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Dec. 9, 1975

Lunch with W. Pettijohn, Parsons, Jordan-Rep. and director of Hecla. Following information re: Lakeshore Mine.

- 1. Expect full production end of second quarter 1976-positive cash flow third quarter 1976 with increased price for copper.
- 2. Oxide ore leaching is in stream with purchased acid and scrap iron. Flotation plant is working and stacking concentrates.
- 3. Cathodes are under contract to Southwire, but he does not know grade. Probably will go thru Southwire furnace and refinery in Georgia.
- 4. Roaster has not yet run-neither acid plant which is "Lurgi" design and construction. Questionable?
- 5. Reduction of iron oxide has not yet run—also Lurgi design and built. Similar operation at Falconbridge in Canada failed miserably.
- 6. Including \$15 million working capitol, El Paso has guaranteed \$196 million into the project.
- 7. Pettijohn will arrange technical visit for us.
- 8. The banks have been very cooperative in forwarding operating expenses to Hecla, according to Bill Pettijohn.

AL

Mr. William A. Griffith Research Director Hecla Mining Company Wallace, Idaho 83873

Dear Bill:

This confirms our discussion in Denver on April 22, 1970, and subsequent telephone conversations.

Essex is interested in participating in the Lakeshore Project and would be willing to explore a wide range of mutual programs with Hecla. The possibilities include the following:

- 1. Essex would join with Hecla (and El Paso) in the Lakeshore Project sharing the investment, participating in the revenue and being entitled to an equitable share of the product.
- 2. Essex would participate with Hecla to the extent of funding the concentrate processing plant which at this point it is estimated would require \$25,000,000. This would still provide for Hecla managing the plant as an integral part of the total operation. Essex would have first call on Hecla's share of the output at a price providing a reasonable return on the investment.
- 3. Essex would contract to buy and Hecla to sell all or part of Hecla's share of the copper production on a long term basis. The intent of the contract would be to give Hecla some benefits of the current pricing yet offer long term market security. It was recognized that the quality of electrowon cathodes is not comparable to electrolytic cathodes, thus, a formula for pricing would need to reflect this differential. A minimum quality would be stipulated in a specification.
- 4. Essex would contract for production as in Item 3 above but payment would be in advance to provide capital. Payment would be against delivery of electrowon cathodes at a specified schedule.

Although the above only summarizes the possibilities discussed, it does state the more practical arrangements. Needless to say, these are only

Mr. William A. Griffith
Page 2
April 30, 1970

summaries of the points is agreements or understand standing which would est contracting as referred in I look forward to by Essex in this project.
you feel that I can contri

summaries of the points in our conversation and do not represent any formal agreements or understanding. As I agreed, I am enclosing a letter of understanding which would establish a basis for further discussion on long term contracting as referred in Item 3.

I look forward to an opportunity to establish a basis for participation by Essex in this project. Please do not hesitate to call upon me at any time you feel that I can contribute to the success of your program.

Very truly yours,

Howard Lanier, Manager Copper Processing Operations

HL/mcc

AL COPY

ESSEX

ESSEX INTERNATIONAL, INC.

MAGNET WIRE DIVISION

1601 WALL STREET, FORT WAYNE, INDIANA 46804 • PHONE: (219) 743-0311

April 30, 1970

Mr. William A. Griffith Research Director Hecla Mining Company Wallace, Idaho 83873

Dear Mr. Griffith:

This confirms the intent of Essex International, Inc. to purchase and Hecla to sell electrowon cathodes and "cement" copper from the mining and production facilities at the Lakeshore Project in Arizona, which is a joint venture between Hecla and El Paso Natural Gas Company.

Essex would purchase all of the electrowon cathode production accruing to Hecla from its agreement with El Paso Natural Gas, assuming cathode quality typical of industrial standards for this product is achieved and contingent upon the quality meeting a minimum specification to be established by Essex. The price for the electrowon cathode to be delivered in any month would be determined by a formula as follows:

(PRODUCERS PLUS COMEX) - 2 cents

PRODUCERS means the lowest producer copper quotation for electrolytic cathode copper at the close of business on the first calendar day of each month.

COMEX means the monthly settlement price for the sixth month future commodity exchange quotation for electrolytic cathode copper.

Essex would participate with Hecla in the development of technology for conversion of cement copper into marketable form usable by Essex. An agreement on pricing is contingent upon the quality of the cement copper product and the technology required. However, a minimum price would be the lowest producer electrolytic cathode quotation less our expense for conventional smelting. This is a statement of intent of the parties recognizing the willingness of Essex to participate in the product development giving Essex first rights for all or part of the cement copper production.

The term of this understanding would cover a period of 10 years starting within six months from the initial start-up of production at the Lakeshore Project

Mr. William A. Griffith Page 2 April 30, 1970

with an option by Essex to extend the contract an additional 10 years. This letter is an expression of intent, is not a firm contract to purchase copper, and confers no rights upon Hecla or a third party.

Very truly yours,

Howard Lanier, Manager Copper Processing Operations

HL/mcc

Las By

FILE MEMO. SUBSECT: HECLD MINING CO.

WHILE AT HAZEN RESEARCH ON 3/20/10

I RAW INTO KEN SCHELL, NGER FORMERLY
OF KCL RESEARCH & NOW A PROJECT ENGINEER
FOR PARSON JURDEN IN MY C.

KEN SUGGESTED I CONTACT HECLA MINING
CO IN WALLACE IDAHO REGARDING HANDLING
THEIR COPPER PRODUCTION. THE MAN
IN CHARGE OF THE DEVELOPMENT IS BILL
GRIFFITH. I SHALL CONTACT TO REVIEW
THE PRODUCTION PLANS & DETERMINE IF
OUR PARTICIPATION COULD BANSET THE PARTIES.

4

EL PASO NATURAL GAS COMPANY

LAKESHORE PROPERTY

PRELIMINARY REPORT

A Subsidiary of GFI Computer, Inc.

CORPORATE OFFICE 7107 North Cracle Tucson, Arizona 85704 602/297-1141

RICHARD F. HEWLETT Chairman of the Board

January 14, 1969

El Paso Lakeshore

Total Tonnage

322,319,280

470,000,000 - 1973 Metals Week.

Average Grade

0.80646

24,000,000 - 1.69% (a

181

Tactite Zme.

Planned output - 68,845 TPY copper 30,765 cathode + moly credits RICHARD F. HEWLETT Chairman of the Board

CORPORATE OFFICE 7107 NORTH ORACLE TUCSON, ARIZONA 85704 602/297-1141

LAKESHORE GEOLOGIC ORE RESERVE SUMMARY

cut off grade (high) November 1, 1968 most of computations in regort @ 0.4% Block Caving Reserves (0.50% Cu, +200 Ft. Vertical Columns) Tonnage Grade Proven 107,934,500 0.802 Porphyry 70,022,700 1.728. (24,000,000 - 1973) (1-69)Tactite Probable 24,161,250 0.816 Porphyry Total Proven & Probable 132,095,750 0.805 Porphyry 142,118,450 0.870 Porphyry with Tactite Open Pit Reserves (+0.40% Cu, 50 Ft. Benches) Total 2 Proven, Probable 263,099,260 0.785 and Inferred

> 263,699,260 142 118,450 405,217,718

L. PORPHYRY RESERVES FOR ORE GREATER THAN 200 FEET THICK CUT-OFF GRADE FOR PORPHYRY = 0.50

ORE CLASS	GRADE	TONNAGE	
	~~~		1 1 1 0.40
PROVEN ORE PROBABLE ORE	0.802 0.816	107,934,500 24,161,250	> 200 thick cutiff 0.40
TOTAL ORE	0.805	132,095,750	(News)

NOTE--TOTAL PORPHYRY RESERVES INCLUDES 9,258,700 TONS OF TACTITE WHICH LIES UNDER THE PORPHYRY.

. William forms

out crop area how doep.

2. TACTITE RESERVES FOR THE ENTIRE ORE BODY CUT-OFF GRADE = 1.00

ORE CLASS	GRADE	TONNAGE
PROVEN ORE PROBABLE ORE	1.752 1.967 1.781	16,675,000 2,606,400 19,281,400

3. TACTITE RESERVES OUTSIDE THE PORPHYRY AREA CUT-OFF GRADE = 1.00

ORE CLASS	GRADE	TONNAGE
		***
PROVEN ORE	1.663	7,894,100
PROBABLE ORE	1.967	2,128,600
tion with with the title of the con-		***
TOTAL ORE	1.728	10,022,700

4. OXIDE RESERVES

116.

CUT-OFF GRADE	GRADE	TONNAGE
क्षेत्रक क्षेत्रक क्षेत्रके पर्वेक काल काल काल क्ष्मक क्ष्मक क्ष्मक करन		*** *** *** *** *** *** *** ***
0.20	0.476	206,271,000
0.75	1.085	21,182,900
1.00	1.400	10,826,700

NOTE--TO OBTAIN THE TOTAL SULPHIDE TONNAGE, ADD THE PORPHYRY RESERVES TO THE TACTITE RESERVES OUTSIDE THE PORPHYRY.

TOTAL SULPHIDE = 132,095,750 + 10,022,700 = 142,118,450

AVERAGE GRADE = 0.870

cut of grade

### *LAKE SHORE PROJECT* ORE RESERVES AT +0.50 PORPHYRY --

### PROVEN RESERVES

		1	9/20/68		THICKNESS	1	10/30/68	· ·
,	I	NO.	AVERAGE	TONNAGE	THICKNESS CUT-OFF	NO.	AVERAGE	TONNAGE
	1	1159	0.860	83948128.	. 50.	1396	0.832	119897072.
	· 2	1077	0.858	82648752.	100.	1323	0.830	118729792.
(	3	866	0.834	77033952.	150.	1116	0.813	113230832.
1	4	706	0.819	71231248.	200.	969	0.802	107934576.
1	5	609	0.811	66770416.	250.	869	0.796	103335824.
	6	<b>54</b> 8	0.803	63310208.	300.	813	0.793	100143328.
,	7	472	0.793	58181872.	350.	759	0.791	96535200.
	8	417	0.782	53907288.	400.	696	0.790	91645424.
	9	352	0.768	48180416.	450.	626	0.790	85443744。
	10	310	0.766	44042504。	500.	557	0.790	78611040.

These are the most common height of blocks used in

what does the No. column represent. - # of assays - holes - blocks?

## LAKESHORE OPEN PIT POTENTIAL Proven, Probable, Inferred (0.40% Sulphide Copper Cut-Off)

GEOLOGIC SULPHIDE RESERVES

October 30, 1968

<u>Level</u> 950	<u>Tonnage</u> 1,336,020	Grade 1.078
900	1,841,396	1.055
850	4,091,395	1.024
800	6,637,092	0.750
750	8,854,832	0.716
700	10,720,422	0.638
650	13,653,215	0.819
, 000	17,072,568	0.689
550 ∮ 4 ⁵ °	17,725,793	0.813
500	17,642,460	0.804
450	18,180,094	1.046 7 ALTITE ZONE
400	19,940,845	1.009
350	16,306,439	0.886
300	15,913,966	0.738
250	14,478,484	0.857
200'	11,682,787	0.608
150	12,134,399	0.793
100	9,653,218	0.686
50	9,397,842	0.559
0	6,266,124	0.550
- 50	7,177,414	0.746
- 100 S	7,099,457	0.599
- 150 h	5,870,963	0.707
- 200	1,317,203	0.483
- 250	3.024,191	0.660
- 300 E	5,080,641	0.605
TOTAL \$	263,099,260	0.785
		*

### CONCLUSIONS

1. Smaller tonnage mining methods appear optimum; for high rate of return over a short period of time.

Mining Method	Ore Tonnage	Capital Investment	Rate of Return
Blast Hole Stoping	13,780,000	16,051,250	16.50
Sub-Level Caving	13,780,000	16,037,750	10.05
Blast Hole Stoping	25,000,000	16,878,100	9.40
Block Caving	25,000,000	40,000,000	11.44
Block Caving	60,000,000	42,873,496	<b>60</b> 7 644
@ 41 \$ copper (1968 average price)	)		

A very detailed capital cost estimate must be made to more accurately evaluate the economics of the deposit.

capital costs for blast hole + sub-level cowing will have the lowest united cost. Over the life of the nine block cowing will most certainly have the lowest capital cost. ( providing the ground is careable) Blast hole stopping would be combined with open pit operation - could have high initial capital cost.

## RECOMMENDATIONS

From the following study, the following recommendations are made in order of their importance:

- 1. Drill for more high-grade ore in or near the tactite zone. Where is factife in reference to perphyry.
- 2. Simultaneous with one (1) above, initiate a detailed capital cost study that includes mine layout for the various mining methods considered in this report. Kay Pincock is recommended for this study (Resumé in Appendix C).
- 3. Simultaneous with two (2) above, a computer study should be made to develop optimum mining sequences to maximize the grade for small increments of time to increase the rate of return. The determined sequences should then be re-run through the financial analysis program.
- 4. A trend analysis on future copper prices, was mining costs and the economic unjortence of copper in the vert 20 years.

## RICHARD F. HEWLETT & ASSOCIATES COMPUTER APPLICATIONS CONSULTANTS TO THE MINERAL INDUSTRY

7107 No. Oracle Road
Casas Adobes Center
Tucson, Arizona 85704

Office 297-1141 (602)

May 1, 1968

다 Exploration ☆ Development ☆ Mining ☆ Milling ☆ Metal Processing

Residence

99-9086 (602)

Mr. John R. Reynolds
Supt. of Exploration
Mines Division
El Paso Natural Gas Company
El Paso, Texas

/3 1/2 months from contractual agreement to final report.

Dear Mr. Reynolds:

Attached to this report you will find the computer output as per our proposal of 10 January 1968. The analysis is based on the following criteria and assumptions:

- All assay data was obtained from the El Paso drill hole logs supplied by Mr. Claude Barron.
- 2. A visit to the Lakeshore property was made by Mr. John M. Anderson and Dr. Charles Fair on 19 January 1968. Mr. Jim Synder escorted them on a tour of the property and showed us <u>representative</u> samples of drill core.
- American mining costs, recovery and dilution. It must be realized that an intensive study will be required before a final solution to the most economic method may be resolved. However, this analysis will serve to illustrate to your company the economic impact of varying underground mining costs, recoveries and dilution.

how about

Please note that all assay data are total copper (combined oxide and sulfide.) As per your instructions we have assumed that all assay values in the "tactite" zone are sulfide copper, and hence recoverable. If it appears that the Lakeshore deposit is amenable to a "bulk" mining method such as block caving it will be essential that the copper assay values in the porphyry type rocks be re-evaluated to determine the sulfide content. Gold, silver, molybdenum and iron values have not been included in this economic analysis. During Mr. Reynolds visit to Tucson on 13 March John Anderson reviewed the estimated operating and capital costs for various mining methods and various concentrator capacities. There is no doubt that these costs will require revision as more detailed cost data is acquired by your firm.

MoSe is indicated

5.

- 6. With regard to the feasibility of underground exploration it will be essential that the ore body be further tested to assertain:
  - Metallurgical recovery, grinding index, etc.
  - b. Ground conditions, which will govern mining methods.
  - c. Verifications of tonnage and grade of ore as indicated by drilling.
- 7. From preliminary observations, it appears an exploration shaft might best be located in the area of hole 27.

location 1

potential!

However, before a major expenditure is made for an exploration shaft with underground development work, it is our recommendation that El Paso employ a mining engineer to assertain the most suitable location for an exploration shaft. Due consideration should be given to potential ground subsidence should a caving method be employed. In otherwords, it may be more beneficial to locate the exploration shaft at a great distance from the ore body to insure that it will ultimately be useful. If the shaft is located in such a position that ground subsidence would endanger it, its value as a ventilation shaft, or secondary access would be nullified. Before a shaft is sunk, it is recommended that a diamond drill hole be put down at the proposed site to assertain that no ore is present at that location.

8. Metal prices and other financial criteria, i.e., depreciation, depletion, royalties, taxation rates, etc. are as specified by El Paso. Should you wish any of these factors varied, or when you obtain other capital cost data which will significantly alter this analysis it will be possible to recompute the economics of the Lakeshore deposits. All of the drill hole data is now key punched and any variations to the capital and operating costs data can readily be evaluated.

one anadouse

my finder

Further, more detailed work should be undertaken to establish the gold, silver, molybdenum, and iron values or credits per ton for entry into the financial analysis.

Sincerely,

Richard F. Hewlett

RFH:jag

#### ORE RESERVES

The ore reserves were computed of the total ore body for all rock types, for only the tactite ore body, and for a minimum of 10 and 30 vertical feet as a height cut-off, as well as for grade cut-off's. The three basic alternatives are shown in figure 1. Notice that the tactite ore body is a relatively small tonnage high grade deposit when compared with the total deposit (all rock types). Also, it is obvious that the ore reserves computed using a 10 foot vertical cut-off would have a higher grade for the same tonnage due to the dilution required in thin ore zones to make a 30 foot minimum vertical height. Therefore the following definitions were used for geologic and minable ore reserves:

Geologic Reserves - The total tonnage of material present in the ore body having a grade above the cut-off grade.

Minable: Reserves - The total tonnage of material which would be mined for a given cut-off grade within the ore body.

Geologic and minable reserves are different in several ways. Pockets of material above the cut-off grade but too small to mine, are included in the geologic reserves, but not minable reserves. Pockets of waste within the ore zones which must be mined with the ore are included in minable reserves, but not in geologic reserves. Dilution at the periphery of the ore zone is not included in either estimate.

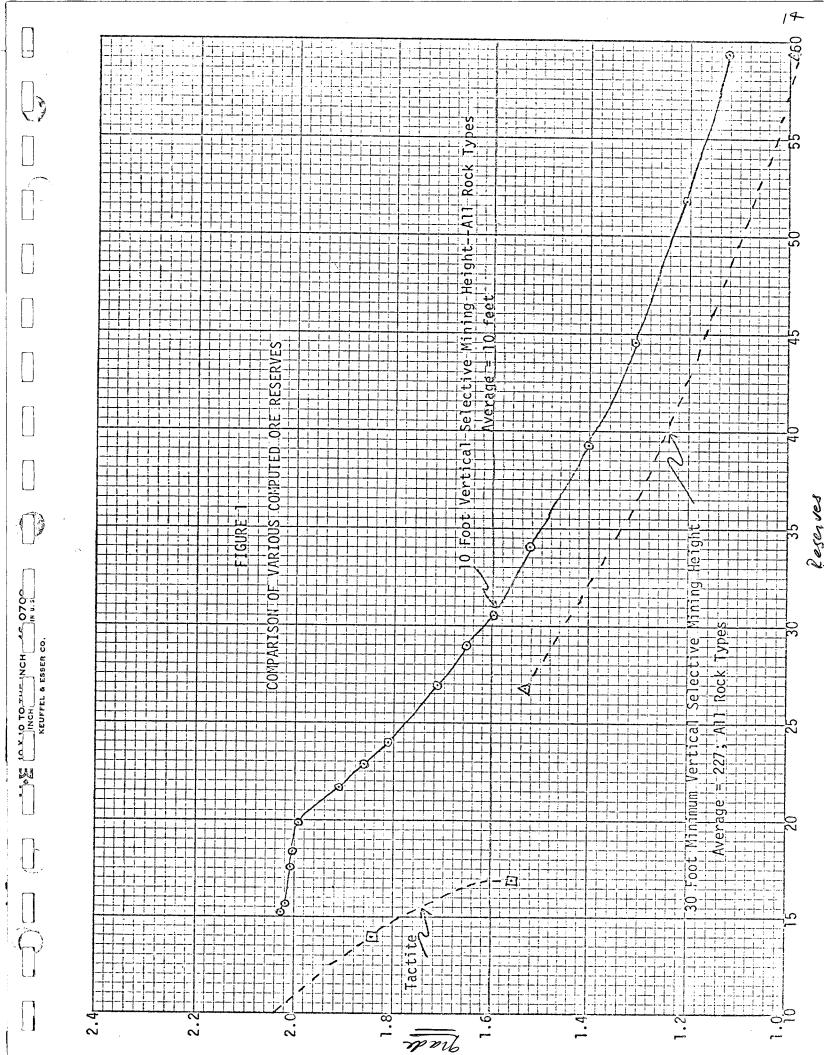


Table 1 presents the computed sulphide ore reserves summary for the deposit in the area drilled. The area considered is shown in other figures. As previously mentioned, the minable ore reserves are lower in grade than are the thinner zoned geologic ore reserves.

Table 2 shows the ore reserves computed for the same total volume and hence tonnage for a 10 foot vertical interval. It is not economically possible to mine the deposit by open-pit or underground using a 10 foot selective mining height for this ore body, but these computed geologic reserves serve to indicate to maximum ore reserves possible by very expensive mining methods. The important factor displayed by comparing tables 1 and 2 is that the grade drop is only from 1.12 to 0.99 when using a minimum of 30 vertical feet as a cut-off.

Table 3 presents the basic drill hole data used to compute 22 holes the minable ore reserves shown in table 1 for all rock types. numbered from

Table 4 shows the computed ore reserves for all rock types for various cut-off thicknesses. Notice that the 0 cut-off is really 30 feet (as a minimum). This table shows that only a very small tonnage is below a 50 foot thickness (a block-caving consideration).

Table 5 presents the basic drill hole data for a 0.75% sulphide copper cut-off grade. Table 6 shows the computed results for various vertical thicknesses. Again, a relatively small tonnage lies below a 50 foot vertical thickness.

The geologic oxide copper ore reserves from the surface to the top of the mixed zone are shown in table 7. For each cut-off grade is a computed tonnage, grade, and plus - or - minus confidence

interval. For example, the confidence interval for a cut-off of 0 is 0.29 - 0.31 and for a cut-off grade of 0.50, the confidence interval is 0.71 - 0.79 (at the 95% level). The total thickness of grade of oxide material per drill hole is presented in table 8.

Table 9 summarizes the elevations of the bottoms of oxide, mixed and sulphide per drill hole.

TABLE 1

(30' Vertical interval?)

LAKESHORE

MINABLE

SULPHIDE ORE RESERVE SUMMARY

(Tactite Zone)

Cut-off	<u>Tonnage</u>	Grade	
0.50	16,837,608	1.55 } Tactite Zone	
0.75	13,780,000	1.84	
1.00	6,669,614	2.19	
2.00	457,202	/	
`	(All Rock Types)	·	
0.50	59,338,007	0.9887 puphyry + befit	e
0.75	26,753,524	1.531	

## TABLE 2

## LAKESHORE GEOLOGIC ORE RESERVES

## SULPHIDE ZONE

ALL ROCK TYPES

10' vertical interval, ninning
height.

Cut-off Grade, % CU	Tonnage	Average Grade
0.50	59,338,007	1.12
0.55	51,790,213	1.21
0.60	44,539,108	1.31
0.65	39,210,555	1.40
0.70	34,036,281	1.52
0.75	31,075,314	1.59
0.80	29,004,418	1.65
0.85	26,933,521	1.71
0.90	24,120,900	1.81
0.95	22,785,795	1.86
1.00	21,604,968	1.91
1.05	19,979,107	1.99
1.10	18,347,312	2.07
1.15	17,463,175	2.11
1.20	15,831,380	2.21
1.25	15,245,934	2.25

	sufor	poit = top 2 = b. Hom2
U)		
	Drill Hole	<u>Top <b>Z</b></u> .
	1.0	<b>53.0</b>

|--|

SULPHIDE

(0.50	Cut-Off	)
-------	---------	---

$\Box$			(0.50 Cut-Off)	(TOPZ-BUTZ)	
	Drill Hole	Top Z.	Bottom Z	Thickness	Grade
	46	510	320	190	1.254
*	<del> 48</del>	500	210	290	1.573
	45	760	260	(500) ^X	0.66326
	47	510	350	160	1.16775
	38	540	430	110	0.94827
	43	790	140	650	0.83979
	40	720	260	460	0.54906
[]* -	<del> 39</del>	600	350	250	1.43804
	29	570	420	150	0.99366
	37	560	450	110	1.15336
	30	790	470	320 *	0.87821
	· IA	820	320	500	0.77099
	3	780	530	250	1.00571
	8	660	540	120	1.23957
	36·	880	850	30	0.52333
	27	810	740	70	0.48128
*-	42:	880	760	120	2.06182
J-	<u> </u>	840	810	30	2.66066
	· 10· (7)	860	820	40	0.69200
	4.	780	710	70	0.75700
*-	—— 42 ⁸	880	760	120	2.06182
*	5	740	650	90	2.21188
	41	ጎ.	7.	600	0.749
$\bigcap$					

looks like on drill hole was added in twice (# 42)

Trate holes 48,39,42,28,5,46

## ORE RESERVES COMPUTED FOR A PERIPHERAL CUT-OFF GRADE OF 0.50% SULPHIDE COPPER

Vertical Thickness Cut-Off, Ft. (+) 0 - (30 f	Tonnage t. min.) 59,338,007	Grade, % S CU 0.98870
<b>(+)</b> 50	58,519,478	A second
<b>(+)</b> 100	<b>56,5</b> 15,628	
(+) 150	<b>50,</b> 360,743	
(+) 200	45,606,731	
(+) 250	41,511,450	
<b>(+)</b> 300	35,028,407	
(+) 350	31,701,169	
(+) 400	28,174,841	
<b>(+)</b> 450	24,812,702	
<b>(+)</b> 500	<b>20,</b> 383,556	
(+) 550	14,151,406	
<b>(+)</b> 600	3,852,291	

can probably block cave 100' blocks and still Maintain

10-30jous Tpd.

## SULPHIDE

(0.75 Cut-Off)

	<u>Drill Hole</u>	Top Z	Bottom Z	Thickness	<u>Grade</u>
	46	500	330	170	1.330
	48	410	210	200	2.036
	45	300	260	40	0.9635
	47	450	350	100	1.4976
	38	520.	460	60	1.25633
	43	790	480	310	1.019
	40		~~		
	39	500	360	140	2.10921
	29	570	450	120	1.09982
	37	560.	470	90	1.28855
$\bigcap$	30	550	470	80	1.58275
	· 1A	510	480	30	4.41766
	3	670	540	130	1.42992
	8	650	550	100	1.36959
	36	870	860	10	1.981
	27		- 4A	<b>60. 60.</b>	
	× 42	880.	770	110	2.19444
	28	840,	810	30	2.66066
	70	840	830	10	1.039
	4	<b>7</b> 50	710	40	0.91650
	42	880.	770	110	2.19444
	5	<b>740</b> .	660	80	2.41862
	41	710	450	260	0.903
L					

# ORE RESERVES COMPUTED FOR A PERIPHERAL CUT-OFF GRADE OF 0.75% SULPHIDE COPPER

Vertical Thickness Cut-off, Ft.	Tonnage	Grade, % S.CU
(+) 0 - (30 ft. min.)	26,753,527	1.531
<b>(+)</b> 50	24,522,052	•
(+) 100	19,183,453	
(+) 150	12,650,079	
(+) 200	8,191,568	
(+) 250	3,976,214	
(+) 300	374,419	
	•	
+300 @ 0.5% 0/0	Res - 35, 028,400	!!
with a Secress of o		

## OXIDE COPPER

## ORE RESERVES IN SULPHIDE AREA

	<u>Cut-off</u>	<u>Tonnage</u>	<u>Grade</u>	±CI
	0.00	206,517,841	0.30	0.01
	0.05	164,367,549	0.38	0.01
	0.10	159,080,692	0.39	0.01
	0.15	146,607,015	0.41	0.02
	0.20	132,315,980	0.44	0.02
	0.25	115,794,553	0.47	0.02
	0.30	96,567,742	0.51	0.02
	0.35	74,201,860	0.56	0.02
	0.40	56,544,585	0.62	0.03
	0.45	43,740,479	0.68	0.03
	0.50	32,485,256	0.75	0.04
4				

Discussion of C. Chase:
This oxide ere has too much Ca Co3 to leach at this
low a grade using acid. An ammum leach may be
used but recordy is to poor.
(acid cost 14/16). Maybe be a break even
proposition if there is and that needs to be rentralized or
wasted.

## TABLE 8

## LAKESHORE

		OXIDE	
	<u>DH</u>	Thickness	Grade
	48	ft. 1092.5	0.236
	46	1025.2	0.182
	45	940.6	0.336
	47	977.4	0.264
	38	954.4	0.265
	43	955.3	0.410
	40	958.0	0.400
	39	924.8	0.305
<u> </u>	29	817.6	0.274
	4	843.9	0.473
	37	902.2	0.126
	10	820.6	0.287
	30	839.7	0.265
	1A	849.7	0.204
	3	853.1	0.358
	5	854.0	0.293
	29	817.6	0.274
	28	757.5	0.612
	8	- 848.1	0.231
	36	839.5	0.086
	27	840.8	0.403
П	42	759.3	0.380

 $\label{lem:LAKESHORE} \textbf{Elevations of Oxide, Mixed, and Sulphide Mineralization}$ 

	Drill Hole	Bottom Top <u>Oxide</u> / <u>Mixed</u>	Bottom Top <u>Mixed</u> / <u>Sulphide</u>	Bottom <u>Sulphide</u>
	48	670	570	- 80
	46	750	710	310
Ļ	45	820	760	70
	47	770	710	200
	38	810	770	360
	43	810	790	100
	40	810	730	200
, 📙	39	840	690	300
	37	870	860	340
	30	920	790	210
	1A	1050	850	250
	. 3	920	.840	-20
	29	930	810	340
	8	920	830	430
	36	940	880	790
	27	930	820	430
	42	940	880	720
	28	990	840	650
	10	970	890	540
	4	940	840	190
	5	920	850	590
	33	1040	920	360
1 1				

### CONFIDENCE INTERVAL ANALYSIS

Tables 10, 11, and 12 show the computer output from the preliminary confidence interval analysis for the sulphide, oxide, and mixed zones, respectively. On these tables INT is the assay cut-off interval (cut-off grade); PCT is the relative percentage of data above the 0.50% copper cut-off grade; AVG is the average geologic grade for the cut-off grade; DEV is the standard deviation of the average geologic grade; and CI is the 95% confidence interval of the average geologic grade indicated by the present drilling(for a 0.50% cut-off, the average grade is 1.12% copper ± 0.08 -- the range of the average grade then is 1.04 to 1.20). The number of additional samples required to produce a desired (acceptable) confidence interval (CI) can be easily computed.

The drilling to date in the sulphide zone has been adaquate for computing ore tonnage due to the geometry of the mineralization. It is shown for blast hole stoping that the rate of return varies with the grade variation as follows:

Confidence Interval	Rate of Return
Lower Average-expected	12.21 16.50
Upper	20.13

This clearly points out on the low end that underground drifting is required at a later date to prove-up the grade and investigate the ground. However, it is not recommended at this time. Additional surface drilling should be done to prove up more high-grade ore

(plus 1.15%). A spacing similar to the previous is more than adaquate for that purpose.

TABLE 10 *LAKE SHORE* CUTOFF GRADES FOR 10-FOOT COMPOSITES IN THE SULFIDE ZONE. 4/19/5 INT. FREQ PCT _AVG_ DEV CÌ INT. 95% confilme interval 0.50 401 100.00 1.12 0.85 0.08 0.50 0.55 350 87.28 1.21 0.09 0.88 0.55 0.60 301 75.06 1.31 0.90 0.10 0.60 0.65 265 66.03 1.40 0.93 0.11 0.65 230 0.70 57.36 1.52 0.94 0.12 0.70 0.75 210 52.37 1.59 0.95 0.13 0.75 0.80 196 48.88 1.65 0.96 0.14 0.80 0.85 182 45.39 1.71 0.97 0.14 0.85 0.90 163 40.65 1.81 0.98 0.15 0.90 0.95 154 38.40 1.86 0.98 0.16 0.95 146 1.00 36.41 1.91 0.99 0.16 1.000 1.05 135 33.67 1.99 0.99 0.17 1.05 1.10 124 30.92 2.07 0.99 0.18 1.10 1.15 113 2.11 29.43 0.99 0.18 1.15 1.20 107 26.68 1.00 2.21 0.19 1.20 1.25 103 25.69 2.25 1.00 0.20 1.25 1.30 94 23:44 2.34 0.99 0.20 1.30 1.35 29 22.19 2.40 0.99 0.21 1.35 1.40 84 20.95 2.46 0.99 0.22 1.40 1.45 79 19.70 2.53 0.98 0.22 1.45 1.50 75 18.70 2.58 0.98 0.23 Jang Jaleyn grade

	encoderant and one one and and and and				TABLE 1	11	186 - 1870 - 1880 - 1880 - 1880 - 1880 - 1880 - 1880 - 1880 - 1880 - 1880 - 1880 - 1880 - 1880 - 1880 - 1880 -			
*LAKE	\$HORE*	CUTOFF	GRADES	FOR	10-F00T	COMPOSITES	IN THE	OXIDE	ZONE,	4/19/68.
UINT.	FREQ	PCT	AVG	DEV	CI_	INT	100° 600° 500° 600° 500° 500° 600° 600° 6			
0.00		100.00	0.30	0.28		0.00		. The first thin was also also with any was		
0.05	1462 1415	79.59 77.03	0.38 0.39	0 • 2 6 0 • 2 6		0.05 0.10				
0.15	1304	70.99	0.41	0.26		0.15				· · · · · · · · · · · · · · · · · · ·
0.20	1177	64.07	0.44	0.26	0.02	0.20	*** ••** to or or or or or or or or or			
0.25	1030 859	56.07	0.47	0.27		0.25				
0.35	660	46.76 35.93	0.51 0.56	0.28		0.30 0.35				وه جوم جوم ۱۹۵۰ انتخار المنافق
0.40	503	27.38	0.62	0.31		0 40				
0.45	389	21.18	0.68	0.34		0.45				
0.50	289	15.73	0.75	0.36	0.04	0.50				
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						and their field title entry note with this pass was done and out out out out				**************************************

TABLE 12 CUTOFE GRADES FOR 10-FOOT COMPOSITES IN THE MIXED ZONE , 4/19/68 ... INT. FREQ PCT AVG DEV CI INT. 0.50 65_100.00 0.79 C . 64 0.16 0.50 0.55 50 76.92 0.87 0.20 0.71 0.55 0.60 37 56.92 0.97 0.80 0.27 0.60 0.65 23 35.38 1.19 0.96 0.42 0.65 0.70 17 26.15 1.36 1.07 0.55 0.70 0.75 11 16.92 1.71 1.20 0.81 0.75 0.80 11 16.92 1.71 1.20 0.81 0.80 0.85 10 15.38 1.80 1.23 0.88 0.85 0.90 9 13.85 1.90 1.26 0.97 0.90 7 0.95 10.77 2.19 1.30 1.20 0.95 1.00 7.69 2 . 67 1.22 1.52 1.00 1.05 5 7.69 2.67 1.22 1.52 1.05 1.10 7.69 2 . 67 1.22 1.52 1.10 1.15 7.69 2.67 1.22 1.52 1.15 5 1.20 7.69 2.67 1.22 1.52 1.20 5 1.25 7.69 2.67 1.22 1.52 1.25 1.30 5 7.69 2.67 1.22 1.52 1.30 1.35 3 4.62 3.56 0.11 0.27 1.35 1.40 4.62 3.56 0.11 0.27 1.40 1.45 4.62 3.56 0.11 0.27 1.45 1.50 4.62 3 • 5 6 0.11 0.27 1.50 Standard deviation is much to big

#### PRELIMINARY FINANCIAL ANALYSIS

For this analysis costs and calculation procedures detailed in this report have been assumed. Based on these assumptions a simulation model has been developed relating the cash flow of the property to ore reserves, mining method, price, costs, and financing method.

The following variables were included in the analysis:

- 1. mining cost/ton
- 2. milling cost/ton
- 3. plant cost/ton
- 4. admin. cost/ton
- 5. capital investment required per ton of daily production capacity
- 6. pre-production costs
- 7. working capital
- 8. underground development costs per ton of ore
- 9. percent dilution and dilution grade
- 10. mill recovery
- 11. mine recovery
- 12. price of cu/lb.
- 13. ton/day capacity
- 14. rate for present value calculation —
- 15. interest rate on loan
- 16. total tons of ore

- 17. grade of ore
- 18. percent of capital investment for equipment which must be depreciated and replaced
- 19. life of equipment
- 20. royalty on net smelter return
- 21. method of repayment of loan

Since the time between initiation of the project and the beginning of production will vary with the mining method, all cases were analyzed using the point of time when production starts as the base for present value and rate of return calculations.

No credit for values contained in the ore other than copper was used.

Appendix A describes the calculations in detail and Appendix B contains some examples of the computer printout for financial analysis of the various mining mehtods.

what other credits may be in the one

C. Chase- Au + Ag credite are indicated because to the complicated process in which the milling + electroning is being done. Could be that the copper is almost by preduct in nature.

# WRIGHT ENGINEERS LIMITED:



PHONE 684-9371 . CABLE "WRIGHTENG" . TELEX 04-50360

1101 WEST PENDER STREET . VANCOUVER 1, B.C., CANADA

March 11, 1968

Mr. John Anderson, 7107 North Oracle Road, Tucson, Arizona

Re: Sampling Plant

Dear John:

As discussed with you on the phone Friday, I am pleased to send you some information concerning the sampling plant that was used for Brenda and is now being used at Highmont.

The equipment, consisting of a Model S25 Automatic sampling system, a Syntron vibrating feeder, a No. 12 Denver gyratory crusher and a 40" Denver vezin sampler, cost approximately \$6,000. U.S.

The Tower steelwork, the installation cost for labour and material and the electrical installation cost totalled another \$6,000. U.S. for a total of \$12,000.

Not included in the foregoing was the site preparation which was done by the client.

In addition to the foregoing, we rented a portable crushing plant, an H90B payloader, an H70 payloader and a light truck which cost about \$495. U.S. per day.

As power was not available, we rented a 15 KV electric set at \$435. U.S. per month.

I hope this preliminary information will be useful to you and your client and when you get back to Vancouver we will be very pleased to discuss the details with you. We, of course, have detailed drawings of this system all of which worked very well.

Yours sincerely,

H. M. Wright

#### DISCUSSION OF FINANCIAL ANALYSIS RESULTS

Tables 14 thru 22 give the results of the financial analysis showing the effect of changes in mining methods, costs, grades and other variables.

Table 14 shows that blasthole stoping of 13,780,000 tons at 1.84% Cu is the best method of mining from an economic point of view. This case was used to show the effect of changes in other variables on the total cashflow and rate of return.

Table 15 shows the effect of mill recovery on cashflow and rate of return. A change of 1% in mill recovery results in a change of approximately 1 million in total cashflow.

From Table 16, it is obvious that the capital investment required is a critical factor. A change of 10% in the capital investment causes a change of about 15% in the rate of return from 16.50% to either 19.16% or 14.21%.

Table 17 relates the change in mining costs (or any other operating cost) to the cashflow and rate of return. An increase of \$.50 per ton in operating costs could cause a change of about 5.2 million in total cashflow.

Table 18 shows the effect of changes in the interest rate for bank financing on the cashflow and rate of return. The effect of any change in the royalty rate is shown in Table 19.

Table 20 shows the effect of price changes and Table 21 the effect of grade variations. If the grade for the example case is actually 1.70% instead of 1.84 the rate of return would drop from 16.50% to 12.21% and the cashflow from 39.5 million to 32.9 million.

The financial analysis indicates that:

- A more detailed capital cost estimated should be made for blasthole stoping, sub-level caving and block caving.
- 2. Further work should be done with the ore reserve estimates in order to develop mining sequences. If it is possible to mine the higher grade material in the early years of the mine life, the rate of return would increase considerably.
- 3. The distribution of gold, silver, and molybdenum values

  should be determined and their value included in the financial analysis.

Apparently there are a substanceal amount of Au, Ay values.

#### PRE PRODUCTION COSTS

Acquisition and pre-production costs of surface drilling. To 1 April, 68.	\$500,000	
Shaft cost (to 1400 Ft.) not incl. headframe or hoist (based on Centennial quote). I station and loading pocket. Shaft site test hole (water). Pumping shaft.	(293/m) \$410,000 20,000 25,000 80,000	2,100,000
Headframe and hoist installed.	55,000	6,000,000
3000 Ft. u.g. development @ \$85 Ft. (assume contracted).	255,000	360,000
U.G. diamond drilling 50,000 Ft. @ \$5.00.	250,000	500,000
U.G. percussion drilling _50,000 Ft. @ \$1.50	75,000	200,000
Sampling plant (installed).	30,000	100,000
Preparation of leach area for waste development, bins for bulk samples & misc. surface installations.	100,000	500,000
Total	\$1,800,000	\$10,260,000
PRE-PRODUCTION & PRODUCTION SCHEDULES	•	
1. Assume shaft sinking commences	l July, 19 <u>6</u> 8	
12 months to complete to 1400	1 July, 1969 —	6-8 months
2. 3000 Ft. u.g. development		
@ 500 Ft./month = 6 months	1 Jan., 1970	
3. U.G. drilling and feasability study		

4. Plant construction &

6 months

primary mine development commences

1 July, 1970

1 July, 1970

5. Construction complete & production commences

1 July, 1972

CAPITAL CO	ST SCHEDULE				• •	
METHOD	BLOCK	SUB LEVEL	BLASTHOLE	CUT & FILL	SQUARE SET	
Tons/day	10,000	3000	3000	2000	1000	
Cost/ton capacity	\$4000	( ⁴ -800) \$5000	\$5000	\$5500	\$6000	
Cost	40,000,000	15,000,000	15,000,000	11,000,000	6,000,000	
Less pre-prod.	1,800,000	1,800,000	1,800,000	1,800,000	1,800,000	
Less u.g. prim.	Cos	<b>t</b> determined l	oy ore reserv	e x \$0.35/ton	) (Tows x	#/+x = A

Capital cost per ton capacity

Yields

for a 50,000 tpd opn - 200,000,000 capital cust.

# BLOCK CAVING MINING - 2.60 MILLING - 0.85 HAULAGE 0.04 3.49 0.349 IITDA .07 Smelting .04 Refining .03 0,489 /16 cm

TABLE 13 LAKESHORE

#### ESTIMATED COSTS PER TON AND ASSUMPTIONS USED FOR FINANCIAL ANALYSIS

	MINING METHOD	BLOCK CAVING	SUB-LEVEL CAVING	BLASTHOLE STOPING	CUT & FILL	SQUARE SET
			Z.60			
<u>-</u>	Mining	2.00	3.25	2.75	5.25	9.00
	Milling	0.75	0.90	0.90	1.10	1.10
	Plant	0.25	0.30	0.30	0.35	0.35
	Administration	0.85	0.90	0.90	1.00	1.00
	Marketing	See Sme	lter Schedu	ıle		
	Total Excl.	<b>#2</b> 0.5	<b>A.</b>			
	marketing	\$3.85	\$5.35	\$4.85	\$7.70	\$11.45
	Daily Capacity	10,000	3000	3000	2000	1000
	Mine Recovery	▶85%	87%	90%	95%	95%
	Dilution	12%	18%	10%	7%	5%
	Cut Off Grade	To be Ca	alculated			

check San Manuel, Chinax recovery averages

TABLE 14

#### ECONOMIC COMPARISON OF DIFFERENT MINING METHODS

	MINING METHOD	TONNAGE AND GRADE	TOTAL CASH FLOW	CAPITAL INVESTMENT	RATE OF RETURN
*	Block-Caving	25,000,000 at 1.53	59,909,608	40,000,000	11.44
*	Block-Caving	60,000,000 at 0.99	- 5,519,327	42,873,496	
	Sub-Level Caving	25,000,000 at 1.53	24,291,324	17,776,648	2.28
	Sub-Level Caving	13,780,000 at 1.84	30,230,980	16,037,750	10.05
:	Blast Hole Stoping	25,000,000 at 1.53	43,383,832	16,878,100	9.40
	Blast Hole Stoping	13,780,000 at 1.84	39,516,352	16,051,250	16.50
	Cut & Fill	13,780,000 at 1.84	- 2,565,135	12,149,398	
	Cut & Fill	6,669,615 at 2.19	12,905,636	11,681,356	2.02
	Square Set	6,669,615 at 2.19	-14,159,052	6,367,115	600 GO CO

Development cost to obtain 40,000 Tpd -?

#### TABLE 15

#### LAKESHORE

# EFFECT OF MILL RECOVERY ON FINANCIAL ANALYSIS *

MILL RECOVERY	TOTAL CASHFLOW	RATE OF RETURN
.90	37,695,440	, 15.31
.91	38,678,808	15.94
.92	39,516,352	16.50
.93	40,353,896	17.06
. 94	41,173,064	17.62

^{*} Case used in mining 13,780,000 tons at 1.84% Cu using blasthole stoping.

TABLE 16
LAKESHORE

# EFFECT OF CAPITAL INVESTMENT REQUIRED PER TON OR MILL CAPACITY ON FINANCIAL ANALYSIS *

CAPITAL REQUIRED PER TON DAILY MILL CAPACITY	TOTAL CASHFLOW	CAPITAL INVESTMENT	RATE OF RETURN
3500	38,025,488	11,101,250	26.37
4500	39,118,248	14,401,250	19.16
5000	39,516,352	16,051,248	16.50
5500	39,711,056	17,701,252	14.21
6500	39,639,832	21,001,240	10.42
7500	39,278,544	24,301,252	7.39

^{*} Case used is mining 13,780,000 tons at 1.84 % Cu using blasthole stoping.

# EFFECT OF MINING COST ON FINANCIAL ANALYSIS *

MINING COST PER TON	TOTAL CASHFLOW	RATE OF RETURN
2.25	43,386,952	19.20
2.75	39,516,344	16.50
3.25	34,328,648	13.14
3.75	28,833,492	9.45

^{*} Case used in mining 13,780,000 tons at 1.84% Cu using blasthole stoping.

## TABLE 18

#### LAKESHORE

# EFFECT OF INTEREST RATE FOR BANK LOAN ON FINANCIAL ANALYSIS *

INTEREST RATE	TOTAL CASHFLOW	RATE OF RETURN
.05	40,251,632	17.31
.06	39,892,608	16.91
.07	39,516,352	16.50
.08	39,122,328	16.08
.09	38,694,960	15.65

^{*} Case used in mining 13,780,000 tons at 1.84% Cu using blasthole stoping.

# EFFECT OF ROYALTY PAYMENT ON FINANCIAL ANALYSIS *

ROYALTY	TOTAL CASHFLOW	RATE OF RETURN
.05	43,215,872	19.08
.06	42,507,264	18.59
.07	41,793,080	18.10
.08	41,049,376	17.58
.09	40,299,016	17.05
.10	39,516,344	16.50
.11	38,669,336	15.93
.12	37,651,128	15.29

^{*} Case used in mining 13.780,000 tons at 1.84% Cu using blasthole stoping.

TABLE 20

# EFFECT OF PRICE CHANGES ON FINANCIAL ANALYSIS *

PRICE	TOTAL CASHFLOW	CAPITAL INVESTMENT	RATE OF RETURN	CHANGE
38	27,894,824	16,051,250	8.80	os au
39	30,918,468	16,051,250	10.87	2.07
40	33,883,584	16,051,250	12.85	1.98
41	36,792,000	16,051,250	14.74	1.89
42	39,516,352	16,051,250	16.50	1.76
43	41,909,064	16,051,250	18.11	1.61
44	44,220,088	16,051,250	19.63	1.52
45	46,463,824	16,051,250	21.10	1.47
46	48,630,056	16,051,250	22.49	1.39

I figured over a short life

^{*} Case used is mining 13,780,000 tons at 1.84% Cu using blasthole stoping.

TABLE 21

## EFFECT OF GRADE VARIATION ON FINANCIAL ANALYSIS *

GRADE	TOTAL CASHFLOW	RATE OF RETURN
1.70	32,914,896	12.21
1.74	34,854,768	13.49
1.78	36,792,968	14.74
1.82	38,705,256	15.96
1.84	39,516,352	16.50
1.86	40,327,424	17.05
1.90	41,908,248	18.11
1.94	43,457,232	19.13
1.98	44,979,904	20.13

^{*} Case used in mining 13,780,000 tons at 1.84% Cu using blasthole stoping.

# EFFECT OF OPERATING COST PER TON ON THE FINANCIAL ANALYSIS *

Operating Cost / Ton	Total Cashflow	Rate of Return
2.85	53,555,232	25.86
3.35	50,198,096	23.69
3.85	46,840,968	21.52
4.35	43,386,952	19.20
4.85	39,516,352	16.50
5.35	34,328,648	13.14
5.85	28,833,488	9.45
6.35	22,899,368	5.21

^{*} Case used is 13,780,000 tons at 1.84% Cu mined by blasthole stoping. Operating cost includes mining, milling, administrative and plant.

 $\wedge$ 

APPENDIX A

Mine Recovery (93%, recovery)

A = 55,8 x10 tous

 $\cap$ 

#### FINANCIAL ANALYSIS MODEL

#### MINE RECOVERY

 $A = B \times C$ 

where:

A = Tons of ore mined

B = Tons of ore in minable ore zones

C = Mine recovery

# DILUTION

Ore =  $A + A \times D$ 

 $GO = (GD \times A + DG \times A \times D) / Ore$ 

#### where:

Ore = Tons of material mined and sent to mill

GO = Grade of ore sent to mill

A = Tons of ore mined

GD = Grade of ore

DG = Grade of dilution

D = Percent dilution

#### CAPITAL INVESTMENT-ORIGINAL

 $TCAP = CT \times TPD$ 

where:

TCAP = Total capital investment initially

CT = Capital required per ton of daily capacity

where was this figure found

TPD = Tons per day mill capacity

```
CAPITAL INVESTMENT-ORIGINAL (CONTINUED)
          UGC = OR \times DC
     where:
          UGC = Underground development cost
          OR = Tons of ore reserves
              = Underground development cost per ton of ore reserves
          DC
          WC = 90 \times OPC \times TPD
     where:
          WC = Working capital based on 90 days operating costs
          OPC = Operating cost per ton
          TPD = Tons per day mill capacity
          PP = \$1,800,000.00
     where:
          PP = Preproduction cost
DEPRECIATION
          BASE = TCAP - UGC - WC - PP
          DPL = (BASE - PCT \times BASE) / LIFE
          DPQ = (PCT \times BASE) / EQL
          DEP = DPL + DPO
     where:
          BASE = Initial total to be depreciated
          PCT = Percent of base for equipment
          LIFE = Mine life
          EQL = Equipment life
          DPL = Yearly amount for depreciation of capital over mine life
               = Yearly amount for depreciation of capital for equipment
          DPQ
                 over life of equipment
          DEP = Total yearly depreciation
```

At the end of every EQL years [BASE x PCT] is required to replace

equipment

#### YEARLY PRODUCTION

 $PRO = TPD \times 360$ 

where:

PRO = Yearly production rate

TPD = Daily production rate

#### NET SMELTER RETURN

 $V = G \times REC \times TON \times 20.0 \times 26.5 / 28.0$ 

where:

V = Gross value of ore

G = Grade of ore (including dilution)

REC = Mill recovery

TON = Yearly production rate

 $RCU = G \times 20.0 \times REC \times TON$ 

 $ACU = RCU \times 26.5 / 28.0$ 

where:

RCU = Pounds Cu recovered

ACU = Pounds Cu accountable

 $SC = RCU \times 27.265 / 560$ 

 $FC = 4.58 \times RCU / 509.6$ 

 $RC = .0425 \times ACU$ 

where:

SC = Smelting cost

FC = Freight cost to Hayden

RC = Refining and delivery cost

NET = V - FC - SC - RC

where:

NET = Net Smelter return

```
ROYALTY
```

 $ROY = PCT \times NET$ 

where:

ROY = Royalty payment

PCT = Percent royalty

NET = Net Smelter Return

**INTEREST** 

 $INT = RATE \times BAL$ 

where:

INT = Interest Payment at year end

RATE= Interest rate

BAL = Loan Balance

TAXATION

 $TAX = .54 \times TAXIN - CRDT$ 

where:

TAX = Federal tax, no allowance for local, and state taxes

TAXIN= Taxable income after allowable deductions for depreciation, depletion, interest, royalty, and development

CRDT = Capital investment credit at .07 of capital invested and deducted from tax up to 50% of tax

Depletion taken as smaller of 15% of new smelter return or 50% of taxable income

CASHFLOW CALCULATION

CF = NET - OPC - ROY - INT - TAX

where:

CF = Cashflow

NET = Net smelter return

OPC = Operating costs

ROY = Royalty payment

INT = Interest payment

TAX = Federal tax

#### REPAYMENT OF LOAN

$$PAY = CF \times PCT$$

#### where:

PAY = Loan payment

CF = Cashflow

PCT = Percent of cashflow to be used each year for loan repayment

BAL = Loan balance

#### PRESENT VALUE AND RATE OF RETURN

$$PV = \sum_{n=1}^{n=L} \frac{CF_n}{(1+R)^n}$$

#### where:

PV = Present value at rate R

 $CF_n$  = Cashflow for year N

L = Life of mine

R = Rate of return

#### when:

$$\begin{array}{ccc}
n = L & \frac{CAP_n}{\Sigma} & \frac{\Gamma}{(1 + R)^n} & \frac{\Gamma}{n = 1} & \frac{CF_n}{(1 + R)^n}
\end{array}$$

R = Discounted rate of return

 ${\sf CAP}_n = {\sf Capital}$  investment in year N

 $CF_n = Cashflow for year N$ 

L = Life

# RICHARD F. HEWLETT & ASSOCIATES COMPUTER APPLICATIONS CONSULTANTS TO THE MINERAL INDUSTRY

7107 No. Oracle Road Casas Adobes Center Tucson, Arizona 85704

Office 297-1141 (602)

May 8, 1968

Mr. Windsor H. Nordin Mining Division El Paso Natural Gas Company Box 1492 El Paso, Texas

Dear Mr. Nordin:

Residence

99-9086 (602)

☆ Exploration

☆ Development ☆ Mining ☆ Milling ☆ Metal Processing

Enclosed is a description of the method used to calculate the rate of return as requested by you in our telephone conversation May 7. Also I have enclosed a copy of an example of the calculation procedure for a simple case. This is the method used by the program.

After reviewing the method I found that the replacement capital was not discounted, resulting in a lower rate of return than would be the case. Enclosed is also an example discounting the capital for replacement of equipment and the results of reruning the main cases with the new method.

If you have any questions concerning the methods and/or results, please do not hesitate to call me.

Sincerely,

I medecick Banfield, JR

A. Frederick Banfield, Jr.

AFB:jag enclosure

#### RATE OF RETURN CALCULATION

(Procedure Used in Lakeshore Financial Analysis Program)

C = Total Capital Investment

 $CF_n$ = Cashflow for Year

R = Rate of Return - Unknown

The rate of return is that rate which when used to discount the cashflow back to the present results in a present value of the cashflow equal to the capital investment.

OR

$$c = \frac{CF_1}{(1.+R)} + \frac{CF_2}{(1.+R)^2} + \frac{CF_3}{(1.+R)^3} - \frac{CF_n}{(1.+R)^n}$$

where:

N is Last Year of Mine Life

CF is known for Each Year

R is determined by successive approximations (trial and error)

## EXAMPLE:

YEAR	CASHFLOW	CAPITAL INVESTMENT		
1	\$ 5,000	\$16,000		
2	6,000			
3	4,000			
4	4,000			
5	6,000	•		
6	4,000			

Find R so that

$$16,000 = \frac{5,000}{(1+R)} + \frac{6,000}{(1+R)^2} + \frac{4,000}{(1+R)^3} + \frac{4,000}{(1+R)^4} + \frac{6,000}{(1+R)^5} + \frac{4,000}{(1+R)^6}$$

By trial and error

First guess R = .10

	Year (n)	Cashf	low	1 (1+R) ⁿ	CF _n (1+R) ⁿ	1 (1+R) ⁿ	CF _n (1+R) ⁿ	1 (1+R) ⁿ	$\frac{CF_n}{(1+R)^n}$
	1 2 3 4 5	5000 6000 4000 4000 6000 4000		26 51 83 21	4,545 4,956 3,004 2,732 3,726 2,256	.847 .718 .609 .516 .437	4,235 4.308 2,436 2,064 2,622 1,480	.833 .694 .579 .482 .402	4,165 4,164 2,316 1,928 2,412 1,340
TOTAL		29000		2	21,219		17,145		16,325

R = 18%

R = 20%

R = 10%

From the table above, if R = .10 the present value is 21,219. Since this is greater than 16,000, we know R should be greater. For R = .18the present value is 17,145, and for R = .20 the present value is 16,325. Therefore the rate of return is slightly more than 20%. The computer makes basically the same calaulation, but much faster and more accurately.

#### CALCULATION OF RATE OF RETURN

(Revised to Discount Replacement Capital)

For Blasthole Stoping of 13,780,000 tons at 1.84% CU

YEAR	CASHFLOW	CAPITAL	* DISCOUN CASHFLOW	TED AT 17.58% CAPITAL
1970	2967274	15000002	2523479	15000002
1971	3006791	0	2174640	0
1972	3044413	0	1872535	0
1973	3228753	0	1688897	0
1974	3194873	0	1421229	0
1975	3144886	0	1189755	0
1976	3144886	0	1011812	0
1977	3218473	. 1051250	880616	338221
1978	3144886	. 0	731786	0
1979	3144886	0	622338	0
1980	3144886	0	529259	0
1981	3144886	0	450101	. 0
1982	1986476	0	241786	0
TOTA	L 39516352	16051250	15338218	15338218

Rate of Return = 17.58 %

^{*} Capital is discounted from beginning of year

Cashflow is discounted for year end

	** LAKESHORE FINANC	IAL AMALYSIS **	BLASTHOLE STOPING	59
	MIMING COST MILLING COST	2.75 0.90		er er ege variant (i.e.) Salan (
8	ADMIM CAP/TPD	0.30 0.90 5000.00		
	PRE-PRO WORKING CAP	1800000.25 1309500.00 -0.10-		
	DIL MILL REC MINE REC	0.10 0.92 0.90		
	TOTAL TONS  INTERFST  PCT EQUIP	13780002 • 02 		
	LIFE EQUIP PCT-CF PAY LOAN AVG GRADE	8.00 1.00 1.84		
	PRICE TPD	-3000 • 00 0 • 10		
	DILUTION GRADE ROYALTY PERCENT	0.60		
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	TOTAL TONS	25000004.04		
	LIFE EQUIP PCTCF PAY LOAN AVG GRADE	0 • 1 0 8 • 0 0 1 • 0 0		
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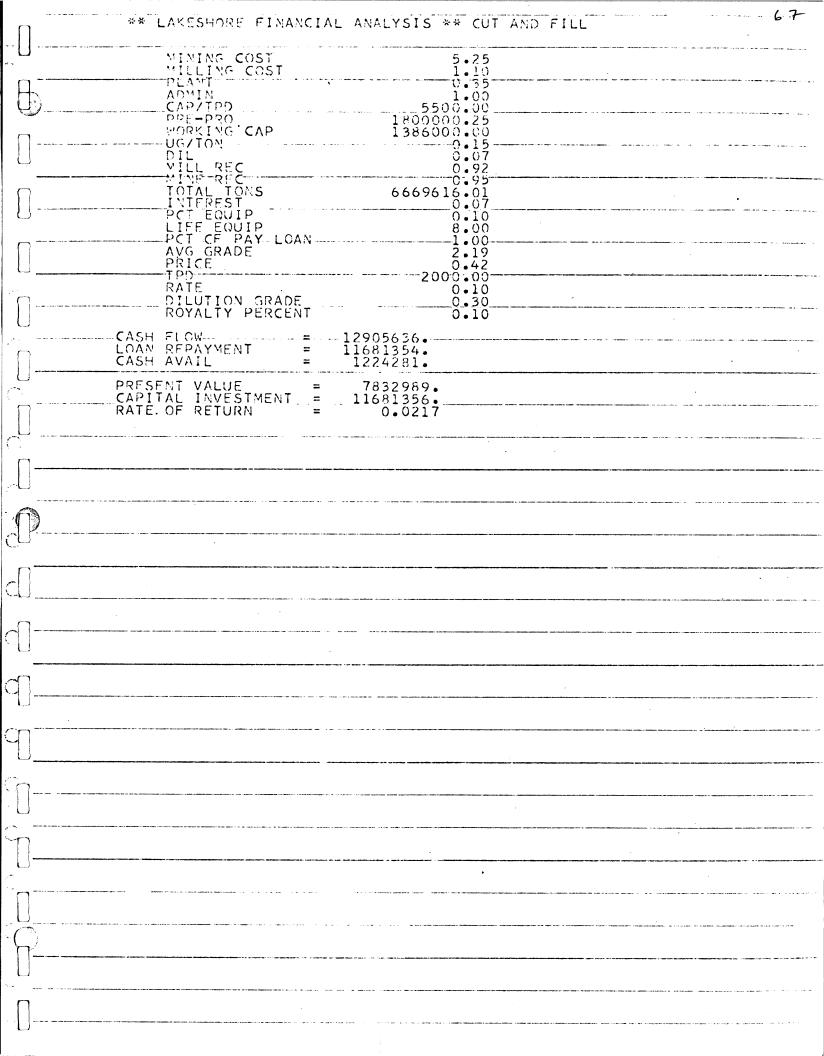
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	ADMIN 0.90 CAP/TPD 5000.00	
	PRE-PRO 1800000.25 WORKING CAP 1444500.00 UC/TON - 0.10	
<u> </u>	DIL MILL RFC 0.92 MINE RFC 0.87	
	TOTAL TONS 25000004.04 INTEREST 0.07 PCT EQUIP 0.10	
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	PRE-PRO 1800000.25 WORKING CAP 1386000.00 UG/TON 0.15 0.07
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APPENDIX B

	es Enrichent - Filanci	AL AMERYSIS, 9%	SLASTHULE STUPING	69
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EL CAVING	OAN-PAY	366360	2371548	2126051.	2153749.	2284159.	2422465	2003997.	1037750.	ċ	ဝံ	6	0	ċ	•	:	16037742.		***************************************		
* SU3 LEVE	ASH FLOW L		1730C/0•	2128051	2153749	2264159.	2477455	2556431.	2467589.	23949:7	2394947.	2394947.	2394947.	2394947	236244.		4607564. 30230980. 16037742. 14193248	1	: : : : : : : : : : : : : : : : : : : :		
ANALYSIS *	FD-TAX C		S	88506	211771.	232124	253709.	289315.	518436.	591079.	591079.	591079	591079	591079.	58305.		4607564.	• • • • • • • • • • • • • • • • • • • •	905		
** LAKESHORE FINENCIAL ENALYSIS ** SUB LEVEL CAVING		. (	ść	327800.	784338	859720	939665	1024451.	1094591.	1094591.	1094501	1094591	1094591.	1094591.	107973.		.0611494.	16088140	0.10		
LAKESHORE	OP-MARGIN DEPLETION		139183	1419714	1.568677	1719440	1879331.	2048903	2189183.	2189183.	2189183.	2189183.	2189183	2189183.	215947.		24400980. 10611494.	VALUE INVESTMENT .	RETURN		
*	YEAR		1970	1072	1973	1974.	1975.	1976.	1977.	1978	1979.	1980	1981	1982	1983.		1	PRESENT VAL	RATE OF RE		
	TOTAL COST		7624842	74895KO•	10000	1000000	6884694	6715122	6574842	A 5 7 4 8 4 2 .		07/101/0	2,10,10	0011010	648561.	Man or applications and a service	3395792.				
-	INTEREST TOT		1049999	**************************************	600000 600000	6607030	309852						i				4274327, 90395792.				
	DPREC INT		796843	100000	10007	706863	796863	706842	706867	10000	10000	10000	20000		78602		- 1				
	CP-COST D		5777999.	0.447770	2111000	6777000	- 0.000.4.5	67777	. 777000.	5777000	2777000	5777000	6777000	111000	569958.		5683872. 1				
L CAVING	ROYALTY C	1	973780	9/3/80	010100	072780	973780	047470	073780	017770	000000	072700	01010	010100	96096		2755198. 7	1		THE REPORT OF THE PROPERTY AND THE PROPERTY OF	
* SUB LEVE	NET SY R		9737806.	9737806	000000000	9797979	9737306	9797806	9737806	0727806	010100	0737006	2001616	010100	960564		7551936. 1				
** LACTO-038 FINANCIAL ANALYSIS ** SUB LEVEL CAVING	IBS ACC N		30761288	30/51/30	000000000000000000000000000000000000000	1010101010101010101010101010101010101010	30761288	40761282	<b>a</b>		000000000000000000000000000000000000000	2010110100	000000000000000000000000000000000000000	2000	3034380.	٠	402931072.127551936. 12755198. 75683872. 10437564.	:			
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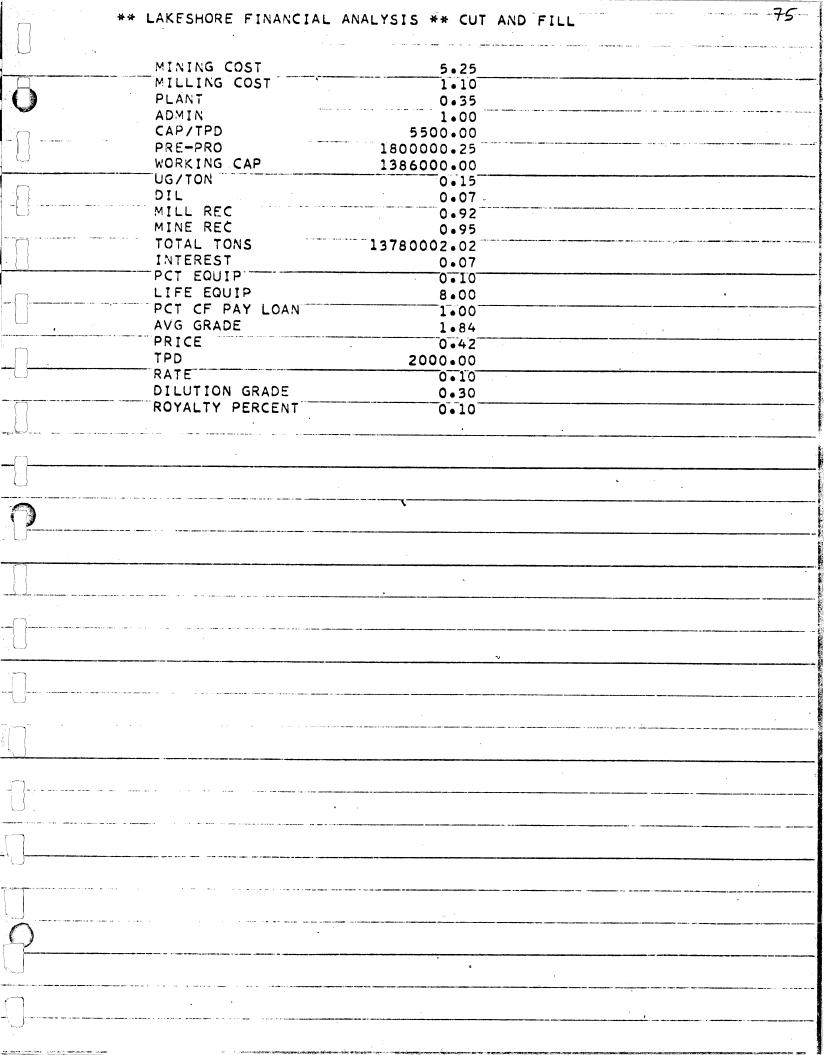
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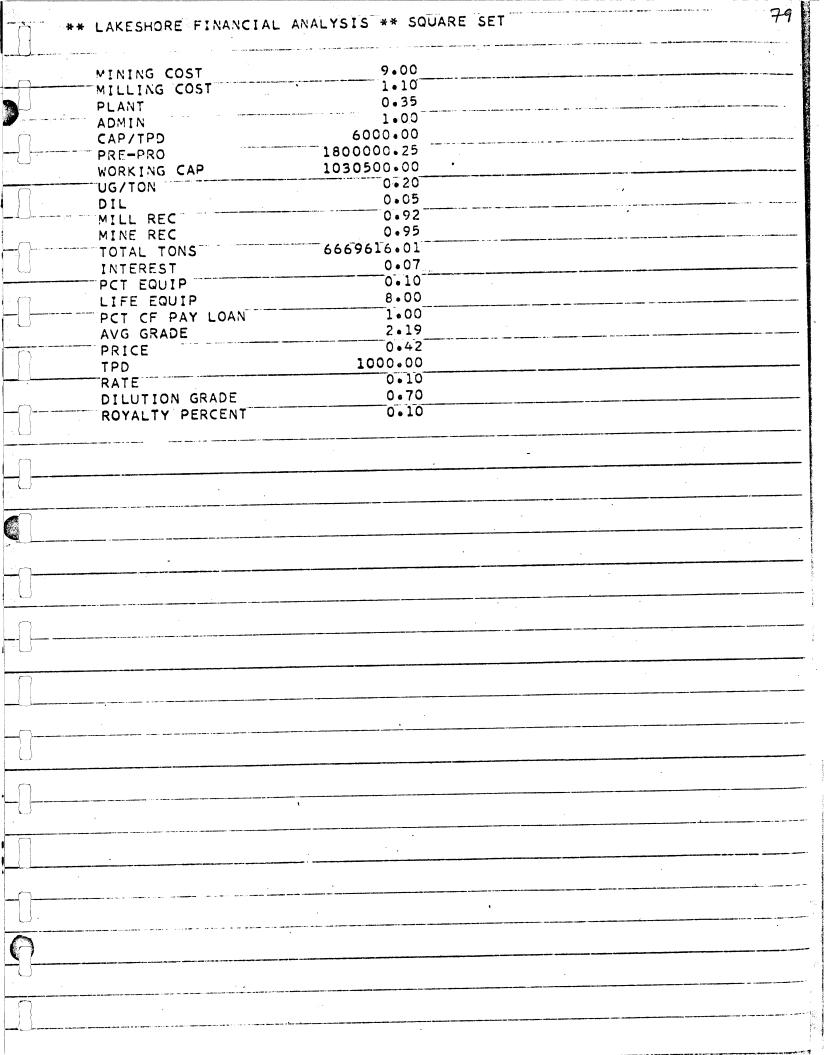
Ť	* LAKESHORE	F INANCIAL	L ANALYSIS	** BLA	BLASTHOLE STO	STOPING				*	LAKESHORE		ANALYS15	** BLA	STHOLE ST	OPING
YEAR	TONS	GRADE	185 ACC	NET SM R	ROYALTY	OP-COST [	DPREC IN	INTEREST TO	TOTAL COST	YEAR	OP-MARGIN D	DEPLETION	FD-TAX C	CASH FLOW	LOAN-PAY	CASH-AVAIL
1970.	1080000	1.4454	7185	50578	5057	2	•	1049999.	6772835.	1970.		o	, i	1457203.	720	
1971.	9000	1.4454	7165276	50578	5057	5238000	484835	947995	6670830.	1971.		ó		1559206.	5595C	• • • •
1972		1.44.04	7485	505782	50578	30	മെ	722066	6444901.	1973.	1300302	3280	1125.	1754011	75401	0
1974	9000	1.4454	7185276	605782	50578	23	oo,	599285.	6322120.	1974.	_	154	2116.	1715802	71580	•
1975	1080000	1.4454	27185276	8605782	860578	5238000	484835	479179.	6202014.	1975	1670567	835283	225526.	1925876	1929876.	• • • •
1977	80000	1.4454	7185276	605782	60578	238000	CO I	216709.	5939544.	1977.	_	9282	3763.	2046730	04673	
1978.	80000	1.44.94	7185276	605782	60578	2380	40	139171.	5862007	1978		941598	. 2926 . 0404	2074439	91996	a) (
0 C C C C C C C C C C C C C C C C C C C	0000	1.4454	7185 7185	503 505 505	7 CO 9 7	ソヘ	1 4 D C		5722835	1980	2022368	01118	*603 *603	1961164		96
1981	9000	1.4454	718527	60578	60578	23800	4.8	0	5722835.	1981.		01118	9609	1561164.		
2	0008	1.4454	718527	60578	60578	23800	849	•	5722835.	1982		C1118	6039	1961164	•	5
1983	00000	1.4454	41.0	202	60578	23	484835°	• •	5722835.	1983.	2022368	1011184	6039.	1961164	• • • •	196
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0000	1.4454	718527	605782	6057	23800	846	0	5722835.	1985.		011164	0365	2026898.	939050	7.6
1986	00040	1.4454	718527	60578	60578	23800	848	٥	5722835.	1986.		6	6039	1961164	•	5
1987	10,000	1.4454	7185276	605782	60578	238000	849	• c	5722835	1987		01116	6039	1951164	• •	3 5
EC (		104634	726817	2 6	7004	23800	10 C	•	5722835	1989	2022368	01118	6039	1961164	•	3
4 C C C C C C C C C C C C C C C C C C C		1 . 4 . 5 . 4	71852	605782	60578	23800	9 4 6		5722835.	1990.	_	01118	6039	1961164.	ò	-1
1991	000000	• •	7185276	605782	60578	238000	848	• 0	5722635.	1991	2022368	20	6039	1961164.	0	1961164.
199	80.96	1.4454	3	88833	883	26108	444400	•	2643131	• 7 6 6 7	• 00 ) ( 00 )	0				
	24749964.	1.4454	622993921-197215328-	i	19721520.	19721520-120037104.	11110788	5345056.13649308	36493088.		41000808.	18350404	8727748	43383832	16878096	26505752.
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** LAKESHORE FINANCIAL ANALYSIS ** CUT AND FILL	K CASH FLOW LOAN-PAY	0101022.		•	010.522.	5101022.	1101023		1101022						1417714					0181475.	082512.	02565135.		
AL ANALYSE	ION FD-TAX	•0	•	•	•	•	•	•	•	5	•	•	•	•	•	•	•	•	•	•	•	•	-1000973. 12149398. 0.0000	
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KESHORE FI	OP-MARGIN DEPLETION	-431474.	-431474.	-431474.	-431474.	-431474.	-431474.	-431474.	-431474	-471703.	-471703.	-471703.	-471703.	-471703.	-471703.	-471703.	-471703.	-511931.	-511931.	-511931.	-232756.	-8993972.	VALUE INVESTMENT RETURN	
/· **	YEAR	1970•	1971.	1972.	1973.	1974.	1975.	1976.	1977.	1978	1979.	1980.	1981	1982.	1983.	1984.	1985.	1986.	1987	1988	1989.		PRESENT VA CAPITAL IN RATE OF RE	
	TOTAL COST	6644451.	6644451.	6644451.	6644451.	6644451.	6644451.	6644451.	6644451.	6694680.				6684680.	6684680.	6684680.	:		6724908	6724908	i	129865216•		
	INTEREST T	.086847	769999	169999	169999	769999	169999	169999	169999	810228	810228	e10228.	810228	810228	810228	810228	810228	850457	850457	850457	386669	28834. 15579856.129865216		
	DPREC 1	330452	350452	330452	330452	330452	330452.	330452.	330452.	330452	330452.	330452.	330452	330452.	330452	330452	336452	330452	330452	330452	150243	6428834.		
	0P-C0ST	5543999.	5543999	5543999	9543595	5543999	5543999.	9543999	*6662755	9243999	5543999.	5543999.	5543999	5543999.	5543999	5543999	5543999	5563999	5543999	5543999	2520639.	7856464		
	ROYALTY	690330	690330	690330	690330	690330	690330.	690330	690330	690330	690330	690330	690330	690330.	690330	690330	690330	690330	690330	60030	313866.	3430140.10		
CUT AND F.	NET SM R	6903307	6903307	6903307	6903307	6903307	6903307	6903307.	6903307.	6903307	6903307	6903307.	6903327.	6903337.	6903307.	6903307	6903307	6903307	6903307	6003307	3138662	34301376. ]	- Lagrance materials (A a) of A con-	
LAKISHORE FINANCIAL AMALYSIS ** CUT AND FILL	185 ACC	21807236.	21807236	21807236.	21607235	21827236.	21637236.	21807236.	21837236.	21807236.	21827236.	21807236.	21807235.	21857236.	21807236.	21807235.	21867236.	21807236	21897236	21807236	9914894	2555555 134301376 13430140-107856464		
Thancial A	SAADE	1.7392	1.7392	1.7392	1.7392	1.7392	1.7352	1.7392	1.7392	1.7392	1.7392	1.7392	1.7352	1.7392	1.7392	1.7392	1.7392	1 - 7 3 9 2	1.7392	1.7202	1.7392	1.7392 4	1 !	
AKE SHORE F	3.01	120000	420004	420000	120000	720000	720000	720000	720000	720000	720009	720000	4200004	720000	720000	720000	720000	100001	4200024	100000	327355	14007334.		
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*1	LAKESHORE FINANCIAL	ANALYSIS ** CUT AN	VÐ FILL
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	MINING COST	5 • 25	
	MILLING COST	1.10	•
	PLANT	0.35	
	ADMIN CAP/TPD	1.00 5500.00	
	PRE-PRO	1800000.25	
	WORKING CAP	1386000.00	
	UG/TON	0.15	
• ) (	DIL	0.07	
	MILL REC	0.92	
· · · · · · · · · · · · · · · · · · ·	MINE REC TOTAL TONS	0.95	
	INTEREST	6669616.01 0.07	
<del></del>	PCT EQUIP	0.10	
	LIFE EQUIP	8.00	
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	AVG GRADE	2.19	
	PRICE	0.42	
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٠.	RATE DILUTION GRADE	0.10 0.30	
	ROYALTY PERCENT	0.10	
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	LAKESHORE F	FINANCIAL	ANALYSIS **	CUT AND	F 3.L.L					*	LAKESHORE FI	FINANCIAL AND	414LY515 ** C	CUT AND FILE	_1	
7. 8.	1048	GRADE	IBS ACC	NET SK R	ROYALTY	OP-COST [	DPREC INT	INTEREST TO	TOTAL COST	YEAR	OP-MARGIN D	DEPLETION P	FD-TAX CA	SH FLOW	LOAN-PAY CA	CASH-AVAIL
10000000000000000000000000000000000000	00000	00000	25908536 25908536 25908536 25908536 25908536	00000	820161. 820161. 820161. 820161.	50000000000000000000000000000000000000	698389• 698389• 698389• 698389•	1	7012388. 6937666. 6857713. 6772164.	1970. 1971. 1972. 1973.	369066 443788 523741 609290	00000	0000	1267456. 11222131. 1222131. 1397680.	1067456. 1142:78. 1222:13:. 1307680.	00000
10.01.00	777700000 777000000 777000000 777000000	2.0663 2.0663 2.0663 2.0663	25908536. 25908536. 25908536. 25908536. 10782950.	820161 820161 820161 341349	2000	5543999 5543999 5543999 5543999 2307373		0,000	678766 6483976 6380746 6318961 2598037	1976- 1976- 1978- 1979-		746000000000000000000000000000000000000		474708 564002 617446	1093901	523544 700736
The second secon	6779654.	2.0663	243959680.	77227952.	7722796.	52203336.	6576169.	3845430.	62624936.		_ :	2039899.	550772. 1	2905636. 1	11681354.	1224281.
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YE18	8701	GRADE	IBS ACC	NET SK R	ROYALTY	0P-C05T	DPREC IN	INTEREST TO	TOTAL COST	YEAR	OP-MARGIN 3	DEPLETION	FC-TAX	CASH FLON	FLOW LCAN-PAY	CASH-AVAIL	
10404	•		13284606.		420537.	412	109893.	419999.	4651892.	1970.	-867049.	0	0	-757156.	ò	-757155	
	00		3284626	42053A	420537.	4121999	109893.	419999.	4651892.	1971.	8	•		-757156	•	-757156.	
:972.	0	٠.	309782	4205380	420537	4121999	109893	419999	4651892.	1972		0	• •	-757156	0 0	-757156.	
0 1: 1 1) (	* (C)	2.1190	13254606.	420538	420537	714	109893	419999	4651892.	1975				27		-157156	
90.01	20	: -:		90	420537	412199	109853.	419999	4651892.	1975.	ł	0	•	-757156	•	-757155.	
1976	0	-:	3	420538	420537	412199	109693.	419999	4651892.	1976		•	000	-757156	•	-757156	!
1977	8	٦,		4205380	420537	4121999	109693	419999	4651892.	1977	1867049	• d	36	-770005		1770009	
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	0 0	7	328450	4235340	420537	4121	109893.	432849.	4664741.	1981	į	0	•	-170005	•	-470005-	
- CR 50 1	0	7	328	420538	420537	4121	109893.	432849.	4664741.	1987		•	•	-170005	•	-770005	
***	8	•	3284606	420538	420537		109898	432849	4664741.	1983	-879898	ó	ċċ	-770005-	o c	1440000	
*7867	8	٠,٠	3224606	420538	420537	417	*********	436649	100000000000000000000000000000000000000	1006		• •	ć	-770005		770005	
10 i	0 0	7	NO	420538	420337	3 3	* # 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	445697	4677590	1986	-892747		ó	-782854		-782654	
0.0	) C	•	3246	420538	420537	3	109893	445697	4677590	1987	-892747	0	•0	-762854	0	-782854.	
- 100 (2)	72931	-	381472	202012	202012.	1980067.	52788.	214098.	2246954.	1988.	-428845.	•	ċ	-376056.	•	-376056.	i
	6652922	2.1190	245534364.	77716896	7771685	76175968	2030863.	1928275. 8	86135120.	•	-16189916.	; ;	- 0	-14159052.	0	014159052.	-
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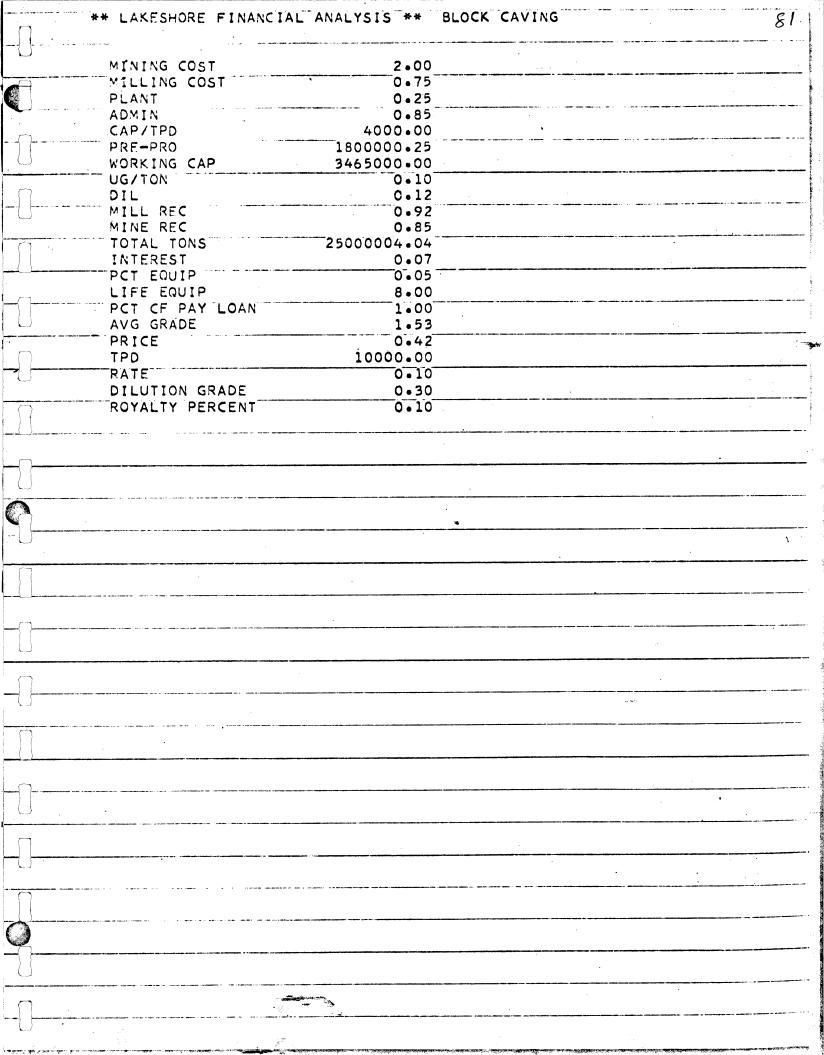
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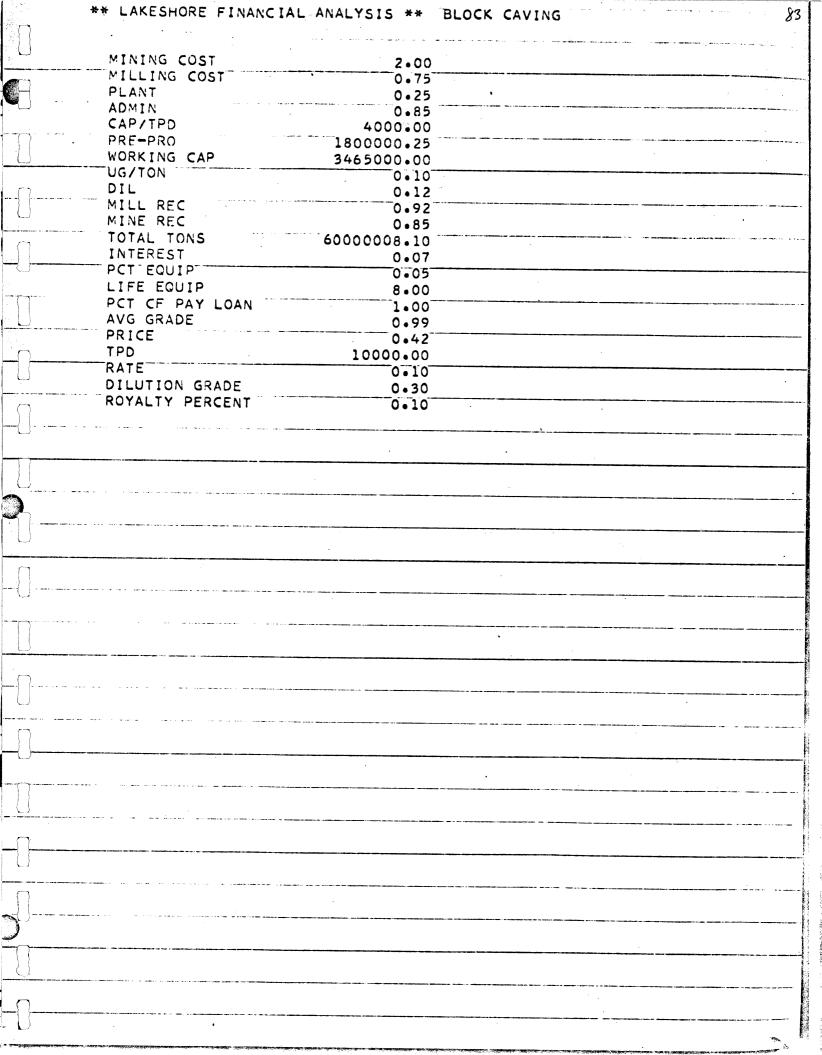
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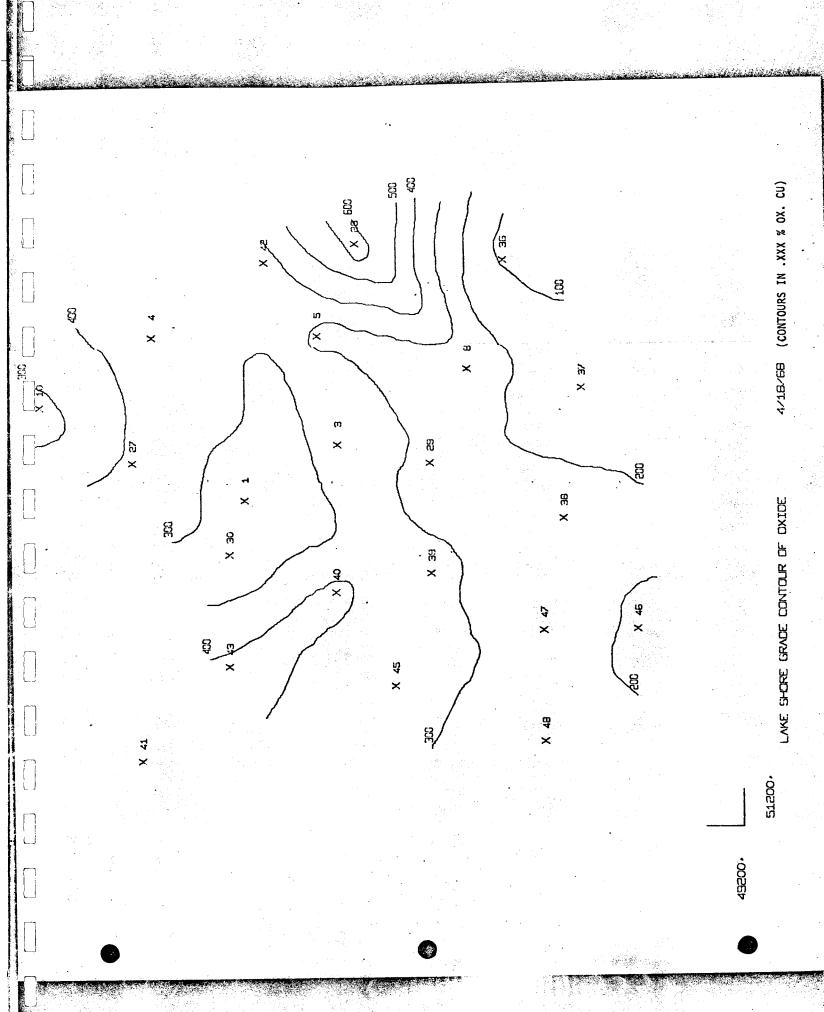


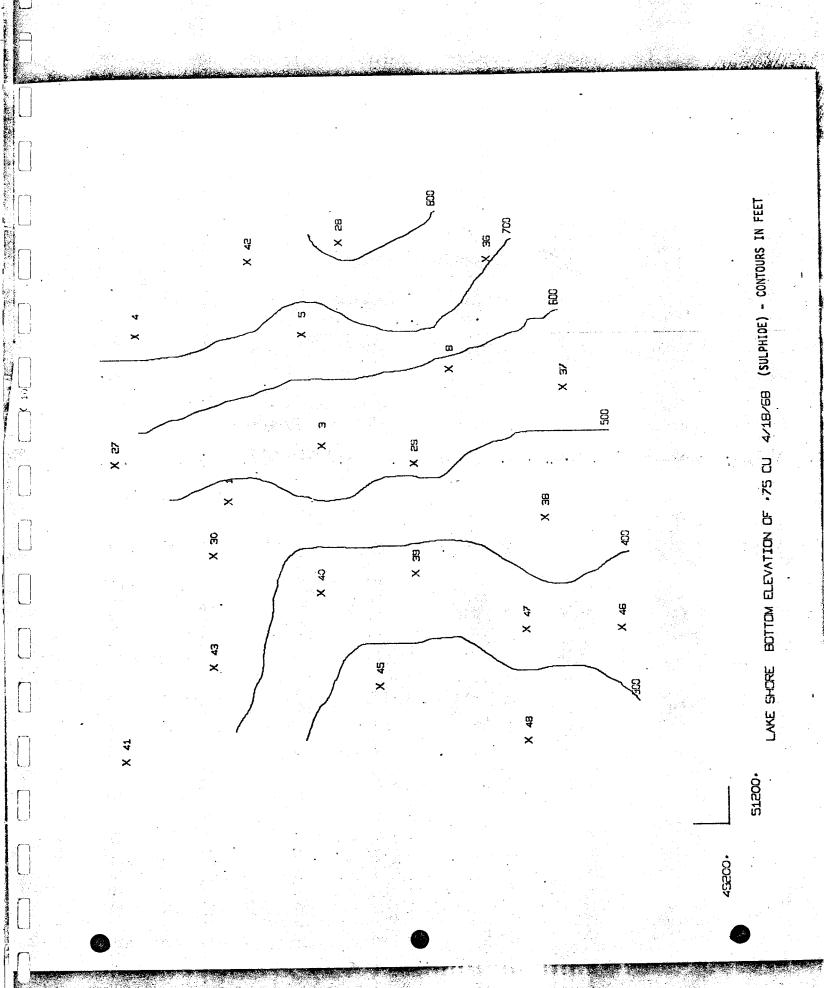
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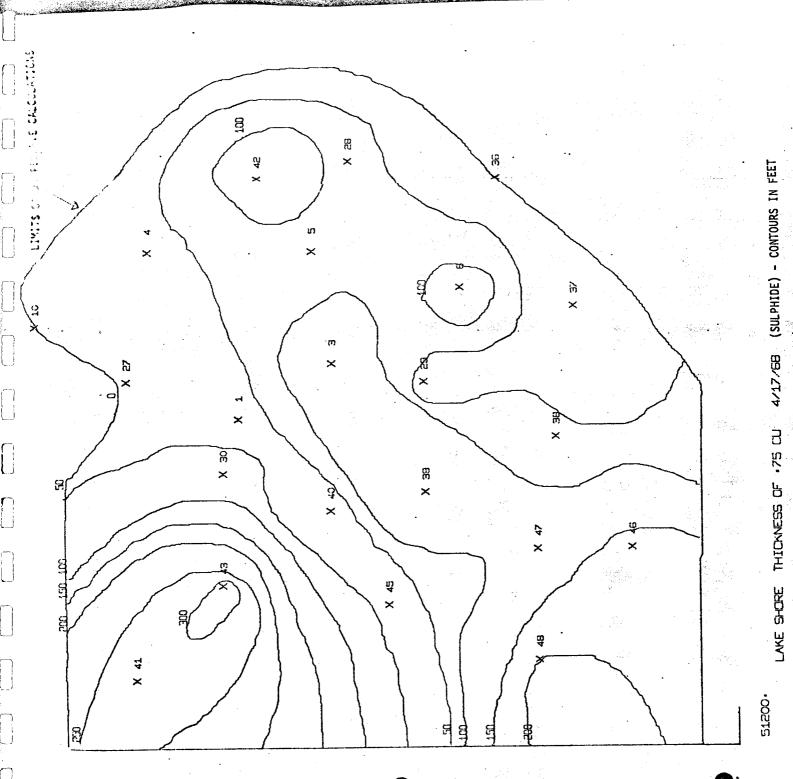
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APPENDIX D

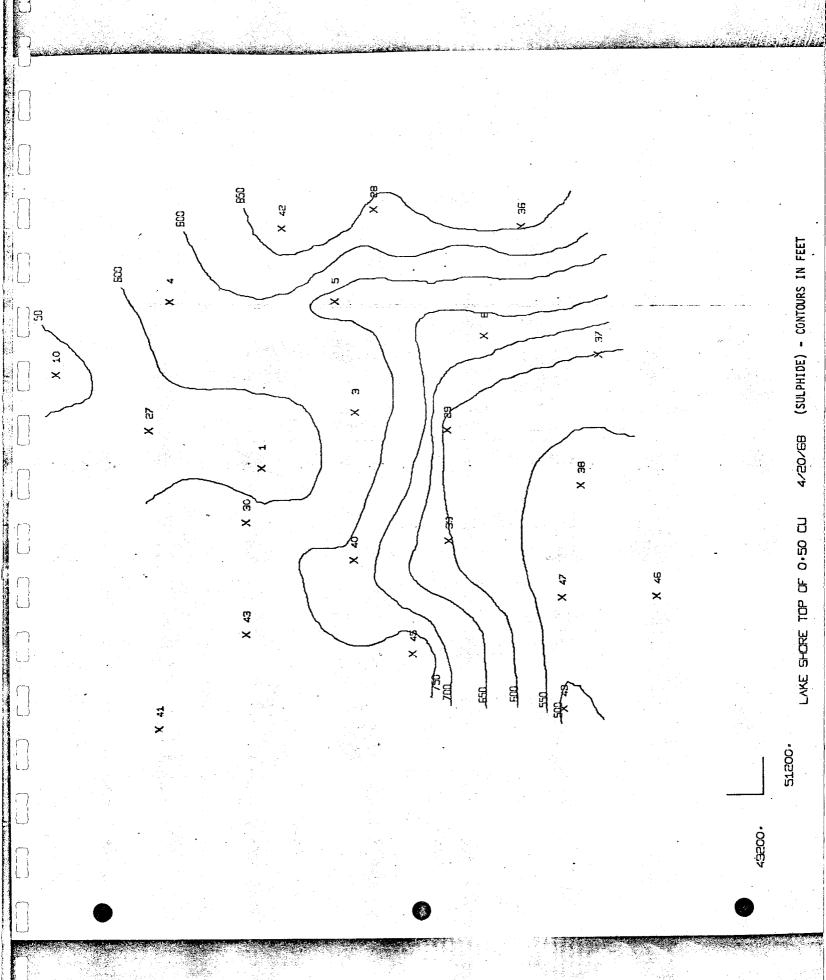


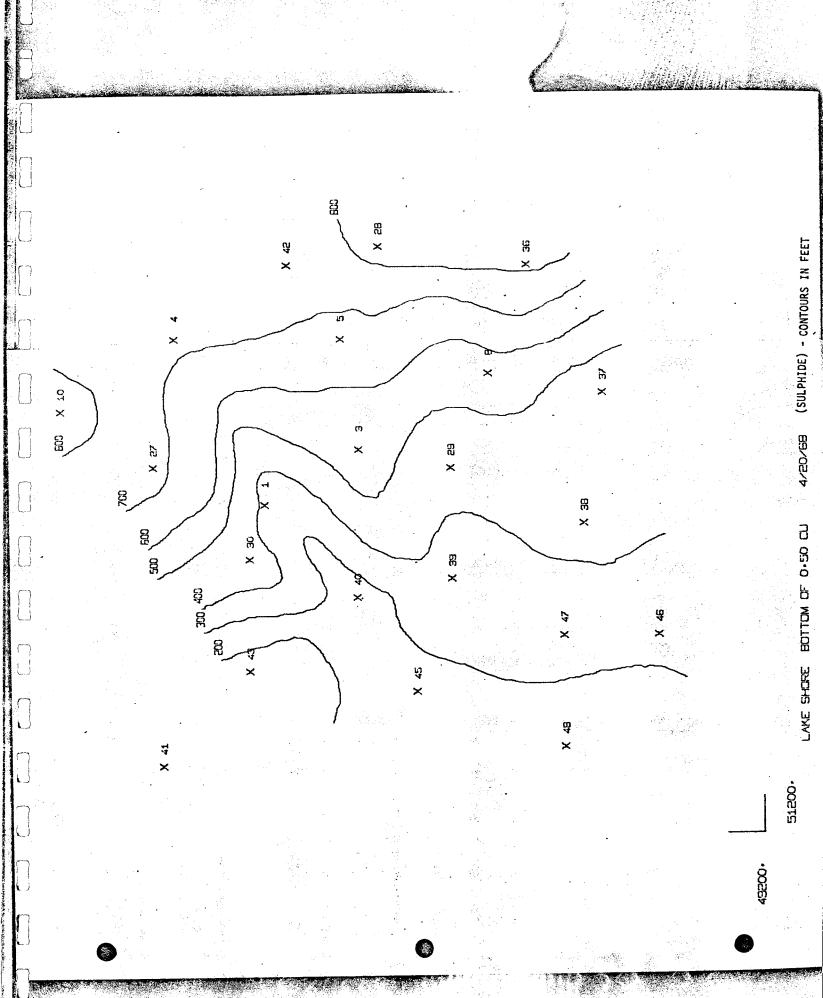


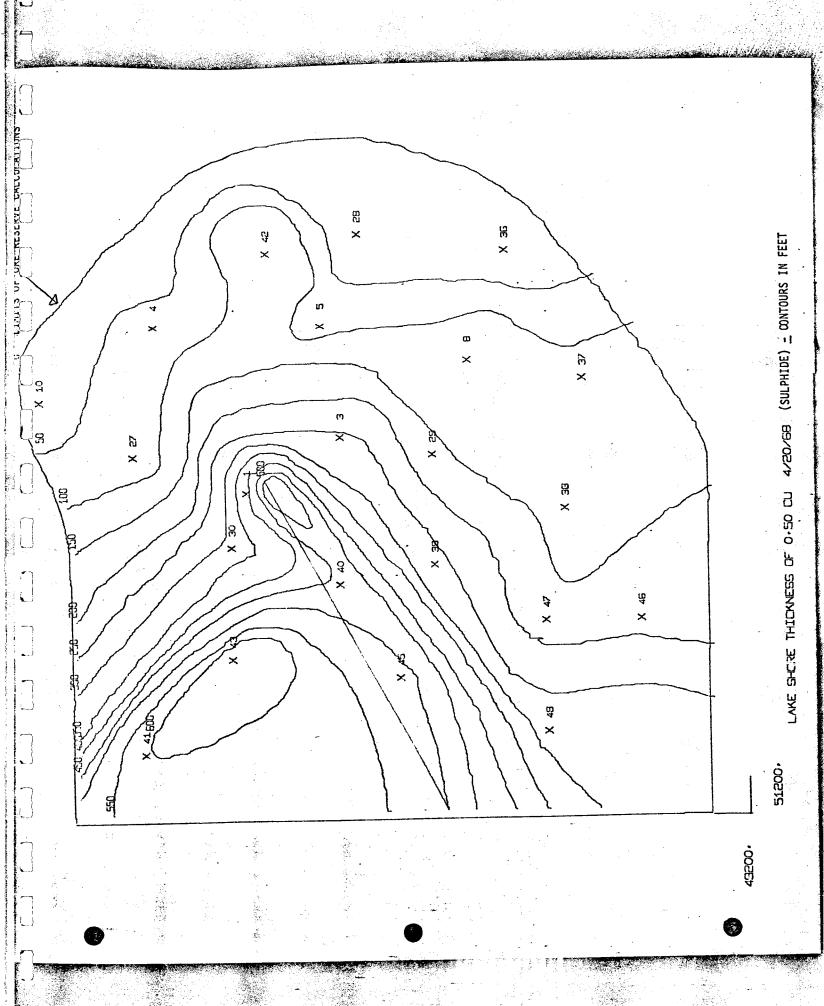


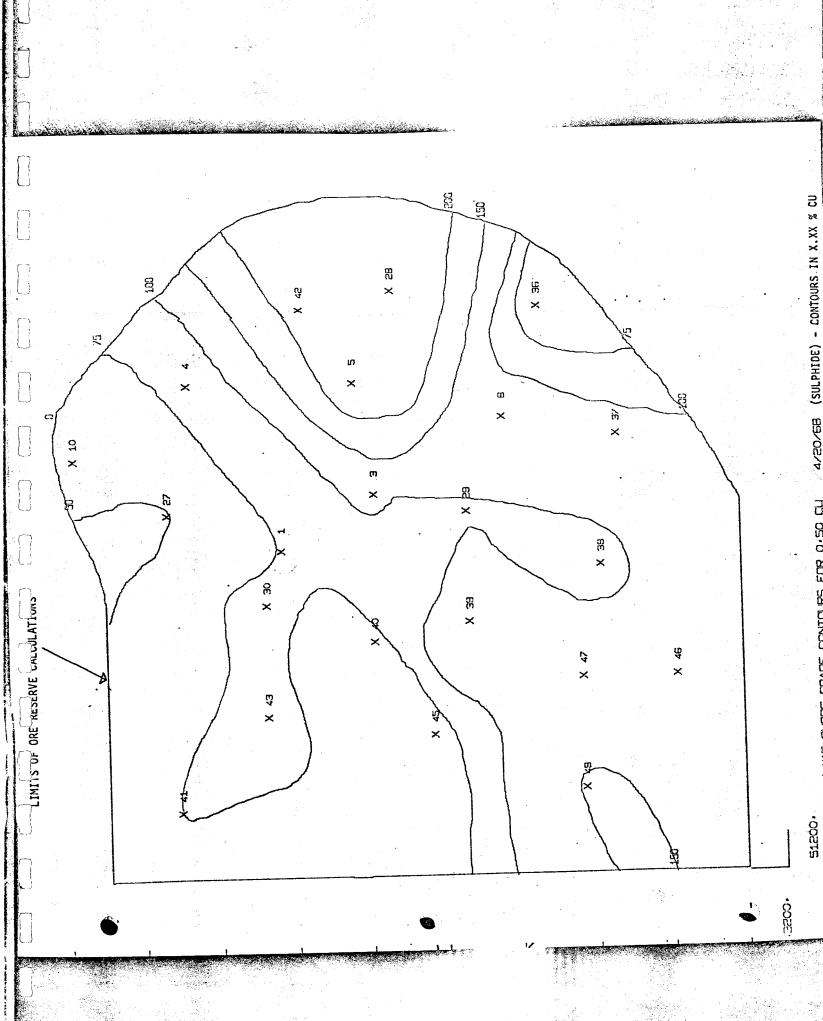
4/17/68 LAKE SHORE THICKNESS OF .75 CU

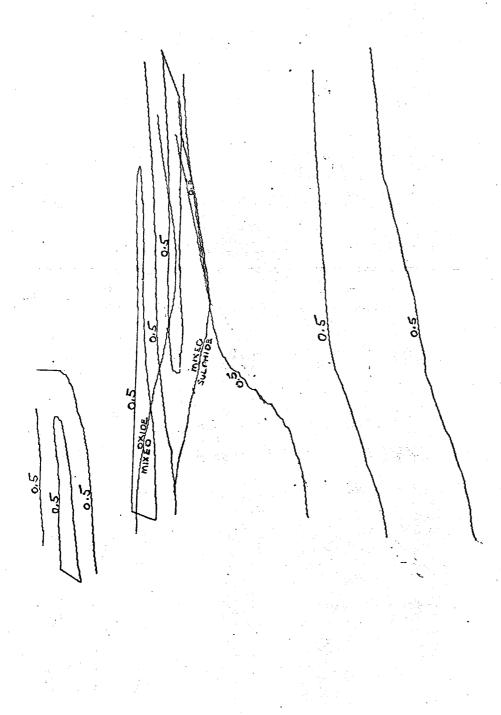




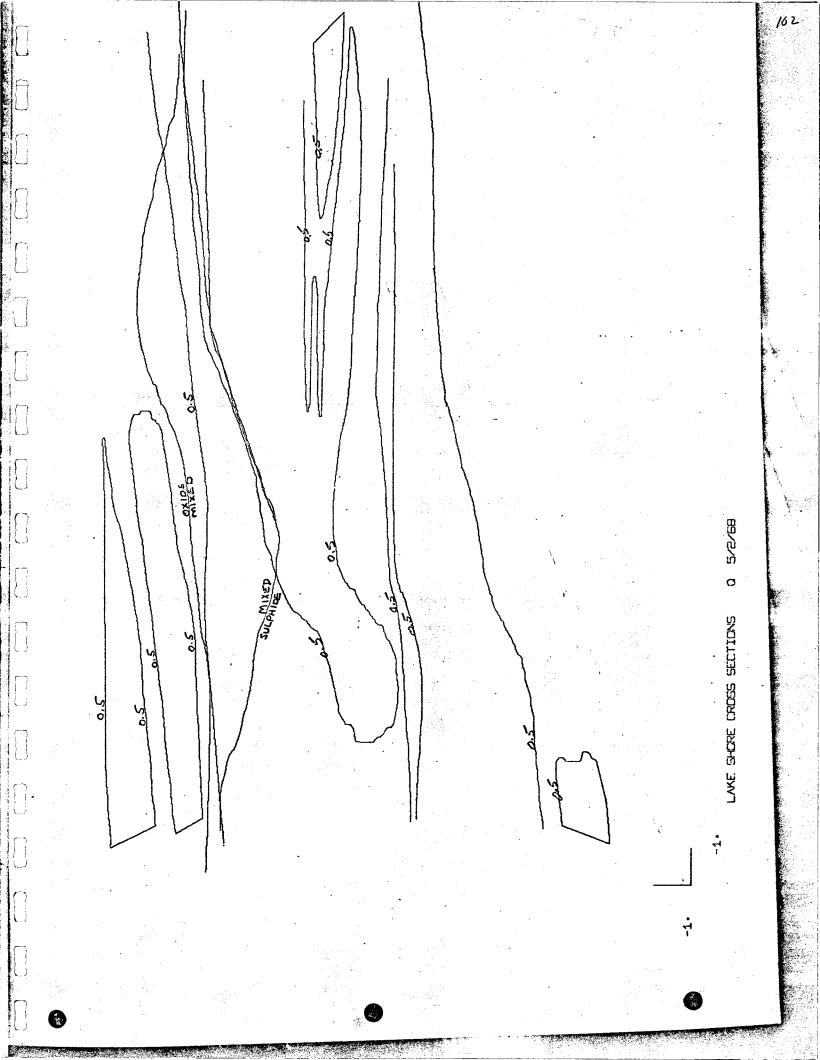


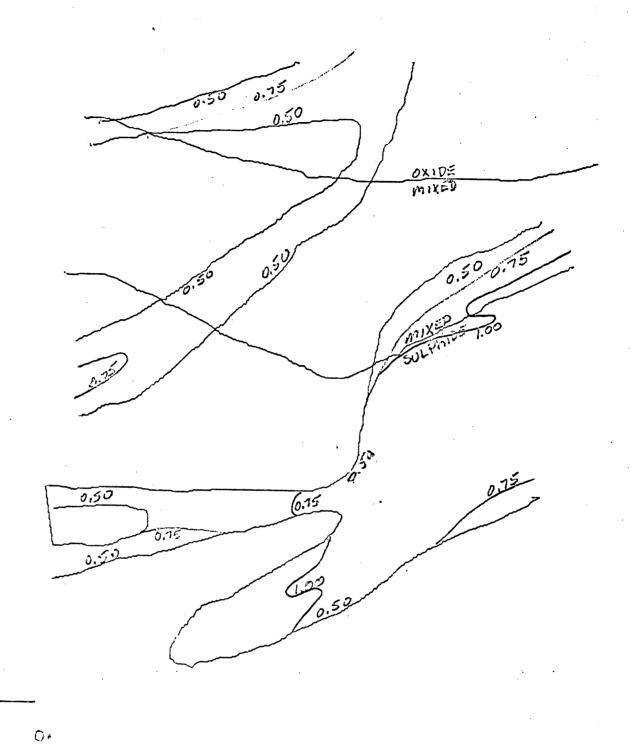






LAKE SHORE CROSS SECTIONS P 5/2/68





LAKE SHORE CROSS SECTIONS T 5/2/68

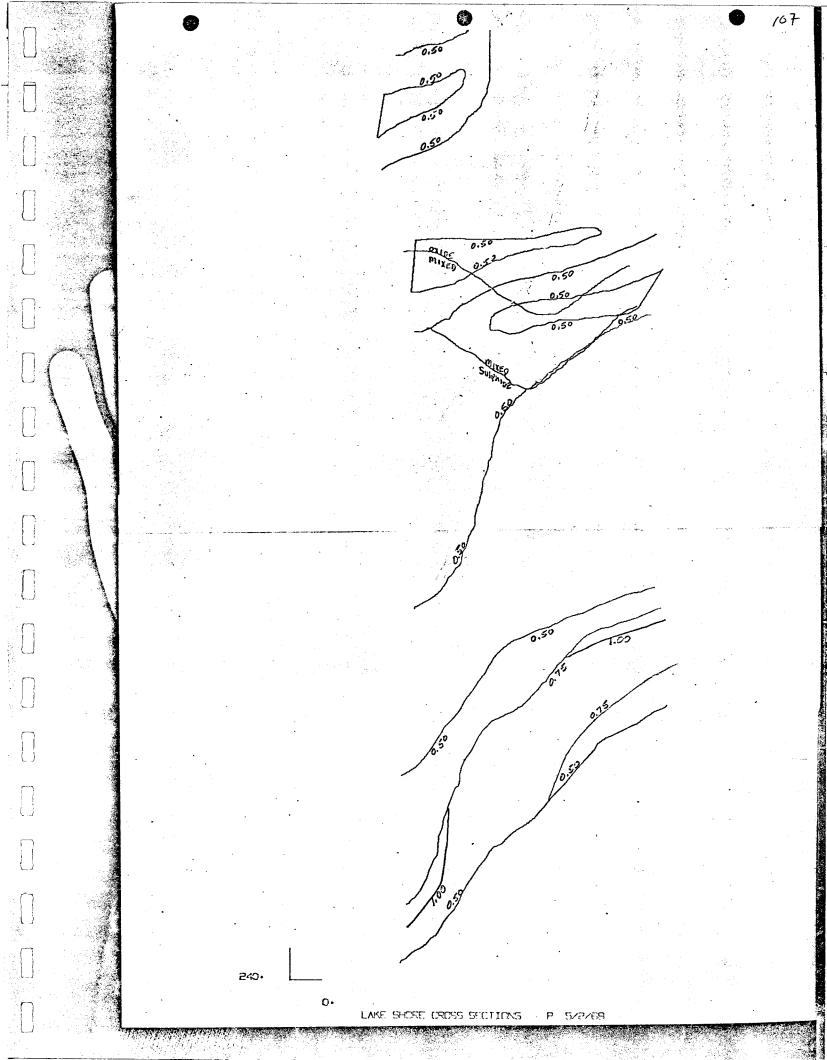
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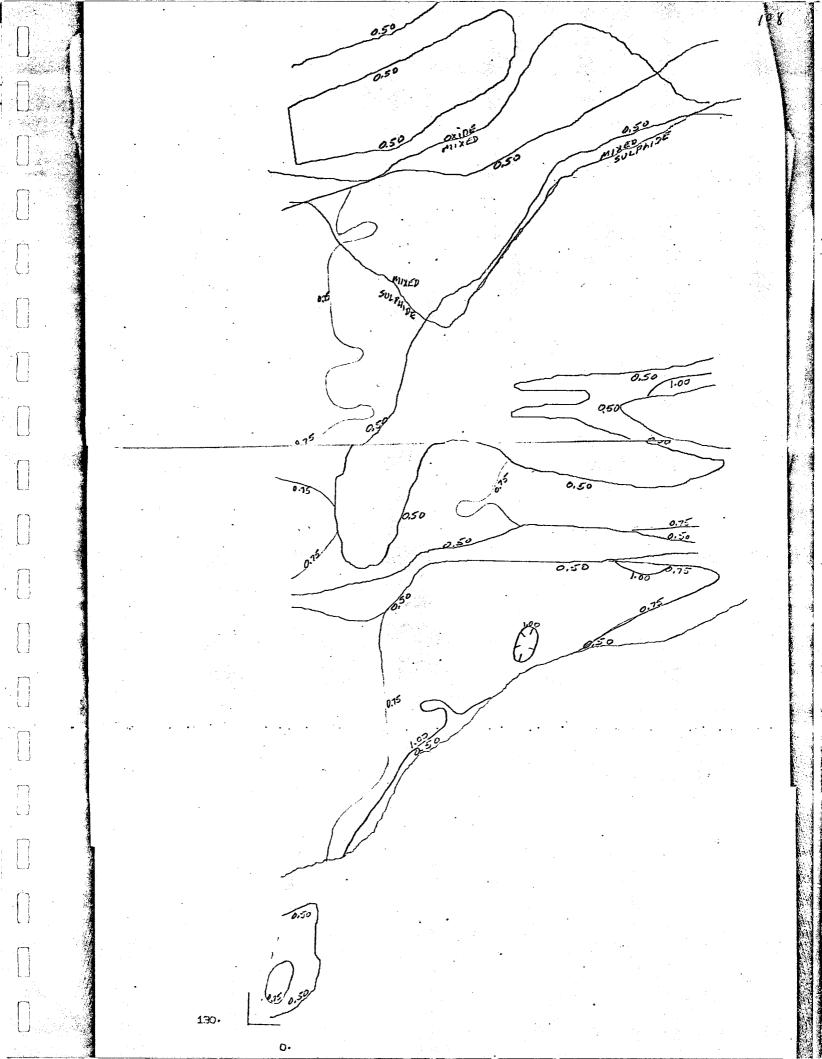
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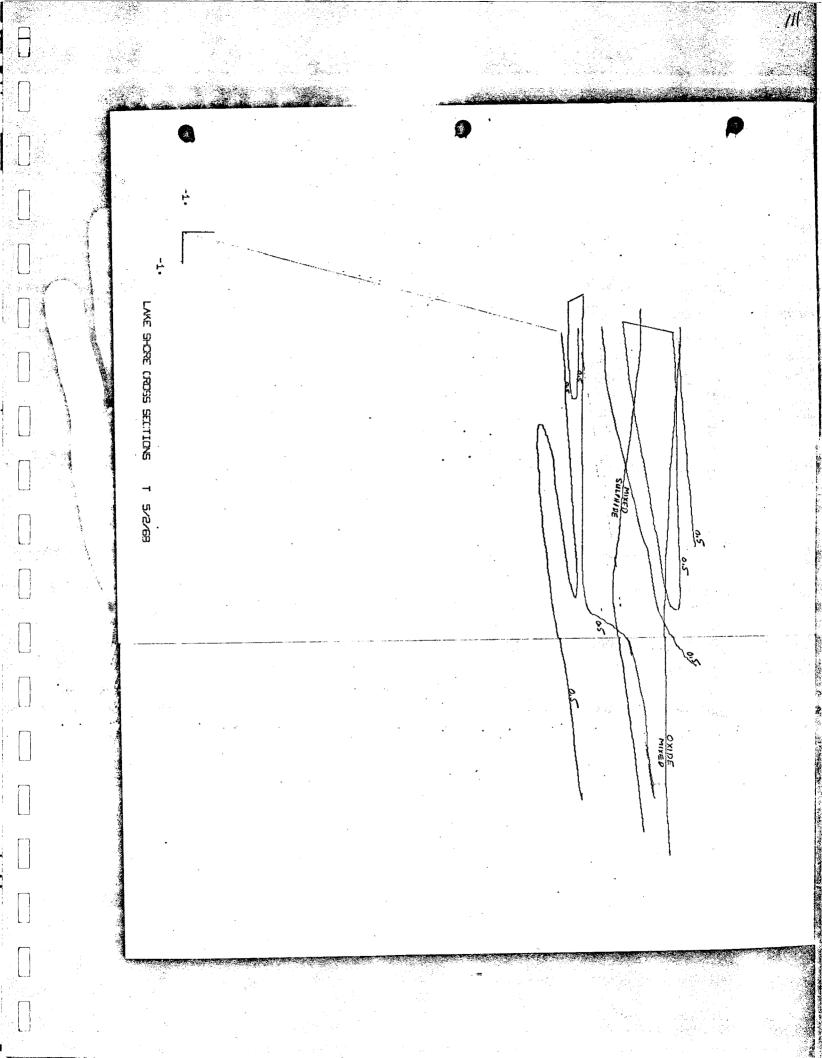
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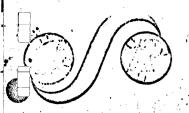
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LAKE SHORE CROSS SECTIONS N 5/2/68









# COMPUTECH RESEARCH, LTD.

Subsidiary of GFI Computer Industries

1019 WEST PRINCE ROAD TUCSON, ARIZONA 85705 887-2220, AREA CODE 602

September 24, 1968

Mr. C. L. Perkins
El Paso Natural Gas Company
24th Floor
American General Building
2727 Allen Parkway
Houston, Texas

Dear Mr. Perkins:

Enclosed please find the summary of the updated ore reserves for the Lake Shore project.

Mr. John R. Reynolds requested that this summary be sent to you. Twelve copies of the summary with supporting documentation are provided.

Sincerely,

William L. Meyer

Systems Development Division

WLM/rcm

Enclosures

Registered Mail, Return Receipt Requested
Special Delivery

#### NOTES ON THE LAKE SHORE SUMMARY OF ORE RESERVES:

- 1. The computer analysis was performed on all data received through Tuesday, September 17, 1968.
- 2. 'PROVEN ORE' is defined as that material totally within the boundary of the actual drilling.
- 3. 'PROBABLE ORE' is defined as that material outside the immediate boundary of the drilling, within a distance consistent with established valuation practices.
- 4. The top of the porphyry zone was taken as the bottom of the mixed oxide-sulfide zone, as specified on the geologic summary sheets received from Claude Barren. Some difference of opinion exists as to the actual top of the porphyry zone, which could add a considerable tonnage to that shown under Item 1 on the summary.
- 5. Tactite reserves are included within the porphyry reserves shown under Item 1 on the summary.

Willia L. Mayor

William L. Meyer
Director
Systems Development Division

WLM/rcm

	E SHORE PROJECT				
1.	PORPHYRY RESER CUT-OFF GRAD	VES FOR E FOR PO	ORE GREATER TO PRPHYRY = 0.50	HAN 200 FEET	THICK
·	ORE CLASS	GRADE	TONNAGE		
	PROVEN ORE PROBABLE ORE		14,665,400		
1	TOTAL ORE	0.808	85,896,650		
	•				
. 2.	TACTITE RESERV CUT-OFF GRAD			BODY	
	ORE CLASS	GRADE	TONNAGE		
	PROVEN ORE PROBABLE ORE	1.752 1.967	2,606,400		,
	TOTAL ORE	1.781	19,281,400		
	and and and any and also and and any out and and also and				
3.	TACTITE RESERV	/ES OUTS	IDE THE PORPHY O	RY AREA	
	ORE_CLASS	GRADE_	TONNAGE		
	PROVEN ORE PROBABLE ORE	1.663	7,894,100 2,128,600		ري الله الله الله الله الله الله الله الل
	TOTAL ORE	1.728	10,022,700		
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4.	OXIDE RESERVES				
	CUT-OFF GRADE	GRADE	TONNAGE		
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·	4 1271	0.457	184809568.	200.		
	5 1257	0.456	184157920.	250.		
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	7 1227	0.454	182258112.	350.		
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U	5 705	1.098	18986460.	50.		, 	
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	I NO.	AVERAGE	TONNAGE					
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<u> </u>	2 721	1.405	10324584.	20.				
	3 593	1.410	96806 <b>26</b> 。	30.				
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Server El Paso Natural Gas Company

El Paso, Texas 1999

November 28, 1969

Mr. E. Grover Heinrichs Vice President Heinrichs Geoexploration Company P. O. Box 5671 Tucson, Arizona 85703

BOX 5671 THOSON, ARIZONA 85763

Phone: (AREA 602) 623-0578

Dear Mr. Heinrichs:

In answer to your request I am enclosing a copy of the paper on exploration at Lakeshore that I prepared for the annual meeting of the New Mexico Mining Association which was held in El Paso on November 16 - 19, 1969.

Thank you.

Sincerely,

5/cm al E. Briston

Claude E. Barron Senior Mining Geologist Mining Division

CEB:mp

EXPLORATION AT LAKESHORE MINE

Pinal County, Arizona

By

Claude E. Barron
Senior Mining Geologist
El Paso Natural Gas Company

ABSTRACT

As the result of a general reconnaissance of the Slate Mountain area, an interpretation of the geology was made that assumed (1) the oxide tactite ore body in the Lakeshore Pit had been overturned by tilting to the northwest, (2) that these metasediments would be in place underlying the andesite west of the pit and would trend generally northwest parallel to the trend of the Slate Mountains, and (3) that the strong northwest and north-south fault and fracture system which was exposed in the pit would offer channels for migrating mineralized solutions permitting the deposition of sulphides at depth.

A proposed correlation of this interpretation with Induced Polarization anomalies involved an area that extended to the south and northwest of the Lakeshore Pit. This area was recommended for deep drilling to test the weak I. P. anomalies for sulphide mineralization.

Contour maps based on assay and geological data from gyroscopically surveyed drill holes offered control for delineation and computer evaluation of the discovered ore body.

EXPLORATION AT LAKESHORE MINE

Pinal County, Arizona

Claude E. Barron

Senior Mining Geologist

El Paso Natural Gas Company

The Lakeshore mineral deposit outcrops on the southwest piedmont of the Slate Mountains in Section 25, T10S, R4E, Pinal County, Arizona. This location is in the Papago Indian Reservation, approximately 30 miles south of Casa Grande, Arizona.

In the Basin and Range Province of southwest Arizona, the Slate Mountains form an arcing outcrop that trends from northwest to north, and reaches an elevation of 3330 feet at Prieta Peak near the center of the range. The Lakeshore Mine, about 2 miles south of Prieta Peak, is at an elevation of approximately 1800 feet. Vegetation in the valley is of the desert variety, capable of surviving in the hot summer temperature and the few inches of annual precipitation.

PREVIOUS WORK

Rocks in the Slate Mountains were described in an unpublished thesis by Hogue (1) in 1940. The Lakeshore copper deposits were investigated by the U. S. Bureau of Mines (2) in 1950. Precambrian and Paleozoic sedimentary rocks of the area were described by McClymonds (3) in 1959. Geologic maps prepared by the Arizona Bureau of Mines (4) in 1960 show rocks in the Slate Mountain area range in age from Precambrian to Quaternary. Sedimentary rocks of the northern Slate Mountains have been described in detail in an unpublished thesis by Hammer (5) in 1961. Other work describing surface geology and sub-surface data obtained from shallow drilling is contained in several unpublished reports made by consultants for Transarizona.

O

HISTORY

The mineral outcrop, consisting primarily of copper silicates and iron oxides, was located by Trout and Atchison in the early 1880's. Abandoned in 1884, the property was relocated by B. S. Wilson in 1905. In 1914 Wilson sold the property to Frank M. and Charles Leonard.

The Leonards, who developed the ore body on three levels while working through a 225 foot vertical shaft, leased the property in 1917. This lease was terminated in 1919. The next noteworthy work to be conducted was an examination of the property by the U. S. Bureau of Mines in 1942 which initiated an investigation that started in 1948 and concluded with a report in 1950.

In November 1955, the three patented claims of the Lakeshore property and the Drake claims, consisting of three patented and 19 unpatented claims, were obtained by George Freeman under a lease-option agreement from Treasure State Mining Company. In 1956, a 580 acre lease surrounding these claims was obtained from the Bureau of Indian Affairs by Dwight McClure and George Freeman. In 1960 the Bureau of Indian Affairs approved an assignment of the lease to Transarizona Resources Inc.

El Paso Natural Gas Company's interest in the property was initiated by an invitation to examine the property in September 1962. At that time, the writer made an examination of the mine and plant. Transarizona had developed the mine as a small open pit. Exploration drilling on a closely-spaced drill pattern indicated \pm 1.5 million tons of \pm 1.75% copper oxide. Level maps and cross-sections prepared from the drill data indicated the mineral deposit formed a V-shaped trough that plunged to the southwest, and was controlled by faults.

The Plant had been designed for a copper segregation process that was followed by flotation.

As a result of the examination, a recommendation for a more complete evaluation of the property was made but the request was not approved. However, in June 1963, a limited amount of drilling was conducted in the open pit and a feasibility study of the segregation process was made.

In August 1966, under the direction of the Mining Division of El Paso
Natural Gas Company, an induced Polarization survey was conducted on the Lakeshore property by McPhar Geophysical Limited and, at the same time, the writer
began a general geological survey of the area.

In September 1966 a core drilling program was initiated to investigate the I. P. anomalies that were discovered on the property.

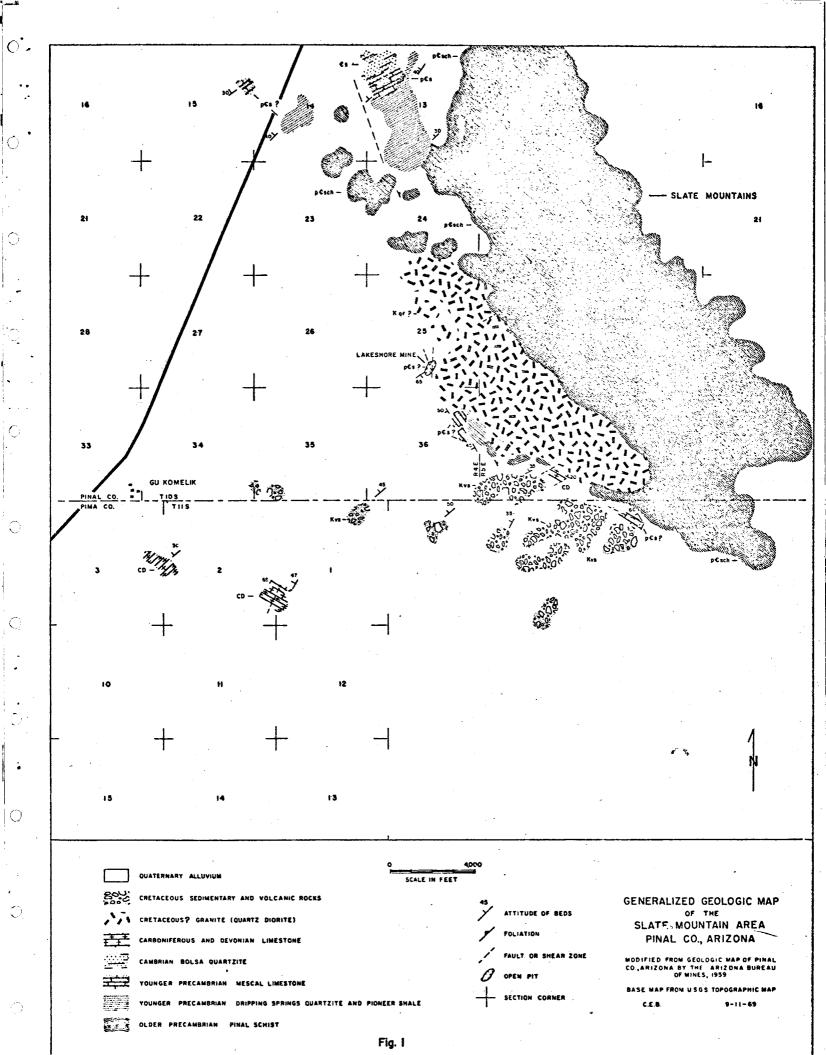
In February 1969, El Paso Natural Gas Company announced an agreement with Hecla Mining Company for development of a major new copper discovery made by the Mining Division on the Lakeshore property.

Reconnaissance of the Slate Mountain Area

The Slate Mountains (Fig. 1), composed primarily of the Pinal Schist formation of Precambrian age (4), strike N ± 45W and dip ± 50° NE. Near the center of the mountains, an elongated mass of quartz diorite has intruded the schist. This intrusive mass tends to parallel the foliation of the schist and was identified as being Precambrian in age (4). However, recent work by P. E. Damon and R. L. Mauger (6) has dated this intrusive by the potassium-argon process as Laramide (Cretaceous-Tertiary). Along the northeast slopes of the mountains, the schist dips under the alluvium and fanglomerates at the edge of the valley.

At the north end of the Slate Mountains, the Pioneer Shale, the Dripping Springs Quartzite, and the Mescal Limestone of the Precambrian Apache Group (4) strike N + 40° E and dip + 45° NW. These northwest dipping metasediments overlie the northwest trending Pinal Schist with angular unconformity. Overlying the Apache Group is the Abrigo Limestone and Troy Quartzite of Early Cambrian age (4) and the limestone, quartzite and shales of Devonian and Carboniferous age (4). Along the southwest slope of the Slate Mountains and to the southeast, outcrops of these formations generally dip to the southwest and strike parallel with the trend of the mountains.

Around the southwest periphery of the Slate Mountains and protruding through the valley fill, are outlying hills of Devonian and Carboniferous limestone, Cretaceous volcanic and sedimentary rocks and Tertiary andesite and breccia (4). The Devonian



and Carboniferous limestone and dolomite have been folded along an apparent northwest trending axis and then tilted to the northwest. In the area southwest of the Lakeshore mine, the breccia and the underlying Cretaceous volcanic and sedimentary rock strikes $N \pm 50^{\circ}$ E and dips $\pm 45^{\circ}$ NW.

Small faults have apparently displaced sedimentary bedding and igneous and sedimentary contacts in these outlying hills. However, any evidence of large faults has been covered by the alluvium. The poles of the measured attitudes of joints and fractures, plotted on a stereographic projection, indicates a preferred orientation of N 30° E with 45° SE dip, N 40° E with 45° NW dip, and N 65° E with 66° SE dip.

Geology of the Lakeshore Pit

C

At the Lakeshore Mine, a small open pit was excavated by Transarizona (Fig. 2). Near the center of the pit, mineralized banded tactite overlaid by a fine-grained quartzite, striking $N \pm 50$ E and dipping $\pm 60^{\circ}$ SE, was exposed. These metasediments terminate on the east side of the pit where they are in contact with diorite along a very strong oblique slip dip fault that strikes NW and dips 65° SW. Merging with this fault is a strong north-south fault that dips 74° W.

Along the west wall of the pit, altered and fractured andesite occurs on the footwall of an andesite and metasediment contact which shows slickensides. This contact, striking $N \pm 40^{\circ}$ E and dipping $\pm 50^{\circ}$ SE, forms the footwall of the oxide ore body.

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MET SEDIMENTS (TACTITE) ATITUDE OF METASEDIMENTS BANDED METASEDIMENTS OC-S USBM. DRILL HOLE FOLIATION FAULT At the north end of the pit, a fine-grained, banded quartzite, striking $N\pm10^\circ$ W with vertical dip, has been exposed in contact with the diorite on the footwall side of the NW striking fault zone.

The south end of the pit has been cut through highly altered and fractured andesite with foliation striking $N\pm30^\circ$ E and dipping $\pm45^\circ$ SE. This andesite overlays the metasedimentary rock and forms the hanging wall of the oxide ore body.

Drill hole data from close space drilling, conducted by Transarizona, indicated that the northeast end of the ore body had been offset to the northwest on the footwall side of the NW striking fault zone.

Drilling conducted by the U. S. Bureau of Mines (2) in 1948 had encountered quartzite underlying andesite at 460 feet in hole C-2, and at 270 feet in hole C-4. In hole C-5, from 455 feet to 545 feet, copper oxides were encountered in a section described by the Bureau as a shear zone (Fig. 3).

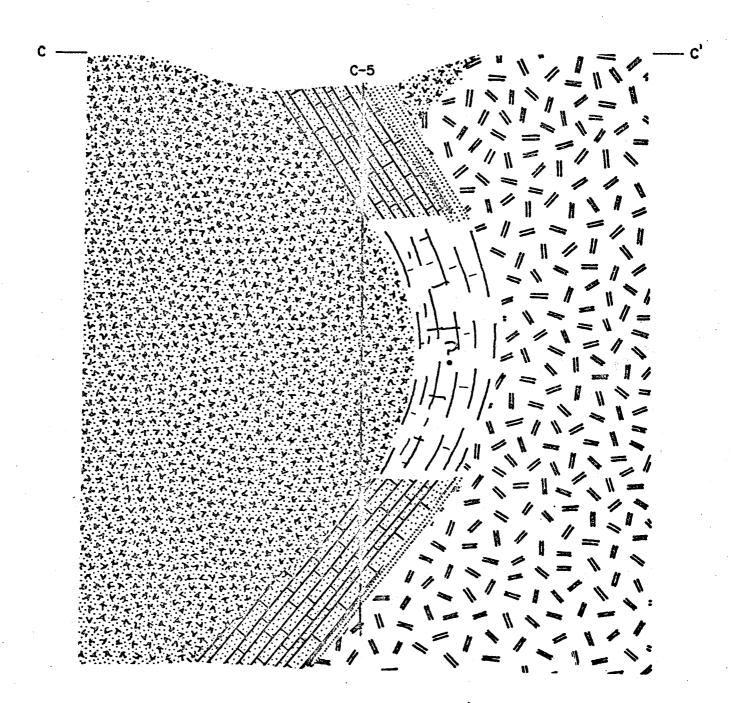
GEOPHYSICAL SURVEY

Induced Polarization Survey

During August and September of 1966, a combined resistivity and induced polarization survey was conducted on the mineral lease and the claims southwest of the Slate Mountains (Fig. 4).

A dipole-dipole electrode configuration, with 500 foot electrode spread length, was used to apply current and measure potential along parallel north-south lines, with ± 1200 foot east-west separations. Alternating current of 0.3 and 5 cycles per second were used to determine the l.P. effect. In addition to the north-south survey, an east-west survey, using shorter electrode spread lengths, was made over the Lake-shore fault system.

Fig. 3



CROSS-SECTION C-C'
LOOKING N 55 E
SCALE I"= 100

INTERPRETATION, BY THE WRITER, OF THE MINERALIZATION ENCOUNTERED BY THE U.S.B.M. IN CHURN DRILL HOLE No.C-5

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Testing I. P. Anomalies

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Several I. P. anomalies were recorded along the north-south survey lines. To test the anomalies, core drilling began at locations D-1 and 605 (Fig. 4). Core hole D-1 was located in the area of a reported anomaly ± 1200 feet southwest of the Drake oxide pit. This test hole was cored for 500 feet through andesite breccia without encountering sulphide mineralization and then abandoned. Hole 605 was an old rotary drill hole which had been terminated in a weakly mineralized porphyry at a drill depth of ± 288 feet. This location was on an I. P. anomaly ± 750 feet north of the Lakeshore pit. Core drilling began at 288 feet and copper oxide mineralization was encountered along fractures in an altered biotite porphyry and in and near the contacts of the biotite porphyry and sections of altered andesite of varying thickness. This hole was anandoned at 790 feet because of drilling conditions without encountering sulphide mineralization.

With the completion of D-1 and 605, the testing of two additional I. P. anomalies began at locations P-1 and P-2 (Fig. 4). Drill hole P-2 was located on an I. P. anomaly ± 1500 feet northwest of hole 605. Core drilling was conducted through 800 feet of fanglomerate without encountering oxide or sulphide mineralization, and the hole was abandoned. The fanglomerate consisted of angular to sub-angular fragments of sedimentary and volcanic rock that was weakly cemented but did not display the prominent high-angle slickenside fracture system that had been encountered in hole 605.

At Hole P-1, located on an I. P. anomaly ± 700 feet west of the Lakeshore pit, low grade copper oxide mineralization was encountered in a fractured and altered andesite and andesite breccia. These andesites had been intruded by a few thin sill-like masses of biotite porphyry. At a drill depth of 750 feet where the drill was still in oxides, a re-evaluation of the I. P. data and a review of the geology was made.

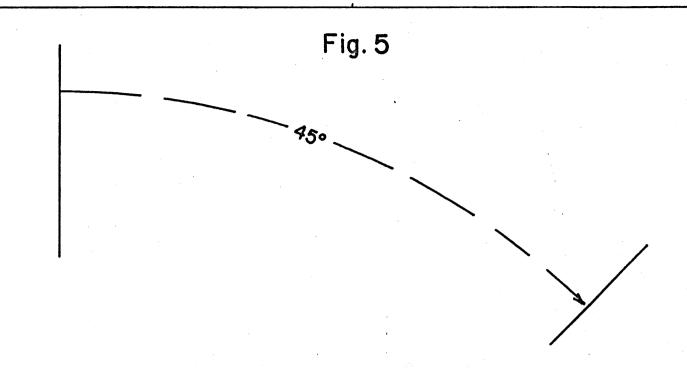
INTERPRETATION OF GEOLOGY

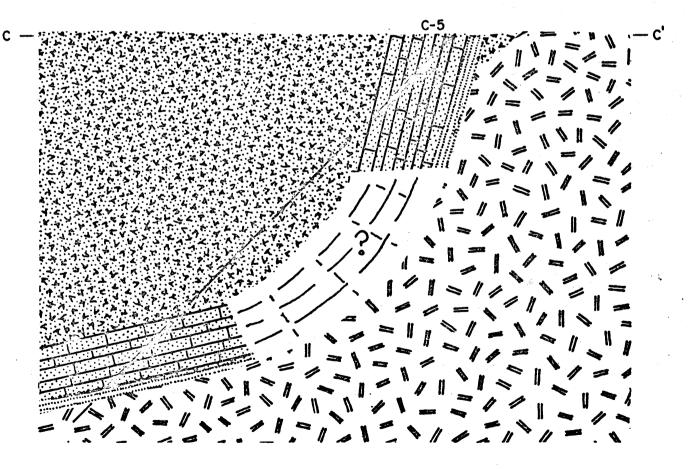
In an attempt to correlate surface geology with subsurface data obtained from core holes, the writer assumed:

(1) The andesite and breccia encountered in drill hole P-1 are extrusive and the biotite porphyry encountered in hole 605 and P-1 is younger than the andesite and younger than the biotite hornblende porphyry that has intruded the Pinal Schist to the east;

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- (2) The high angle slickenside fracture system encountered in hole P-1 and 605 is parallel to the fault and fracture system observed in the Lakeshore pit;
- (3) The present attitude of the Cretaceous volcanic and sedimentary rocks cropping out southwest of the Slate Mountains represents the youngest structural trend in the area, and that this trend, striking $N \pm 50^{\circ}$ E and dipping $\pm 45^{\circ}$ NW, has been superimposed on the older structural system in the area;





CROSS-SECTION C-C'
LOOKING N 55 E
SCALE I"= 100'

ASSUMED ATITUDE OF THE METASEDIMENTS PRIOR TO TILTING TO THE NORTHWEST

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- (4) If the metasediments outcropping in the Lakeshore pit
 were rotated about a horizontal axis trending N 50° E
 to a pre-45° tilt attitude, the metasediments would then
 be dipping steeply to the northwest and be overlaid by
 the andesite (Fig. 5).
- (5) The mineralization, encountered by the U. S. Bureau of Mines (2) in churn drill hole C-5 at a drill depth of 455 feet to 545 feet, is the continuation down dip of the mineralized metasediments and these metasediments would continue to the northwest to underlie the andesite (Fig. 3).

In summation then, this interpretation requires that the metased tend down dip from the oxide outcrop and lie under the andesite to the not the trend of the metasediments is controlled by the northwest trend of the Mountains, the strong northwest and north-south fault and fracture systematical intrusive. Movement of mineralized solutions were controlled by this proving the vironment and sulphide mineralization should be encountered at depth.

RECOMMENDED DRILLING TARGET

To try to correlate this interpretation with the indicated I. P. and plotted anomalies extending to the south of the Lakeshore pit and the and echelon to the northwest of the pit were encircled. This enclosed an arm wide extending from near the center of Section 36 north to Section 25, the to the west line of Section 25 (Fig. 4). This area offered the best possit of projected geology and plotted I. P. anomalies. The enclosed area was

as the drilling target for the Lakeshore project.

DELINEATION OF MINERALIZATION

Drilling and Recording of Data

With the encounter of sulphide mineralization in metasediments, an accelerated drilling program began. Rotary drilling was used to penetrate the andesites and breccias. When the rotary hole was completed to a pre-determined depth, casing was set and a wire line diamond drill was then moved onto the prepared location. NX size tools (2-1/8 inch core diameter) were used until drill depth or drilling conditions required the hole diameter to be reduced; then BX size tools (1-5/8 inch core diameter) were used. Average recovery of core was over

From the recovered core, the following data and observations were recorded and sketched on the logs: rock type, alterations, mineralization, amount of fracturing, angle of fracturing and pitch of the slickensides, fault breccia and gouge, and contacts of major rock type changes.

When core holes were completed, they were surveyed for drift and inclination with a multiple-shot gyroscopic survey instrument. Degree of inclination and bearing of drift were recorded on 100 foot intervals and at major contacts.

With this drill hole survey data, the assay and geological data could be plotted in both vertical and horizontal positions with a high degree of accuracy (Fig. 6).

Subsurface Mapping

To maintain control of drilling and indicate attitude and limits of assay and geological data, the following subsurface contour maps were prepared:

- (1) The andesite-tactite contact
- (2) The tactite-quartzite contact
- (3) The quartzite-diorite contact
- (4) The top and bottom of mineralization within the tactite
- (5) The upper contact of the mineralized biotite porphyry
- (6) The top and the lower drilling cut off of sulphide
- (7) The top and bottom of oxide
- (8) Base of the fanglomerate

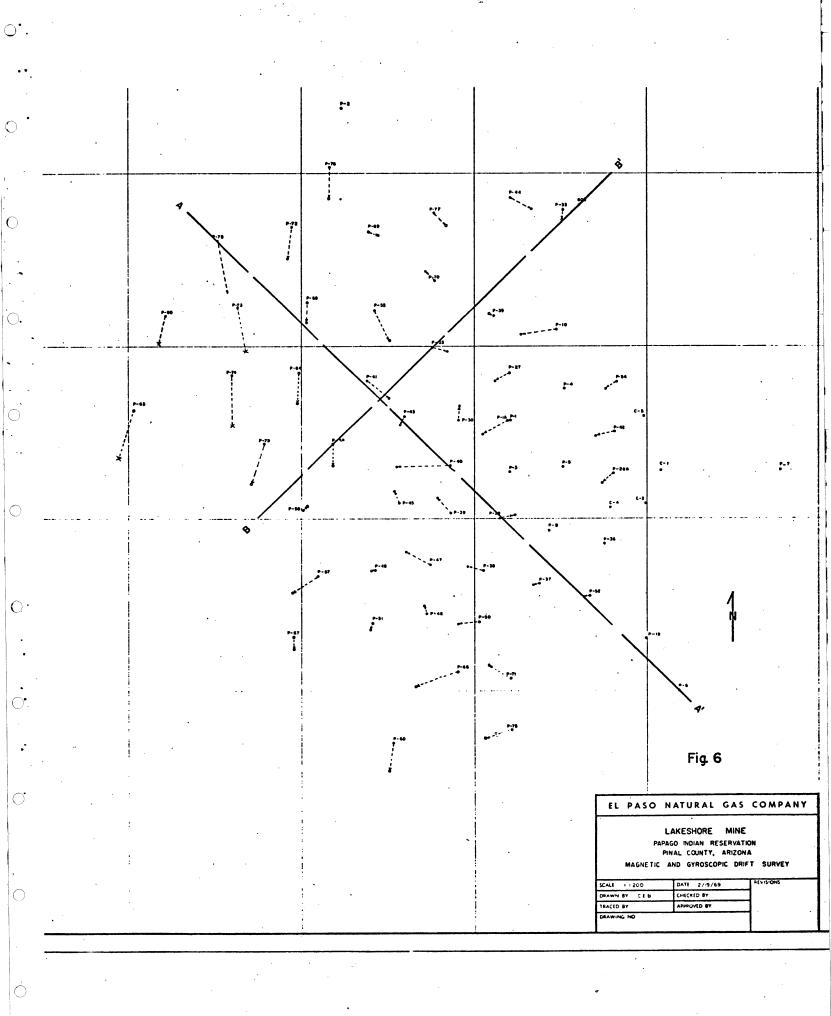
With the above contoured data, isopach maps were drawn indicating direction and thickness of high grade oxides, sulphides, tactite, and mineralization within the tactite.

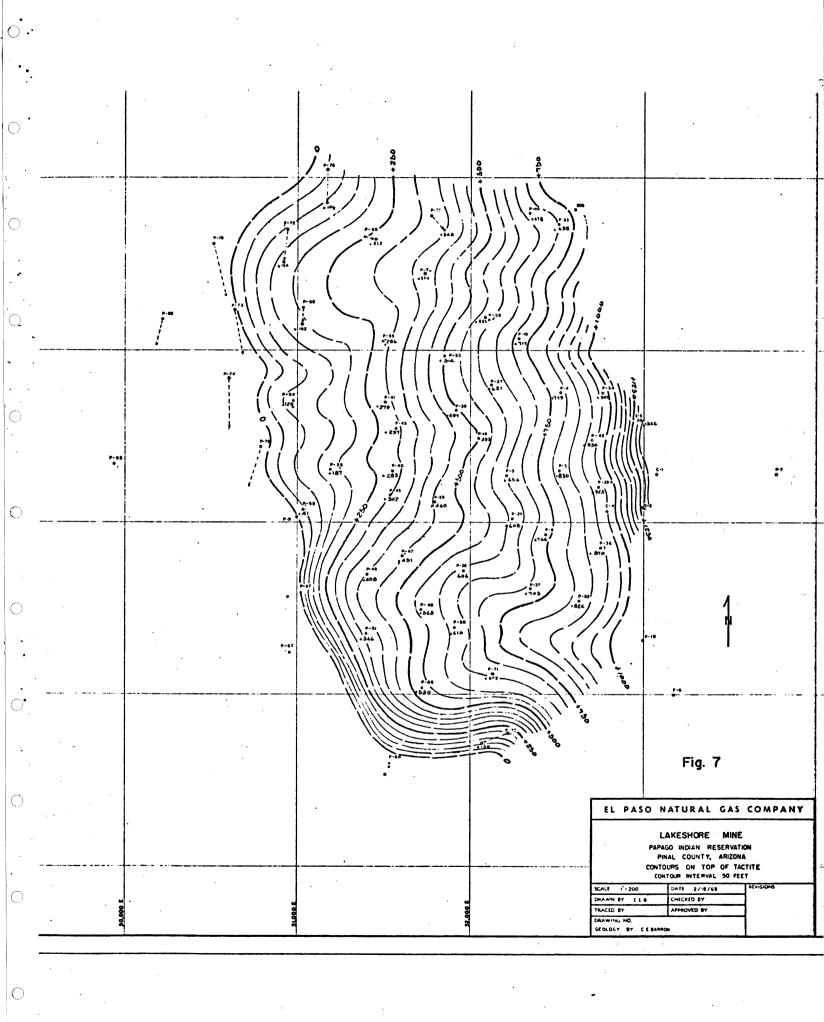
With the same contour maps, cross-sections could be drawn in any direction without regard to drift or alignment of core holes.

Interpretation of Subsurface Data

From the subsurface data, the following interpretations were made:

- (1) The contours of the andesite-tactite contact form a subsurface that strikes \pm north and dips \pm 30° W (Fig. 7).
- (2) The contours at the tactite-quartzite contact form a subsurface that strikes $N\pm20^\circ$ W and dips $\pm20^\circ$ SW, then turns to the northeast and dips to the northwest (Fig. 8). The curving contours





 \circ Fig. 8 EL PASO NATURAL GAS COMPANY LAKESHORE MINE
PAPAGO RIDIAN RESERVATION
PINAL COUNTY, ARIZONA
CONTOURS ON TOP OF QUARTZITE
CONTOUR INTERVAL 30 FEET DATE 2/9/69 CHECKED BY THACED BY APPROVED BY DRAWING NO

form a weakly nosing subsurface structure that plunges to the southwest. As the overlying andesite-tactite contact approaches this plunging structure, a thinning of the tactite occurs along a northeast trend and wedge-like thicknesses of tactite occur to the northwest and southeast of this zone of thinning. This thickening and thinning is best illustrated by an isopach of the tactite (Fig. 15).

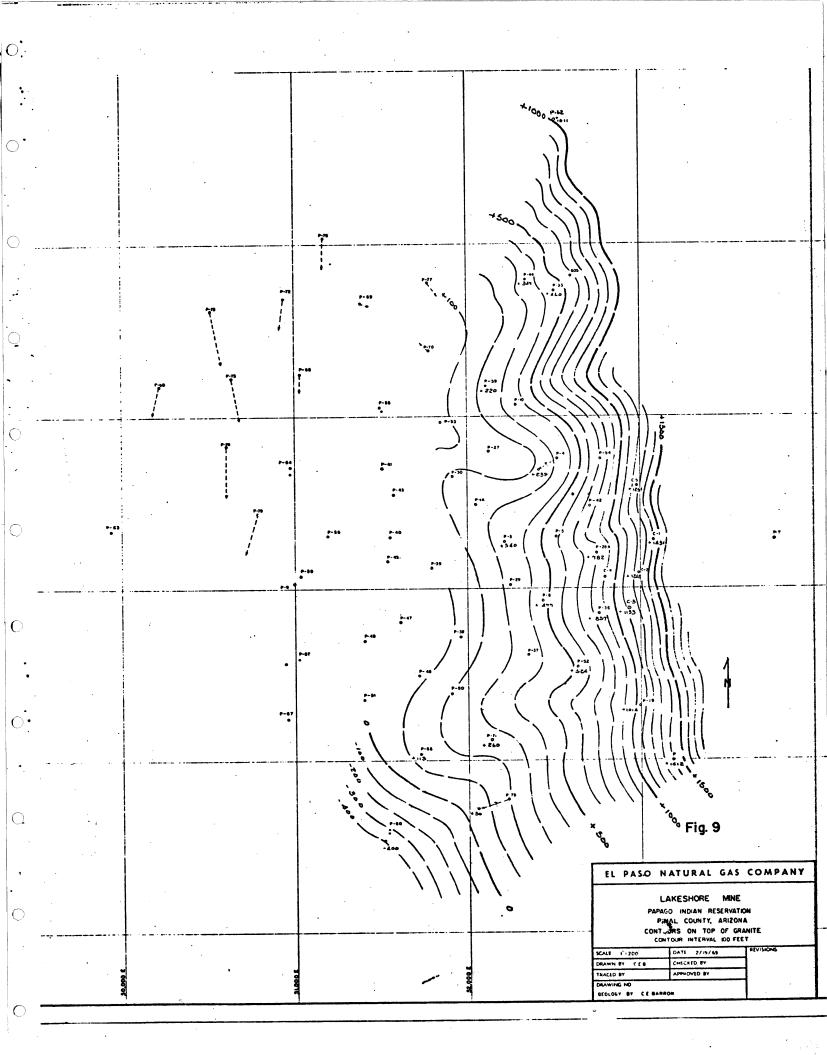
The more consistent thickness of mineralization, within the (3) tactite, occurs in the wedge-like thickness southeast of the zone of thinning. Contours on the top and bottom of this mineralized thickness conform with the N 20 W strike and 20° SW dip of the underlying quartzite. The line of intersection of this mineralization with the overlying andesite trends NE and plunges SW, and terminates this thickness of mineralization in the zone of thinning. To the south and southeast of the zone of thinning, an increasing thickness of massive garnet and epidote occurs over the mineralization, and the mineralized horizon is divided into an upper and lower mineral thickness by an interbedded, fine-grained quartzite. Underlying this sulphide mineralization, a black and gray banded tactite is in contact with the underlying quartzite. This sequence of metasediments, which has been intruded by diabase and biotite porphyry, continues to the south and southeast until it has apparently been displaced by a major fault that trends $N\pm20~W_{\bullet}$

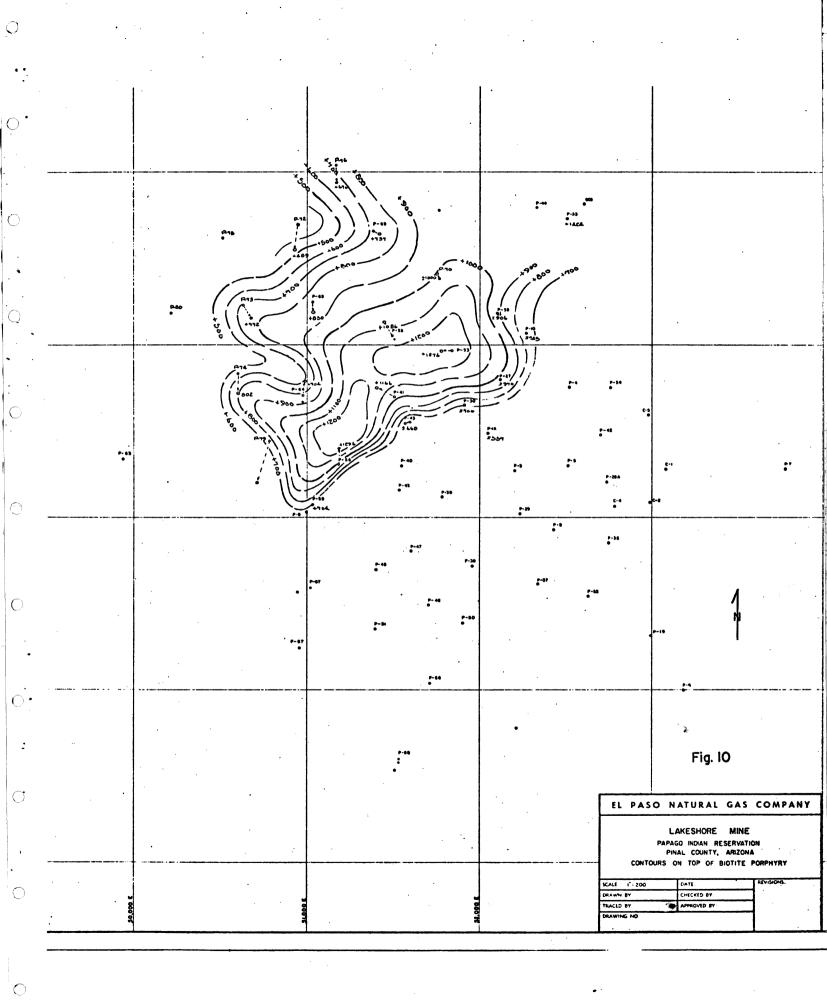
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- (4) To the east the metasediments are in contact with the diorite.

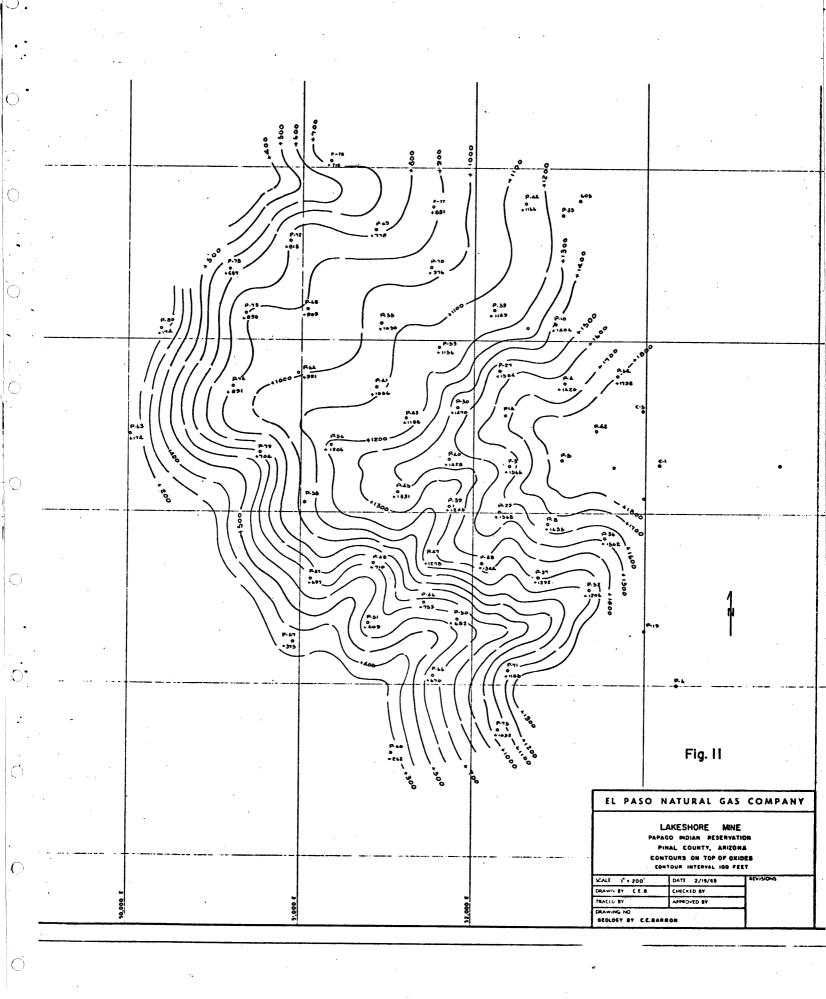
 Contours on this contact form a north trending subsurface that dips \pm 60° W (Fig. 9).
- (5) To the west the metasediments have been intruded by the biotite porphyry along a northeast trending contact zone. Along this contact zone the intrusive forms sills of irregular masses that occur in both the metasediments and the andesite. Better grade mineralization occurs along this zone of multiple sills (Fig. 16).
- (6) Northwest of this contact zone the stock-like intrusive forms a more homogenous emplacement within the andesite but continues to form sills within the metasediments. Further to the northwest, the intrusive again forms a contact zone of multiple sills within the andesite (Fig. 16).
- Contours on top of the oxidized intrusive trend N 55 E and form $a \pm 40^{\circ}$ slope along the northwest side (Fig. 10). On the southeast side the contours indicate a much steeper slope, and to the southwest, the intrusive apparently has been displaced in this horizon by a high angle normal fault that strikes \pm N 20 W. Limits of the intrusive have not been determined to the north and northeast.
- (8) Contours on top of the oxide mineralization form an irregular horizon in the subsurface west of the Lakeshore pit; then this horizon forms a northwestern dip and passes through the top of the mineralized intrusive. As the oxide zone passes through the

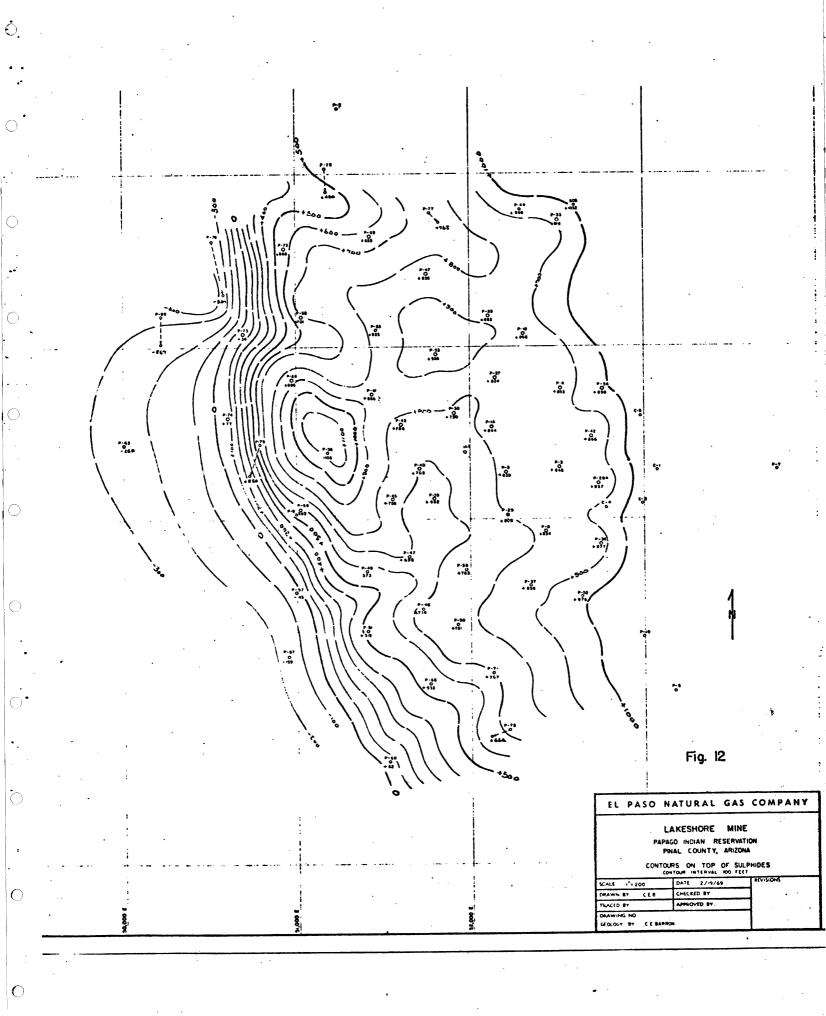


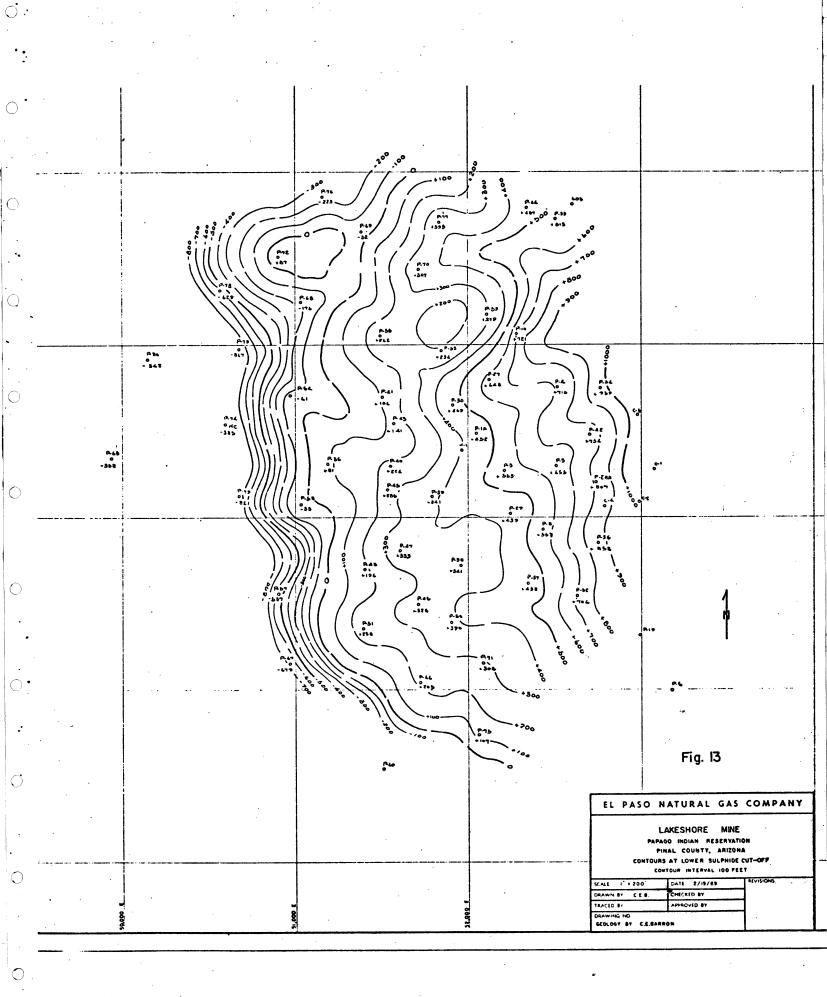


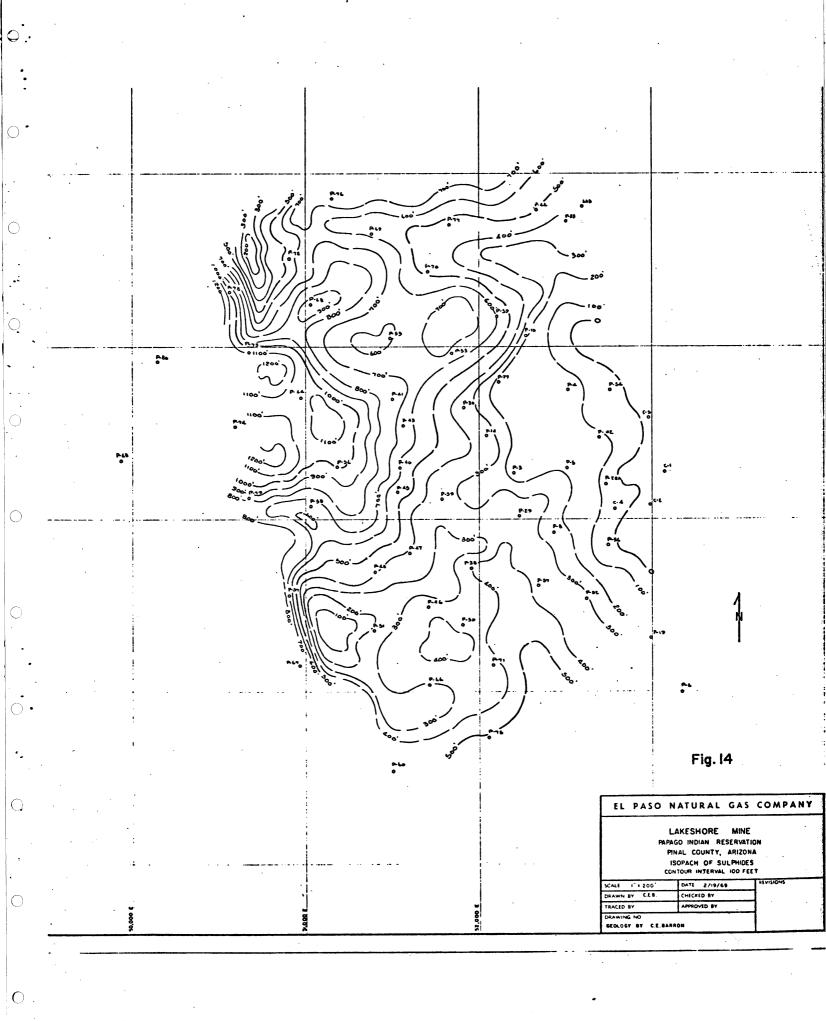
upper part of the intrusive, a \pm 100 foot thick blanket of \pm 1.5% copper oxide mineralization occurs at the base of the oxides. This mineralization trends to the northeast along the top of the intrusive and dips to the northwest. As the dip of the oxide mineralization increases to the northwest, the high grade oxide mineralization thins and a zone of chalcocite has formed an enriched upper thickness of sulphide mineralization (Fig. 11).

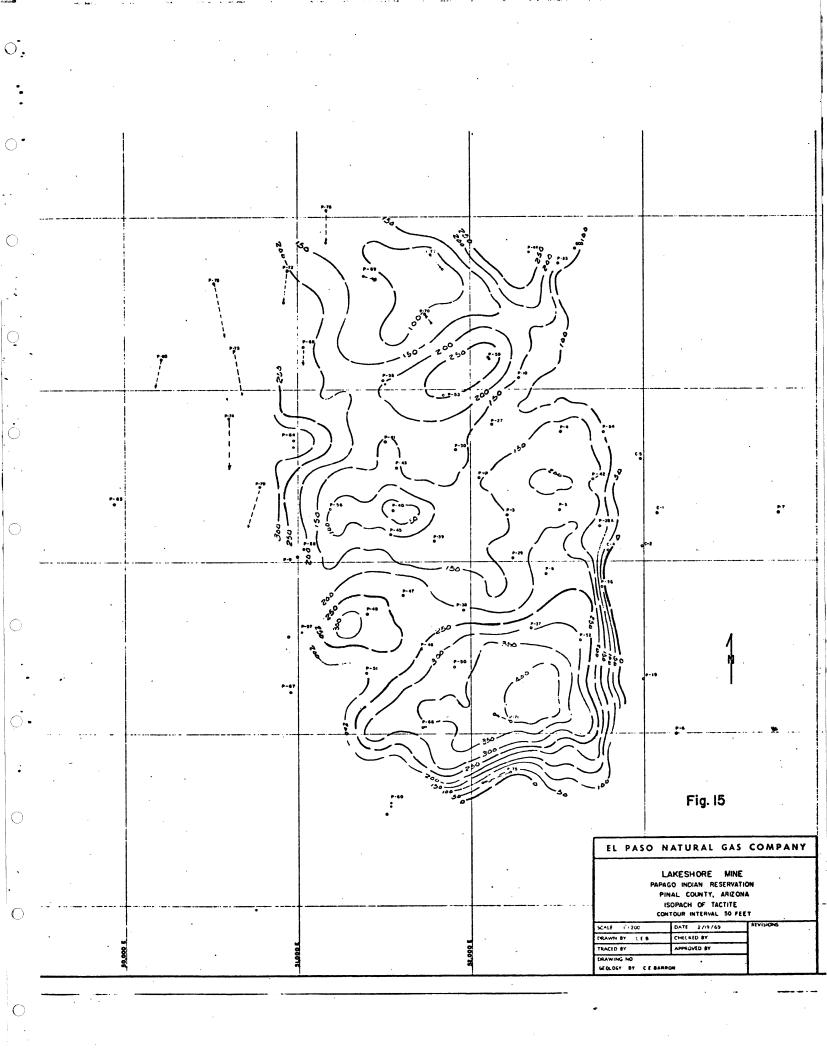
- (9) Contours at the top of sulphide mineralization form a low trough that plunges to the southwest along the southeast flank of the biotite porphyry intrusive. This oxide-sulphide transition horizon then climbs to its highest elevation within the top of the intrusive and forms a northeast trend that dips to the NW. To the southwest the contours turn sharply to the northwest or southeast and form a $N \pm 20^{\circ}$ W trending horizon that dips $\pm 70^{\circ}$ SW (Fig. 12).
- (10) The isopach of the sulphides indicates a wedge-like thickness of mineralization. The thin edge, ±300 feet thick, occurs along the northeast trending contact zone of the intrusive and the metasediments. To the northwest of this contact zone and along the apparent fault zone, the mineralized zone thickens to over 1000 feet. Some core holes in this zone have an average assay value of .85% copper for 1000 feet of recovered core. The limits of mineralization to the northwest and north of this area have not been determined (Fig. 14).

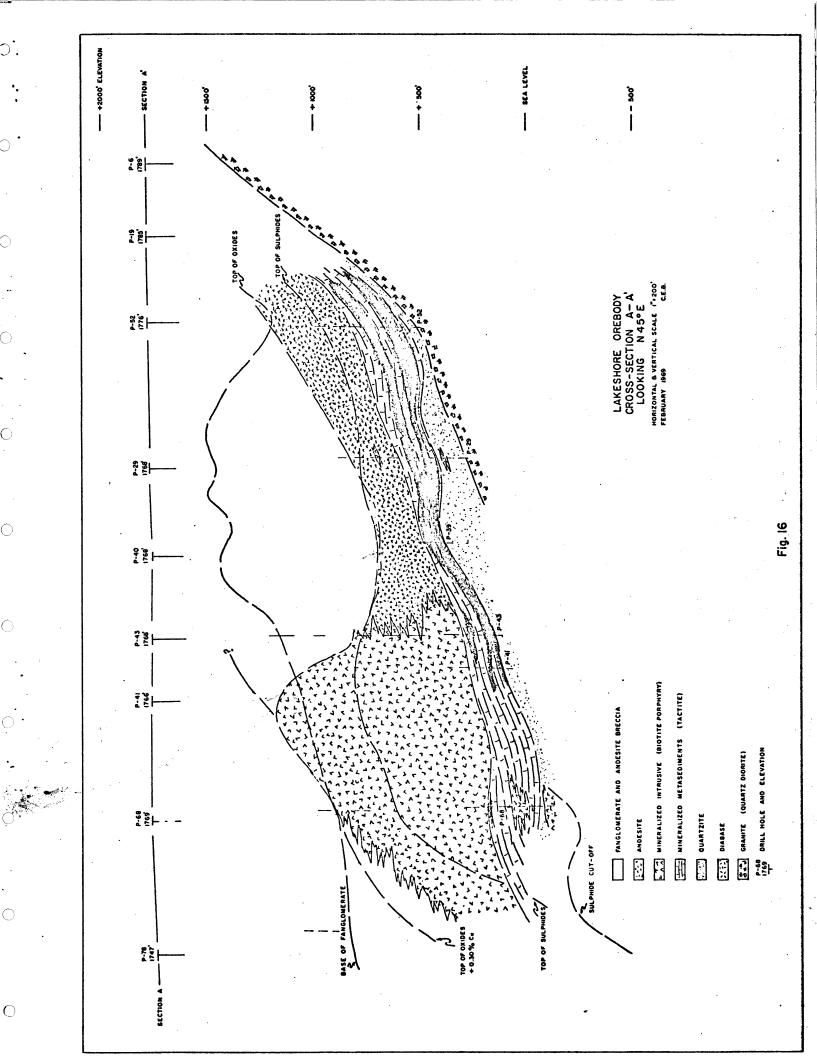




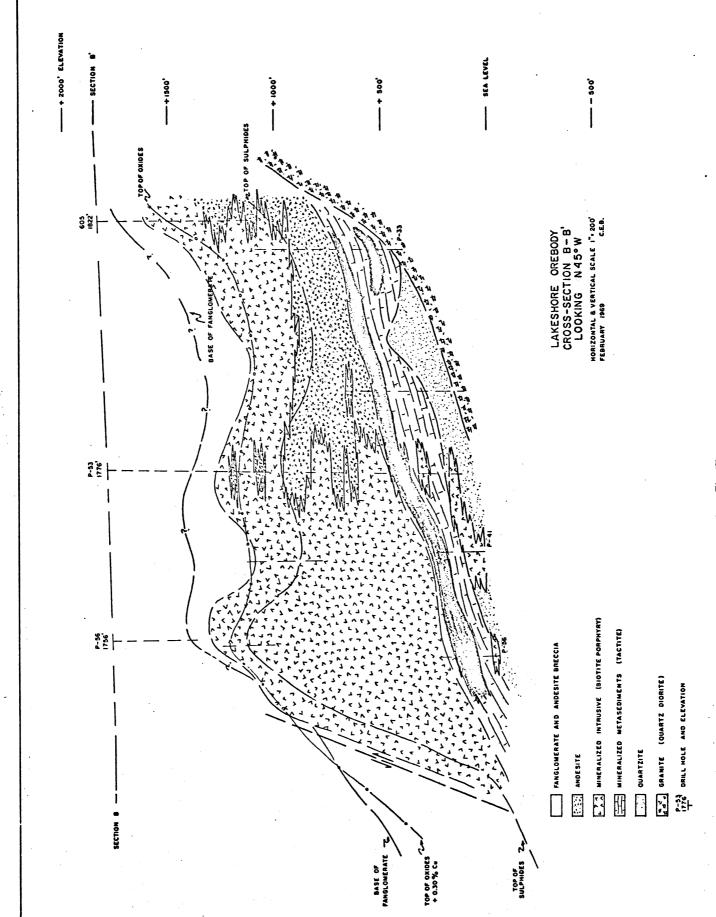








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Fig. 17

Overlying the highly fractured and altered andesite, biotite porphyry and tactite is a relatively unfractured, weakly cemented fanglomerate that thickens from ± 100 feet at the edge of the valley to ± 1500 feet around the southwest end of the biotite porphyry and is apparently in contact with the altered and oxidized top of this intrusive.

In summation, the geological data indicates the occurrence of mineralization at Lakeshore to be the result of the emplacement of a weakly mineralized biotite porphyry. This stock-like mass formed a multiple sill contact with eroded and deformed metasediments and the overlying andesites and breccia. The processes of contact metamorphism formed tactite or skarn in the metasediments and a higher grade of sulphide mineralization was deposited in the more favorable carbonates. Post-mineral faulting and fracturing formed channels for erosion, leaching, and enrichment of mineralization. This mineral deposit was tilted to the northwest and underwent a second period of erosion and oxidization. This oxidized and fractured surface was then buried by the present overlying fanglomerate (Fig. 17).

COMPUTER EVALUATION

During March and April of 1968, a computer evaluation of the assay and geological data from 23 core holes was performed by an independent consultant (7).

This evaluation provided the following information:

(1) Ore reserves, tonnage and grade of the sulphide and oxide mineralization for various cut-off grades and thicknesse.

- (2) Level plans at various vertical intervals showing contours of sulphide copper values;
- (3) Vertical cross-sections of the sulphide copper values;
- (4) A confidence interval analysis to determine future drilling requirements; and
- (5) A financial analysis based on ore reserves of varying cut off grades, and the following parameters mining cost and mining methods, concentrator capacity and recovery, metal prices, capital requirements and financing, royalty, sales agreements, and taxation.

In May 1968, ore reserves based on assay and geological data from 23 holes was reported as follows:

Tactite reserves, based on a cut-off grade of 0.75% copper,
 were 13.7 million tons with an average grade of 1.84% copper.

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2. Porphyry reserves including tactite, based on a cut-off grade of 0.50% copper, were 59 million tons with an average grade of 0.99% copper.

During September 1968, the assay and geological data was again submitted to an independent consultant (8) for computer evaluation. The following reserves were reported:

1. Porphyry reserves based on mineralization with a thickness greater than 200 feet and a cut-off grade of 0.50% copper were 86 million tons with an average grade of 0.81% copper. This included tactite material lying under the porphyry.

2. Tactite reserves, outside the porphyry area and with a cut-off grade of 1.00% copper, were 10 million tons with an average grade of 1.73% copper.

In November 1968, with the data from 42 core holes, the following up-dated ore reserves, classified as a total of proved and probable, were reported:

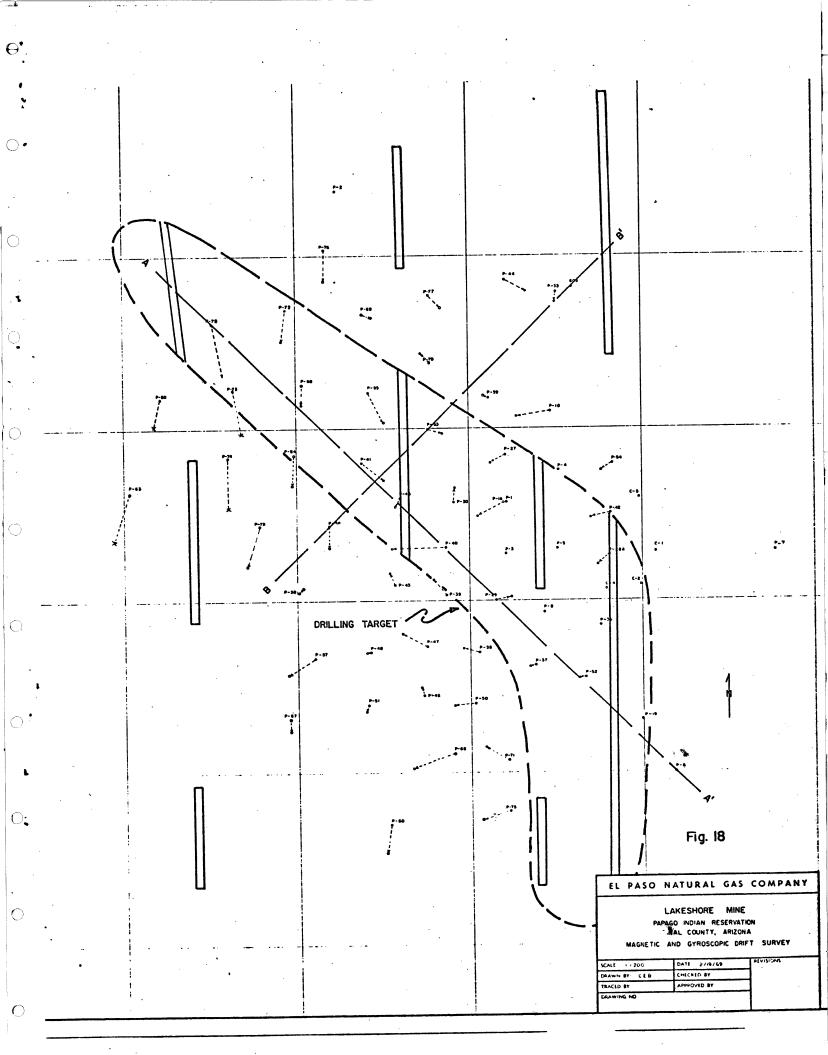
- 1. Porphyry reserves based on mineralization with a thickness greater than 200 feet and a cut-off grade of 0.50% copper, were 132.0 million tons with an average grade of 0.81% copper. This included 9 million tons of tactite material lying under the porphyry.
- 2. Tactite reserves, outside the porphyry area and with a cut-off grade of 1.00% copper, were 10 million tons with an average grade of 1.73% copper.
- 3. Oxide reserves, based on a cut-off grade of 0.50% copper, were 85 million tons with an average grade of 0.81% copper.

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On February 7, 1969, with data from 51 core holes, the following ore reserves classified as a total of proved and probable, were reported:

- 1. Porphyry reserves, based on a cut-off grade of 0.40% copper, were 241 million tons with an average grade of 0.70% copper.
- Tactite reserves, based on a cut-off grade of 1.00% copper,
 were 24 million tons with an average grade of 1.69% copper.
- Oxide reserves, based on a cut-off grade of 0.40% copper, were207 million tons with an average grade of 0.71% copper.



CONCLUSION

In the opinion of the writer, the discovery of sulphide mineralization at

Lakeshore was the result of a successful interpretation of combined geologic and
geophysical data. The rotation of the mineralized metasediments to an assumed
pre-tilt attitude gave a reason for projecting these metasediments to the northwest. The I. P. anomalies were correlated with this assumed northwest projection.

At the end of this phase of the exploration program, the majority of mineralized core holes have been collared within or near the limits of the proposed drilling target (Fig. 18). The interpretation that assumed overturning of metasediments by tilting to the northwest has been strengthened by three core holes which were collared in the oxide ore body and again entered mineralized metasediments at depth after penetrating the andesites. The discovery of the mineralized tactite led to the discovery of sulphide mineralization in the biotite porphyry intrusive and a "porphyry copper" deposit.

The gyroscopic drift survey of drill holes accurately located the subsurface position of the assay and geologic data that was obtained from the diamond drill cores, and gave the necessary vertical and horizontal control for the preparation of subsurface maps and cross sections and for computer evaluation of the mineral deposit.

Computer evaluation proved to be an efficient and rapid method of obtaining and updating grade and tonnage estimates during the exploration program.