



CONTACT INFORMATION  
Mining Records Curator  
Arizona Geological Survey  
3550 N. Central Ave, 2nd floor  
Phoenix, AZ, 85012  
602-771-1601  
<http://www.azgs.az.gov>  
[inquiries@azgs.az.gov](mailto:inquiries@azgs.az.gov)

The following file is part of the Walter E. Heinrichs, Jr. Mining Collection

### **ACCESS STATEMENT**

These digitized collections are accessible for purposes of education and research. We have indicated what we know about copyright and rights of privacy, publicity, or trademark. Due to the nature of archival collections, we are not always able to identify this information. We are eager to hear from any rights owners, so that we may obtain accurate information. Upon request, we will remove material from public view while we address a rights issue.

### **CONSTRAINTS STATEMENT**

The Arizona Geological Survey does not claim to control all rights for all materials in its collection. These rights include, but are not limited to: copyright, privacy rights, and cultural protection rights. The User hereby assumes all responsibility for obtaining any rights to use the material in excess of "fair use."

The Survey makes no intellectual property claims to the products created by individual authors in the manuscript collections, except when the author deeded those rights to the Survey or when those authors were employed by the State of Arizona and created intellectual products as a function of their official duties. The Survey does maintain property rights to the physical and digital representations of the works.

### **QUALITY STATEMENT**

The Arizona Geological Survey is not responsible for the accuracy of the records, information, or opinions that may be contained in the files. The Survey collects, catalogs, and archives data on mineral properties regardless of its views of the veracity or accuracy of those data.

## INDUCED POLARIZATION

## SENDER NOTES

Project: Big JimLine: S 1/2 #1 (500)Date: 8-22-64

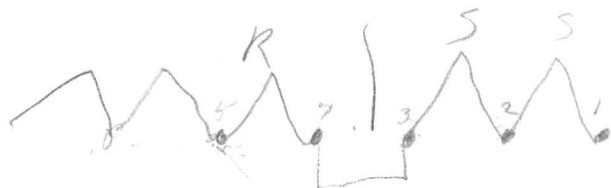
Send	2-3	12	34	23	12	45	34	23	12	45	34	2-3
Receive	→	→	→	→	→	→	→	→	→	→	→	→
Time												
Range	2x800	2x400	2x1000	2x800	2x400	2x1600	2x1000	2x800	2x400	2x1000	2x1000	2x800
Current	1600	800	2000	1600	800	2600	2000	1600	800	2000	2000	1600
Send	12	45	34	23	12			CA/				
Receive	→	→	→	→	→			2x100				
Time												
Range	2x400	2x1600	2x1600	2x800	2x400			3x100				
Current	800	2000	2000	1600	800			300				

## INDUCED POLARIZATION

## SENDER NOTES

Project: Big JimLine: N 1/2 # 1Date: 8-21-64

Send	3/4	4/5	2/3	3/4	4/5	12	23	34	4/5	12	23	34
Receive	N	→	N	→	N	→	N	→	N	→	N	→
Time												
Range	2x800	2x800	2x800	2x800	2x800	2x400	2x800	2x1600	2x1600	2x400	2x800	2x1000
Current	1600	1600	1600	1600	1600	600	1600	2000	2000	800	1600	2000
Send	4/5	12	23	34	4/5			CA/	3x100			
Receive	→	N	→	→	→			300				
Time												
Range	2x1000	2x400	2x800	2x1000	2x1000							
Current	2000	800	1600	2000	2000							



4-5	3-4	2-3	1-2
2000	2000	1600	800



## INDUCED POLARIZATION - RECEIVER NOTES

PAGE

Project: Biochim Insp. Line: 1 (500) N<sup>1</sup>/<sub>2</sub> Int. Cal \_\_\_\_\_ Date: Nov 22 66

Send	3-4	45	2-3	3-4	4-5	1-2	2-3	3-4	4-5	1-2	2-3	3-4
Rec.	1-2N	→	2-3N	→	3-4N	→	→	→	→	4-5N	→	→
Time	100	30	100	30	10	100	30	30	10	30	10	10
DC-1	68.0 67.0	13.6	34.5	15.7	5.2 4.95	56.1 55.0	12.7 12.9	9.6 9.6	3.65 3.90	14.6	5.4 5.4	4.35 4.55
DC-2	67.5 67.0	13.3	35.0	16.4	5.1 5.0	56.1 55.0	12.8 13.0	9.5 9.6	3.75 3.90	14.9	5.4 5.3	4.50 4.85
Σ	134.5	26.9	69.5	32.1	10.15 10.1	111.1	25.6 25.8	19.2 19.1	7.55 7.65	29.5	10.8 10.7	8.90 8.95
DC-3	67.5	13.6	34.5	15.7	4.95 5.0	56.0 55.0	12.8	9.7	3.90 3.75	14.5	5.35 5.45	4.55 4.55
Dc-4	67.0	13.3	35.0	16.4	5.0 5.0	56.0 55.0	13.0	9.5	3.80 3.85	14.8	5.35 5.40	4.55 4.50
Σ	134.5	26.9	69.5	32.1	10.0 10.0	111.0	25.8	19.2	7.65 7.65	29.3	10.80 10.75	9.00 9.00
DC-AV	134.5	26.9	69.5	32.1	10.0	111.05	25.7	19.2	7.65	29.4	10.75	8.97
AC-1	61.0	12.1	32.0	14.3	4.6	57.0	11.4	8.2	3.4	12.9	4.65	3.90
AC-2	61.0	12.0	32.0	14.3	4.6	57.0	11.4	8.4	3.5	13.0	4.65	3.90
Σ	122.0	24.0	64.0	28.6	9.2	102.0	22.8	16.9	6.9	25.9	9.30	7.80
S. P.	12.7	13.2	25.7		35.0	47.5			44.0	85.5		
AC-N	06±1 56.0		08		08 sp 0.04	0.04			04	04		
									55.5			

## INDUCED POLARIZATION - RECEIVER NOTES

PAGE

Project: \_\_\_\_\_ Line: 1(500) N<sup>1</sup>/<sub>2</sub> Int. Cal \_\_\_\_\_ Date: \_\_\_\_\_

Send	4-5	1-2	2-3	3-4	4-5		CAL.				
Rec.	→	5-6	→	→	→		2-3				
Time	3.0	3.0	3.0	3.0	1.0		30				
DC-1	1.97 2.06	2.98 2.93	1.42 1.48	1.38 1.38	.64 .67		15.4 15.3				
DC-2	5.0 2.03	2.95 2.96	1.43 1.52	1.40 1.37	.65 .65		15.3 15.3				
Σ	4.03 4.03	5.91 5.91	2.90 2.95	2.78 2.77	1.31 1.30						
DC-3	2.0 2.05	2.95 2.96	1.44 1.46	1.37 1.36	.65 .64		15.3 15.3				
Dc-4	1.94 2.15	2.93 2.98	1.46 1.43	1.40 1.36	.68 .63						
Σ	4.05 4.09	5.91 5.91	2.98 2.90	2.78 2.76	1.39 1.31						
DC-AV	4.06	5.91	2.97	2.75	1.30		30.6				
AC-1	1.77	2.6	1.25	1.16	.59		15.2				
AC-2	1.76	2.58	1.25	1.16	.59		15.2				
Σ	3.53	5.18	2.50	2.32	1.18		30.4				
S. P.	79.7	46.0			67.0						
AC-N	.040	.02			.02						
	55.0				55.0						

## INDUCED POLARIZATION - RECEIVER NOTES

PAGE

Project: Big JimLine: 1-5 1/2

(500')

Int. Cal

Date: Apr 22, 60

Send	3-2	2-1	4-3	3-2	2-1	5-4	4-3	3-2	2-1	5-4	4-3	3-2
Rec.	1-25	→	2-35	→	→	3-45	→	→	→	4-55	→	→
Time	100	10	100	30	10	100	30	10	3.0	30	10	3.0
DC-1	37.5	6.8 6.9	64.0	12.4 11.6	3.5 3.75	40.0 39.5	14.3 13.8	3.6 3.25	1.09 1.35	9.0 8.6	4.85 5.0	1.65 1.64
DC-2	37.5	6.9 6.9	64.0	12.4 11.6	3.55 3.75	40.0 39.8	14.3 13.8	3.6 3.25	1.07 1.36	9.1 8.6	4.9 5.0	1.64 1.65
Σ	75.0	13.7 13.8	128.0	24.0 24.0	7.05 7.50	79.5 79.3	28.1 28.1	6.85 6.75	2.44 2.43	17.6 17.7	9.85 9.9	3.29 3.29
DC-3	37.0	6.85 6.4	64.5	12.4	3.75	40.0 39.8	14.3 13.8	3.6 3.20	1.06 1.32	9.2 8.5	4.90 5.0	1.64
Dc-4	37.5	6.85 6.85	64.5	11.6	3.55	39.8 39.0	14.3 13.8	3.62 3.20	1.03 1.40	9.2 8.5	5.0 4.95	1.65
Σ	74.5	13.75 13.7	129.0	24.0	7.30	79.8 79.8		6.81 6.82	2.43 2.43	17.7 17.7	9.90 9.95	3.29
DC-AV	75.0	13.75	128.5	24.0	7.32	79.8	28.1	6.83	2.43	17.7	9.90	3.29
AC-1	33.5	6.15	58.5	10.7	3.3	37.0	12.7	3.15	1.14	8.3	4.55	1.54
AC-2	33.5	6.15	58.5	10.7	3.28	37.0	12.7	3.15	1.14	8.3	4.55	1.53
Σ	67.0	12.30	117.0	21.4	6.58	74.0	25.4	6.30	2.28	16.6	9.10	3.07
S. P.	-3.0	-1.6	-1.0		-0.9				-2	.04		
AC-N	.2	.15	.06		-.15							
	55.5	55.5			55.0							

$$\begin{array}{r}
 2.9 \\
 4.35 \\
 \hline
 7.25
 \end{array}
 \qquad
 \begin{array}{r}
 2.9 \\
 4.40 \\
 7.30
 \end{array}$$

.48

.60

.42

.60

.57

.56

.57

.54

1.08

1.02

1.02

1.17

1.13

1.13

1.11

1.08

1.00

31

## PAGE

Project: S. J.

Line:

1.  $5\frac{1}{2}$  (500')

Int.Cal

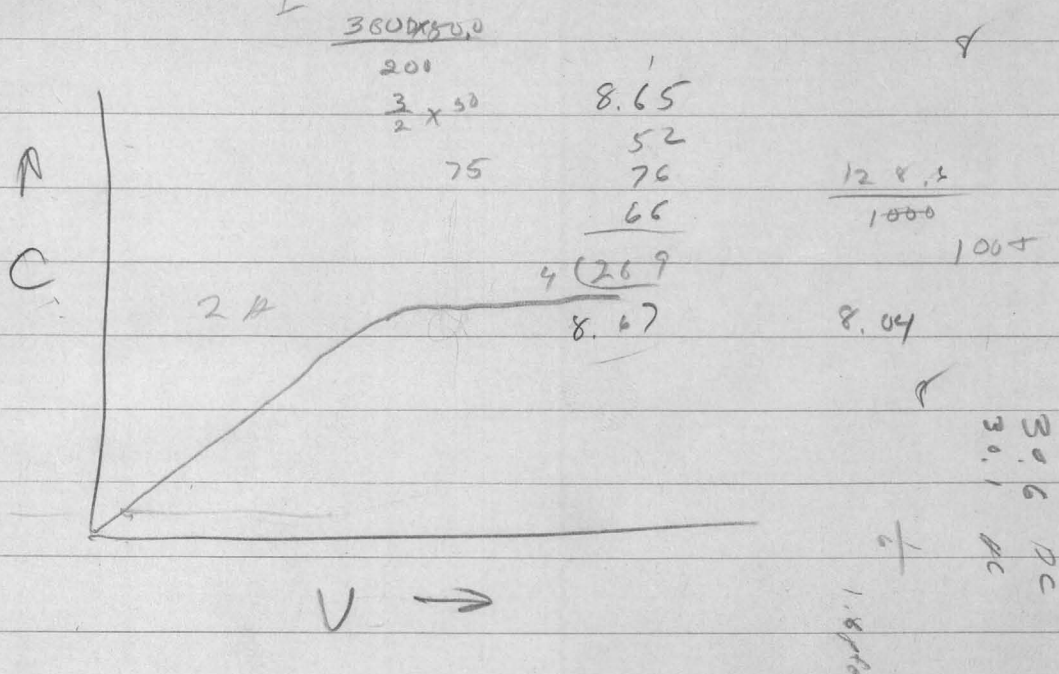
Date:

[illegible]

# Big Jim - Line #1

R	12	→	235	→	395	→	455	→	455	→
S	23	12	39	23	12	45	39	23	12	45
Range	2x1000	2x500	2x1000	2x500	2x1000	2x500	2x1000	2x500	2x1000	2x500
I	2000	1000	2000	2000	1000	2000	2000	2000	1200	2000
K			→	505	→	Cal				
S	39	23	12	45	39	23	12	45		
K										
I	2000	2000	1200	2000	2000	2000				

$$pdc = \frac{K_n(V)}{I}$$



## INDUCED POLARIZATION

## SENDER NOTES

Project: Big JimLine: N 1/2 #1Date: 8-19-64

Send	34	45	23	34	45	12	23	34	45	12	23	34
Receive	12N →	23N →	34N →	45N →								
Time												
Range	2X1000	2X1000	2X1000	2X1000	2X1000	2X600	2X1000	2X1000	2X1000	2X600	2X1000	2X1000
Current	2000	2000	2000	2000	2000	1200	2000	2000	2000	1200	2000	2000
Send	45	12	23	34	45		CA12-3					
Receive	→ 56N											
Time												
Range	2X1000	2X600					3X100					
Current	2000	1200	2000	2000	2000		300					

1-2  
~~800~~  
~~1000~~  
600

2-3

1000

34

2000

45

2000



HEINRICHS GEOEXPLORATION COMPANY  
INDUCED POLARIZATION SURVEY COMPUTATION SHEET

Page \_\_\_\_\_

Project Big Jim Line 1 56 Field date 8-12-64 Data page \_\_\_\_\_ Comp. date 8-16-64 . Comp by KH

(A) Send	23	12	34	23	12	45	34	23	12	45	34	23
(B) Receive	125		235			345				455		
(C) n separation	30	10	30	10	3	100	10	10	3	30	10	3
(D) I	2000	1000	2000		1000	2000			1200	2000		
(E) Vdc (avg)	50.1	8.67	36.1	8.95	2.14	73.25	14.95	5.25	2.00	18.6	5.37	2.56
(F) DCcal	.983											
(G) Kn x 10 <sup>-3</sup>	3	12	3	12	30	3	12	30	60	12	30	60
(H) $\rho_{dc} = ExFxGx10^3/D$	73.7	102	53.1	52.7	63.1	108	88.0	78.6	98.3	110	79.0	75.5
(I) Vac $\Sigma$	46.2	8.04	33.6	8.36	2.05	70.40	13.90	4.98	1.91	17.4	5.00	2.38
(J) AC noise x 2												
(K) Vac (corr) = $\sqrt{I^2 - J^2}$												
(L) AC-DC cal.	.985	.985				1.005	.985					
(M) $\rho_{dc}/\rho_{ac} = ExL/K$	1.068	1.063	1.060	1.056	1.030	1.045	1.060	1.059	1.031	1.052	1.058	1.060
(N) PFE = (M-1)(10 <sup>2</sup> )	6.8	6.3	6.0	5.6	3.0	4.5	6.0	5.9	3.1	5.2	5.8	6.0
(O) MCF = (M-1)(10 <sup>5</sup> )/H	92	62	113	106	48	42	68	75	32	47	73	80

Project \_\_\_\_\_ Line \_\_\_\_\_ Field date \_\_\_\_\_ Data page \_\_\_\_\_ Comp. date \_\_\_\_\_ Comp by \_\_\_\_\_

(A) Send	12	45	34	23	12		CH2					
(B) Receive		565					4-5					
(C) n separation	1	10	3	3	1		30					
(D) I	1200	2000			1200		300					
(E) Vdc (avg)	1.025?	10.15	4.24	2.07	1.01?		30.55					
(F) DCcal							.983					
(G) Kn x 10 <sup>-3</sup>	105	30	60	105	168							
(H) $\rho_{dc} = ExFxGx10^3/D$	88.1	150	125	107	138							
(I) Vac $\Sigma$	.960	9.42	3.91	1.89	1.01		30.1					
(J) AC noise x 2												
(K) Vac (corr) = $\sqrt{I^2 - J^2}$												
(L) AC-DC cal.	1.045	.985			1.045		.985					
(M) $\rho_{dc}/\rho_{ac} = ExL/K$	1.116?	1.061	1.070	1.079	1.045							
(N) PFE = (M-1)(10 <sup>2</sup> )	11.6?	6.1	7.0	7.9	4.5							
(O) MCF = (M-1)(10 <sup>5</sup> )/H	132?	41	56	74	32?							

100 R = +2% cal  
1 R +6% cal

# HEINRICHS GEOEXPLORATION COMPANY INDUCED POLARIZATION SURVEY COMPUTATION SHEET

Page         
Comp. by KH+PB

Project Big Jim Line 1N<sup>1</sup>/<sub>2</sub> Field date 8-19-64 Data page        Comp. date 8-20-64

(A) Send	34	45	23	34	45	12	23	34	45	12	23	34
(B) Receive	12N		23N		34N					45N		
(C) n separation	100	30	100	10	10	30	10	10	3	3	3	1
(D) I	2000					1200	2000			1200	2000	
(E) Vdc (avg)	58.5	17.35	72.0	19.1	9.06	53.1	19.15	10.15	5.67	2.45	2.05	1.10
(F) DCcal	.980											
(G) Kn x 10 <sup>-3</sup>	3	12	3	12	30	3	12	30	60	12	30	60
(H) $\rho_{dc} = ExFxGx10^3/D$	86.0	102	106	112	118	130	112	149	167	289	308	323
(I) Vac $\Sigma$	53.5	16.0	66.0	17.35	8.5	46.7	16.6	7.1	5.11	2.57	1.84	1.03
(J) AC noise x 2												
(K) Vac (corr) = $\sqrt{I^2 - J^2}$												
(L) AC-DC cal.	1.007	.987	1.007	.987								1.047
(M) $\rho_{dc}/\rho_{ac} = ExL/K$	1.100	1.070	1.100	1.087	1.060	1.120	1.139	1.099	1.095	1.132	1.096	1.115
(N) PFE = (M-1)(10 <sup>2</sup> )	10.0	2.0	10.0	8.7	6.0	12.0	13.9	9.9	9.5	13.2	9.6	11.5
(O) MCF = (M-1)(10 <sup>5</sup> )/H	116	68	94	73	51	93	116	66	58	457	312	356

Project        Line        Field date        Data page        Comp. date        Comp by       

(A) Send	45	12	23	34	45		cc1					
(B) Receive		56N					12					
(C) n separation	1	1	1	1	1		20					
(D) I		1200	2000									
(E) Vdc (avg)	.82	.62	.465	.57	.41		30.6					
(F) DCcal												
(G) Kn x 10 <sup>-3</sup>	105	30	68	105	118							
(H) $\rho_{dc} = ExFxGx10^3/D$	42.2	15.2	13.6	29.3	33.7							
(I) Vac $\Sigma$	.81	.60	.47	.56	.38		30.2					
(J) AC noise x 2												
(K) Vac (corr) = $\sqrt{I^2 - J^2}$												
(L) AC-DC cal.	1.047						.987					
(M) $\rho_{dc}/\rho_{ac} = ExL/K$	1.059	1.082	1.035	1.064	1.128							
(N) PFE = (M-1)(10 <sup>2</sup> )	5.9	8.2	3.5	6.4	12.8							
(O) MCF = (M-1)(10 <sup>5</sup> )/H	140	537	257	214	392							

9.70

30 }  
10 } .987  
3 }

100 + 2% = 1.007  
1 + 1% = 1.047

3m 52.0

Rx	TV	RANGE	DC.	AC	N-AC	S.P.	DC. Av.
45	5	45	30				
			9.5		.04-.07	-4.6	
			9.0	8.7			18.6
			18.5	8.7		9.4	
			9.5	17.4		9.2	(17.4)
			9.1			18.6	
			18.6			9.4	
						9.2	

34	10		2.62	2.5		2.70	2.60	2.6	2.6	
			2.75			2.75	2.90	2.85	2.9	5.37
			5.37	2.5		5.45	5.50	5.45	5.30	(5.00)
			2.65	5.00		2.50	2.42	2.4	2.7	
			2.70			2.90	2.50	2.9	2.65	
			5.35			5.40	5.22	5.30	5.35	

23	3.0		1.28	1.18		1.25	1.24	1.25		
			1.24			1.30	1.35	1.27		
			2.52	1.20		2.55	2.59	2.52		2.56
			1.40	2.38		1.30	1.28	1.30		(2.38)
			1.20			1.30	1.34	1.23		
			2.60			2.60	2.62	2.52		

12	1.		.40	.48						
			.40							
			1.00	.98						1.025 ?
			.35	.96						(.960) ?
			.70							
			1.05							

52.0

.05-.1

-1.4



Rx	Ty	RANLE	DC	Ac	N. Ac	S. P.	DC Au.
565	45	10	$\begin{array}{r} 5.20 \\ 4.95 \\ \hline 10.15 \\ 5.15 \\ 4.90 \\ \hline 10.05 \end{array}$	$\begin{array}{r} 4.70 \\ 4.72 \\ \hline \$9.42 \end{array}$		$\begin{array}{r} 922 \\ 5.20 \quad 4.95 \\ 5.0 \quad 5.30 \\ 10.20 \quad 10.25 \\ 10.05 \quad 10.20 \\ 4.95 \quad 4.90 \\ 5.10 \quad 5.30 \end{array}$	$\begin{array}{r} 10.15 \\ (9.42) \end{array}$
	34	3.0	$\begin{array}{r} 2.10 \\ 2.20 \\ \hline 4.30 \\ 2.05 \\ 2.15 \\ \hline 4.20 \end{array}$	$\begin{array}{r} 1.96 \\ 1.95 \\ \hline \$3.91 \end{array}$		$\begin{array}{r} 2.15 \quad 2.05 \\ 2.10 \quad 2.15 \\ 4.25 \quad 4.20 \\ 2.15 \quad 2.1 \\ 2.15 \quad 2.10 \\ 4.30 \quad 4.20 \end{array}$	$\begin{array}{r} 90.8 \\ 4.24 \\ (3.91) \end{array}$
	23	3.0	$\begin{array}{r} 1.0 \\ 1.15 \\ \hline 2.15 \\ .90 \\ 1.05 \\ \hline 1.95 \end{array}$	$\begin{array}{r} .95 \\ .94 \\ \hline \$1.89 \end{array}$		$\begin{array}{r} 1.25 \quad 1.05 \\ .85 \quad 1.05 \\ 2.10 \quad 2.10 \\ 1.25 \quad .95 \\ .80 \quad 1.15 \\ 2.05 \quad 2.10 \end{array}$	$\begin{array}{r} 2.07 \\ (1.89) \end{array}$
	12	1.0	$\begin{array}{r} .4-.5 \\ .5-.55 \\ .90 \quad 1.05 \\ .45-.55 \\ .5-.6 \\ .95 \quad 1.15 \end{array}$	$\begin{array}{r} .50 \\ .51 \\ \hline \$1.01 \end{array}$	$\begin{array}{r} .05-.09 \\ \text{SPICET } 1.5 \end{array}$	$\begin{array}{r} 91.0 \end{array}$	$\begin{array}{r} 1.01? \\ (1.01) \end{array}$
			$\begin{array}{r} \text{BAY } 51.5 \end{array}$			$\begin{array}{r} 91.0 \end{array}$	

TX 3-2

BAT 54.5

L1 Bus Jan

S.P. -7.1

Rx	S	RANG	DC	AC	Noise AC	Noise DC	AC <del>E</del>	D.C. Av.
1-25	1	30	1 24.8 2 25.3	23.1		24.7 25.3	46.2	50.1
	23		T 50.1	23.1		50.0		
			2 24.6 4 25.5			24.7 25.6		
		Total	50.1			50.3		
		10	1 43.0 2 43.5	4.02		4.35 4.41		
	1-2		T 8.65	4.02		8.76	8.04	8.67
			3 4.22 4 4.30			4.25 4.41		
✓			T 8.52			8.66		
2-35		30	1 18.3 2 17.7	16.80		17.7 18.2 18.4 18.0	S.P. -6.6	
	34		T 36.0	16.80		36.1 36.2	33.6	36.1
			3 17.6 4 18.3			17.6 18.3 18.4 17.9		
		Total	35.9			36.0 36.2		
		10	1 4.45 2 4.50	4.18		4.50 4.45 4.50 4.40	8.36	
	23		T 8.95	4.18		9.00 8.85		8.95
			3 4.50 4 4.50	8.36		4.55 4.65 4.45 4.25		
			T 9.00			9.00 8.90		
		3	1 1.23 2 1.90	1.03		1.10 1.10 1.90 1.15	1.15 1.12 1.05 1.03	
	12		2.13	1.02		2.00 2.25	2.10 2.15	
			1.35 1.75	2.05		1.15 1.0 1.95 1.16	1.10 1.10 1.08 1.12	2.14
✓			2.10			2.13 2.16	2.18 2.27	
		CAL	15.3 15.2	15.1				
		30	30.5	15.0				
			15.3 15.3	30.1				
			30.6					30.55

2 Bat 154.5

-1.4

Rx	TY	RANK	DC.	AC.	N-AC	S.P.	D.C. Ave
345	45	100	32.2 36.0 73.2 37.5 35.9 73.4	35.2  35.2 E70.4	.05	36.2 36.0 32.0 32.0 73.2 73.0 36.2 36.0 36.8 32.2 73.0 73.7	73.25
34	10		2.3 2.4 14.70 2.55 2.50 15.5	6.95 6.95 13.90		2.50 7.58 7.45 2.45 7.62 7.55 14.96 15.26 15.00 2.50 2.20 2.56 2.45 2.70 2.45 14.96 14.90 14.95	14.95
23	10		2.7 2.65 5.35 2.6 2.8 5.40	2.50 2.48 4.98		2.70 2.70 2.65 2.55 5.35 5.25 2.75 2.75 2.55 2.58 5.40 5.33	5.35
12	3.0		.80 1.10 1.90 .85 1.15 2.00	.96 .95 1.91		.78 1.08 .9 1.05 .85 1.1 2.03 2.00 1.0 .98 .98 1.15 1.85 2.10	2.00
			BAT. 52.0			-1.5	



HEINRICHS GEOEXPLORATION COMPANY  
INDUCED POLARIZATION SURVEY COMPUTATION SHEET

Page \_\_\_\_\_

Project Big Jim Line 1 (500) N<sub>2</sub> Field date 8-21-64 Data page \_\_\_\_\_ Comp. date 8-21-64 Comp by 114

(A) Send	34	45	23	34	45	12	23	34	45	12	23	34
(B) Receive	12N	→	23N	→	34N	→	45N	→	12N	→	23N	→
(C) n separation	100	30	100	30	10	100	30	30	10	30	10	10
(D) I	1100	→	800	1600	2000	→	800	1600	2000	→	800	1600
(E) Vdc (avg)	139.5	26.9	69.5	32.1	10.0	111.05	25.7	19.2	7.65	29.4	10.75	8.97
(F) DCcal	980	→	→	→	→	→	→	→	→	→	→	→
(G) Kn x 10 <sup>-3</sup>	1.5	6	1.5	6	15	1.5	6	15	30	6	15	30
(H) $\rho_{dc} = ExFxGx10^3/D$	128.0	98.7	63.8	118.0	92.0	204.	94.4	141	112	216	98.9	132
(I) Vac $\Sigma$	122.0	24.0	64.0	28.6	9.2	102.0	22.8	16.9	6.9	28.9	9.30	7.80
(J) AC noise x 2												
(K) Vac (corr) = $\sqrt{I^2 - J^2}$												
(L) AC-DC cal.	1.013	993	1.013	993	→	1.013	993	→	1.013	993	→	1.013
(M) $\rho_{dc}/\rho_{ac} = ExL/K$	1.159	1.112	1.101	1.113	1.079	1.102	1.120	1.122	1.101	1.129	1.148	1.142
(N) PFE = (M-1)(10 <sup>2</sup> )	15.9	11.2	10.1	11.3	7.9	10.2	12.0	12.2	10.1	12.9	14.8	14.2
(O) MCF = (M-1)(10 <sup>5</sup> )/H	124	114	158	95	85	50	127	87	99	60	149	108

Project \_\_\_\_\_ Line \_\_\_\_\_ Field date \_\_\_\_\_ Data page \_\_\_\_\_ Comp. date \_\_\_\_\_ Comp by \_\_\_\_\_

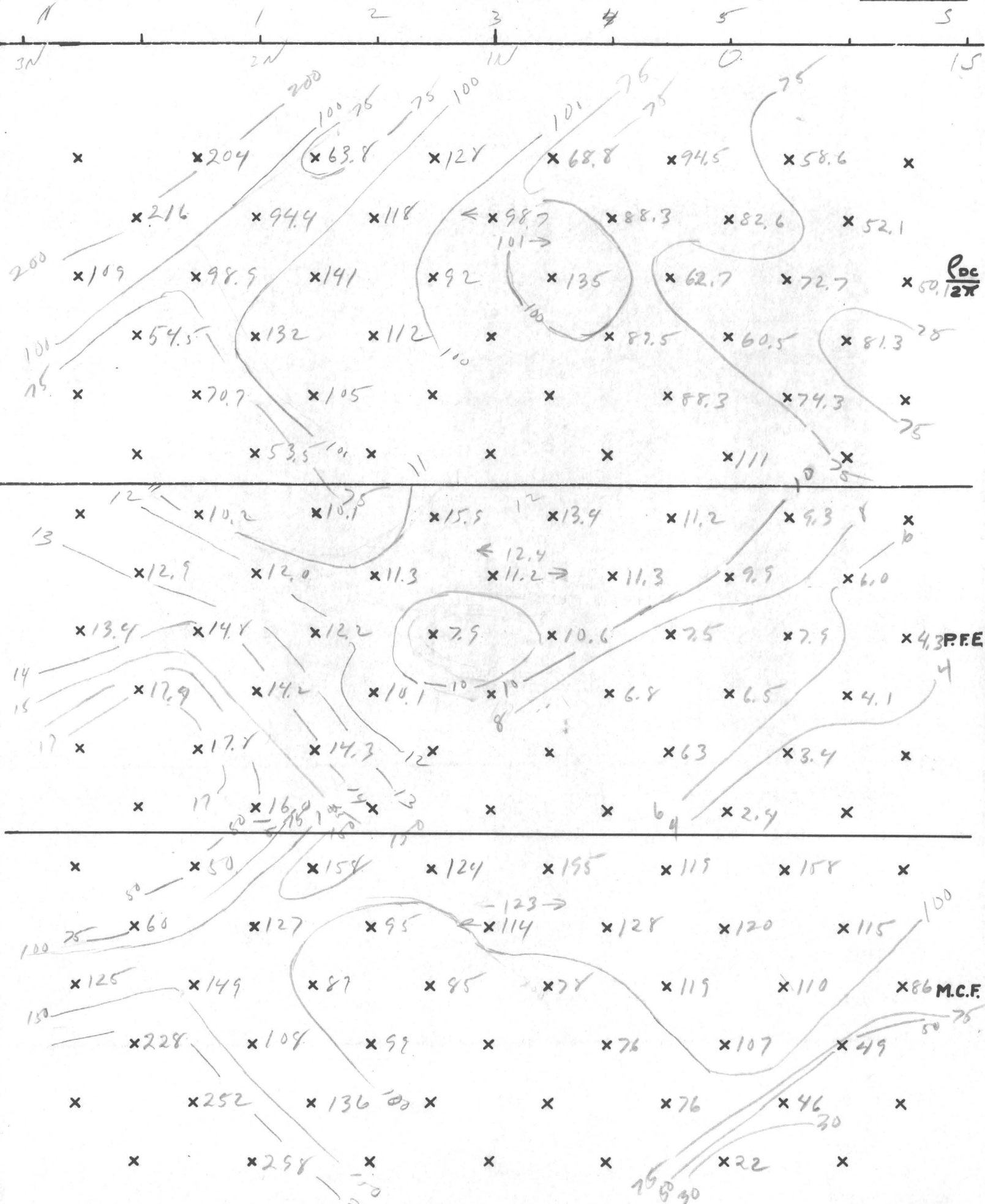
(A) Send	45	12	23	34	45		Cal					
(B) Receive	→	56N	→	→	→		12					
(C) n separation	3	3	3	3	1							
(D) I	→	800	1600	2000	→							
(E) Vdc (avg)	4.06	5.91	2.97	2.75	1.30		30.6					
(F) DCcal	→	→	→	→	→							
(G) Kn x 10 <sup>-3</sup>	52.5	15	30	52.5	84							
(H) $\rho_{dc} = ExFxGx10^3/D$	105	109	54.5	70.7	53.5							
(I) Vac $\Sigma$	3.53	5.18	2.50	2.32	1.18		30.4					
(J) AC noise x 2												
(K) Vac (corr) = $\sqrt{I^2 - J^2}$												
(L) AC-DC cal.	→	→	→	→	1.053							
(M) $\rho_{dc}/\rho_{ac} = ExL/K$	1.143	1.134	1.179	1.178	1.160		793					
(N) PFE = (M-1)(10 <sup>2</sup> )	14.3	13.4	17.9	17.8	16.0							
(O) MCF = (M-1)(10 <sup>5</sup> )/H	136	125	228	252	298							

30 } 993  
10 }  
3 }

100 + 2 1.013

1 + 6 1.053

# HEINRICHS GEOEX. INDUCED POLARIZATION SECTIONAL DATA PLOT, LOOKING \_\_\_\_\_





623 0578



**HEINRICHS GEOEXPLORATION COMPANY**  
**INDUCED POLARIZATION SURVEY COMPUTATION SHEET**

Page \_\_\_\_\_

Project Big Jim Line 1 (500) Field date 8-22-64 Data page \_\_\_\_\_ Comp. date 8-22-64 Comp by KJPB

(A) Send	23	12	34	23	12	45	34	23	12	45	34	23
(B) Receive	125		235			345				455		
(C) n separation Range	100	10	100	80	10	100	30	10	3	30	10	3
(D) I	1600	800	2000	1601	800	2000		1600	800	2000		1600
(E) Vdc (avg)	75.0	13.75	128.5	24.0	7.32	29.8	28.1	6.83	2.43	17.7	9.90	3.29
(F) DCcal	980											
(G) Kn x 10 <sup>-3</sup>	1.5	6	1.5	6	15	1.5	6	15	30	6	15	30
(H) $\rho_{dc} = ExFxGx10^3/D$	68.8	101	94.5	88.3	135	58.6	82.6	62.7	89.5	52.1	72.7	60.5
(I) Vac $\Sigma$	67.0	12.30	117.0	21.4	6.58	74.0	25.4	6.30	2.28	16.6	9.10	3.07
(J) AC noise x 2												
(K) Vac (corr) = $\sqrt{I^2 - J^2}$												
(L) AC-DC cal.	1.013	993	1.013	993		1.013	993					
(M) $\rho_{dc}/\rho_{ac} = ExL/K$	1.134	1.124	1.112	1.113	1.106	1.093	1.099	1.075	1.068	1.060	1.079	1.065
(N) PFE = $(M-1)(10^2)$	13.4	12.4	11.2	11.3	10.6	9.3	9.9	7.5	6.8	6.0	7.9	6.5
(O) MCF = $(M-1)(10^5)/H$	195	123	119	128	78	158	120	119	76	115	110	107

Project \_\_\_\_\_ Line \_\_\_\_\_ Field date \_\_\_\_\_ Data page \_\_\_\_\_ Comp. date \_\_\_\_\_ Comp by \_\_\_\_\_

(A) Send	12	45	34	23	12		Cal					
(B) Receive		565										
(C) n separation	1	10	10	3	1							
(D) I	800	2000		1600	800							
(E) Vdc (avg)	13.7	6.72	5.52	2.31	1.08		30.6					
(F) DCcal												
(G) Kn x 10 <sup>-3</sup>	52.5	15	30	52.5	84							
(H) $\rho_{dc} = ExFxGx10^3/D$	88.3	50.1	81.3	74.3	111							
(I) Vac $\Sigma$	13.35	6.40	5.27	2.22	1.10		30.9					
(J) AC noise x 2												
(K) Vac (corr) = $\sqrt{I^2 - J^2}$												
(L) AC-DC cal.	1.043	993			1.043							
(M) $\rho_{dc}/\rho_{ac} = ExL/K$	1.063	1.043	1.041	1.034	1.024							
(N) PFE = $(M-1)(10^2)$	6.3	4.3	4.1	3.4	2.4							
(O) MCF = $(M-1)(10^5)/H$	76	86	49	46	22							

30  
10  
3 } .793

100 + 2% 1.013  
1 + 6% 1.043



# Inspiration Consolidated Copper Company

INSPIRATION, ARIZONA

September 23, 1964

Mr. Clyde W. Doran  
Supervisor, Coronado National Forest  
130 South Scott Street  
Tucson, Arizona



Dear Sir:

This is to inform you of the results obtained from a geophysical survey made on the Big Jim Claim in the Harshaw Mining District, Santa Cruz County, Arizona, and owned by Miss Virginia Hay, Patagonia, Arizona.

Actually, we have conducted two geophysical surveys which have been extended across the Big Jim Claim workings. In November, 1962, the Heinrichs Geoexploration Company of Tucson conducted a Jalander Hand Magnetometer Survey which crossed the Big Jim workings in a N 75° E direction. On the mine dumps at the shaft of the Big Jim location, the magnetometer showed a sharp narrow high of 1442 gammas as compared to a gamma value of -190 gammas, about 200 feet S 75° W of it, and a gamma value of -440 gammas about 200 feet N 75° E of it. A portion of the high reading may be due to artificial objects such as pipe or old mine rails, but it is believed that most of the high reading was due to magnetite occurring in association with other minerals in a vein which has been somewhat prospected and mined. In addition to this a second magnetic high was disclosed about 600 feet N 75° E of the Big Jim shaft which has a value of 70 gammas as compared to a low -310 gammas, 100 feet S 75° W and a low -400 gammas, 350 feet N 75° E of the high. This is possibly showing an anomalous zone east of the mine dump which to date has not been prospected.

For the year September, 1963, to September, 1964, the Inspiration Consolidated Copper Company employed the Heinrichs Geoexploration Company of Tucson to conduct a geophysical survey by the induced potential method. A Report of Geophysical Survey will be filed in the Santa Cruz County Recorder's Office as annual assessment work on our claims and Miss Virginia Hay's claim in that vicinity. The induced potential geophysical survey revealed an area of fairly strong anomalism indicating from 0.8 to 2.4% sulfides by volume from about 100 to 400 feet below surface. This anomaly begins at a point near the middle of the American Camp Claim about 600 ft. south of Miss Hay's house and extends northwest across the Big Jim shaft and claim and on to the northwest to beyond the north side line of the OCCI Claim Group.

These are essentially the findings of the geophysical survey relative to the Big Jim Claim. If there are more questions pertaining to this matter, I advise you to contact Mr. Walter E. Heinrichs or Grover Heinrichs of the Heinrichs Geoexploration Company in Tucson as they are much better qualified to answer your questions.

Thank you for your consideration of this matter.

Very truly yours,

*Hugh W. Olmstead*

Hugh W. Olmstead  
Mining Geologist

cc: Mr. E. F. Reed  
Mr. W. E. Heinrichs  
Miss Virginia Hay

C  
O  
P  
Y





HEINRICH'S GEOEXPLORATION COMPANY

806 WEST GRANT ROAD, TUCSON, ARIZONA, 85703. P.O. BOX 5671. PHONE: (AREA CODE 602) 623-0578

September 12, 1964

Mr. E. F. Reed, Chief Geologist  
Inspiration Consolidated Copper Co.  
Inspiration, Arizona

Dear Bert:

Enclosed is an original and two copies of the affidavit of labor <sup>(2 pages)</sup> and report of geophysical survey <sup>(3 pages)</sup> submitted for your approval and addition of the docket and page numbers of the recorded claim notices. Under separate cover are the two sectional data sheets and plan location map, one mylar of each and five black line prints of each. You may wish to edit out some of the interpretational reference anomalism on material to be recorded.

The report of geophysical survey is quite brief and therefore we will mention certain points in this letter to clarify matters. The most interesting anomalism noted on this survey is from 3.5NW to the NW end of the line and perhaps further. The anomalism indicates from 1.5 to 4.0% sulfides by volume and could be economically significant. Since this anomalism is off the claim group, no specific mention was made in the report of geophysical survey. On your property, however, from 1.0SE to 3.5NW there is fairly strong anomalism indicating from 0.8 to 2.4% sulfides by volume from about 100 to 400 feet below surface. The sulfide percentage apparently diminishes rapidly below 400 ft. Also, no anomalism was found to be directly related to the Big Jim workings. The anomalism appears to be due to disseminated sulfides rather than discrete bodies and veins.

In our opinion, this area may deserve more detail and geology as well as further I. P. coverage of both detailed and reconnaissance nature in order to make a valid economic appraisal. Geochemical assaying may also prove useful in

Mr. E. F. Reed

- 2 -

September 12, 1964

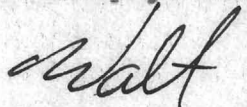
outlining the more copper rich areas.

We trust you will find all in order.

Sincere regards,

HEINRICHS GEOEXPLORATION CO.

Chris S. Ludwig  
Sr. Geophysicist



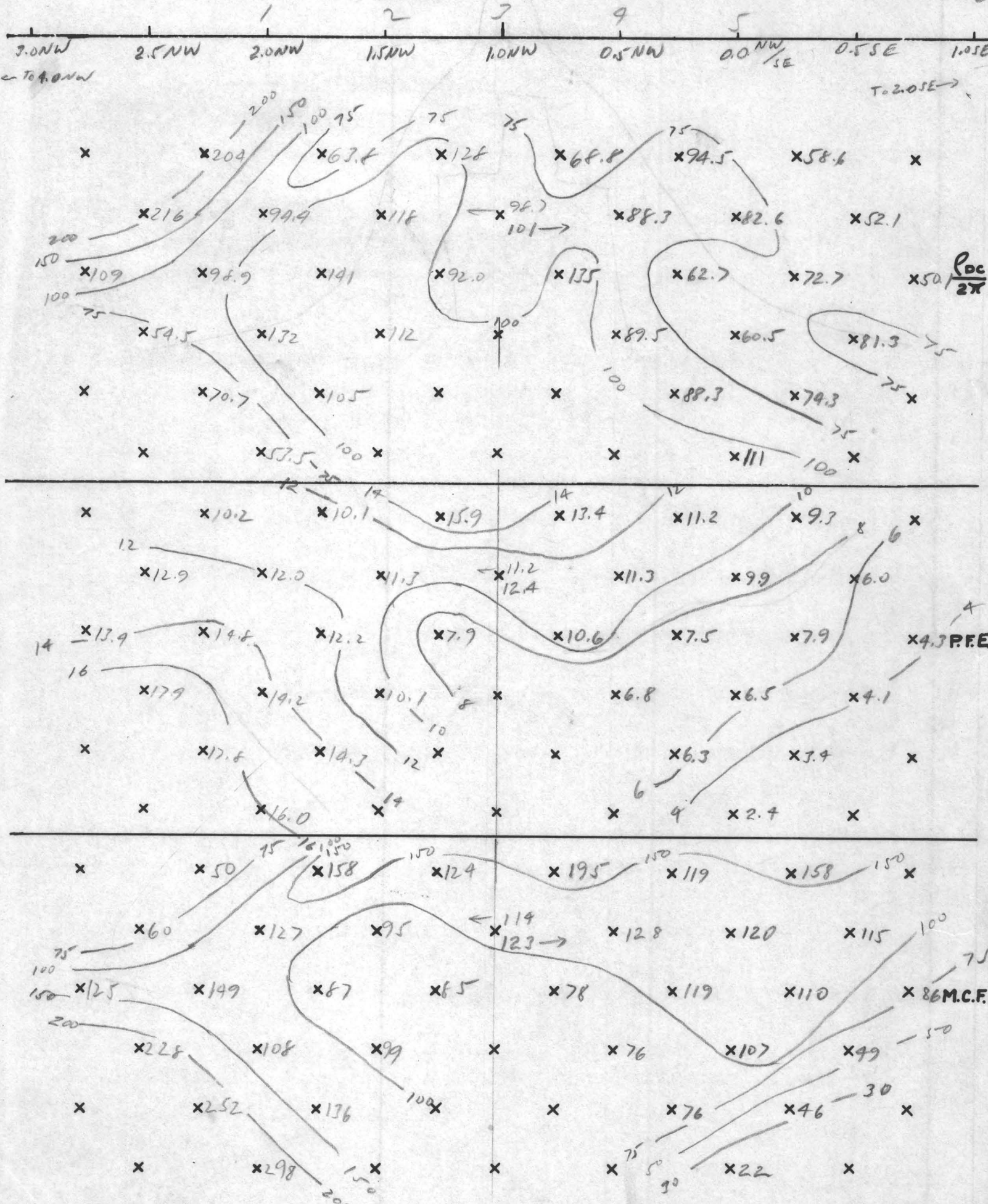
Walter E. Heinrichs, Jr.  
President & General Manager

CSL/WEH/jh

cc: Extra Encl.



# HEINRICHS GEOEX. INDUCED POLARIZATION SECTIONAL DATA PLOT, LOOKING Northeast

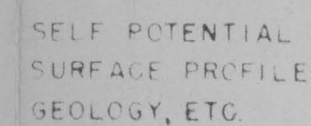
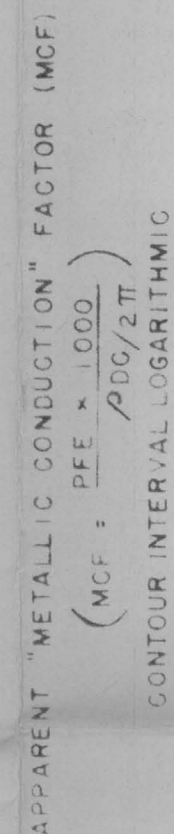
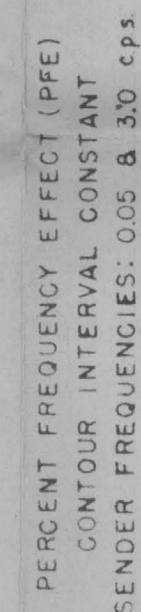
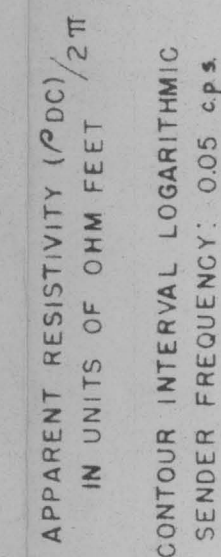


[illegible]





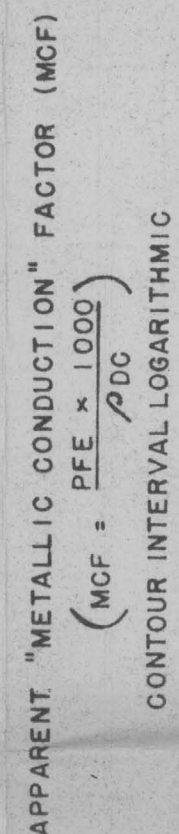
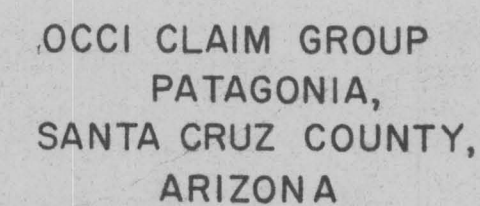
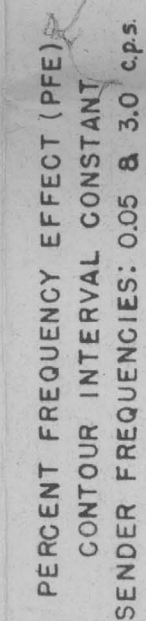
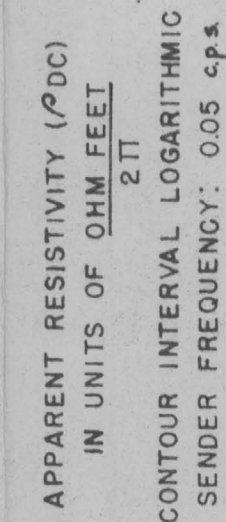




FOR  
INSPIRATION CON. COPPER CO.

LOOKING      NORTHEASTERLY





LOOKING NORTHEASTERLY

SELF POTENTIAL  
SURFACE PROFILE  
GEOLOGY, ETC.

HEINRICH'S GEOEXPLORATION COMPANY  
SCALE: 1"=1000'      DATE: AUG. 1964