	0	0.939	II .
39 7- 3 398 - 3	90	0.009	0.018	0.153	ŏ	0.885	U-
390-3 399-4	99	0.009	0.016	0.115	0.01	1.216	11
400-4		0.005	0.021	0.131	0	0.721	11
401-4		0.014	0.017	0.184	0	0.631	sltstn & ligni
402-4		0.012	0.017	0.099	0	0.374	11 11
403-4		0.005	0.007	0.077	0	0.090	mdstn
404-4		0.003	0.009	0.105	0	0.050	"
405-4		0.004	0.008	0.191	0.01	0.280	11
406-4		0.005	0.012	0.203	0.01	0.109	
407-4		0.012	0.024	0.169	0	0.159	n
408-4		0.039	0.034	0.166	0	0.093	11
409-4		0.139	0.150	0.278	0	1.216	mdstn & ligni
410-4		0.032	0.036	0.080	0,	1.979	sltstn & ligni
411-4	12	0.008	0.013	0.020			sltstn

^{*}Closed can gamma only assay for eU308.

AM - lc

Table 2. Core hole interval summary of assays from the Anderson Mine.

	· ·					
Log depth ft.	Thickness ft.	eU ₃ 08 % by _wt	cU ₃ 08 %by wt.	V_2O_5 % by wt.	CO2 % by wt.	Total sulfur % by wt.
95.5-98.0 100.0-102.5 104.5-107.5 111.5-116.5 Total	3.0 3.0 3.5 <u>5.5</u> 15.0	.061 .057 .042 .055	.037 .065 .037 .058	.029 .067 .085 .050		
Weighted as	verag e	.054	.050	.057	, '- " ·	
<u>.</u>		сизов:	eU308 =	.926		
		AM	- 7c	* *	i .	
18.5-23.0 98.0-99.5 Total	5.0 2.0 7.0	.095	.110	.130 .014	.08	·3 ¹ 4 ·28
Weighted a	verage	.077	.083	.097	.06	•32
		cU308:	eU ₃ 0 ₈ =	1.072		
			<u>- 13c</u>			
125.5-138.5	13.5	.040	.019	.054	10.57	.02
Total	13.5					
Weighted a	verage	.040	.019	.054	10.57	.02
		cU308:	eU308 =	.475		
		<u>AM</u>	<u>- 16c</u>			
249.0-254.0 273.5-276.0 298.5-315.5 Total	5.5 3.0 17.5 26.0	.135 .080 .052	.155 .055 .045	.142 .072 060		
Weighted a	verag e	.073	.069	.079		
		cU308:	eU ₃ 08 =	.945		

AM - 170

Table 2. (Continued)

	· ·		1			
Log depth ft.	Thickness ft.	eU ₃ 08 % by wt.	cU ₃ 08 %by wt.	V ₂ O ₅ % by wt.	CO2 % by wt.	Total sulfur % by wt.
149.0-150.5 204.5-207.0 Total	2.0 3.0 5.0	.033	.032	.080	.03	.01
Weighted av	rerag e	.038	.037	.099	.02	.02
		cU308:	eU ₃ 08 =	.974		
×		AM	- 18c	*		
281.5-285.5 289.5-293.0 295.5-301.5 Total	4.5 4.0 6.5 15.0	.051 .081 .065	.090 .060 .048	.059 .191 .048	21.06 5.02 11.14	0.84 0.66 0.72
Weighted a		.065	.063	.089	12.48	0.74
		cU308:	eU308:	.938		
			1 - 26c			200
627.5-629.0 631.5-640.0 722.5-725.0 Total	2.0 9.0 3.0 14.0	.042 .082 .111	.031 .064 .139	011	15.62 24.38 0.39	
Weighted a	verage	.083	.075	.016	17.99	0.30
		cU308:	eU308 =	969		
			v lioo			
			м - 49c		- 6 0-	2.21
615.0-622.5 632.5-639.5 Total	8.0 <u>7.5</u> 15.5	.055 .038	.039	.108	1.90	0.31
Weighted a	average ~ ~	.047	042	::088	9.63	0.75
		cU ₂ O ₂ :	eU ₂ O _Q	= .894	Markey S	

AM - 51c

Table 2. (Continued)

Log depth ft.	Thickness ft.	eU ₃ 08 %by wt.	cU ₃ 08 %3by wt.	V ₂ 0 ₅ % by wt.	CO ₂ % by wt.	Total sulfur % by wt.
396.0-401.0 403.0-411.5 442.5-450.0 466.0-471.0 Total	5.5 9.0 8.0 <u>5.5</u> 28.0	.033 .038 .087 .205	.018 .026 .072 .288	.024 .055 .084 .319	.01 .02 11.40 0.04	0.32 1.01 0.30 0.50
Weighted av	rerag e	.084	.089	.109	3.27	0.52
		cU308:	eU ₃ 08 = 1.	.06 0		
			AM - 79c			
45.5-47.5 Total	2.5 2.5	•037	.029	.028	22.36	0.22
Weighted a	verag e	.037	.029	.028	22.36	0.22
		eU308:	eu ₃ 0 ₈ = .'	784		
			AM - 113c			
301.5-306.0 342.5-347.5 Total	5.0 <u>5.5</u> 10.5	.049 .061	.029 .047	.150 .026	0 0	0.89 0.43
Weighted a	verag e _	.055	.039	.085	0	0.65
		cu ₃ 08:	eu ₃ 0 ₈ = •	709		
			AM - 119c			
122.0-127.0 132.0-134.5 Total	5.5 3.0 8.5	.045 .123	.044 .163	.045 .092	23.51 12.28	1.03 1.80
Weighted a	verag e :	.073	.086	.062	19.55	1.30
		cU308:	eU ₃ 08 = 1	.178		

AM - 135c

Table 2. (Continued)

Log depth ft.	Thickness ft.	eU ₃ 08 %by wt.	cU ₃ 08 % by wt.	V ₂ O ₅ % by wt.	CO2 % by wt.	Total sulfur % by wt.
386.0-391.0 458.0-465.0 468.0-477.5 Total	5.5 7.5 10.0 23.0	.053 .115 .175	.053 .085 .127	.067 .337 .084	0.002 1.06 10.36	0.95 1.14 1.17
Weighted av	verag e	.126	.096	.162	4.85	1.11
er gerraria.	irus • -	cu ₃ 08:	$eu_3o_8 = .$	762		
			AM - 149c			
382.5-388.0 393.5-396.0 398.0-399.5 407.0-413.0 Total	6.0 3.0 2.0 6.5 17.5	.050 .044 .034 .061	.036 .035 .024 .039	.014 .150 .362 .066	0.19 0.01 0 0.002	0.44 0.72 0.91 0.59
Weighted a	verage	.051	.036	.096	0.07	0.60
人名英格兰克 化二氯甲基苯甲基甲基苯甲基		- 77 . 00 -	011-00 -	706		

Table 3. Calculation summary sheet for Anderson Mine disequilibrium study.

	* .					•	
Hole No	Thickness (ft.)	Average eU ₃ 08 (wt.%)	A	eighted verage eU308 t.% ft.)	Average cU308 (wt.%)	Weighted Average cU308 (wt.% ft.)	Diseq.
AM-1c AM-7c AM-13c AM-16c AM-17c AM-18c AM-26c AM-26c AM-51c AM-79c AM-113c AM-113c AM-119c AM-135c AM-149c	15.0 7.0 13.5 26.0 5.0 15.0 14.5 28.5 10.5 23.0 17.5	.054 .077 .040 .073 .038 .065 .083 .047 .084 .057 .055 .073		0.810 0.539 0.540 1.898 0.190 0.975 1.162 0.729 2.352 0.093 0.578 0.621 2.898 0.893	.050 .083 .019 .069 .037 .063 .075 .089 .089 .086 .096	0.750 0.581 0.257 1.794 0.185 0.945 1.050 0.651 2.492 0.073 0.410 0.731 2.208 0.630	0.92 1.07 0.47 0.94 0.93 0.98 0.78 0.70 0.70
 Total Weighted	201.0 Totals			14.278		12.757	
Weighted	Grade Avera	ge		.071		.063	
	Disequi	librium Met	thod	total	wt. eU308 wt. eU308	or 12.757	= .893
							1

Disequilibrium Method #2

total wt. disequilibrium or 177.761 total thickness 201

study.

Ι	Diseq.	Weighted Diseq.	Average (wt.%)	Weighted Average V2 ⁰ 5 (wt.% ft	Average CO2 (wt.%)	Weighted Average CO2 (wt.% ft.	Average total sulfur) (wt.%ft)	Weighted Average to sulfur (wt.% ft.	
	0.926 1.078 0.475 0.945 0.938 0.969 0.894 1.060 0.784 0.709 1.178 0.762 0.706	13.890 7.546 6.413 24.570 4.870 14.070 13.566 13.857 29.680 1.960 7.445 10.013 17.526 12.355	.097 .054	0.855 0.679 0.729 2.054 0.495 1.335 0.224 1.364 3.052 0.070 0.893 0.527 3.726 1.680	0.06 10.57 0.02 12.48 17.99 9.63 3.27 22.36 0 19.55 4.85 0.07	0.42 142.70 0.10 187.20 251.86 11.30 91.56 55.90 0 166.18 111.55 1.23	0.32 0.02 0.02 0.74 0.30 0.75 0.52 0.65 1.30 1.11 0.60	2.24 0.27 0.10 11.10 4.20 11.63 14.56 0.55 0 11.05 25.53 10.50	
		177.761		17.683		1020.00		91.73	
				.088		6.38		.057	

.893

 $\frac{7.761}{201} = .884$

Table 4. Summary of Emission Spectrographic Analyses, Anderson Mine, September, 1976.

	,									
ole # ore Depth ithology	AM-i35c 460-461 lignite & sltstn	AM-135c 469-470 mar1	AM-135c 472-473 mar1 & lignite	AM-119c 119-120 mar1	AM-119c 132-133 lignite	AM-113c 300-301 lignite & sltstn	AM-7c 18-19 mdstn	AM-17c 131-132 mdstn		
Fe	1.5%	.2%	1.5%	.5%	2%	2%	2%	3%		
Ca	.5%	15%	10%	20%	.7%	.2%	.3%	.2%		
Mg	.5%	.2%	.2%	1%	1%	.3%	1.5%	2%		
Ag	<1	<1	<1	<1	<1	<1	<1	<1		
As	<500	<500	500	<500	<500	<500	<50 0	<500		
B	20	10	15	15	20	20		30		
Ba	200	10	7	150	300	200	200,	100		
e	<2	<2	<2	<2	<2	<2	<2	2		
Bi	<10	<10	<10	<10	<10	<10	<10	<10		
Cd	<50	<50	<50	<50	<50	<50	<50	<50		
Co	<5	<5	<5	<5	10	5	7	10		
Cr	20	10	70	10	30	50	70	50		
Cu	10	2	15	2	20	20	20	30		
Ga	<10	<10	<10	<10	<10	<10	<10	<10		
Ge	<20	<20	<20	<20	<20	<20	<20	<20		
La	20	20	20	20	50	30	50	70		
Mn	50	150	150	200	100	150	150	200		
Mo	5	70 ●	300 ●	2	50 ●	30 ●	<2	<2		
Nb	<20	<20	<20	<20	<20	<20	<20	20		
Ni	15	<5	30	5	20	30	20	20		
Pb Sb Sc Sn Sr	10 <100 <10 <10 150	<10 <100 <10 <10 <10 700	10 <100 <10 <10 300	10 <100 <10 <10 2,000	20 <100 10 <10 200	15 <100 <10 <10 <10	20 <100 10 <10 150	10 <100 15 <10 150		
T1 V W Y Zn	500 5,000 ◆ <50 10 <200 50	200 200 <50 <10 <200 30	200 500 ● <50 <10 <200 <20	500 150 <50 <10 <200 30	1,000 500 ◆ <50 15 <200 50	700 700 ◆ <50 10 <200 50	1,500 1,000 ◆ <50 20 <200 50	1,500 200 <50 20 <200 50		

[•] Anomalous value V-29

Table 4. Summary of Emission Spectrographic Analyses, Anderson Mine, September, 1976.

Hole # Core Depth Lithology	AM-149c 408-409 mdstn	AM-51c 445-446 lignite & mdstn	AM-51c 446-447 lignite & mdstn	AM-51c 464-465 lignite & sltstn	AM-51c 446-467 sltstn	
Fe	1%	1%	1%	2%	1.5%	
Ca	.3%	.5%	.2%	.2%	.2%	
Mg	.3%	.5%	.5%	.2%	.5%	
Ag	<1	<1	<1	<1	<1	
As	<500	<500	<500	<500	700	
B	20	10	15	15	15	
Ba	150	100	150	200	100	
Be	<2	<2	<2	<2	<2	
Bi	<10	<10	<10	<10	<10	
Cd	<50	<50	<50	<50	<50	
Co	<5	<5	<5	<5	5	
Cr	70	30	50	50	30	
Cu	20	10	7	20	15	
Ga	<10	<10	<10	<10	<10	
Ge	<20	<20	<20	<20	<20	
La Mn Mo Nb Ni	30 70 15 ● <20 15	30 50 <2 20	20 50 <2 <20 5	20 50 10 ◆ <20 10	20 100 <2 <20 5	
Pb	10	<10	<10	<10	10	
Sb	<100	<100	<100	<100	<100	
Sc	<10	<10	<10	<10	<10	
Sn	<10	<10	<10	<10	<10	
Sr	150	100	150	200	150	
Ti	500	500	500	300	300	
V	700 ●	500 ●	700 ●	1,000 ●	1,500 ♥	
W	<50	<50	<50	<50	<50	
Y	15	10	<10	10	10	
Zn	<200	<200	<200	<200	<200	
Zr	30	70	20	20	20	
	2 4 4 7 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		The state of the s			

[•] Anomalous value

Table 4. Summary of Emission Spectrographic Analyses, Anderson Mine, September, 1976.

				5 g	· · · · · ·	<u> </u>		•
Hole #	AM-18c	AM-26c	AM-26c	AM-26c	AM-26c	AM-49c	AM-49c	AM-149
Core Depth	297-298	636-637	720=721	721-721.25		612-613	615-616	393-394
Lithology	1ignite	1s & s1str	s s	88	8 8	chert	cherty 1s	lignite&
	1.5%	. 5%	3%	2%	5%	2%	.2%	1%
Fe		15%	1%	1% .	1.5%	. 5%	10%	. 2%
Ca	10%	.2%	1.5%	1%	1.5%	. 5%	.3%	. 2%
Mg	. 5%	<1	<1	<1	<1	<1	<1	<1
Ag	<1	<50 0	50 0	<50 0	<50 0	<50 0	< 50 0	<50 0
As	< 50 0	1300					(10	50
В	15	<10	20	30	15	15	<10	5 0 5 0
Ba	100	20	700	700	700	100	10	⟨2
Вe	<2	<2	2	2	2	<2	<2	
B i	<10	<10	<10	<10 ·	<10	<10 -	<10	<10
Cd	<50	<50	<50	<50	<50	<50	<50	<50
		214	15	5	15	<5	<5	<5
Co	<5	<5	100	50	100	70	<10	15 0
Cr	50	15		30	30	20	2	10
Cu	20	5	50		10	<10	<10	<10
Ga	<10	<10	10	<10 <20	<20	<20	<20	<20
Ge	<20	<20	<20	(20				
	20	20	50	50	50	30	20	30
4	500	300	200	200	200	70	50 0	20
n	15	<2	<2	<2	2	<2	<2	20
Мо	<20	<20	20	<20	20	<20	<20	<20
Nb	15	\25 5	50	20	70	15	5	10
N1					20	10	<10	<10
РЪ	10	<10	30	20	<100	<100	<100	<100
Sb	<100	<100	<100	<100	20	<10	<10 .	<10
Sc	<10	<10	15 •	10 •		<10	<10	<10
Sn	<10	<10	<10	<10	<10	70	500	100
Sr	1,000	200	1,000	1,000	1,000			
	500	100	2,000	1,000	3,000	500	100	500
Ti		30	200	300	300 ●	1,000	100	700
V	50	<50	<50 ·	<50	<50	<50	<50	<50
W	<50	<10	30	10	20	20	<10	10
Y	<10	<-200	<200	<200	< 200	<200	<200	<200
Zn	<200		50	30	50	30	20	50
Zr	20	20	20					Section 1

[•] Anomalous value



