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HEINRICHS GEOEXPLORATION COMPANY

806 WEST GRANT ROAD, TUCSON, ARIZONA, 85703. P.O. BOX 5671. PHONE: (AREA CODE 602) 623-0578

November 30, 1966

Mr. Woodrow Mullin
Box 455
Turkey, Texas

Dear Mr. Mullin:

As per your request in our discussions in our office between John Langs and E. Grover Heinrichs and Mr. Molloy on November 16, 1966, the following proposals are suggested to best evaluate the water potential on your property on the Pierce Area, Arizona.

From the well data given on wells 1 through 4 drilled in Section 15, T17S, R25E, the apparent subsurface structure is a generally north trending trough, as shown on the enclosed cross section. However, the strike of this trough may be concordant with major northwest trending structure in the area. The water table dips to the north indicating subsurface flow in this direction. The maximum production out of well #1 shows the relationship between increased depth of alluvium and corresponding thickness of water zone and increased rate of production.

Improved water production is related to locating increased depth to bedrock and corresponding head.

The following methods of exploration are recommended and presented for consideration. Proposed lines are shown on the enclosed plan view of Section 15.

1. Gravity is the first choice and would give the most accurate picture of the subsurface bedrock topography. A minimum of 9 line miles, at $150.00/mile with a $1,000.00 minimum fee, is recommended if this method is used.

2. Resistivity is second choice, and should give a good indication of bedrock topography and possible depth to

water table. Three line miles, at $500.00/mile is recommended if this method is used.

3. Magnetics is third and would give a general indication of the shape of the trough. This method will not give as good information as gravity or probably resistivity, but it may show the location of thickest alluvium. Nine miles at $50.00/mile is recommended if this method is used.

For increased effectiveness, a combination of two or all three of the above methods should be considered.

Respectfully submitted,

HEINRICHS GEOEXPLORATION COMPANY

John McDonnell

John McDonnell
Geologist

APPROVED: _____
Walter E. Heinrichs, Jr.

Registered Professional Engineer (Mining) CERTIFICATE EXPIRES WALTER E. HEINRICHS JR. DEC. 31, 1966 ARIZONA, U.S.A.

Gravity Survey for Mullen + Molloy

12/15/66

P6

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STA.	TIME	READ.		LOOP DRIFT	O.A DRIFT	
S31	—	1416.1	+4	0	-5.9	1409.7
S32	—	1416.6	+4	0		1410.2
S33	—	1416.7	+4	0		1410.3
S34	—	1416.8	+4	0		1410.4
S35	11:27	1416.1	+4	0		1409.7
S30	11:32	1416.3	+4	0		1409.9
S-1	11:46	1365.7	+4	0		1358.7
S108	11:49	1364.4	+5	0		1357.0
S109	—	1360.6	+5	+0.1		1353.7
S110	—	1357.3	+5	+0.1		1350.4
S111	—	1354.8	+5	+0.2		1347.5
S112	—	1352.3	+5	+0.2	-6.0	1345.5
S113	12:00	1350.7	+5	+0.3		1344.0
S-1	12:04	1365.4	+5	+0.3		1358.7
S113	12:08	1350.7	+5	0		1344.0
S114	—	1349.7	+6	0		1343.1
S115	—	1348.9	+6	0		1342.3
S116	—	1348.5	+6	+0.1		1341.9
S117	—	1348.5	+6	+0.1		1341.9
S118	—	1349.1	+6	+0.1		1342.6
S119	12:22	1348.7	+6	+0.2		1342.2
S113	12:26	1350.5	+7	+0.2		1344.0
S119	12:30	1348.7	+7	0		1342.2
S120	—	1348.4	+7	0		1341.9
S121	—	1347.4	+7	0		1340.9
S122	—	1346.5	+7	-0.1		1339.9
S123	—	1345.7	+7	-0.1		1339.1
124	12:40	1344.1	+7	-0.2		1337.4
119	12:44	1348.9	+7	-0.2		1342.2
BASE	12:51	1407.8		—	-6.0	1401.8

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12/14/66
P.4

Gravity Survey For Mullen + Molloy

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Sta	Time	Read	Loop Drift	O.A Drift	
S89	1:52	1417.3	+0.2 -2.1	-2.9	1415.2
S84	1:55	1412.9	0 1.6	-2.9	1410.3
S83	-58	1411.8	0 1.6	-3.0	1410.2
S82	-02	1410.9	-0.1 1.6	-3.1	1409.3
S81	-05	1410.5	-0.1 1.6	-3.1	1408.9
S80	-10	1409.5	-0.2 1.6	-3.2	1407.9
S79	2:15	1410.0	-0.2 1.5	-3.3	1409.5
S78	2:19	1409.7	-0.3 1.5	-3.3	1408.2
S84	2:28	1412.7	-0.3 1.4	-3.4	1410.3
S78	—	1410.0	0 (-1.8)	-3.5	1408.2
S77	—	1409.1	-0.1 1.1	-3.5	1407.3
76	—	1408.3	-0.2 1.9	-3.6	1406.4
75	—	1406.8	-0.2 1.0	-3.7	1405.8
74	—	1405.4	-0.3 1.0	-3.7	1404.4
73	—	1403.3	-0.3 1.1	-3.8	1402.2
72	—	1400.4	-0.4 1.1	-3.9	1397.3
S78	3:15	1410.4	-0.4 2.2	-3.9	1408.2
BASE	3:30	1405.8	-4.0	-4.0	1401.8
S1	3:35	1362.7	0 -4	-4.0	1358.7
S2	—	1365.6	0 .1	-4.0	1361.6
S3	—	1371.0	0 .1	-4.1	1367.0
S4	—	1374.7	0 .1	-4.1	1370.6
S5	—	1379.0	-0.1 .1	-4.1	1373.9
S6	3:48	1381.8	-0.1 .1	-4.2	1377.7
S1	3:52	1362.8	-0.1 4.2	-4.2	1358.7
S6	3:55	1381.9	0 4.2	-4.2	1377.7
S7	—	1386.0	-0.1 4.2	-4.3	1381.8
S8	—	1389.0	-0.2 4.2	-4.3	1384.6
S9	—	1390.9	-0.3 4.4	-4.3	1386.5
S10	—	1393.5	-0.4 4.5	-4.4	1388.9

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Gravity Survey For Mullen & Molloy

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STA.	TIME	READ	LOOP DRIFT	O.A. DRIFT	
S-11	4.07	1395.7	-0.5	-4.4	1391.1
S-6	4.10	1382.4	-0.5	-4.5	1377.7
BASE	4:18	1406.3	-4.5	-4.5	1401.8
BASE	9:20	1407.6	-5.8	-5.8	1401.8
S11	9:27	1397.5	0	5.8	1391.7
S12	—	1399.6	0	5.8	1393.8
S13	—	1400.3	0	5.9	1394.4
S14	—	1401.8	-0.5	5.9	1395.9
S15	—	1402.6	-0.1	5.9	1396.7
S16	9:40	1403.5	-0.1	6.0	1397.5
S17	—	1404.9	-0.2	6.0	1398.5
S18	9:46	1405.0	-0.2	6.0	1399.0
S11	9:50	1397.7	-0.2	6.0	1391.7
S18	9:55	1405.1	0	6.1	1399.0
S19	—	1405.3	0	6.1	1399.2
S20	—	1406.4	0	6.1	1400.3
S21	—	1406.4	0	6.1	1400.3
S22	—	1406.6	+0.1	6.2	1400.4
S23	—	1408.1	-0.1	6.2	1401.9
S24	10:12	1409.5	-0.1	6.2	1403.3
S18	10:24	1405.2	0	6.2	1399.0
S24		1409.5	0	6.2	1403.3
S25		1410.0	0	6.2	1403.8
S26		1411.6	0	6.2	1405.4
S27		1413.2	0	6.2 5.9	1407.0
S28		1414.2	+0.1	6.2	1408
S29		1414.2	+0.1	6.1	1408.1
S30		1416.0	+0.1	6.1	1409.9
S24	11:06	1409.4	+0.1	6.1	1403.3
S30	11:13	1416.3	0	6.4	1409.9

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Gravity Survey For Mullen + Molloy

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			Loop Drift	O.A. Drift	
S104	2.34	1418.4	-0.2	-1.2	1417.6
BASE	3.00	1403.0	-1.2	-1.2	1401.8
BASE	9.00	1405.4	-3.6	-3.6	1401.8
S 54	—	1389.5	-3.6	-3.6	1385.9
S 55	—	1392.4	+0.1 -3.5	-3.6	1388.9
S 56	—	1395.6	+0.2 -3.5	-3.5	1392.1
S 57	—	1397.8	+0.2 -3.4	-3.5	1394.4
S 58	9.10	1400.8	+0.3 -3.4	-3.5	1397.4
S 54	9.15	1389.2	+0.3 -3.3	-3.5	1385.9
S 58	9.20	1400.8	0 -3.4	-3.4	1397.4
59	—	1401.7	+0.1 -3.3	-3.4	1398.4
60	—	missing	+0.2 -3.2	-3.4	—
61	—	1404.9	+0.3 -3.1	-3.4	1401.8
62	—	1406.1	+0.4 -3.0	-3.3	1403.1
63	9.33	1407.2	+0.5 -2.8	-3.3	1404.3
58	9.38	1400.1	+0.7 -2.7	-3.3	1397.4
63	9.43	1407.3	0 -3.0	-3.3	1404.3
64	46	Missing	0 -3.0	-3.2	—
65	49	1408.5	0 -3.0	-3.2	1405.5
66	52	1408.4	0 -3.0	-3.2	1405.4
67	54	1409.0	+0.1 -2.9	-3.2	1406.1
68	9.56	1409.6	+0.1 -2.9	-3.1	1406.7
63	10.01	1407.2	+0.1 -2.9	-3.1	1404.3
68	10.07	1409.2	0 -2.5	-3.1	1406.7
69	14	1410.3	0 -2.5	-3.1	1407.8
70	20	1411.0	0 -2.5	-3.0	1408.5
71	27	1411.4	-0.1 -2.6	-3.0	1408.8
53	33	1407.9	-0.1 -2.6	-3.0	1405.3
68	10.39	1409.3	+0.1 -2.6	-3.0	1406.7
53	10.52	1407.6	0 -2.3	-2.9	1405.3

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Gravity Survey for Mullin & Molloy

Starting at NW corner of Sec 15 heading East.

Sta	Time	Read		LOOP DRIFT	O.A. DRIFT	
Base	12.15	1401.8		0	0	1401.8
S90	12.20	1403.7		0	0	1403.7
S91	12.23	1405.5		0	-0.1	1405.5
S92	12.26	1407.4		+0.1	-0.1	1407.5
S93	12.31	1408.6		+0.1	-0.2	1408.7
S94	12.36	1409.2		+0.2	-0.2	1409.4*
Base	12.40	1401.6		+0.2	-0.3	1401.8
S94	12.50	1409.1	1409.4	+0.3	-0.3	1409.4*
S95		1410.0		0 +0.3	-0.4	1410.3
S96		1410.5		0 +0.2	-0.4	1410.7
S97		1411.7		-0.1 +0.2	-0.5	1411.9
98		1412.5		-0.2 +0.1	-0.5	1412.6
99	1.09	1413.5		-0.2 +0.1	-0.6	1413.6*
94	1.17	1409.4		-0.3 0.0	-0.6	1409.4*
99	1.27	1413.5		0 +0.1	-0.7	1413.6*
100		1414.0		-0.1 +0.1	-0.7	1414.1
101		1414.2		-0.1 0.0	-0.8	1414.2
102		1414.7		-0.1 0.0	-0.8	1414.7
103		1416.3		-0.2 0.0	-0.9	1416.3
104	1.45	1417.6		-0.2 0.0	-0.9	1417.6*
99	1.54	1413.7		-0.2 -0.1	-0.9	1413.6*
104	2.02	1418.2		0 -0.6	-1.0	1417.6*
105	2.06	1417.3		0 -0.6	-1.0	1416.7
106	2.10	1419.3		-0.1 -0.7	-1.1	1418.6
107	2.15	1419.4		+0.1 -0.7	-1.1	1418.7
42 S89	2.29	1414.8		-0.2 -0.8	-1.2	1414.0
S104	2.34	1418.4		-0.8		1417.6*

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Gravity Survey for Mullen & Malloy

STA.	TIME	READ	LOOP DRIFT	O.A DRIFT	
S52	—	1406.5	0 -2.3	-2.9	1404.2
S51		1405.9	0 -2.3	-2.9	1403.6
S50	11:02	1405.3	0 -2.3	-2.9	1403.0
S49		1404.2	0 -2.3	-2.8	1402.9
S48		1403.9	-0.1 -2.4	-2.8	1401.5
S47		1402.9	-0.1 -2.4	-2.8	1400.5
S46		1402.0	-0.1 -2.4	-2.8	1399.7
S53	11.25	1407.7	-0.1 -2.4	-2.7	1405.3
S46	11.35	1401.8	0 -2.2	-2.7	1399.6
S45	-42	1400.6	+0.1 -2.1	-2.7	1398.5
S44	-.66	1398.8	+0.2 -2.0	-2.7	1396.8
S43	-.67	1397.2	+0.3 -2.6	-2.6	1395.2
S42	-.51	1395.3	+0.3 +1.9	-2.6	1393.4
S46	11.55	1401.4	+0.4 +4.8	-2.6	1399.6
42	11.58	1395.3	0 -1.9	-2.6	1393.4
41	-.60	1392.1	0 -1.9	-2.5	1390.2
40	-.73	1389.0	+0.1 -1.8	-2.5	1387.2
39	-.95	1385.7	+0.1 -1.8	-2.5	1383.9
38	-.8	1382.5	+0.2 -1.7	-2.5	1380.8
37	-.71	1378.4	+0.2 -1.7	-2.4	1376.7
36	12.15	1373.6	+0.3 -1.6	-2.4	1372.0
42	12.20	1395.0	+0.3 -1.6	-2.4	1393.4
BASE	12.28	1404.2	—2.4	-2.4	1401.8
BASE	1.09	1404.2	—2.4	-2.4	1401.8
S89	1.22	1417.5	0 -2.3	-2.5	1415.2
S88	—	1415.5	0 -2.3	-2.5	1413.2
S87	—	1414.8	+0.1 -2.2	-2.6	1412.4
S86		1413.9	+0.1 -2.2	-2.7	1411.7
S85		1413.5	+0.1 -2.2	-2.7	1411.3
S84		1412.4	+0.2 -2.1	-2.8	1410.3

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GRAVITY SURVEY

IN THE

PEARCE AREA, COCHISE COUNTY, ARIZONA

For

Mr. Woodrow Mullin

December 1966

By

Heinrichs Geoexploration Company
P.O. Box 5671 Tucson, Arizona 85703
Phone: 623-0578 Area Code: 602

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IN MAP POCKET: (1 Piece)	
Bouguer Gravity Contour Plan	

INTRODUCTION

As a result of a letter to Mr. Mullin dated November 30, 1966 from Heinrichs Geoexploration Company which outlined methods of exploration to evaluate water potential in Section 15, T17S, R25E, in Cochise County, near Pearce, Arizona, a telephone conversation was held December 6, 1966 between Mr. Woodrow Mullin and John W. Langs of Geoex. It was decided that Geoex would conduct a preliminary semi reconnaissance-semi detailed gravity survey consisting of five lines totaling seven line miles. Mr. Roy Molloy of Cochise, Arizona would conduct the level survey and locate stations as directed by Geoex.

Other Geoex personnel involved were R. E. Palmer, field party chief, and M. J. Fraker, field assistant, interpretation by Chris S. Ludwig, senior geophysicist, and report by John McDonnell, geologist.

A gravity contour and interpretation plan at a scale of one inch to 500 feet with a contour interval of 0.25 milligals is included in the report.

PROCEDURE

The topographic level survey conducted by Roy Molloy consisted of 124 stations with a 300 foot station spacing on five E-W lines. Of these lines the southern-most was three miles in length, and the other four were one mile in length. Lines were located 1/4 mile apart.

A Texas Instruments gravity meter with a scale constant of 0.09640 milligals per scale division was used. Maximum observed instrumental drift was 0.67 milligals and all drifts were loop corrected. The combined Bouguer and free air correction factor was 0.06854 milligals per foot with an inferred alluvial density of 2.0 g/cc. The latitude correction factor was 1.175 milligals per mile.

INTERPRETATION, CONCLUSIONS, AND RECOMMENDATIONS

Gravity values in the area increase to the east from the west boundary of Section 15 showing a decrease in depth to bedrock to the east. The least gravity value (and therefore, approximate location of probable thickest alluvium) in the entire survey is on the south boundary of Section 16 at Station 113. A channel trending NW across Section 15 from the SW quarter is indicated.

If Section 16 is available, the most favorable location according to the entire survey, is in the vicinity of Station 113, with an inferred depth of about 740 feet to bedrock. The depth increase over well #1 is about 110 feet giving a probable head of approximately 410 feet. This location is marked on the map as proposed well site #1.

The most favorable water well location in Section 15, from the standpoint of the gravity results is in the SW corner of the section. Inferred depth to bedrock here is about 690 feet with an increase of about 60 feet over depth to bedrock in your well #1. Probable head should be around 330 feet. This location is marked on the map as proposed well site #2. Another low point is noted in the NW corner of Section 15. Inferred depth to bedrock there is approximately 550 feet. Assuming relatively uniform character of the alluvial sediments, a well in this location would probably give less production than well #1 because of less head. This location is marked on the map as proposed well site 3.

Should Section 16 be available, two additional line miles of gravity survey are recommended to define the suggested trough-like feature between Stations 112 and 114. The two lines should be run E-W with 300 foot spacings between stations. One line should be run 1/2 mile north of the south boundary of the section and the other across the north boundary of the section.

Because of the proximity of existing well #1 to this proposed well site, cost of drilling versus increased production should be considered. A 50% increase over well #1 would give

about 1700 gallons per minute. This increase is calculated on the basis of increased depth alone with no consideration of lateral feed from the deeper area to the west. Dual production from the proposed well and well #1 versus shutdown of well #1 should be considered. Drawdown from the proposed well could decrease production from well #1 to make its shut-down necessary.

From the data presently available, 2,000 gallons per minute does not appear likely from a single well in Section 15. A combined production from the proposed well and other wells on the section could give equivalent production.

The NW-SE trending buried bedrock stream channel through Section 15 could be water bearing, but with a limited head, and is not recommended for testing at this time.

Respectfully submitted,

HEINRICHS GEOEXPLORATION COMPANY

John McDonnell

John McDonnell
Geologist

APPROVED: _____
Walter E. Heinrichs, Jr.

Registered Professional Engineer (Mining) CERTIFICATE EXPIRES WALTER E. HEINRICHS JR. DEC. 31, 19 67 ARIZONA, U.S.A.

Tucson, Arizona
January 4, 1966

SECTION 16

SECTION 15

SECTION 14

SECTION 21

SECTION 22

SECTION 23

T 17 S

R 25 E

POSSIBLE BEST WATER PRODUCTION ZONE (BURIED BEDROCK STREAM CHANNEL ABOUT 700' BELOW SURFACE)

BURIED BEDROCK STREAM CHANNEL ?

1 @ (740' ± 50')

2 @ (690' ± 50')

3 @ (550' ± 75')

1 @ (740' ± 50') PROPOSED WELL SITE (AND PROBABLE DEPTH TO BEDROCK)

① EXISTING WELLS

S 48 • GRAVITY STATION

• 40.66 GRAVITY VALUE IN MILLIGALS

SECTION CORNER

PEARCE AREA
COCHISE COUNTY, ARIZONA

CONTOUR INTERVAL = 0.25 MILLIGALS

HEINRICHS GEOEXPLORATION CO.
POST OFFICE BOX 5671 TUCSON, ARIZONA 85703

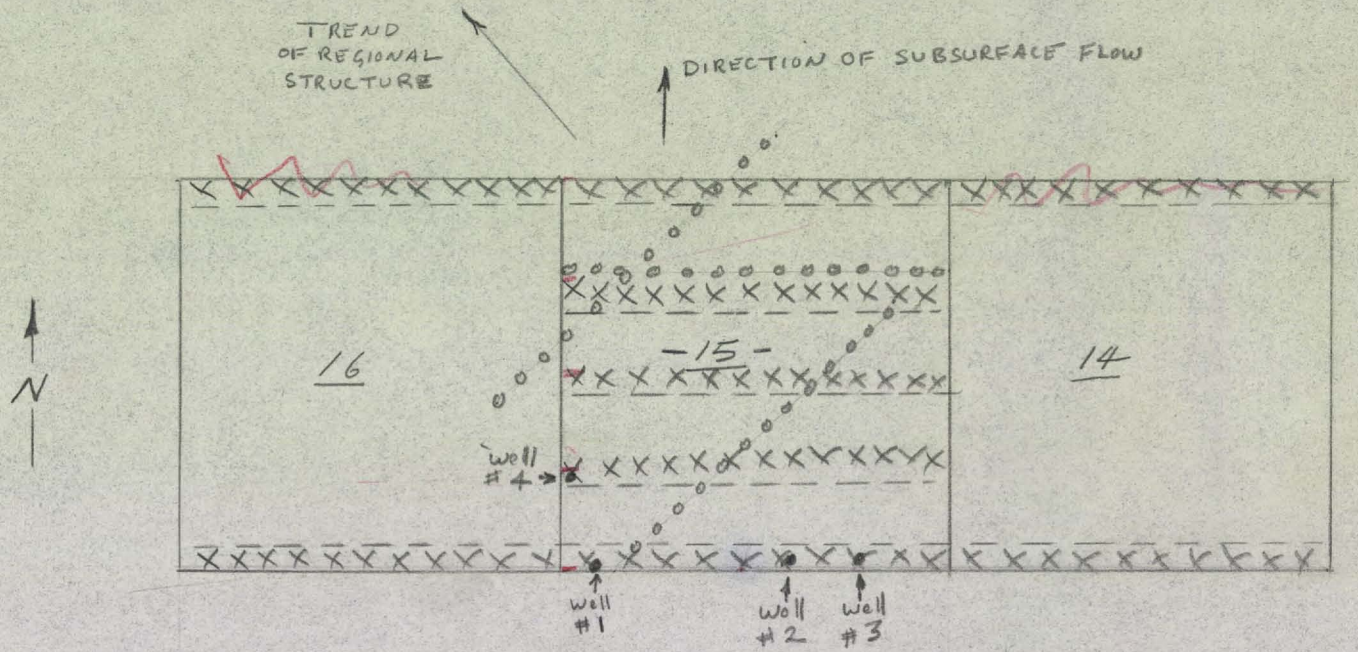
BOUGUER GRAVITY
CONTOUR PLAN
FOR
MULLIN & MOLLOY

Scale 1" = 500' | Date DEC. 1966

T17S, R25E

LOCATIONS OF RECOMMENDED LINES

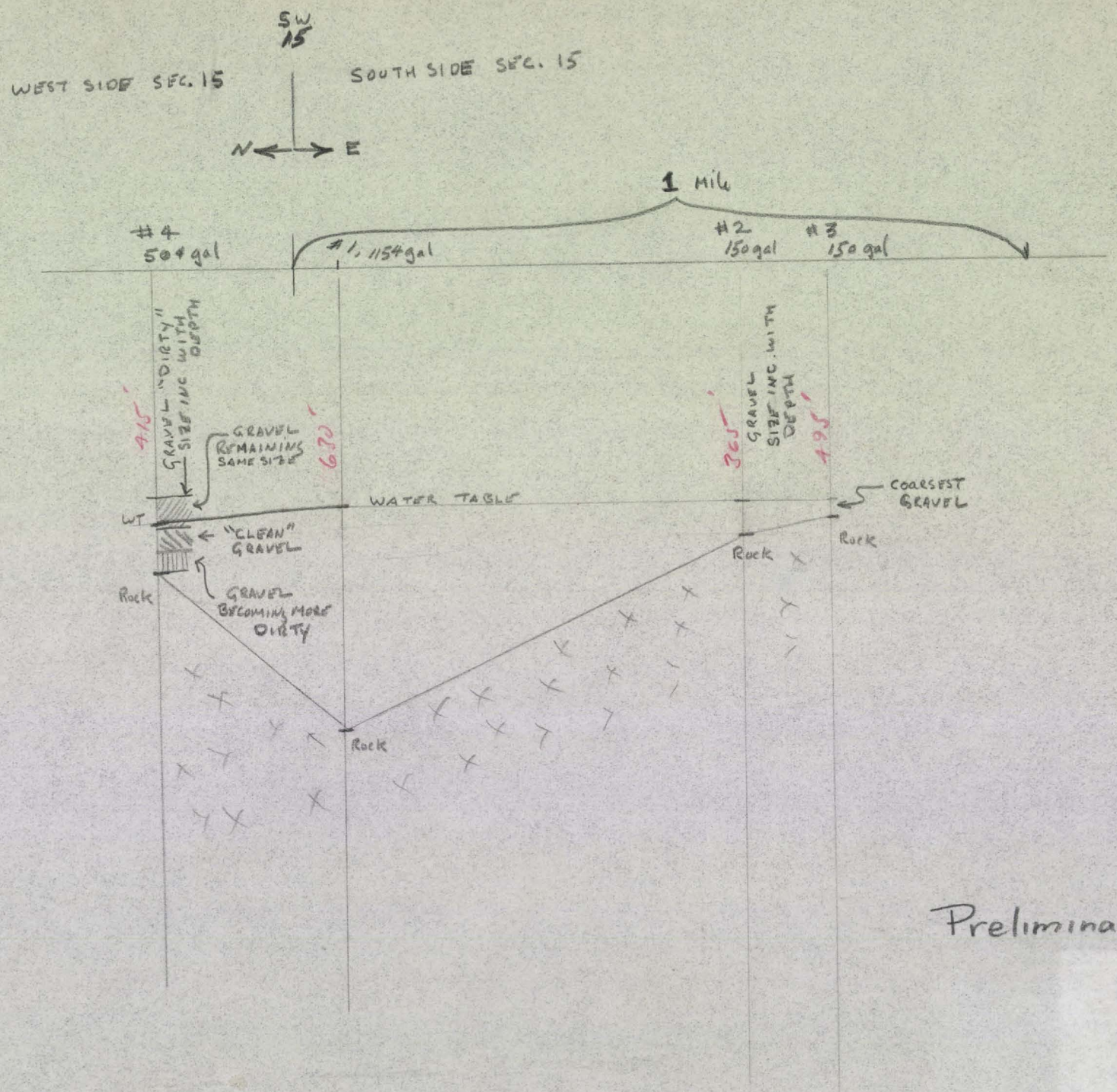
1) GRAVITY ××××
2) RESISTIVITY o o o o
3) MAGNETICS — — — —



DATE: 11-30-66

Preliminary SKETCH

T17S, R25E



Preliminary Sketch

DATE: 11-30-66
VERTICAL SCALE 1" = ~~50'~~ 200'
HORIZONTAL SCALE 5" = 1 MILE

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(1) Sta	(1) Corrected Reading	(2) Correction gal (1) x 0.0964 (in mgal)	(3) Mile N. correct = Miles x 1.175 (in mgal) (Mile)	(4) Elevations	(5) Combined free air, Bouguer correction (4) x 0.06854	(6) Bouguer gravity (2) - (3) + (5)
1	13587	13098	0 0	100 -	6 85	137 83
2	13616	13126		99 72	6 83	138 09
3	13670	13178		98 58	6 76	138 54
4	13706	13213		97 32	6 67	138 80
5	13739	13244		96 71	6 63	139 07
6	13777	13281		97 32	6 67	139 48
7	13818	13321		94 31	6 46	139 67
8	13846	13347		93 91	6 44	139 91
9	13855	13356		93 33	6 40	139 96
10	13889	13388		92 54	6 34	140 22
11	13917	13416		92 12	6 31	140 47
12	13938	13436	0	91 32	6 26	140 62
13	13944	13442		90 70	6 21	140 63
14	13959	13456		89 64	6 14	140 70
15	13967	13464		90 0	6 17	140 81
16	13975	13472		89 67	6 15	140 87
17	13985	13482		89 02	6 10	140 92
18	13990	13486		89 84	6 15	141 01
19	13992	13488		88 98	6 10	140 98
20	14003	13498		87 85	6 02	141.00

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Sta	Corrected ① Reading	Correct mgal ② ① x 0.0964	③ Mile N. corr. mile x 1.175 (Mile)		④ Elevations	⑤ combined Bouguer correction ④ x 0.06854	⑥ Bouguer gravity
21	14003	13498	0	0	8782	602	14100
22	14004	13498			8771	601	14099
23	14019	13514			8649	593	14107
24	14033	13528			8677	595	14123
25	14038	13533			855	586	14119
26	14054	13548			856	587	14135
27	14070	13563			847	581	14144
28	14080	13573			8498	582	14155
29	14081	13574			8511	583	14157
30	14099	13591			8327	571	14162
31	14097	13590			840	576	14166
32	14102	13594			8465	580	14174
33	14103	13595			8549	586	14181
34	14104	13596			8614	590	14186
35	14097	13590	0	0	8817	604	14194
36	13720	13226	.25	29	9547	654	13851
37	13767	13271		29	9402	644	13886
? 38	13808	13311		29	9291	637	13919
39	13839	13341		29	9209	631	13943
40	13872	13373		29	9137	626	13970

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Sta	Correct Read (1)	(2) Corr. at magnet = (1) x .0964	(3) Mile N. correct = Mile x 1.175 (mile)	Elevations	(5) Combined free air Bouguer correction (4) x 0.06854	(6) Bouguer gravity
41	13902	13402	.25 29	9086	623	139.96
42	13934	13432	29	8920	611	140 14
43	13952	13450	29	8869	608	140 29
44	13968	13465	29	8848	606	140 42
45	13985	13482	29	8747	600	140 53
46	13996	13492	29	8741	599	140 62
47	14005	13501	29	8828	605	140 77
48	14015	13510	.25 29	8673	594	140 75
49	14019	13514	29	8649	593	140 78
50	14030	13525	29	8602	590	140 86
51	14036	13531	29	8668	594	140 96
52	14042	13536	29	8638	592	140 99
53	14053	13547	29	8553	586	141 04
54	13859	13360	.50 59	8764	601	139 02
55	13889	13389	59	~~9711~~ ?87.11	597	139 27
56	13921	13420	59	8803	603	139 64
57	13944	13442	59	8736	599	139 82
58	13974	13471	59	8686	595	140 07
59	13984	13481	59	8628	591	140 13
60	—	—	—	8593	589	—

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Stem	① correct Reading	② Correct angle ① x 0.0964	③ mile N. Correct = Mile N x 6175 (Mile)	Elevations	⑤ combined free air Bouguer correction ④ x 0.06854	⑥ Bouguer gravity
	°	°	°			
C1	14018	13513	.5 59	8407	576	140.3
C2	14031	13526	59	8306	569	140.36
C3	14043	13537	59	8288	568	140.46
C4	—	—	—	8250	565	—
C5	14055	13549	59	8209	563	140.53
C6	14054	13548	59	824	565	140.54
C7	14061	13555	59	8205	562	140.58
C8	14067	13561	59	8150	559	140.61
C9	14078	13571	59	8076	554	140.66
D0	14085	13578	59	7977	547	140.66
D1	14088	13581	59	7944	544	140.66
D2	13993	13489	.75 88	8149	559	139.60
D3	14022	13517	88	8035	551	139.80
D4	14044	13538	88	8011	549	139.99
D5	14058	13552	88	7952	545	140.09
D6	14064	13558	88	7897	540	1401
D7	14073	13566	88	7875	540	140.18
D8	14082	13575	88	7870	539	140.26
D9	14095	13588	88	7863	540	140.4
80	14079	13572	88	7851	538	140.22

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Sta	(1) correct Reading	(2) correct mgal = (1) × 0.0964	(3) M.G.N correct = M.G. + 1.175 (M.G.)	Elevations	(5) Combined free air, Bouguer correction (6) × 0.06854	(6) Bouguer gravity
81	14089	13582	88	7747	531	14025
82	14093	13586	88	7742	531	14029
83	14102	13594	88	7723	529	14035
84	14103	13595	88	7683	527	14034
85	14113	13605	88	7625	523	14040
86	14117	13609	88	7687	527	14048
87	14126	13617	88	7616	522	14051
88	14132	13623	88	7481	513	14048
89	14152	13643	88	7304	501	14056
90	14037	13532	1175	7472	512	13926
91	14055	13549	1175	7417	508	13939
92	14075	13568	1175	7452	511	13961
93	14087	13580	1175	7472	512	13974
94	14094	13587	1175	7448	510	13977
95	14103	13595	1175	7427	509	13986
96	14107	13599	1175	7445	510	13991
97	14119	13611	1175	7451	511	14004
98	14126	13617	1175	7375	505	14009
99	14136	13627	1175	7347	504	14013
100	14141	13632	1175	7328	502	14016

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Sta.	(1) Correct Ready	(2) Correct mgal = (1) x 0.0964	(3) M.L.N. correction = M.L. x 1.175 (M.L.)	(4) Elevations	(5) combined free air Bouguer correction (4) x 0.06854	(6) Bouguer gravity
101	1414 2	136 33	10 1175	73 19	5 02	140 17
102	1414 7	136 38	1175	73 28	5 02	140 22
103	1416 3	136 53	1175	71 02	4 87	140 22
104	1417 6	136 66	1175	69 65	4 77	140 25
105	1416 7	136 57	1175	70 89	4 86	140 25
106	1418 6	136 75	1175	69 37	4 75	140 32
107	1418 7	136 76	1175	69 39	4 76	140 34
108	1357 0	130 81	0	100 4	6 88	137 69
109	1353 7	130 50		102 87	7 05	137 55
110	1350 4	130 18		105 14	7 21	137 39
111	1347 5	129 90		108 94	7 47	137 37
112	1345 5	129 71		109 72	7 52	137 23
113	1344 0	129 56		111 73	7 66	137 22
114	1343 0	129 47		113 23	7 76	137 23
115	1342 3	129 40		115 42	7 91	137 31
116	1341 9	129 36		117 49	8 05	137 41
117	1341 9	129 36		117 99	8 09	137 45
118	1342 6	129 43		118 43	8 12	137 55
119	1342 2	129 39		118 75	8 14	137 53
120	1341 9	129 36		121 01	8 29	137 55

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Sta	(1) Correct Road	(2) Correct mgc (1) x 0.0964	(3) Mile N correction (mile); M x 1.125	(4) Elevations	(5) Combined Sea Ale, Bouguer correction (4) x 0.06854	(6) Bouguer gravity
121	13409	12926	0	12189	835	13761
122	13399	12917		12325	845	13762
123	13391	12909		12467	854	13763
124	13374	12892		12719	871	13764