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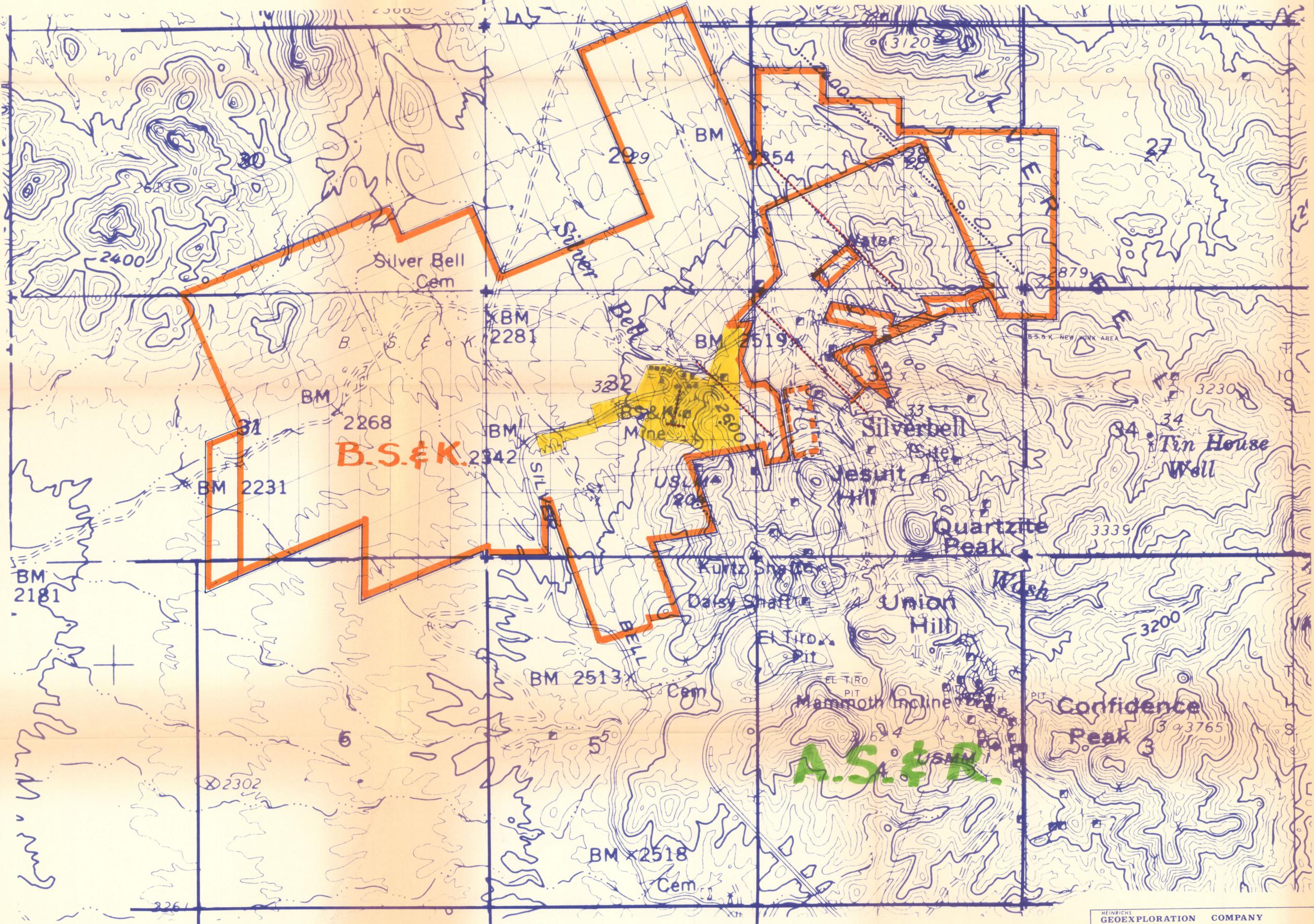
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T. 10 S.
T. 11 S.



WEAK STRONG I. P. ANOMALISM (GEOEX, CANADIAN AERO & MCPHAR)

R. 8 E.

- B. S. & K. BOUNDARY
- B. S. & K. PATENTED CLAIMS
- B. S. & K. 2/3, STEINFELD 1/3

For Abe Kalaf

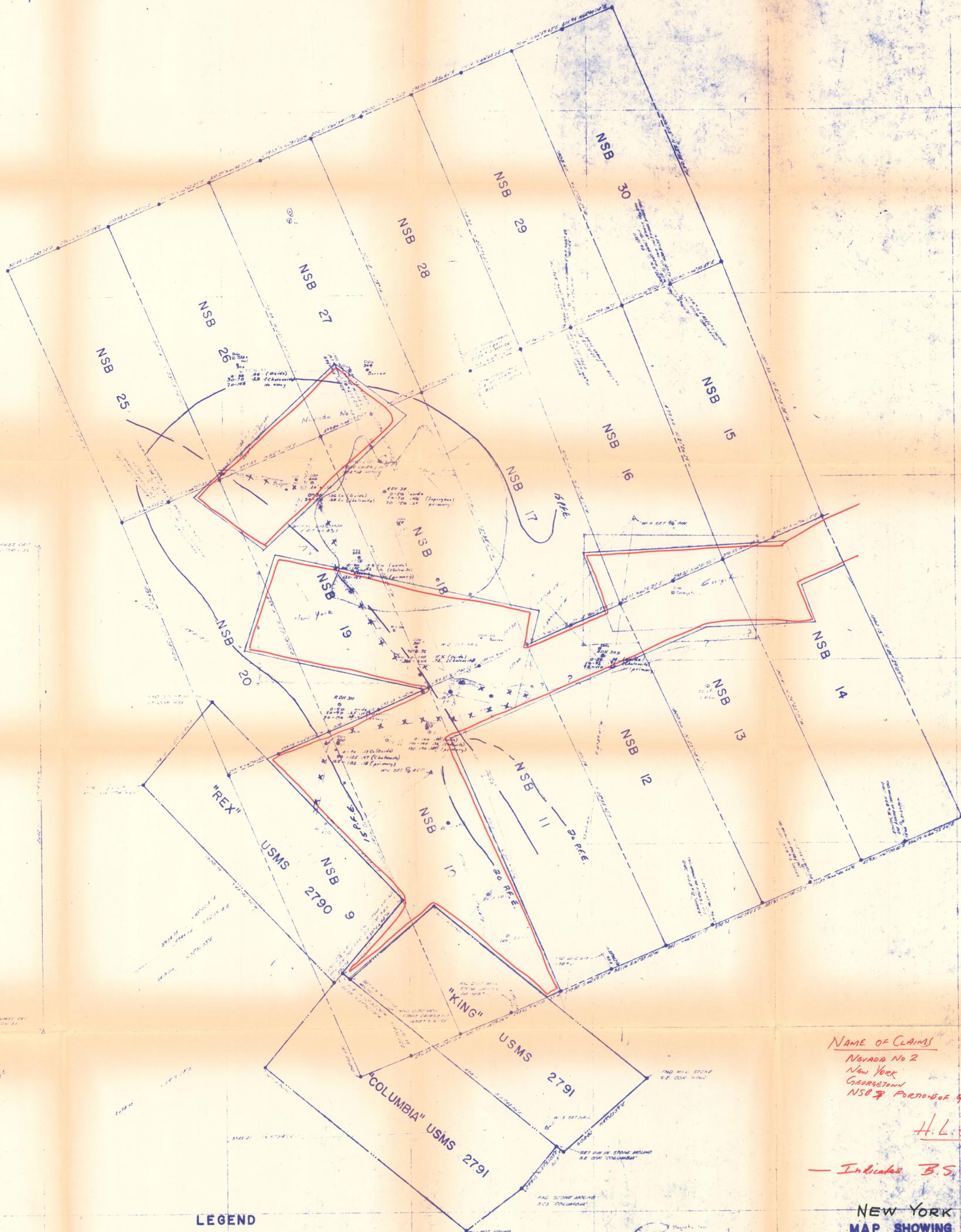
HEINRICHS
GEOEXPLORATION COMPANY
 POST OFFICE BOX 5671, TUCSON, ARIZONA 85703
 Phone: 602/623-0578 Cable: GEOEX-Tucson
 vancouver sydney

B.S. & K. MINING CO.
 ATLAS MINE & VICINITY
 PIMA COUNTY, ARIZONA

OWNERSHIP

FOR
 ESSEX INTERNATIONAL INC.

SCALE 1" = 1000' DRAWN BY EGH & JGD DATE MARCH 1970



SCALE 1" = 200'

PREPARED BY
blanton & cole
ARCHITECTS — ENGINEERS
TUCSON, ARIZONA
AUG 4, 1965

NAME OF CLAIMS
 Nevada No 2
 New York
 GARRETTON
 NSB PORTIONS OF 9, 10, 11, 12, 13, 14

H.L. COPP. (incomplete)

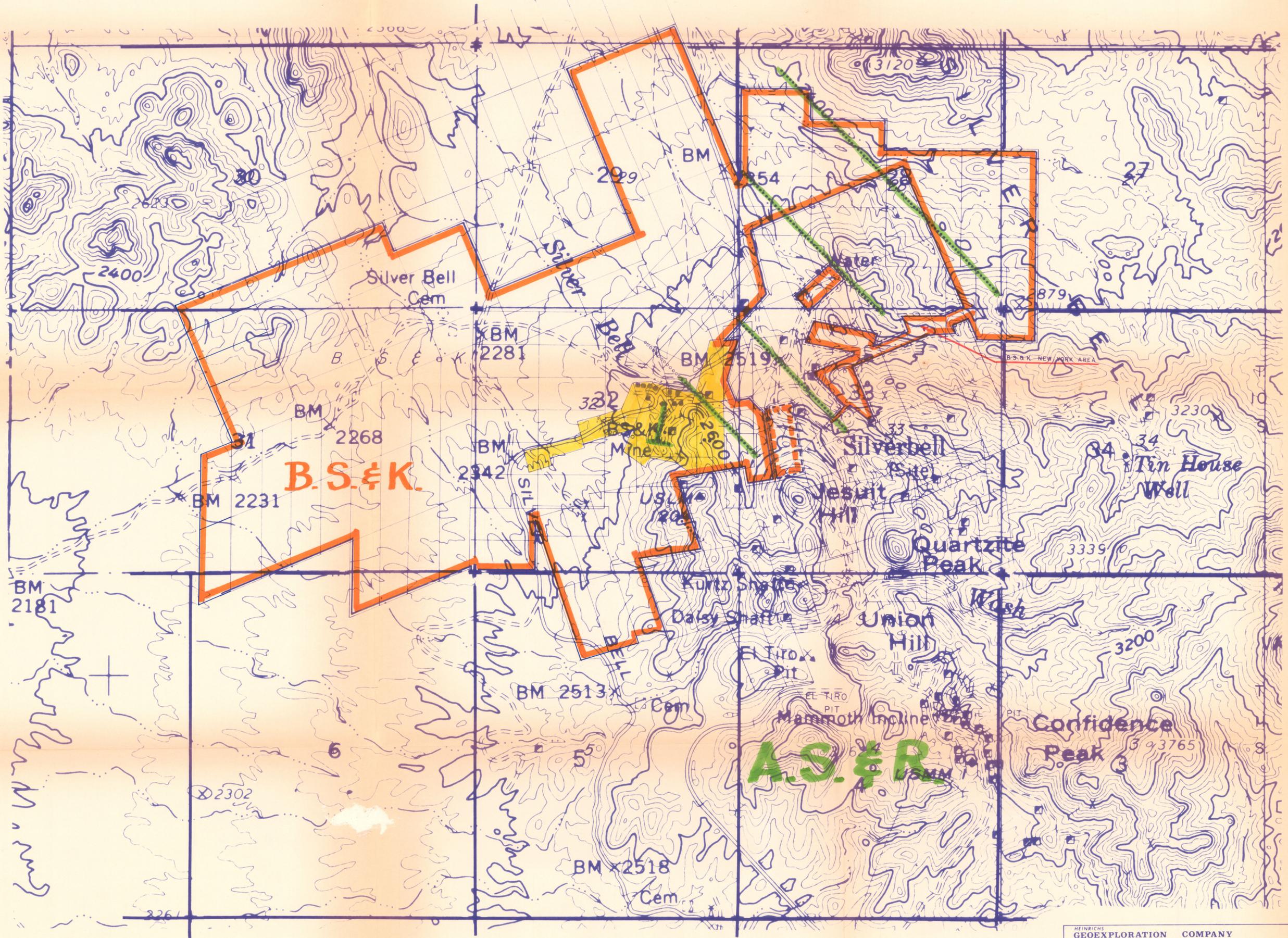
— Indicates B.S. & K.

LEGEND

INDICATES POINTS NOT FOUND IN STONE
 UNLESS OTHERWISE NOTED
 NOTICE INDICATES LOCATION NOT FOUND

NEW YORK AREA
 MAP SHOWING RESULTS
 OF SURVEY OF
 MINING CLAIMS IN
 SECTIONS 25 & 30 T-11-S, R-8-E,
 PIMA COUNTY, ARIZONA

T. 10 S.
T. 11 S.



WEAK STRONG I.P. ANOMALISM (GEOEX, CANADIAN AERO & MCPHAR)

R. 8 E.

- B. S. & K. BOUNDARY
- B. S. & K. PATENTED CLAIMS
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HEINRICHS
GEOEXPLORATION COMPANY
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vancouver sydney

B.S. & K. MINING CO.
ATLAS MINE & VICINITY
PIMA COUNTY, ARIZONA

OWNERSHIP

FOR
ESSEX INTERNATIONAL INC.

SCALE 1" = 1000' DRAWN BY EGH & JCD DATE MARCH 1970

Concrete vats 18' deep.

Size same as 80 x 120 x 12

Reduce area by $\frac{11}{17} = 9600 \times \frac{11}{17} = 6200 \#$.

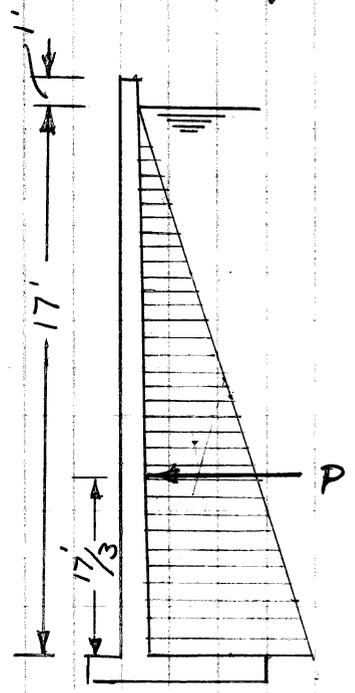
sides same ration $x \propto y$ where $y = 1.5x$

$x \times x \times 1.5 = 6200 \quad x^2 = \frac{6200}{1.5} = 4130$

$x = \sqrt{4130} = 64.2' \quad y = 96.57'$

Use 62' x 100' x 18' deep.

Specific gravity of leaching solution = 1.12



Pressure at bottom of vat

$17 \times 1.12 \times 62.4 = 1188 \#/\#$.

$P = 1188 \times \frac{17}{2} = 10.098 \#$

Moment at bottom of wall

for 1' wide strip of wall

$M = 10.098 \times \frac{17}{3} = 57.222 \text{ Ft}\#$.

Try 2'-0" thick wall $d = 21"$

with 3000 #/sq. i. concrete $f_s = 18,000$

Allowable $f_c = 1350 \quad n = 10 \quad K = 0.403$

$j = 0.866$

$M_c = \frac{1}{2} f_c \times K \times j \times b \times d^2 = 57222 \times 12$

$f_c = \frac{57.222 \times 12 \times 2}{0.403 \times 0.866 \times 12 \times 21^2} = 753.6 \text{ psi}$.

File
Make File B.S. & K. Prospect
Please make 2 Xerox copies
Jancie
EXHIBIT A
November 22, 1965

G. A. Girard

V. F. Hollister

All Concerned

Bacterial Leaching of B.S. & K. Exploration Composite

Abstract

Total copper extraction from the B.S. & K. exploration composite gave a recovery of 77%. Recovery from acid-soluble copper fraction was about 85%; from chalcocite copper was 82%; and about 51% from chalcopyrite.

There is no requirement for purchased acid. An initial acidification would, however, increase the initial copper production.

Microscopic examination of chalcopyrite particles revealed substructures of that mineral species within a network of more soluble chalcocite. The new surface exposure generated by the dissolution of chalcocite is believed to be responsible for the increased extraction from chalcopyrite.

Background

It was requested by the Exploration Department that a bacterial leach test be run on specified drill hole samples from the B.S. & K. location to determine the acid consumption of the ore, the response of the ore to copper recovery by bacteria and to evaluate this response in terms of our laboratory experience with other ores. The test head consisted of specified intervals from drill holes 300, 301, 302, 303 and 305.

Purpose

It was the purpose of this experiment to determine in a bacterial leach process:

1. The total recovery of copper over a four week leach period,
2. The copper recovery from each of the mineral species,
3. The total acid consumed and the purchased acid requirement.

Procedure

The composite sample was crushed to pass 10 mesh, the minus 100 mesh fraction rejected. Four test charges were split out from the minus 10 plus 100 mesh sample fraction. An additional sample was removed for chemical analyses, the results of which appear in Table I.

One hundred grams of sample were charged into each of four percolation columns. One hundred ml of sterile barren leach solution were added to each of the columns. The columns were each inoculated with 25 ml of an 8 day culture of T. ferrooxidans having a population of 1×10^8 bacteria per ml. The percolators had an adjusted air flow of 50 to 75 ml per minute. Each week the solutions were drained from the columns and submitted for copper, iron and pH analyses. The copper present in the sterile barren leach solution was deducted from the total copper recovered.

The ore in columns 1 and 2 were controlled at pH 2.0 by daily adjustment with sulfuric acid.

The ore in columns 3 and 4 was initially fed a solution of pH 2.0. The solutions fed the columns the second and subsequent weeks matched the pH of the effluent solutions of the previous week.

Upon termination of the test the columns were drained and rinsed with 20 ml of pH 2.0 distilled water. The combined solutions were submitted for analysis. The columns were then rinsed with two 25 ml portions of barren leach solution followed by a wash with 100 ml of one normal H₂SO₄ for five minutes. The columns were then rinsed with 20 ml of pH 2.0 distilled water. The combined solution, submitted for analysis, represented desorbed and dissolved ferric and cupric ion. The columns were then given a final rinse with 100 ml of pH 2.0 distilled water to determine the quantity of copper and ferric iron remaining after strong acid treatment. This solution was submitted for analysis.

The ore was removed from the columns, dried and submitted for chemical analysis. The test data are presented below.

TABLE I
B.S. & K. LEACH TEST

| SAMPLE NO. | 1 | 2 | 3 | 4 |
|--|------------|-------|------|-------|
| Assayed Head, % A-S Cu | ----- | ----- | .174 | ----- |
| " " % cc Cu | ----- | ----- | .269 | ----- |
| " " % cpy Cu | ----- | ----- | .091 | ----- |
| " " % Total Cu | ----- | ----- | .535 | ----- |
| Calculated Head, % Cu | .510 | .555 | .481 | .520 |
| Residue, % A-S Cu | .022 | .026 | .023 | .028 |
| " % cc Cu | .048 | .048 | .045 | .050 |
| " % cpy Cu | .046 | .046 | .046 | .043 |
| " % Total Cu | .116 | .120 | .114 | .121 |
| Copper Extracted (#/Ton) | 7.90 | 8.71 | 7.33 | 7.92 |
| #H ₂ SO ₄ Consumed | (Total | 17.0 | 18.1 | - |
| | Per | 12.2 | 13.4 | 11.3 |
| Ton Feed* | (Gangue | 4.8 | 4.7 | - |
| | (Filtrate | 77.5 | 78.5 | 76.2 |
| Distribution) %Cu | (Residue | 22.5 | 21.5 | 23.8 |
| | (Recovered | 2.2 | 2.1 | - |
| #H ₂ SO ₄ Consumed | Per #Cu | 1.7 | 1.6 | - |
| | (Available | 1.7 | 1.6 | - |
| % A-S Cu Recovered | 87.5 | 85.1 | 86.8 | 84.0 |
| % cc Cu " | 82.2 | 82.2 | 83.3 | 81.5 |
| % cpy Cu " | 49.5 | 49.5 | 49.5 | 52.7 |

* The acid consumed by columns 1 and 2 (duplicate) was based upon actual acid addition to maintain a pH of 2.0.

Data and Results:

Copper Extraction

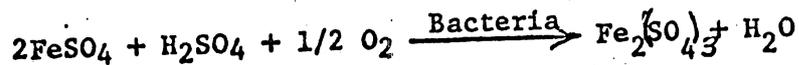
Slightly more copper was extracted from the columns maintained at pH 2.0 (columns 1 & 2) than from the columns with no pH control (columns 3 & 4). An average of 78% copper was extracted from the columns maintained at pH 2.0 while only 76% was

*extraction
78.35%*

the average copper extracted from the columns with no pH control (see Figure I, Table II). With the exception of the first week's extraction, the weekly extraction is identical and indicates that a benefit could be derived from an initial dump acidification.

Acid Consumption by Columns One and Two

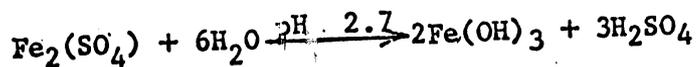
The total acid consumed by the pH controlled columns is given in Table I. Table III representing the average of pH controlled columns gives a breakdown of the acid consumed or produced by the ore and solution each week and cumulatively. Table III and Figures II and III gives specific information on the consumption of acid by oxidized ferrous ion and the net acid consumption by the ore. The total acid consumption is the actual acid necessary to maintain the system at pH 2.0. This acid was consumed by the ore and ferrous ion oxidation in solution:



The total acid consumption by ore and solution and the acid consumption by oxidized ferrous iron are illustrated in Figure III on a weekly and cumulative basis. The net acid consumption by the ore is shown in Figure IV. It will be noted that, after seventeen days, more acid was being produced by the ore than was being consumed by the ore and solution.

Acid Consumption by Columns Three and Four

The acid consumption data by the columns with no pH control is presented in Table IV and illustrated in Figures IV and V. The acid consumption is based on the actual ferric hydroxide formation:



The system is kept below pH 2.7 by the production of acid through ferric precipitation. A rise in the pH of the leach liquor throughout the test represents, also, an acid consumption. These two factors are combined in Table IV and Figure IV under the heading of "total acid consumption from Fe(OH)₃ formation." The acid consumption by oxidized ferrous in solution is deducted from Figure IV to give the net acid consumption represented by Figure V.

Comparison of Acid Consumption Data From Each Column Pair

It will be noted from Figure V that the weekly acid consumption approaches zero asymptotically with time. The pH of this system seems to stabilize at 2.35 over the four week test. In Figure III there is a net acid production. It follows, then, that gangue consumption must be greater in the pH controlled system since acid producing constituents in the ore have been released.

The pH-controlled columns give a true picture of the acid consumption necessary to maintain a pH of 2.0. The columns with no pH control were designed to indicate any need for purchased acid. Other than the benefit to be derived from initial dump acidification, it is concluded that no additional acid need be purchased.

The Structural Nature of Chalcopyrite Used in This Test

It was noted from the results of chemical analysis of the chalcopyrite mineral species that the recovery was 12 to 25 times greater than most reported results both in our laboratory tests and in the literature. Previous work with Battle Mountain ore yielded, in certain cases, results similar to those in this test with

chalcopyrite. These prior results were regarded with suspicion and attributed to inconsistencies in the analytical procedure. Since a recovery of about 51% occurred with this mineral species, it was decided to resubmit the samples for analysis. The samples were leached for seven minutes and twenty minutes with cyanide in two separate tests to determine whether all the chalcocite had been removed prior to the analysis for chalcopyrite. These test results were in agreement with each other and those first reported.

It was then thought that this chalcopyrite must be structurally different from other specimens of the same mineral species. A polished section was made of the sink fraction of a heavy media separation. A microscopic examination of the chalcopyrite particles at 450 power revealed intimate intergrowths of chalcocite replacing chalcopyrite.

A 48 mesh particle of chalcopyrite, for example, exhibited a subparticle size of 400 mesh in many cases. Since chalcocite is readily leached in a bacterial system the surface exposure of chalcopyrite is greatly increased as leaching proceeds.

Based on our laboratory experience with unaltered chalcopyrite from the bottom of the Esperanza pit the recovery from E.S. & K. chalcopyrite is 1040% greater.

A microprojection of a typical chalcopyrite particle, illustrated in Figure VI, was traced on thin translucent paper.

Conclusions

1. Copper extraction over the four week test period gave a total recovery of about 77%. Recovery of copper from chalcopyrite about 51% and was 10.4 times greater than expected. Microscopic examination revealed the special nature of this mineral species.

2. The data indicate that purchased acid is not necessary except for the benefit to be derived from initial dump acidification.

Respectfully submitted,

George A. Girard
George A. Girard
Process Chemist

GAG:jfg

cc: R. W. Livingston (2)
R. W. Flagg
C. H. Curtis
G. E. Atwood
J. E. Frost
E. K. Drechsel
R. R. Nelson
D. J. Bourne

TABLE II

% RECOVERY

| WEEK No. | COLUMN 1 | | COLUMN 2 | | COLUMN 3 | | COLUMN 4 | | AVERAGE CUMULATIVE RECOVERY |
|----------|----------|--------|----------|--------|----------|--------|----------|--------|-----------------------------|
| | WEEKLY | CUMUL. | WEEKLY | CUMUL. | WEEKLY | CUMUL. | WEEKLY | CUMUL. | |
| 1 | 474 | 474 | 440 | 440 | 412 | 412 | 407 | 407 | 407 |
| 2 | 190 | 664 | 170 | 610 | 186 | 598 | 198 | 605 | 597 |
| 3 | 26 | 690 | 150 | 760 | 232 | 830 | 212 | 817 | 767 |
| 4 | 64 | 754 | 65 | 825 | 66 | 891 | 67 | 958 | 834 |

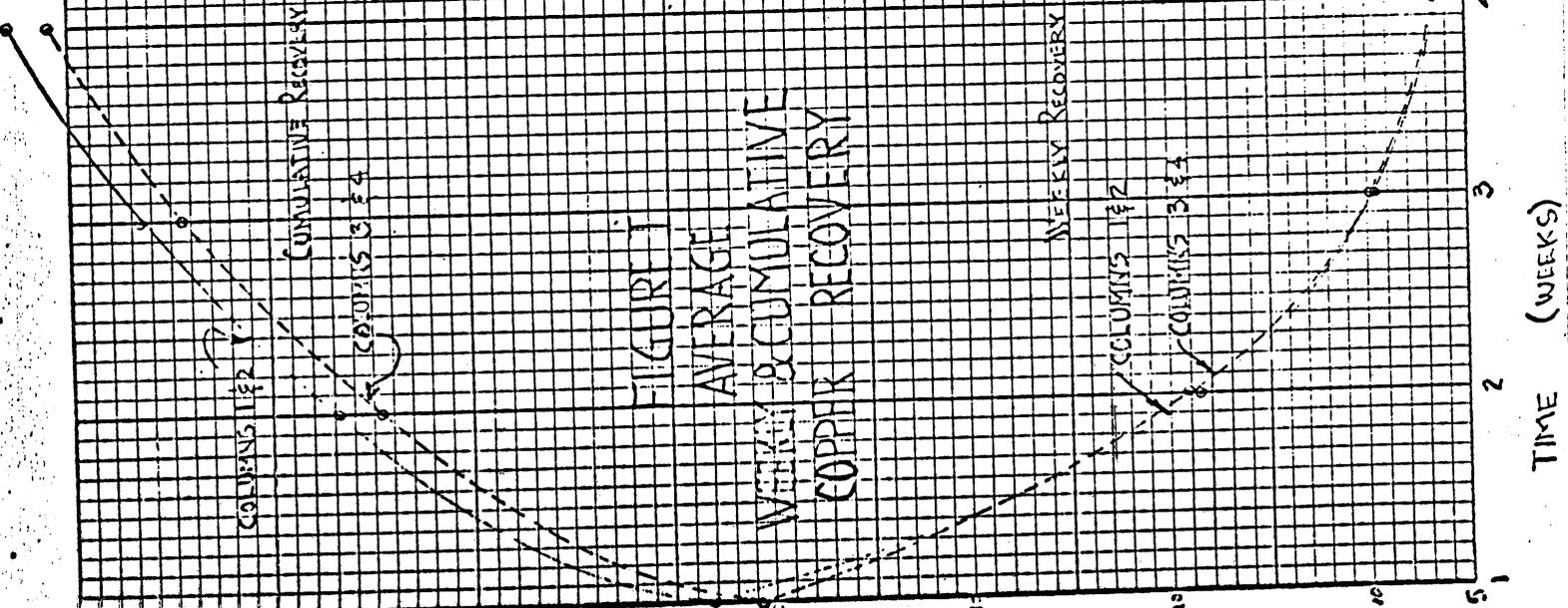


FIGURE 1
AVERAGE
WEEKLY & CUMULATIVE
RECOVERY

% RECOVERY

TIME (WEEKS)

AVERAGE ACID CONSUMPTION OF COLUMN 1302

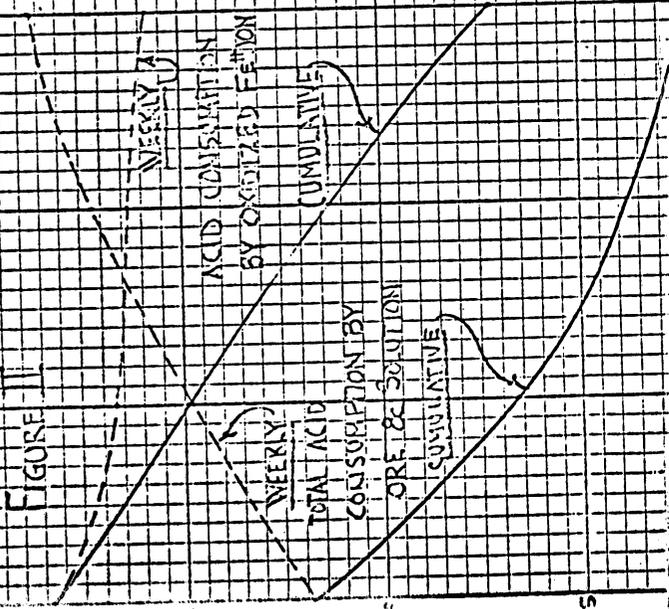


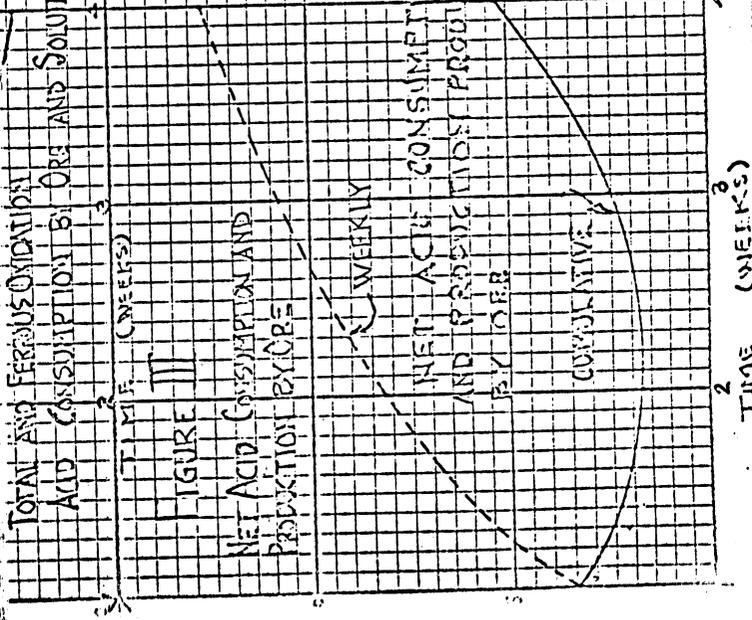
TABLE III

| WEEK NO. | TOTAL ACID CONSUMPTION BY ORE & SOLUTION (#/TON) | WEEKLY CONSUMPTION | ACID CONSUMPTION BY OXIDIZED FE ₂ S (#/TON) | WEEKLY CONSUMPTION | NET ACID CONSUMPTION AND PRODUCTION BY ORE (#/TON) | WEEKLY CUMULATIVE |
|----------|--|--------------------|--|--------------------|--|-------------------|
| 1 | -8.17 | -8.17 | -1.66 | -1.66 | -6.51 | -6.51 |
| 2 | -5.71 | -3.38 | -3.72 | -5.08 | -1.19 | -8.30 |
| 3 | -2.78 | -1.61 | -3.61 | -8.69 | .83 | -7.47 |
| 4 | -1.50 | -1.50 | -4.17 | -12.29 | 2.77 | -4.10 |

FIGURE II

TOTAL AND FERROUS OXIDATION
 ACID CONSUMPTION BY ORE AND SOLUTION

TIME (WEEKS)

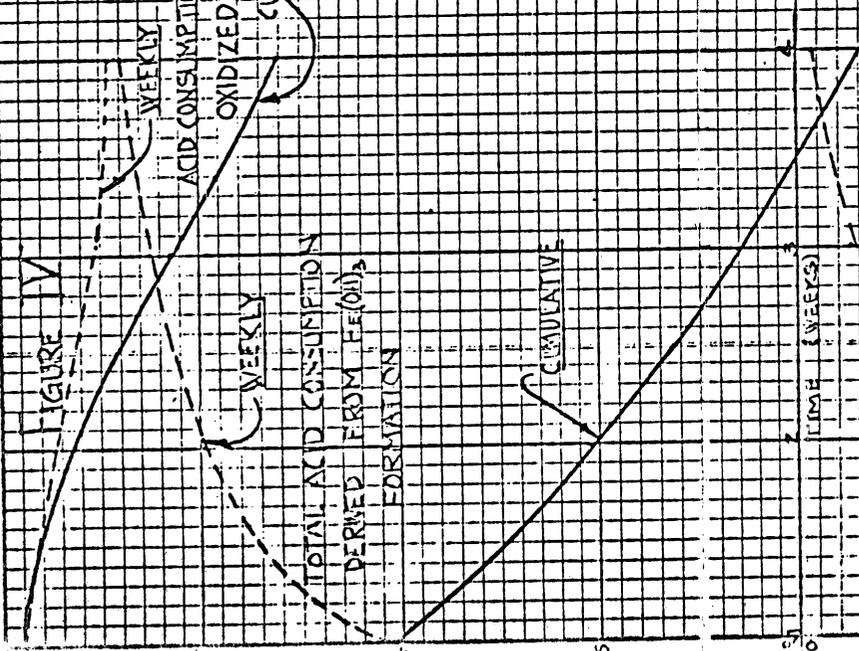


NOTE:
 THE TOTAL ACID CONSUMPTION IS THE ACTUAL ACID ADDED TO MAINTAIN A PH OF 2.0.

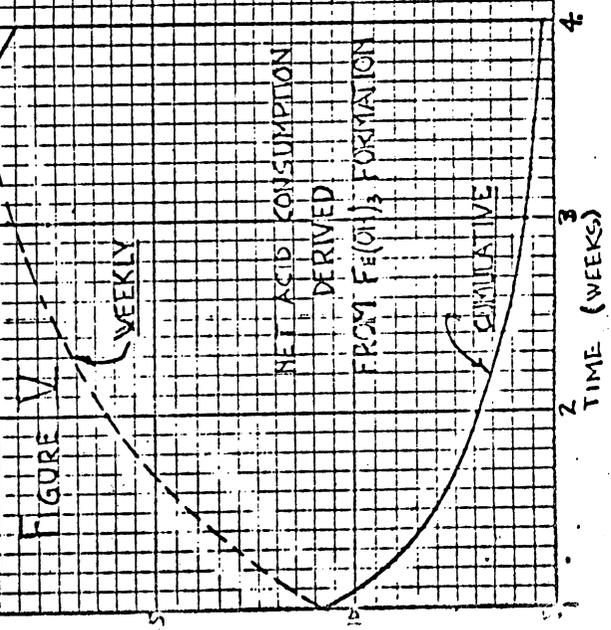
AVERAGE ACID CONSUMPTION DERIVED FROM
 FERRIC HYDROXIDE FORMATION
 IN COLUMNS 3 & 4

TABLE IV

| WEEK NO. | TOTAL ACID CONSUMPTION FROM $Fe(OH)_3$ FORMATION (#/TON) | ACID CONSUMPTION BY OXIDIZED FERROUS ION (#/TON) | NET ACID CONSUMPTION FROM $Fe(OH)_3$ FORMATION (#/TON) |
|----------|--|--|--|
| 1 | -9.70 | +0.53 | -9.23 |
| 2 | -5.06 | +1.28 | -3.78 |
| 3 | -3.74 | +2.45 | -1.31 |
| 4 | -3.09 | +2.70 | -0.39 |
| | | | CUMULATIVE |
| | | | -14.71 |



NOTE: THE TOTAL ACID CONSUMPTION DERIVED FROM $Fe(OH)_3$ FORMATION ALSO INCLUDES ACID CONSUMED THROUGH A SYSTEMIC PH RISE.



2 3 4
 TIME (WEEKS)

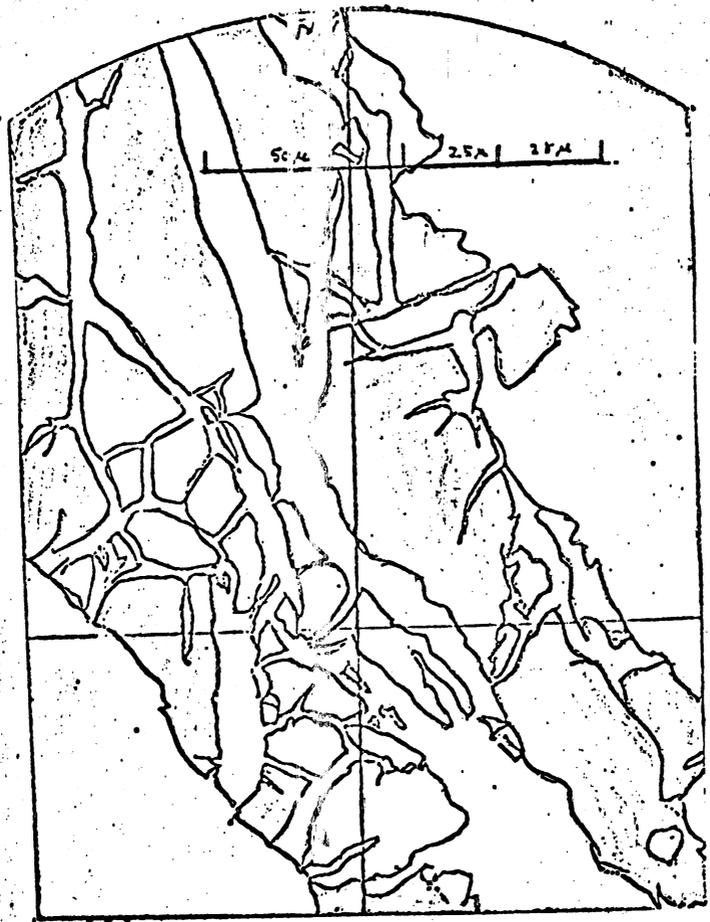


FIGURE VI
MICROPROJECTION TRACING (530X)

PROPOSED DUMP & LEACH AREA

ROUTE 2

ROUTE 1

NEW YORK CLAIM GROUP

ATLAS MINE

2/3 B.S.&K.
1/3 Steinfeld

EL TIRO PIT

IMPERIAL PIT

HEINRICH'S
GEOEXPLORATION COMPANY
POST OFFICE BOX 8871, TUCSON, ARIZONA, 85703
Phone: 602/623-0578 Cable: GEOEX, Tucson
geophysical engineers vannewer sydney

AERIAL PHOTO MOSAIC
of
B. S. & K. MINING CO. PROPERTIES
T 10 & 11 S, R 8 E
PIMA COUNTY, ARIZONA
for
ESSEX INTERNATIONAL INC.

Scale: 1" = 1000' 13 March 1970

RDH
31

New York

Disc NW

BS&K No 5

New York

BS&K 15
Disc Post

RDH 309

RDH
310

Disc
310
15

1" = 200'

RDH
311

New York

Disc NW

BS&K No 5

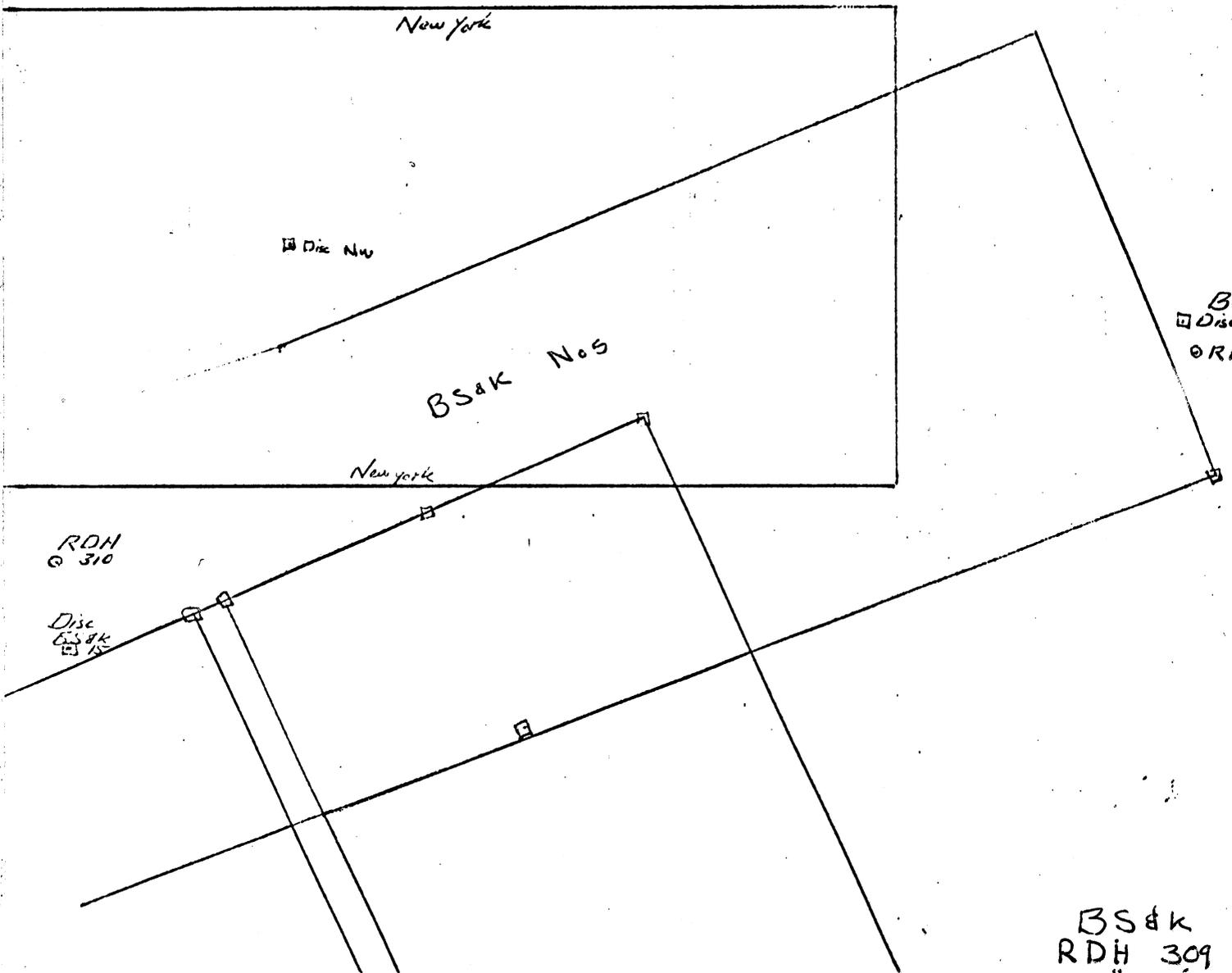
BS&K 15
Disc Post
RDH 309

New York

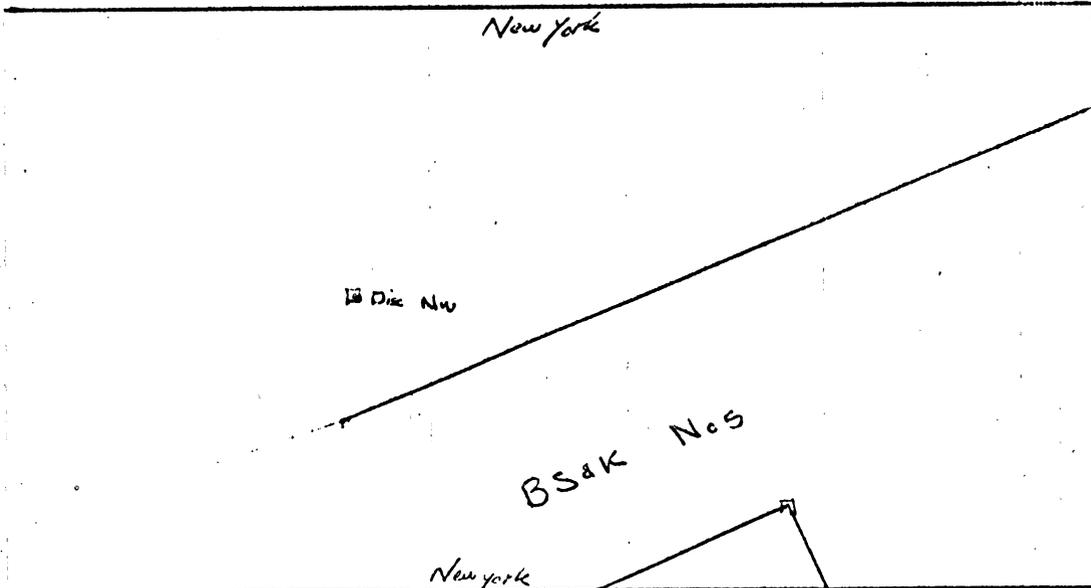
RDH
310

Disc
BS&K
15

BS&K
RDH 309



RDH
311



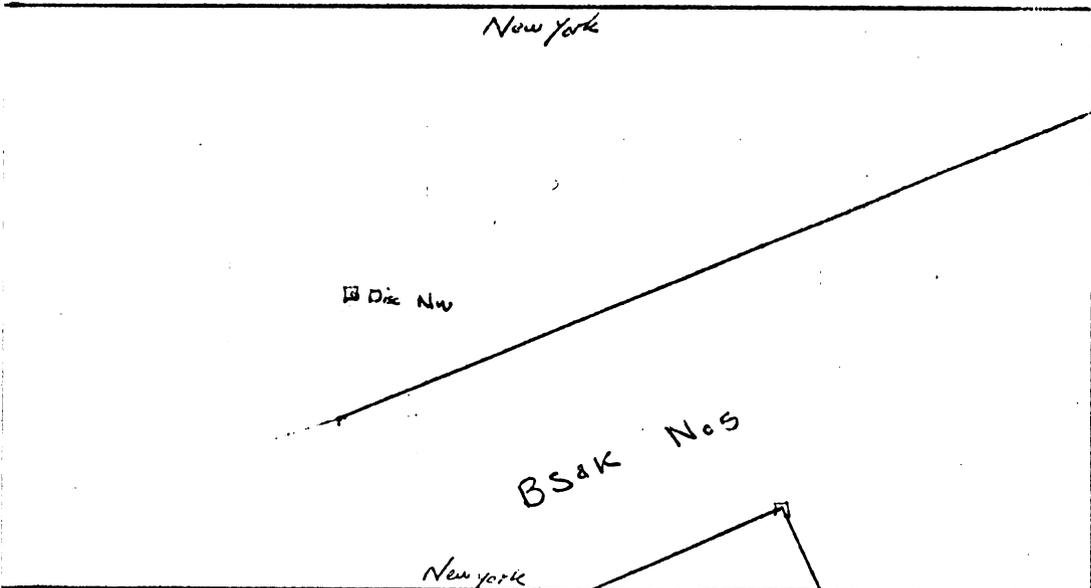
BS&K 15
Disc Post
RDH 309

RDH
310

Disc
BS&K
No 5

BS&K
RDH 310

RDH
311



BS&K 15
Disc Post
RDH 309

RDH
310

Disc
BS&K
15

BS #K
RDH 311

INDUCED POLARIZATION AND
RESISTIVITY SURVEY
BS AND K PROJECT
SILVER BELL DISTRICT
PIMA COUNTY, ARIZONA
FOR
THE HANNA MINING COMPANY

PROJECT 9618

INDUCED POLARIZATION AND
RESISTIVITY SURVEY

BS AND K PROJECT
SILVER BELL DISTRICT
PIMA COUNTY, ARIZONA

FOR

THE HANNA MINING COMPANY

PROJECT 9618

T A B L E O F C O N T E N T S

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Accompanying This Report:

- 9 IP and Resistivity Profiles (Quasi Sections)
- 1 Plan Map
- 1 IP Contour Map
- 1 Resistivity Contour Map

ABSTRACT

A strong IP response representing likely greater than 4% sulfides by volume has been outlined along the southeast side of the survey area. The response is most pronounced on line 52 where the zone has apparent characteristics of a flat-lying trend at a depth of 150'. Response decreases below 800' indicating an apparent thickness of 650'.

The anomaly lies parallel to the profile lines hence its lateral boundaries and depth extent cannot be accurately described by the present data. A suggested profile across the strike of the anomaly is considered a prudent step prior to locating a drill site.

Anomalous response characteristics along the southeast end of lines 48, 50, and 54 indicate that a broad area of response occurs to the south and east of the present survey area, and may extend easterly.

In the west half of the area a response layer occurs at an average depth of 1800' under the Tertiary-Cretaceous volcanics. The response of 15 units could represent 1% sulfides by volume or a background variation due to change in rock type at that depth.

INDUCED POLARIZATION AND
RESISTIVITY SURVEY
BS AND K PROJECT
SILVER BELL DISTRICT
PIMA COUNTY, ARIZONA
FOR
THE HANNA MINING COMPANY

Part I

INTRODUCTION

At the request of Messrs Victor Mejia and Jackie Stephen of The Hanna Mining Company, personnel of Canadian Aero Mineral Surveys Limited were engaged in an induced polarization and resistivity survey in the Silver Bell District, Pima County, Arizona. The project was underway during the period from March 17 to April 10, 1969 and included 9 dipole-dipole profiles covering a total of 77,500 feet of surveyed line.

The survey was under the field direction of Avinash V. Hardas, Engineer for CAMS.

The major rock types that occur in the area include alaskite, granite, monzonite, Gila Conglomerate and the Tertiary-Cretaceous volcanics.

According to Victor Mejia, Gila Conglomerate occupies areas in sections 29, west 1/2 of 32, and southeast 1/4 of 31; flanked by intrusives (granite, monzonite, alaskite) to the east and Tertiary-Cretaceous volcanics to the west. Small patches of limestone occur as irregular isolated outcrops near the BS and K

mine. A contact between granite and dacite porphyry is noted to occur between lines 52 and 54.

PURPOSE OF THE SURVEY

The purpose of the survey was to locate areas of mineralization near the BS and K mine and to describe the extent of related anomalies as being additional occurrences of sulphide mineralization. Also to determine if possible the thickness of overlying Tertiary-Cretaceous volcanic rocks in the western half of the project area; and the occurrence of IP response at depth below the volcanics.

SURVEY PROCEDURES

The induced polarization and resistivity measurements were made in the time-domain mode of operation. A conventional system of measurements which uses a time cycle of 2.0 seconds "on" and 2.0 seconds "off", a 2.0 seconds "on" and 2.0 seconds "off" (current reversed), was employed.

The commencement of the measurement of the secondary voltage is delayed by 0.45 seconds to avoid coupling and other transient effects. The integration is performed during the period from 0.45 seconds to 1.10 seconds after the cessation of current.

To conform to a standard presentation, the integral time constant is adjusted to give induced polarization read-

ings equivalent to those obtained with transmitter cycles of 3.0 seconds "on" and 3.0 seconds "off" with integration of the secondary voltage during the first second of the "off" period.

Throughout the survey except line 44 and 46 a conventional inline dipole-dipole array of seven electrodes was used. For additional data coverage on lines 44 and 46, two additional electrodes were employed, there by obtaining additional coverage to the southeast. A dipole length of 1000' was used for the survey. This dipole length was recommended for greater penetration and greater lateral coverage.

Measurements were made for dipole separation factors (n) 1 to 6. Potential dipole setups occupied positions on both sides of the current-electrode setup. This resulted in obtaining a total line coverage approximately nine times the dipole length where 7 electrodes were used.

Apparent polarization responses is in units of millivolts-seconds per volt, or milliseconds, and apparent resistivity is in units of ohm-meters.

Part II

DISCUSSION OF RESULTS

Line 38: This line clearly indicates a change in rock type at about 500 feet southeast of the center; To the southeast the resistivity is of the order of 40-70 ohm-meters as against 130 to 400 ohm-meters to the northwest. The data is indicative of southeast dipping contact.

Pulse response is of the order of 4.0 to 8.0 milliseconds and does not vary across the resistivity contact. The data is distorted due to fence-power line effects and therefore does not yield an intelligent interpretation.

Line 40: Low resistivity (35-70 ohm-meter) is noticed on south side of the line. Resistivity to northwest ranges from 100-500 ohm-meters. The point at which a change in rock type occurs is noted at 500-700 feet southeast of the center.

Changeability is of the order of 4.0 to 13.0 milliseconds with a slight increase in response at depth. However, it is believed the values are too low to indicate presence of sulphides in economic quantities.

Line 42: Again on this line low resistivity rock occurs to the southeast and high resistivity rock to northwest. This change in physical characteristics of the rocks occurs at 600' southeast from center. To the southeast the resistivity is of the order of 40-60 ohm-meters and to the northwest 100-400 ohm-meters.

Pulse response ranges from 4.8 to 10.2 milliseconds increasing with depth, but again likely represents a high background response or at least minor (less than 1.5% by volume) sulfides at depth.

Line 44: Resistivity contact is noted 500' northwest from the center with high resistivity to northwest and low resistivity to southeast.

Average pulse response of 2.8 to 5.0 is present with

a slight increase in response to 10.0 at depth. This increase could be due to a normal background response at depth with no indication of the presence of substantial amounts of sulphides.

Line 46: A reverse situation occurs on this line where high resistivity occurs to the southeast and low resistivity to the northwest. The high resistivity is related to the granite that outcrop to the southeast. The resistivity of the volcanics and sediments to the northwest is low, varying from 7 to 40 ohm-meters.

Due to the very low resistivity of the rocks, signal could not be obtained at "n's" greater than 3. thus the depth penetration is limited. Background response varies from 2.0 to as much as 15.4 milliseconds.

Line 48: A resistivity contact occurs at the center of the line. Rocks of high resistivity (100-700 ohm-meters) extend southwards from the center and the low-resistivity rocks extend northwards from the center. Rocks to the northwest have resistivity of 16 to 90 ohm-meters.

Average chargeability background response is 6.0 milliseconds with sharp increase in response up to 27.0 milliseconds to the southeast. (Fence interference may cause the few high readings to the south).

The high pulse response is related to the high resistivity indicative of sulfides in granites.

Another gradual increase in response at depth is also

noted in the low resistivity rocks to the northwest. Due to the very low resistivity of the rocks full line coverage at depth could not be obtained.

Line 50: A very clear indication of a lithologic contact is noted on this line at 1000' northwest from the center.

Resistivity of rocks to the southeast range from 184 to 550 ohm-meters and to the northwest from 14 to 150 ohm-meters. The high resistivity zone is associated with high pulse response of 20 to 67 milliseconds and is indicative of 2-3 percent sulphides by volume at a depth less than 400 feet from surface.

Surface pulse response to the northwest is of the order 2.6 to 6.4 milliseconds but increases slightly to more than 15.0 milliseconds at depth. This response zone may be in part due to the power line or fence that tranverse the line.

The low resistivity relates to a broad near-vertical north-south striking of alluvium or Gila Conglomerate zone and is devoid of any substantial amounts of sulphides.

Line 52: Interpretation of resistivity data of this line is a little complex as surface resistivity variation appear related to complex geology. However, in general, rocks of less than 50 ohm-meters resistivity extend northwards from C₃ and are characterized by low pulse response.

Rocks that crop out on the southeast side of the line have resistivity of 90 to 650 ohm-meters and are associated with 10.0 to 80.0 milliseconds response. The anomalous response is related to a broad zone of moderately high resistivity and

and is indicative of 3-4 percent sulphides by volume at a depth less than 200' from the surface. Line 52 does not extend far enough to cover the southern boundary of the zone.

Line 54: Resistivity varies from 190 ohm-meters to as much as 600 ohm-meters with no apparent indication of a lithologic contact.

Background pulse response of 3.0 to 10.0 is observed on the northside of the lines but increases at depth to more than 40.0 milliseconds to the southeast. This relates to a zone of anomalous responses that extends southward from C₇. This line runs parallel to the main zone of response and hence the actual true response obtained from the anomalous zone is not clear. However, there is a slight indication from the resistivity pattern that the response zone may extend to the east at depth. We feel that in order to actually define the anomaly a line at right angles to the strike of the zone should be surveyed.

Part III

INTERPRETATION

The accompanying contour maps of chargeability and resistivity provide a good picture of distribution and extent of response material, i.e. possible sulphide mineralization, and the related rock types in the area.

First look at the resistivity contour map indicates that 3 major rock types occur in the area which govern the resistivity pattern. They are granites, volcanics, and alluvium (Gila Conglomerate?).

In sections 30 and 31 the relatively high resistivity of 100 to 200 ohm-meters is related to the Tertiary-Cretaceous volcanics. The resistivity data indicates increased resistivities at a depth of 1000' plus. The resistivity of the lower layer is as much as 1000 ohm-meters-atypical of volcanic rocks.

A high resistivity anomaly of approximately 1000 ohm-meters occurs in the east 1/2 of section 32, closely associated with the BS and K mine. This anomaly is related to granite which crops out in the area. We suspect silicification (alteration) of the granite has resulted in this abnormal granite resistivity.

Resistivities in the vicinity of the high IP response on line 52 are locally lower (100 to 200 ohm-meters) than the adjacent resistivities (200-400 ohm-meters) on line 50 and 54.

The alteration and mineralization of the granite is believed the cause of the lower resistivity here.

Extremely low resistivity of less than 100 ohm-meters in a north-south trend through sections 29, east half 31, and 32 is related to alluvium and/or Gila Conglomerate.

Effective penetration has been drastically reduced in the area of low resistivity due to loss of signal at the larger electrode spacings. This condition is most severe on line 46 where our ability to see below 1000' is nil.

The chargeability contour map provides a good picture of the distribution of the response material in the area.

High response material of 80 milliseconds occurs in section 28 and 33. The anomaly is controlled to the west by a strong north-south contact (fault). This contact feature is common to both the IP and resistivity data and represents the boundary between the mineralized intrusives on the east and the alluvium (Gila?) on the west.

The BS and K mine occurs along this contact or fault zone. The alluvium or Gila Conglomerate is marked by the area of response of less than 2.0 milliseconds on the IP contour map.

The Tertiary-Cretaceous volcanics to the west have response values of 4 to 8 milliseconds near surface. An increase in response to 15 milliseconds at depths greater than 1800' is associated with higher resistivities and could be related to rocks other than volcanics. This increase in response at depth could be due to high background response or at best minor sulfides of less than 1.5 percent by volume.

CONCLUSIONS

A zone of substantial IP response occurs on the southeast half of line 52. A calculated response of 80 to 100 milliseconds in the rock at depths from 150' to 800' is related to greater than 4 percent sulfides by volume. The zone lies parallel to our present profiles and a line across the strike of the zone is recommended to locate the northeast and southeast contacts.

Substantial response occurs off the southerly ends of lines 46, 48, 50, 52 and 54 indicating a reasonably large zone of response adjacent to the southeast of the property.

A moderately weak response of 15 milliseconds occurs at depths of about 1800' in the area of the Tertiary-Cretaceous volcanic to the west. An increase in resistivity occurs at depths greater than 1000' in this area. We suspect these interfaces indicate a bottom depth to the volcanics, and a high resistivity rock at depth that may have very minor sulfide mineralization.

RECOMMENDATIONS

A drill hole is proposed to test the response zone outlined on line 52. A minimum depth of 1000' is suggested to test the response characteristics. We strongly recommend a profile be run across the zone to better define the boundaries of the anomaly prior to locating a drill site.

Locally the anomalous response appears to be closing out to the northeast. However, further reconnaissance in the area to the north and east should be considered where geologic conditions appear more favorable.

Some consideration might be given to testing the high resistivity, moderate IP response that occurs below the Tertiary-Cretaceous volcanics in sections 30 and 31. However, there is little reason to expect more than 1 percent sulfides

(related to 15 milliseconds response at depth) where a hole to 2000' would be necessary to test the physical property characteristic.

Respectfully Submitted


Avinash V. Hardas, M.S. ^{per WGW}
Geologist-Geophysical Engineer


W. Gordon Wieduwilt
Geophysicist

May 2, 1969
Tucson, Arizona

Part IV

APPENDIX I

The following personnel of CANADIAN AERO MINERAL SURVEYS LIMITED were engaged in an induced polarization - resistivity survey conducted on behalf of THE HANNA MINING COMPANY on their property in the Silver Bell District, Pima County, Arizona.

| | | <u>No. of Man Days</u> |
|---------------------------|--------|------------------------|
| Avinash V. Hardas | Field | 20 |
| Engineer, CAMS Tucson | Office | 6 |
| Gary Carpenter | Field | 20 |
| Helper-Tucson | | |
| Shantikumer Toprani | Field | 16 |
| Helper-Tucson | | |
| David Hunter | Field | 9 |
| Helper-Tucson | | |
| Christian Dahlberg | Field | 3 |
| Helper-Tucson | | |
| Robert Sigafus | Field | 1 |
| Helper-Tucson | | |
| Total number of man hours | | <u>75</u> |

APPENDIX II

APPLICATION OF INDUCED POLARIZATION METHOD

The induced polarization method is basically a volume detecting technique. Effective penetration is governed by the size of target where normally a large volume of polarizable material at depth is required to give measureable response at surface. This method is relatively sensitive and is capable of detecting as little as 1% by volume of metallic sulfides. Because polarization is essentially a "particle surface" phenomenon, the induced polarization effects from a given percentage of metallic sulfides generally increases as particle size is decreased. This characteristic makes this technique especially suitable to exploration for disseminated sulfide occurrences.

Sulfides of metallic lustre produce IP effects i.e., bornite, chalcopyrite, chalcocite, pyrite, pyrrhotite, arsenopyrite, molybdenite, etc.; but not sphalerite. Besides sulfides, some metallic oxides like magnetite and pyrolusite also give rise to IP effects.

Apart from sulfides and oxides, certain minerals with unsatisfied basal charged lattice, when current is applied to the ground, develop a charged double layer which acts as a leaky condenser and gives rise to IP effects. Certain of the

clay mica minerals are active in this sense with montmorillonite and vermiculite exhibiting by far the greatest response. Bentonitic tuff is exceptionally active to IP, while kaolines, chlorites, muscovites, and biotites are not generally active.

Although considerable study has taken place, this method has not yet been improved to differentiate the IP effects arising from metallic sulfides, oxides, graphite, or clay occurrences.

TIME DOMAIN INDUCED POLARIZATION AND RESISTIVITY SURVEY

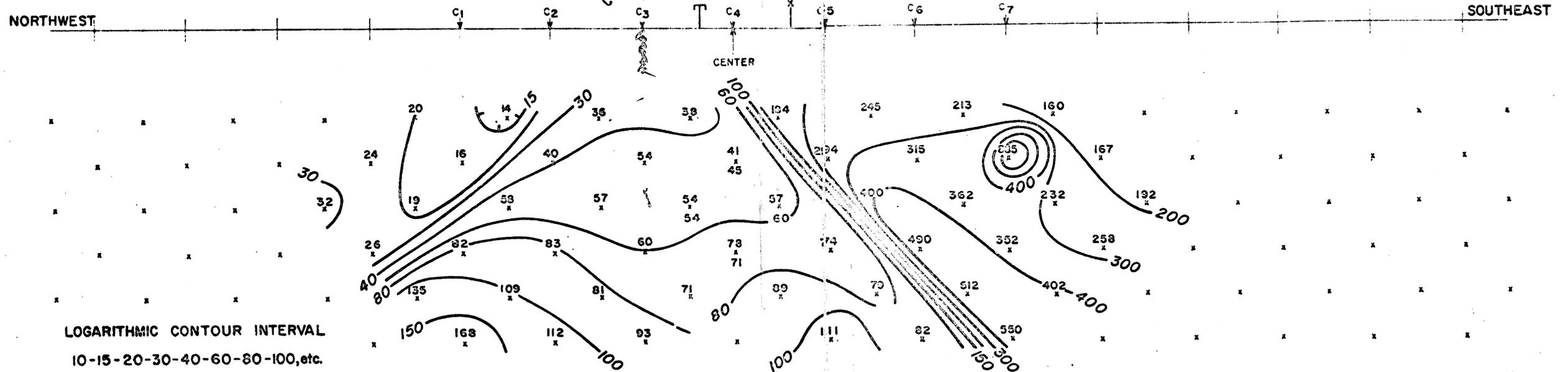
BS & K PROJECT-SILVER BELL DISTRICT-PIMA COUNTY, ARIZONA

FOR

THE HANNA MINING COMPANY

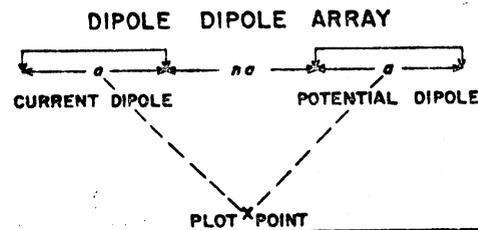
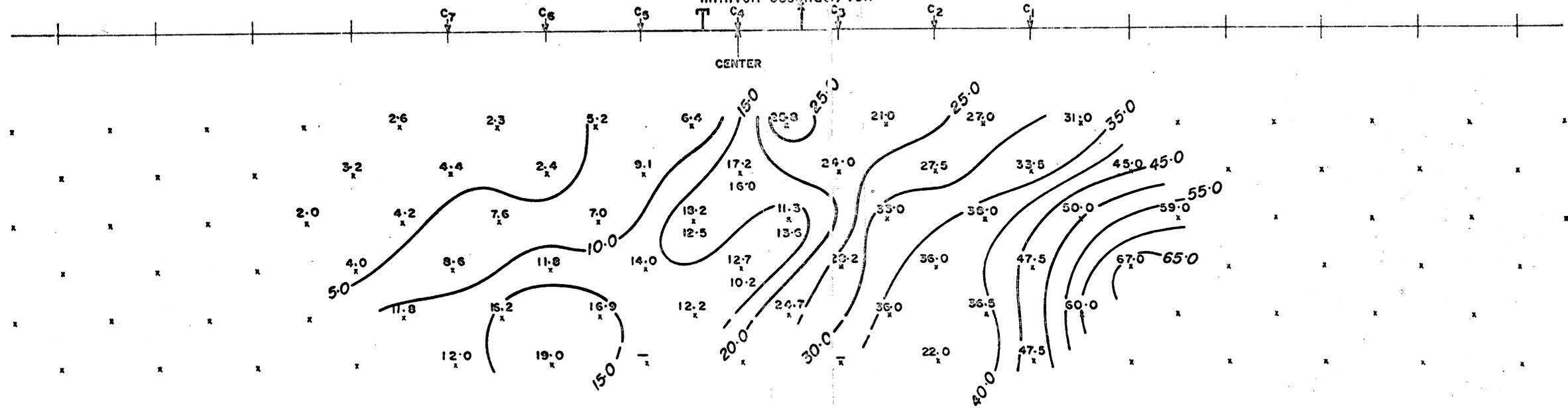
APPARENT RESISTIVITY

ohm meters



APPARENT POLARIZATION

millivolt seconds/volt



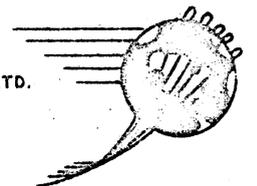
LINE: 50
LOOKING: NE
DIPOLE LENGTH: . . . 1000'
DATE: APR 4, 1969

LEGEND

FENCE: X
PIPELINE: O
POWER LINE: T

CANADIAN AERO

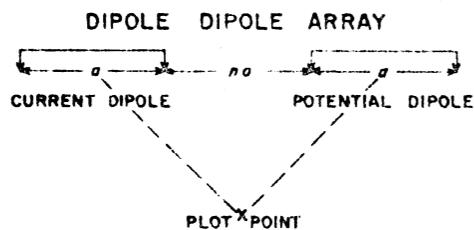
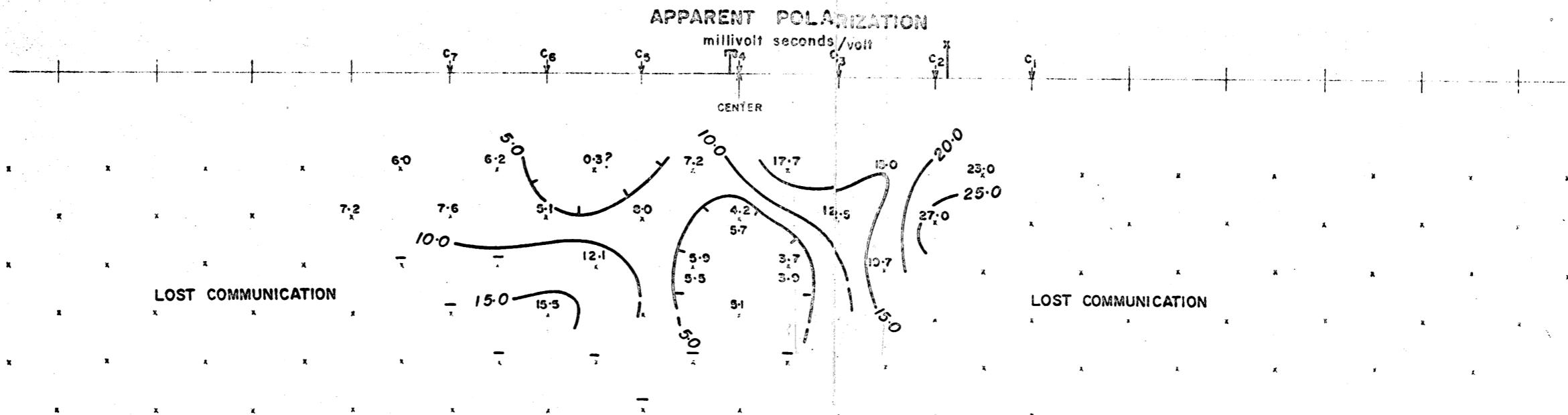
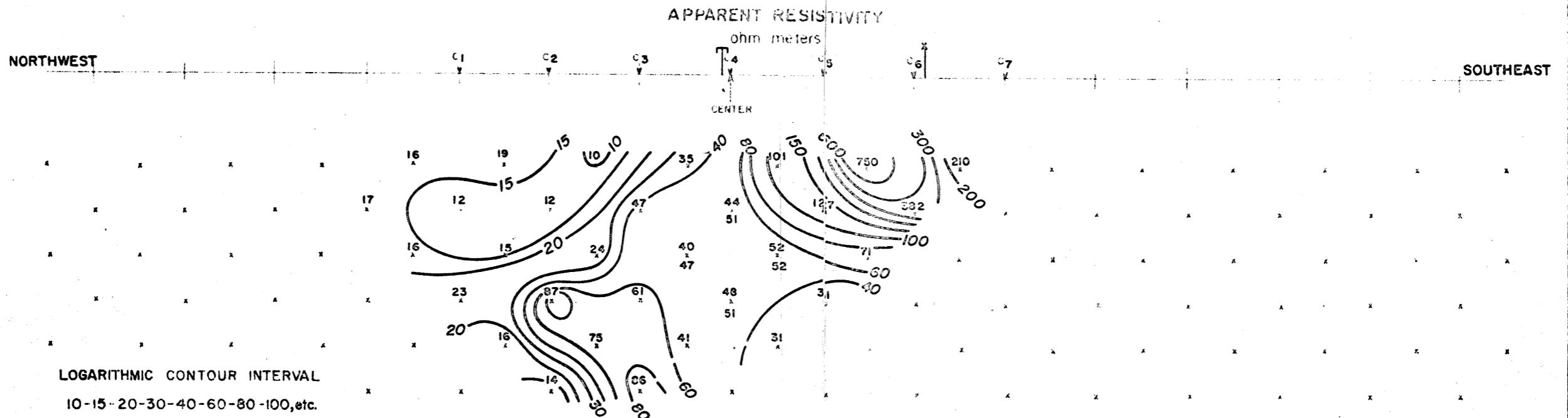
Mineral Surveys LTD.
OTTAWA, ONT. CANADA
TUCSON, ARIZONA U.S.A.



TIME DOMAIN INDUCED POLARIZATION AND RESISTIVITY SURVEY

BS & K PROJECT-SILVER BELL DISTRICT-PIMA COUNTY, ARIZONA

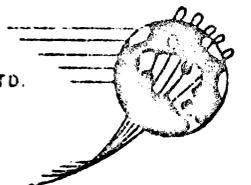
FOR
THE HANNA MINING COMPANY



LINE 48
LOOKING NE
DIPOLE LENGTH 1000
DATE: AP., 3, 1969

LEGEND
FENCE
PIPELINE
POWERLINE

CANADIAN GEO
Mineral Surveys LTD.
OTTAWA, ONT. CANADA
TUCSON, ARIZONA U.S.A.



TIME DOMAIN INDUCED POLARIZATION AND RESISTIVITY SURVEY

BS & K PROJECT-SILVER BELL DISTRICT-PIMA COUNTY, ARIZONA

THE HANNA MINING COMPANY

APPARENT RESISTIVITY

ohm meters

NORTHWEST C1 C2 C3 C4 5 C6 C7 C8 C9 X SOUTHEAST

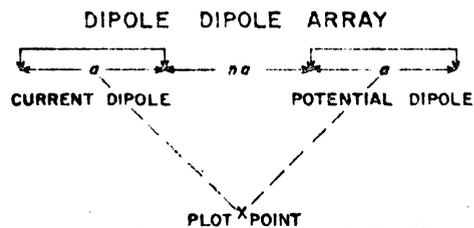
CENTER

LOGARITHMIC CONTOUR INTERVAL
10-15-20-30-40-60-80-100, etc.

APPARENT POLARIZATION

millivolt seconds/volt

CENTER



LINE: 46
LOOKING: NE
DIPOLE LENGTH: . . . 100
DATE: MAR. 31, 1969

LEGEND

FENCE
PIPELINE
POWERLINE

CANADIAN AERO

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OTTAWA, ONT. CANADA
TUCSON, ARIZONA, U.S.A.



TIME DOMAIN INDUCED POLARIZATION AND RESISTIVITY SURVEY

BS & K PROJECT-SILVER BELL DISTRICT-PIMA COUNTY, ARIZONA

FOR

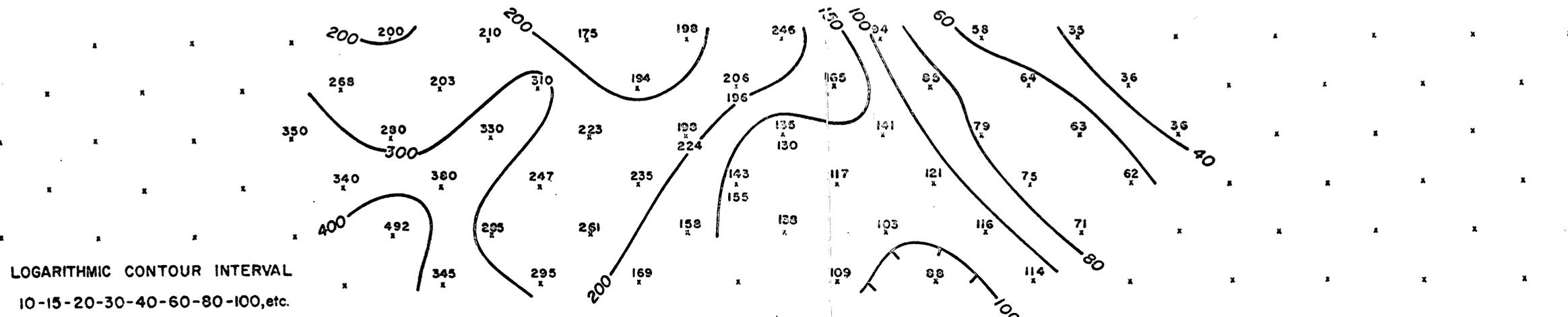
THE HANNA MINING COMPANY

APPARENT RESISTIVITY

ohm meters

NORTHWEST SOUTHEAST

CENTER

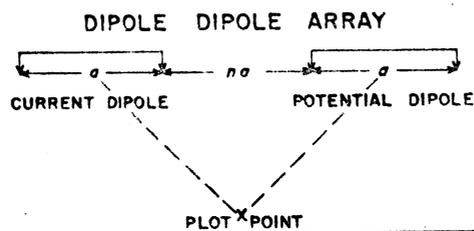
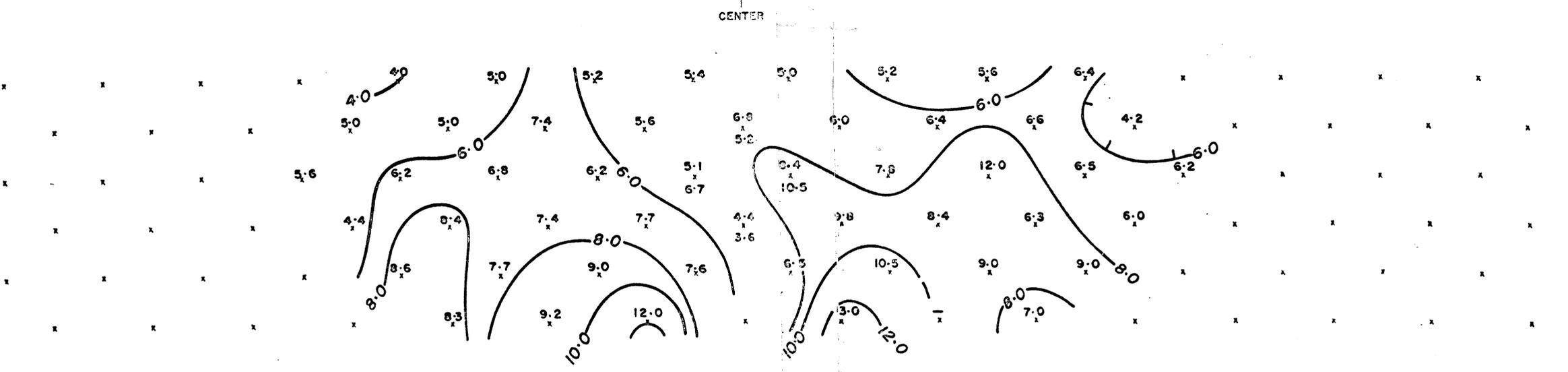


LOGARITHMIC CONTOUR INTERVAL
10-15-20-30-40-60-80-100, etc.

APPARENT POLARIZATION

millivolt seconds/volt

CENTER



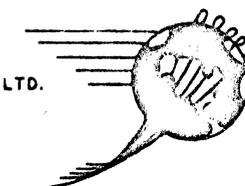
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LOOKING: NE
DIPOLE LENGTH: 1000'
DATE: MAR. 20, 1969

LEGEND

- FENCE
- PIPELINE
- POWERLINE

CANADIAN AERO

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TUCSON, ARIZONA, U.S.A.



TIME DOMAIN INDUCED POLARIZATION AND RESISTIVITY SURVEY

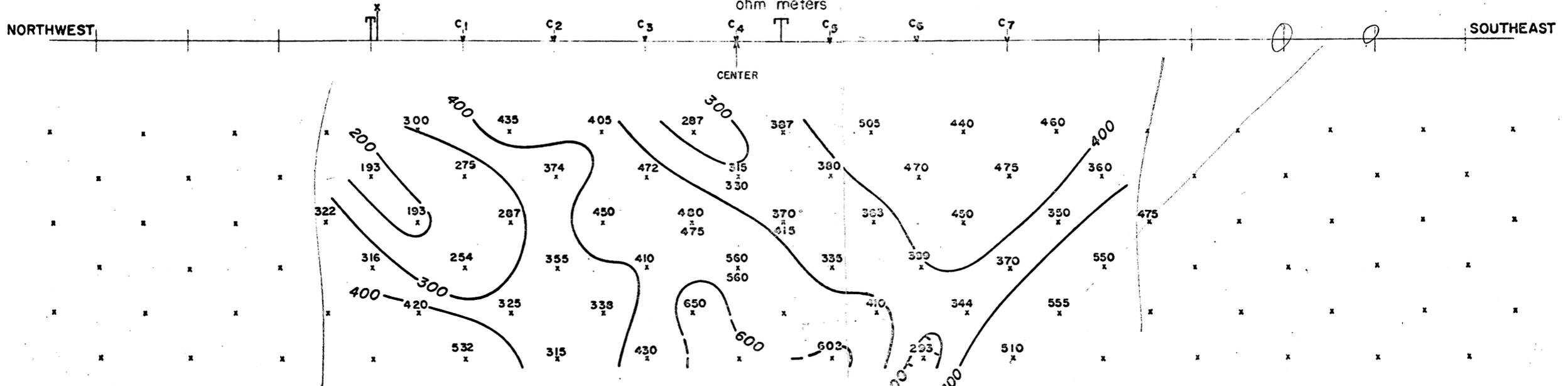
BS & K PROJECT-SILVER BELL DISTRICT-PIMA COUNTY, ARIZONA

FOR

THE HANNA MINING COMPANY

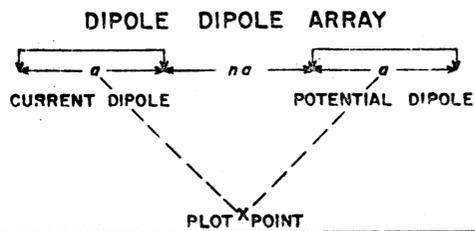
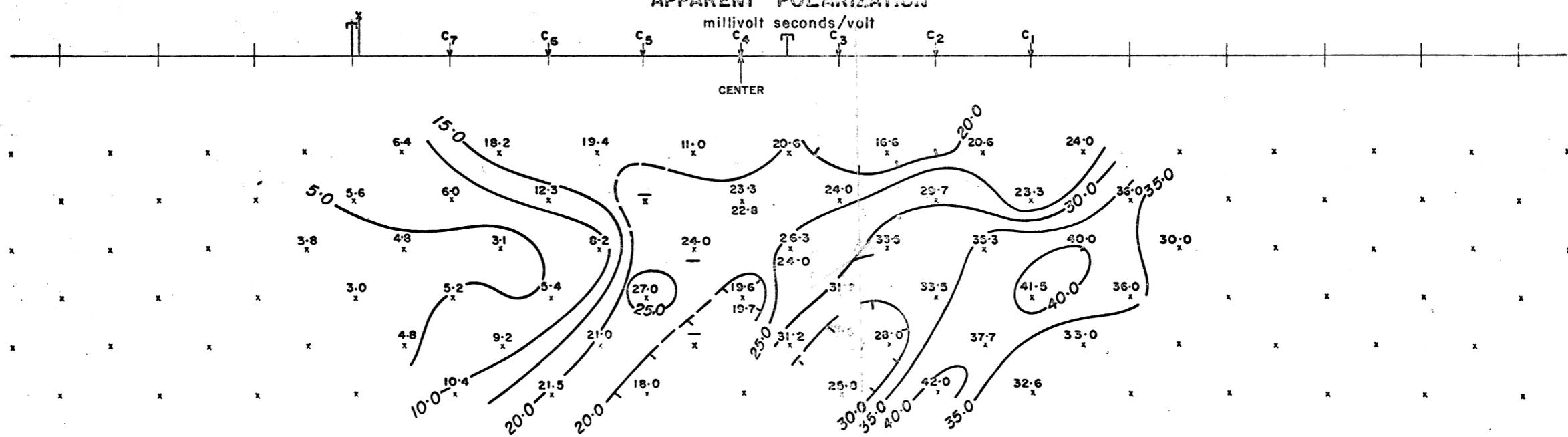
APPARENT RESISTIVITY

ohm meters



APPARENT POLARIZATION

millivolt seconds/volt

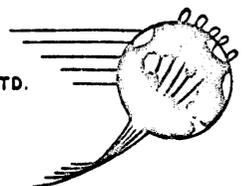


LINE: 54
 LOOKING: NE
 DIPOLE
 LENGTH: . . . 1000'
 DATE: AP., 9, 1969

LEGEND
 FENCE X
 PIPELINE - - -
 POWERLINE T

CANADIAN AERO

Mineral Surveys LTD.
 OTTAWA, ONT. CANADA
 TUCSON, ARIZONA, U.S.A.



TIME DOMAIN INDUCED POLARIZATION AND RESISTIVITY SURVEY

BS & K PROJECT-SILVER BELL DISTRICT-PIMA COUNTY, ARIZONA

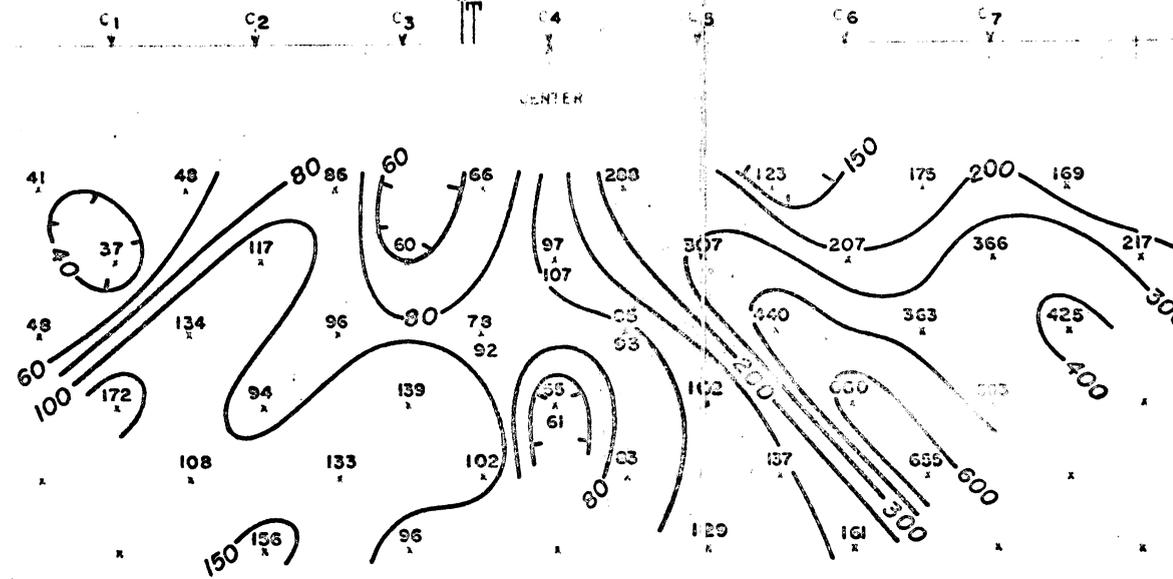
THE HANNA MINING COMPANY

APPARENT RESISTIVITY

ohm meters

NORTHWEST

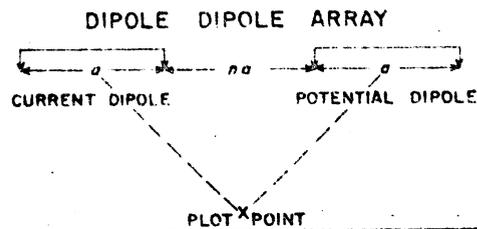
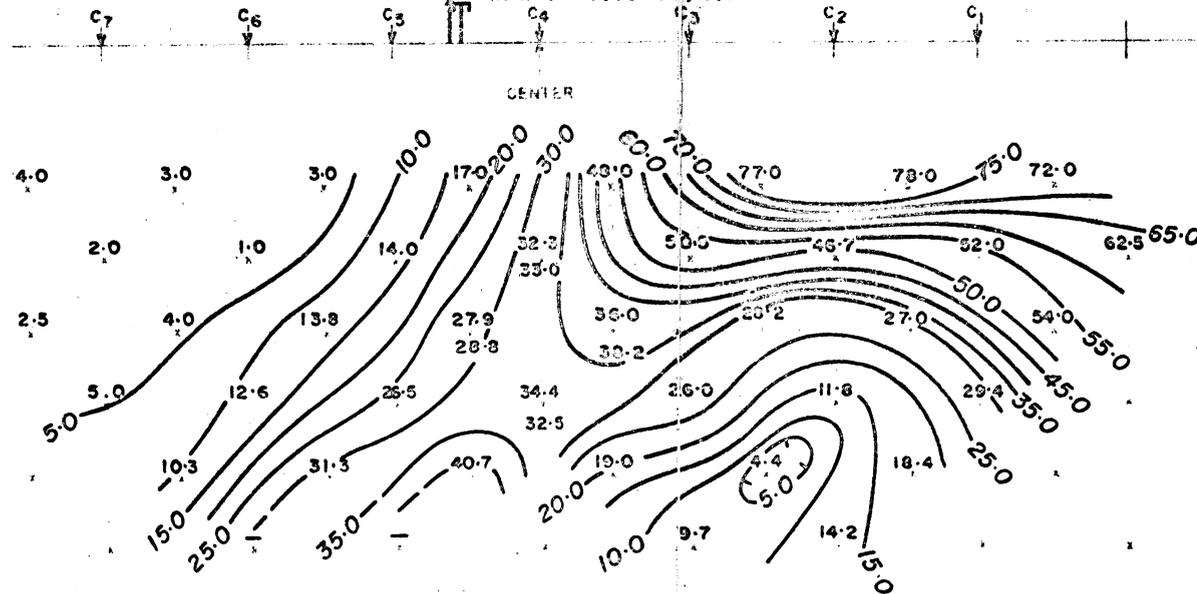
SOUTHEAST



LOGARITHMIC CONTOUR INTERVAL
10-15-20-30-40-60-80-100, etc.

APPARENT POLARIZATION

millivolt seconds/volt



LINE: 52
LOOKING: NE
DIPOLE
LENGTH: . . . 1000'
DATE: AP, 7, 1969

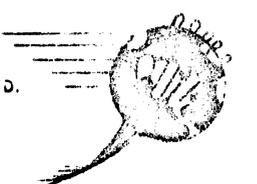
LEGEND

FENCE
PIPELINE
POWER

CANADIAN AERO

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TUCSON, ARIZONA U.S.A.



REPORT ON THE
INDUCED POLARIZATION SURVEY
FOR
B. S. & K. MINING COMPANY, ARIZONA
PART II

*Aug 1958
3298
not included*

McPHAR GEOPHYSICS LIMITED

NOTES ON THE THEORY OF INDUCED POLARIZATION

AND THE METHOD OF FIELD OPERATION

Induced Polarization as a geophysical measurement refers to the blocking action or polarization of metallic or electronic conductors in a medium of ionic solution conduction.

This electro-chemical phenomenon occurs wherever electrical current is passed through an area which contains metallic minerals such as base metal sulphides. Normally, when current is passed through the ground, as in resistivity measurements, all of the conduction takes place through ions present in the water content of the rock, or soil, i. e. by ionic conduction. This is because almost all minerals have a much higher specific resistivity than ground water. The group of minerals commonly described as "metallic", however, have specific resistivities much lower than ground waters. The induced polarization effect takes place at those interfaces where the mode of conduction changes from ionic in the solutions filling the interstices of the rock to electronic in the metallic minerals present in the rock.

The blocking action or induced polarization mentioned above, which depends upon the chemical energies necessary to allow the ions to give up or receive electrons from the metallic surface, increases with the time that a d. c. current is allowed to flow through the rock, i. e. as ions pile up against the metallic interface the resistance to current flow increases. Eventually, there is enough polarization in the form of excess ions at the

interfaces to effectively stop all current flow through the metallic particle. This polarization takes place at each of the infinite number of solution-metal interfaces in a mineralized rock.

When the d. c. voltage used to create this d. c. current flow is cut off, the Coulomb forces between the charged ions forming the polarization cause them to return to their normal position. This movement of charge creates a small current flow which can be measured on the surface of the ground as a decaying potential difference.

From an alternate viewpoint it can be seen that if the direction of the current through the system is reversed repeatedly before the polarization occurs, the effective resistivity of the system as a whole will change as the frequency of the switching is changed. This is a consequence of the fact that the amount of current flowing through each metallic interface depends upon the length of time that current has been passing through it in one direction.

The values of the "metal factor" or "M. F." are a measure of the amount of polarization present in the rock mass being surveyed. This parameter has been found to be very successful in mapping areas of sulphide mineralization, even those in which all other geophysical methods have been unsuccessful. The induced polarization measurement is more sensitive to sulphide content than other electrical measurements because it is much more dependent upon the sulphide content. As the sulphide content of a rock is increased, the "metal factor" of the rock increases much more rapidly than the resistivity decreases.

For example, in one of the large porphyry copper pits, the resistivity contrast between the protore and the enriched zone was found to be only 180/18 or 10/1. The contrast in metal factor in the same pit was found to be 20/10,000. There was less than 1% sulphides in the protore and 5-9% sulphides in the enriched zones. As the sulphide content is increased the metal factor increases until for massive sulphides the values apparently are measured in hundreds of thousands.

Because of this increased sensitivity it is possible to locate and outline zones of less than 10% sulphides that can't be located by E. M. Methods. The method has been successful in locating the disseminated "porphyry copper" type mineralization in the Southwestern United States.

Measurements and experiments also indicate that it should be possible to locate most massive sulphide bodies at a greater depth with induced polarization than with E. M.

Since there is no I. P. effect from any conductor unless it is metallic, the method is useful in checking E. M. anomalies that are suspected of being due to water filled shear zones or other ionic conductors. There is also no effect from conductive overburden, which frequently confuses E. M. results. It would appear from scale model experiments and calculations that the apparent metal factors measured over a mineralized zone are larger if the material overlying the zone is of low resistivity.

Apropos of this, it should be stated that the induced polarization measurements indicate the total amount of metallic constituents in the rock. Thus all of the metallic minerals in the rock, such as pyrite, as well as

the ore minerals chalcopryrite, chalcocite, galena, etc. are responsible for the induced polarization effect. Some oxides such as magnetite, pyrolusite, chromite and some forms of hematite also conduct by electrons and are metallic. All of the metallic minerals in the rock will contribute to the induced polarization effect measured on the surface.

In the field procedure, measurements on the surface are made in a way that allows the effects of lateral changes in the properties of the rocks to be separated from the effects of vertical changes in the properties. Current is applied to the ground at one point, the sender location, and voltage difference measurements are made at several other spots, the receiver locations. The sender location is then changed and the procedure is repeated. The value of apparent resistivity and apparent metal factor for any given pair of sender and receiver locations is plotted on the map at the intersection of grid lines, one from the sender location and one from the receiver location. The resistivity values are plotted above the line and the metal factor values below the line. The lateral displacement of a given value is determined by the location along the survey line of the centre point between the sender and receiver locations. The distance of the value from the line is determined by the separation between the sender and receiver that gave that particular value.

The separation between sender and receiver is only one factor which determines the depth to which the ground is being sampled in any particular measurement. These plots then, when contoured, are not section maps of the electrical properties of the ground under the survey line.

The interpretation of the results from any given survey must be carried out using the combined experience gained from field, model and theoretical investigations.

In the field procedure, the interval over which the potential differences are measured is the same as the interval over which the sender is moved after a series of readings has been made. One of the advantages of the induced polarization method is that the same equipment can be used for both detailed and reconnaissance surveys merely by changing the interval over which the transmitter is moved each time. In the past, intervals have been used ranging from 100 feet to 1000 feet for the basic distance. In each case, the decision as to spread distance is largely determined by the expected size of the mineral deposit being sought, the size of the expected anomaly and the speed with which it is desired to progress.

The speed at which measurements can be made along a line is directly related to the length of spread used. In some detailed surveys in which the area of interest had been outlined by previous drilling and/or geology, spreads of 200 feet have been used. In these cases, distances ranging from 2500 feet to 3500 feet may be covered in a normal day's operation by one crew. In reconnaissance work using a 1000 foot spread distances of 5000 to 8000 feet may be surveyed in one day.

McPHAR GEOPHYSICS LIMITED

REPORT ON THE

INDUCED POLARIZATION SURVEY

FOR

B. S. & K. MINING COMPANY, ARIZONA

PART II

1. INTRODUCTION

During June 1960, an Induced Polarization survey was carried out over a portion of the B. S. & K. Mining Company property in the Silver Bell area of southern Arizona. The investigation revealed the presence of an interesting anomaly to the west of the mine workings and in our report of June 28, 1960, additional surveying was recommended.

This report describes the results obtained from the subsequent investigations carried out in October of this year.

2. PRESENTATION OF RESULTS

The Induced Polarization and Resistivity data are plotted in the manner described in the notes accompanying this report and are shown on the data plots as follows.

| | | |
|---------------|------------------|----------------|
| Line 2 + 00S | 300 foot spreads | Dwg. IP 2771-1 |
| Line A | 300 foot spreads | Dwg. IP 2771-2 |
| Line A | 200 foot spreads | Dwg. IP 2771-3 |
| Line 2 + 00N | 300 foot spreads | Dwg. IP 2771-4 |
| Line 10 + 00W | 300 foot spreads | Dwg. IP 2771-5 |

A sketch of the grid is shown on drawing Misc. 3298 at a scale of 1" = 200'. This is approximate only, being based on pace-and-compass traverses. The definite and possible induced polarization anomalies are indicated by solid and broken bars respectively on this plan map as well as the data plots. These bars represent the surface projection of the anomalous zones as interpreted from the location of the transmitter and receiver electrodes when the anomalous values were measured.

Since the induced polarization measurement is essentially an averaging process, as are all potential methods, it is frequently difficult to exactly pinpoint the source of an anomaly. Certainly, no anomaly can be located with more accuracy than the spread length; i. e. when using 200' spreads the position of a narrow sulphide body can only be determined to lie between two stations 200' apart. In order to locate sources at some depth, larger spreads must be used, with a corresponding increase in the uncertainties of location. Therefore, while the center of the indicated anomaly probably corresponds fairly well with source, the length of the indicated anomaly along the line should not be taken to represent the exact edges of the anomalous material.

Unfortunately the station numbers on the two surveys do not agree. Although the lines coincide in location, the zero point on the present survey is 400' east of the zero point on the original survey. A numbered picket has been placed at each station to avoid any possible confusion in the future.

3. DISCUSSION OF RESULTS

The June survey indicated an interesting anomaly on Line A between stations 4 + 00W and 8 + 00W (i. e. 8 + 00W - 12 + 00W on the new grid). The source appeared to be a sub-vertical tabular body at shallow depth relative to the spread (i. e. less than 400 feet). Line A was re-surveyed in October using 300 foot spreads to confirm the anomaly. Parallel lines were then run 200 feet to the north and south to trace the zone and a fourth line was run along the strike of the anomaly. The results from each line are described below.

Line 2 + 00S

There is an anomaly of moderate strength and intermediate depth at about 9 + 00W on this line. The apparent Metal Factors are smaller than on Line A suggesting that the source is becoming smaller or deeper, or that the line is near the south end of the zone. The results on Line 10 + 00W indicate that this latter interpretation is correct.

Anomalous Metal Factors were also encountered at the west end of the line. These values are based on very low voltages and small frequency effects (1/4 - 3/4%) and hence cannot be considered to be reliable. The associated resistivity low may represent the boundary fault assumed to occur along the west side of the hills.

Line A

The 300 foot data show a moderate anomaly centered at 9 + 00W, corresponding with the feature outlined during the June

survey. Several anomalous values were repeated using a greater frequency spread (D. C. - 2-1/2 cps) with a resultant large increase in the apparent Metal Factor indicative of a metallic source.

In addition, there is a small shallow anomaly centered at about station 0 + 00. The east part of the line was re-surveyed using 200 foot spreads in order to obtain greater detail. This work confirmed the location of the anomaly and indicated a depth of the order of 100 - 150 feet to the source.

Line 2 + 00N

Considerable difficulty was encountered on this line because of interference from the numerous surface features. Even with the power turned off at the mill, it was not possible to obtain reliable data on part of the line. However, the resistivity data indicate the presence of the anomaly on this line and such I. P. values as were obtained seem to confirm that the zone extends this far north.

Line 10 + 00W

A line was run along the axis of the anomaly to determine the length of the zone. The results indicate that the south end occurs near station 0 or between 0 and 3S. Reliable data could not be obtained to the north because of excessive electrical noise from the power lines. The source appears to be shallower on this line, but there may be complicating factors present, especially the tailings dump.

4. SUMMARY & RECOMMENDATIONS

The October survey has confirmed the I. P. anomaly on Line A and has traced the zone farther to the north and south. A second smaller anomaly has been indicated on the eastern part of Line A.

While there are several surface features (mill, tailings dump, water pipe, etc.) which may be expected to interfere with the measurements or give rise to spurious local effects, it is felt that the main anomaly is primarily due to a sub-surface metallic source. Consequently it is recommended that a drill test be carried out to determine the cause of the anomaly. It is suggested that either a 400 foot vertical hole be drilled at 9 + 00W on Line A, or an inclined hole at 12 + 00W, Line A, drilling east at 45° for 450 - 500 feet.

From discussions with Mr. A. Kalaf, it would seem that the anomaly at 0 + 00, Line A is not related to any known ore lenses, but some interesting mineralization is known to occur in this area from previous underground work. If this is the case, then this anomaly should also be drilled. A hole is recommended at 2 + 00W, drilling east at 45°.

On completion of this test programme, the geophysical results should be reviewed in order to plan additional drilling if warranted and to plan a more extensive survey of the remainder of the property.

McPHAR GEOPHYSICS LIMITED

Robert A. Bell.

Robert A. Bell,
Geologist.

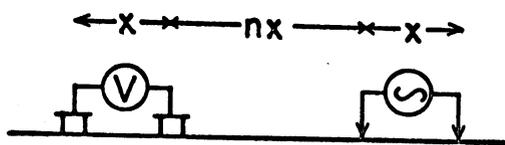
Philip G. Hallof

Philip G. Hallof,
Geophysicist.

Dated : November 8, 1960.

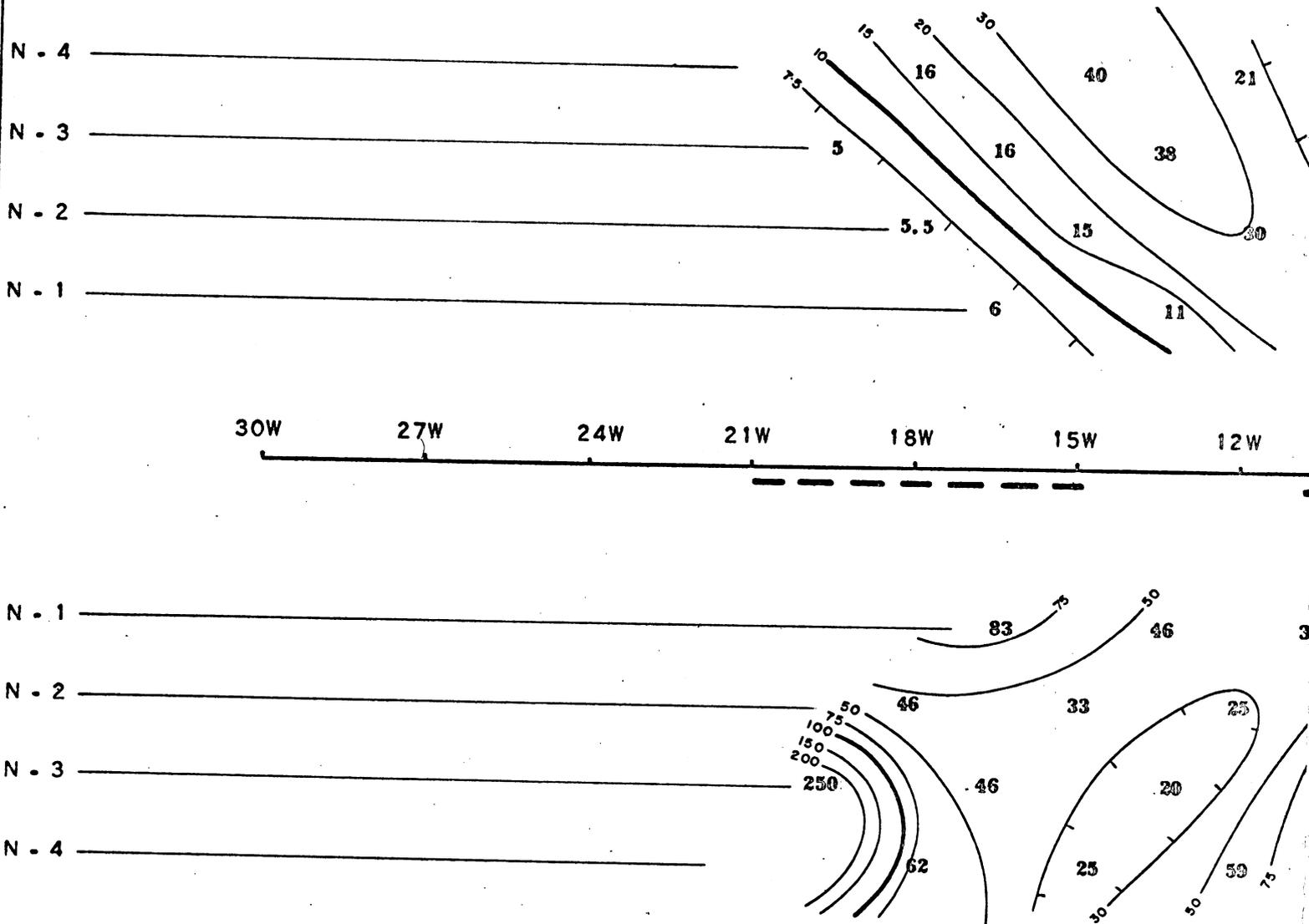
McPHAR GEOPHY

INDUCED POLARIZATION AND



ELECTRODE CONFIGURATION

X = 300



(10) DOUBTFUL READING

N SIGNAL/NOISE TOO LOW

ANOMALOUS ZONE

POSSIBLE ANOMALOUS ZONE

NOTE
LOGARITHMIC CONTOUR INTERVAL

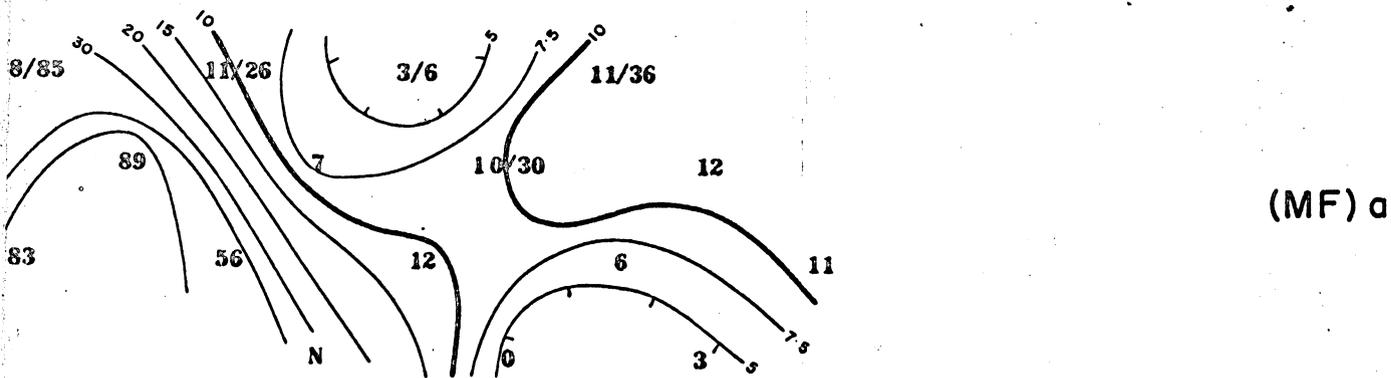
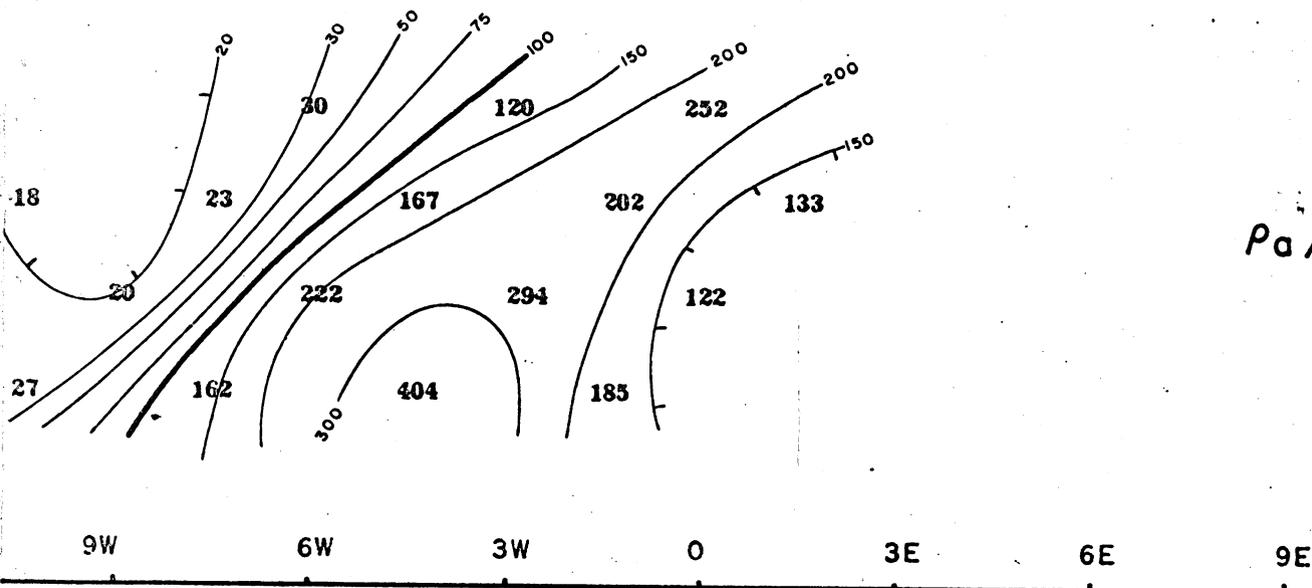
B.S. & K. MININ

PIMA COUNTY

Scale - One inch

SICS LIMITED

RESISTIVITY SURVEY



LINE NO. 2 S

FREQUENCY 25 - 2.5 C.P.S.

DATE SURVEYED JUNE/60

APPROVED RLB.

DATE Nov. 2/60.

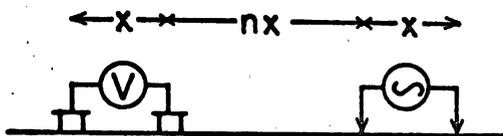
IG COMPANY

- ARIZONA.

= 300 Feet

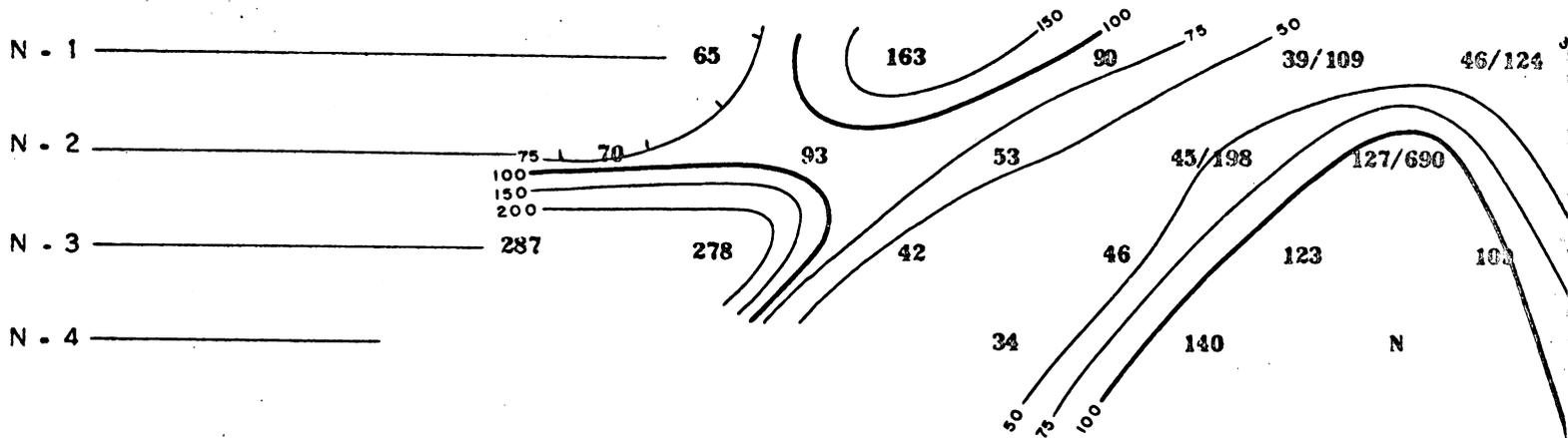
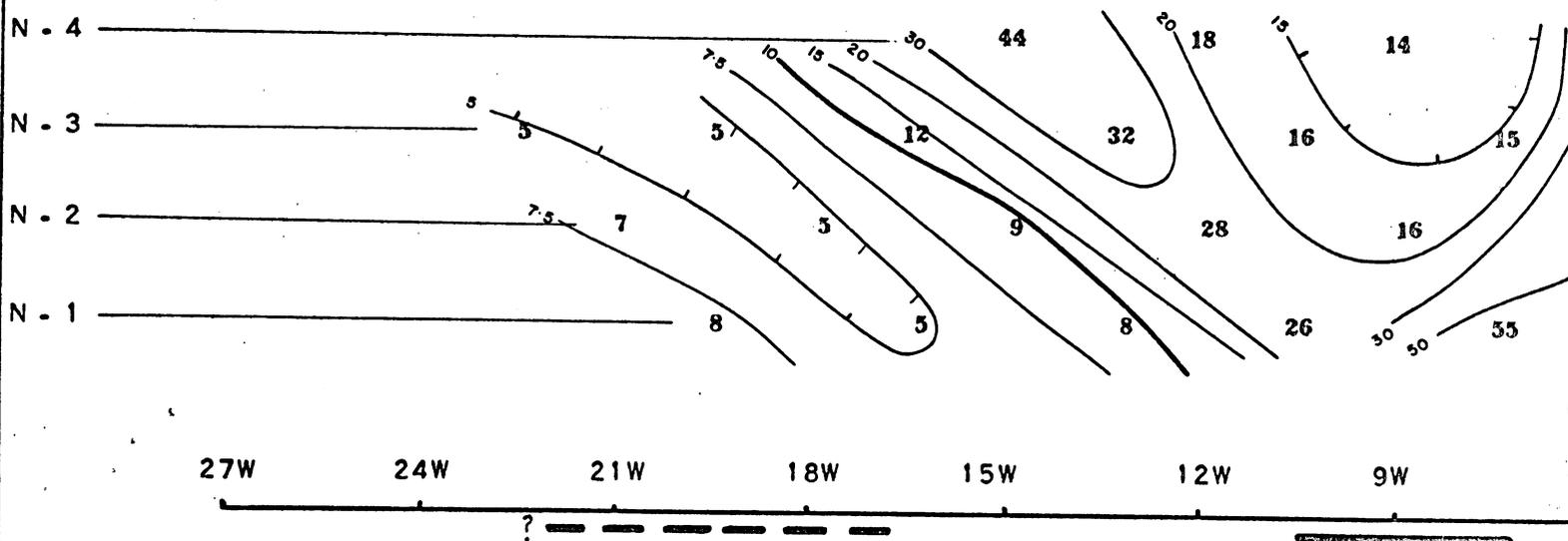
McPHAR GEOPHY

INDUCED POLARIZATION AND



ELECTRODE CONFIGURATION

X = 300



34/106 — .25-2.5/D.C.-2.5 CPS

(10) DOUBTFUL READING

N SIGNAL/NOISE TOO LOW

ANOMALOUS ZONE

POSSIBLE ANOMALOUS ZONE

NOTE
LOGARITHMIC CONTOUR INTERVAL

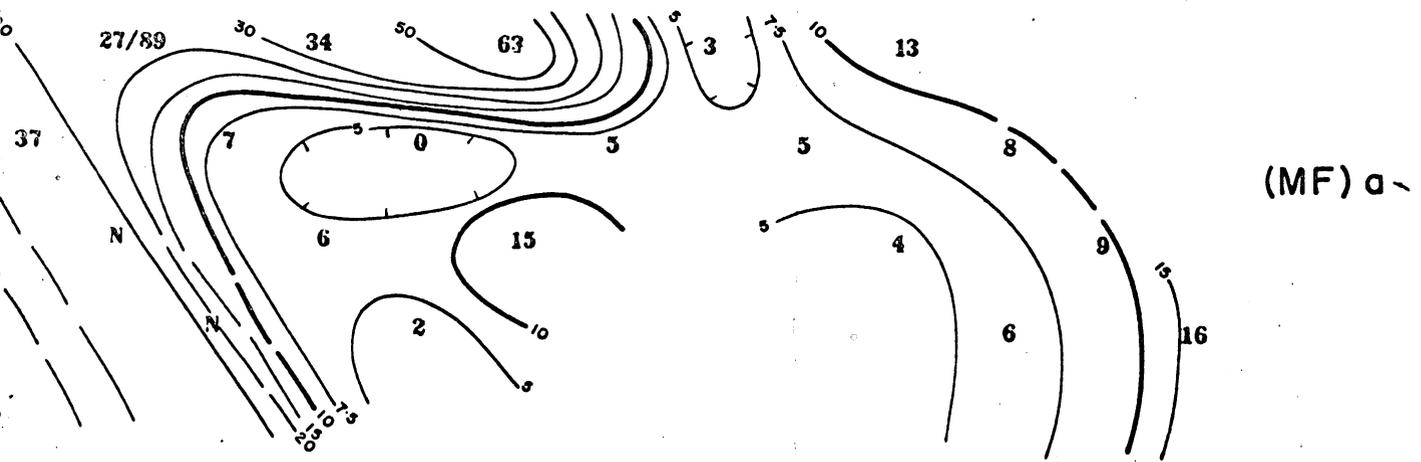
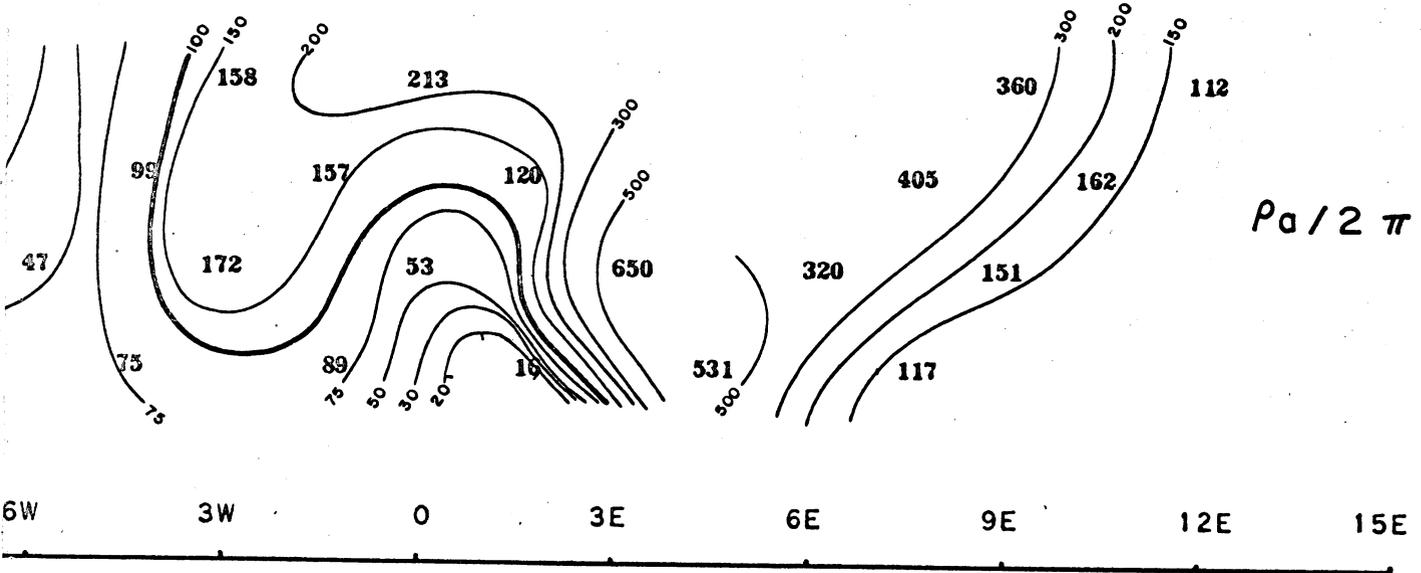
B.S. & K. MININ

PIMA COUNTY

Scale - One inch

SICS LIMITED

RESISTIVITY SURVEY



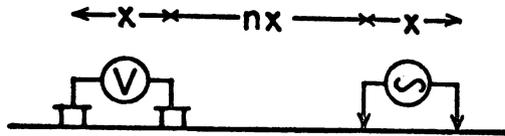
JG COMPANY
ARIZONA.
= 300 Feet

FREQUENCY 25-25 C.P.S.
DATE SURVEYED JUNE/60
APPROVED REB.
DATE Nov 2/60

LINE NO. "A"

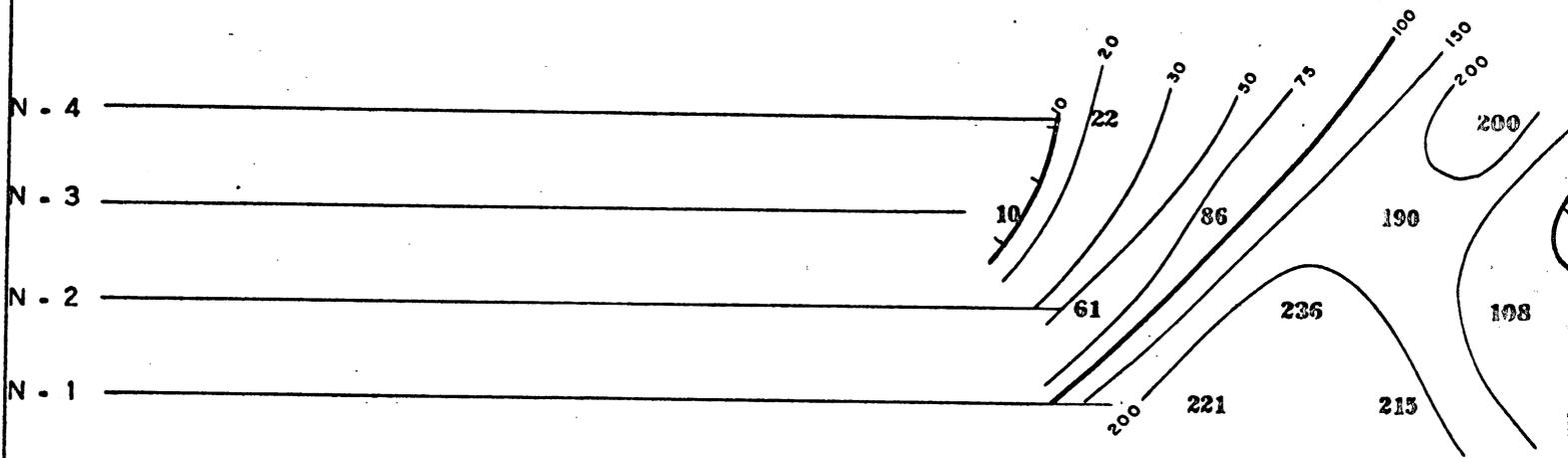
McPHAR GEOPHYSICS

INDUCED POLARIZATION ANOMALY



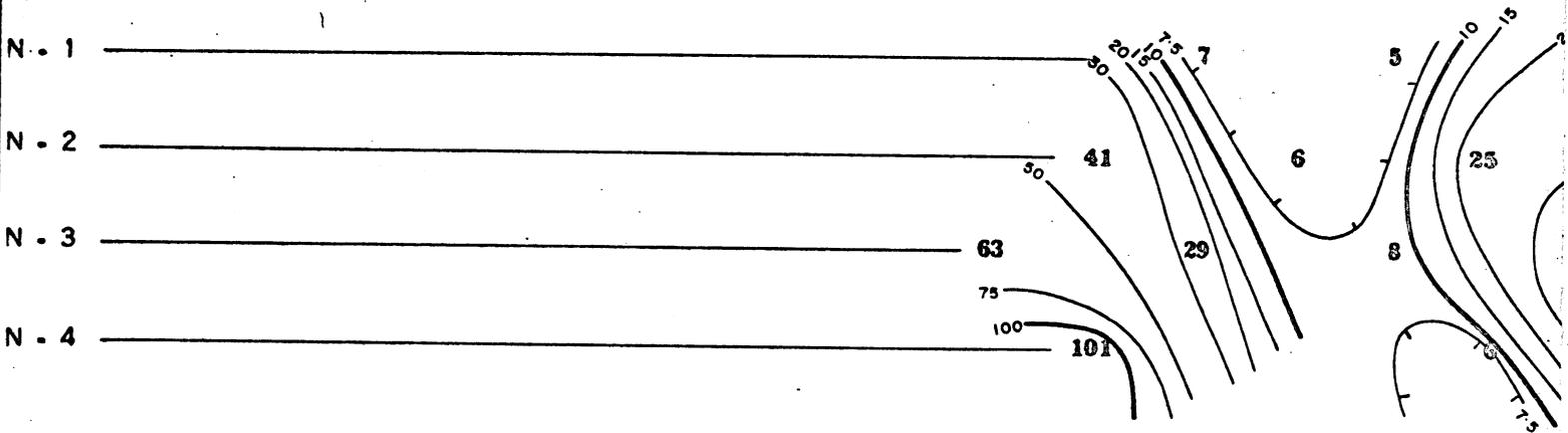
ELECTRODE CONFIGURATION

X - 200



12W 10W 8W 6W 4W 2W

?



(10) DOUBTFUL READING
 N SIGNAL/NOISE TOO LOW

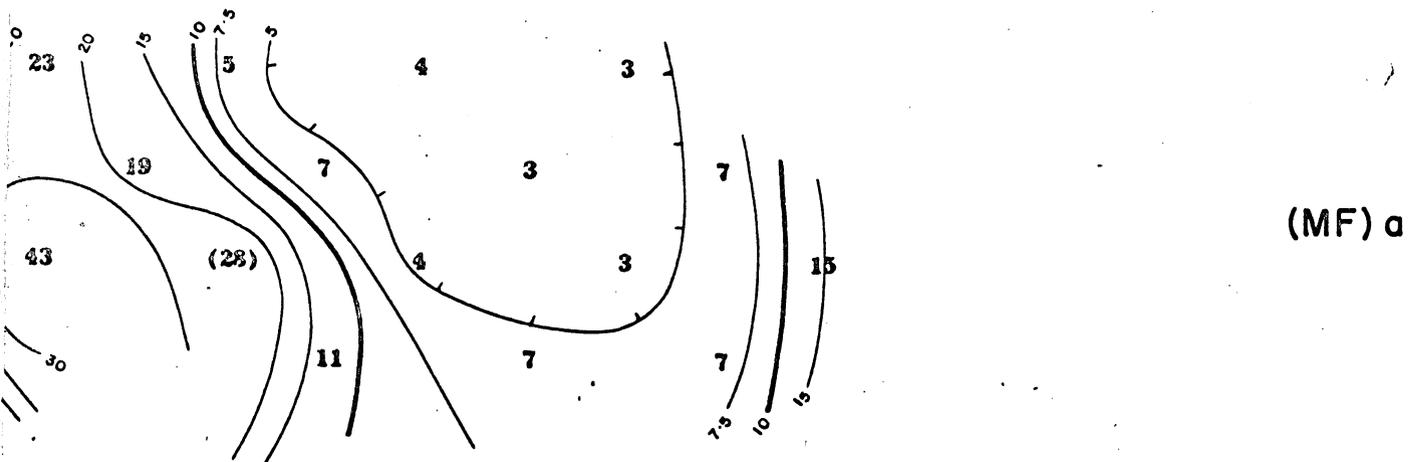
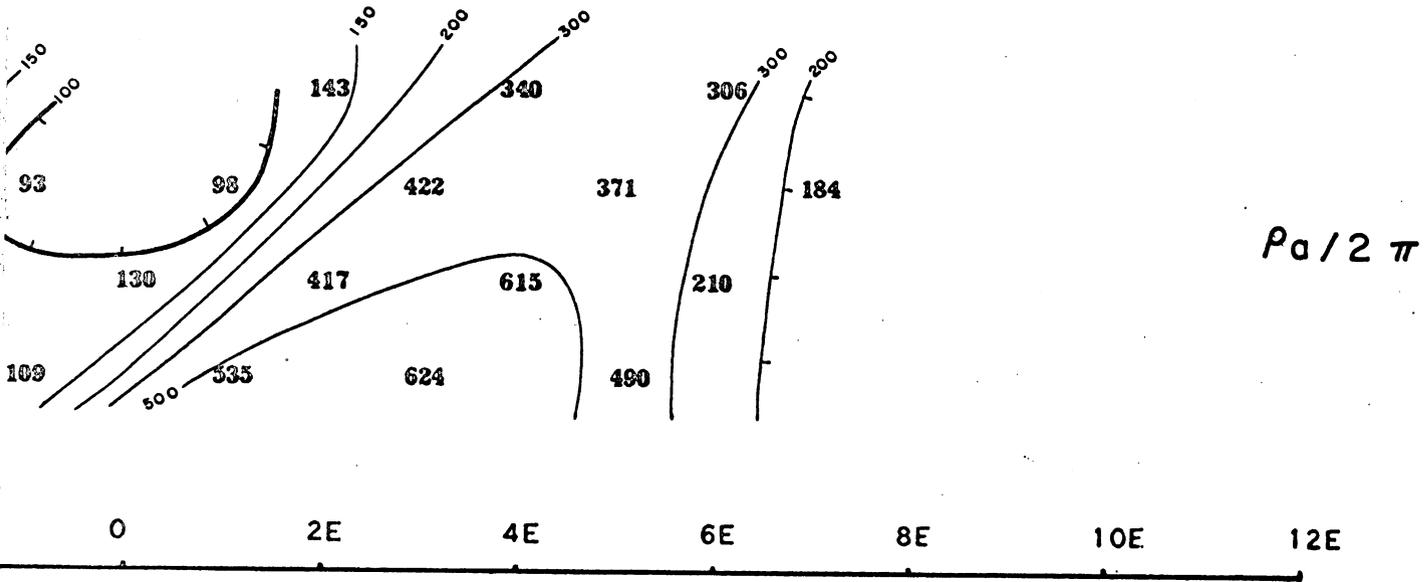
ANOMALOUS ZONE 
 POSSIBLE ANOMALOUS ZONE 

NOTE: LOGARITHMIC CONTOUR INTERVAL

B. S. & K. MINIER
 PIMA COUNTY
 Scale - One inch

PHYSICS LIMITED

D RESISTIVITY SURVEY



LINE NO. "A"

FREQUENCY 25 -2.5 C.P.S.

DATE SURVEYED JUNE/60

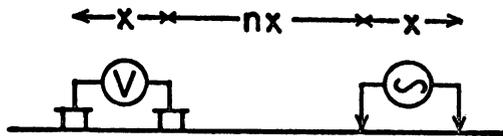
APPROVED R.C.B.

DATE Nov 2/60

ING COMPANY
Y - ARIZONA.
= 200 Feet

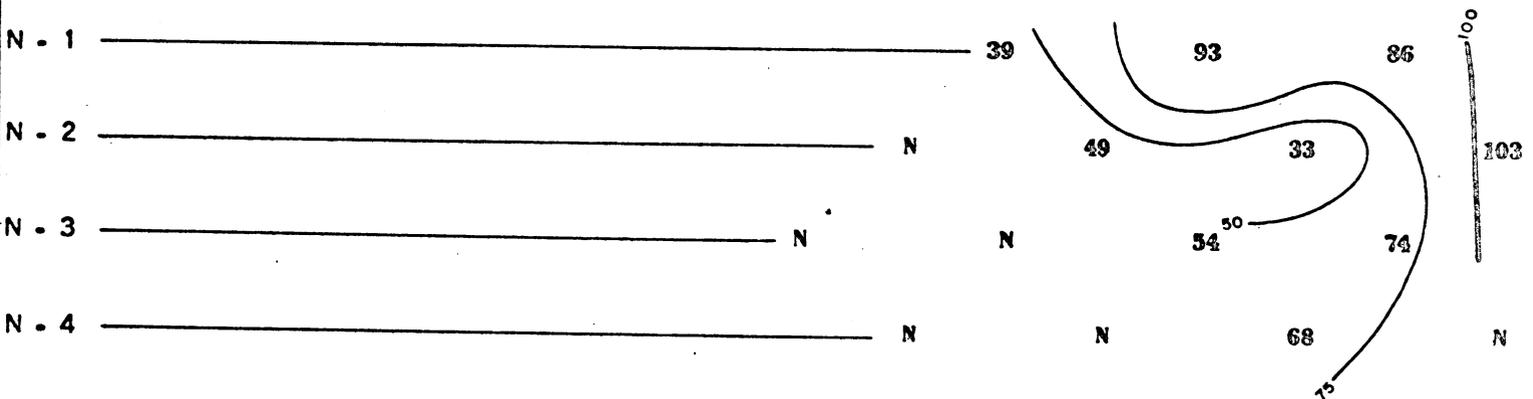
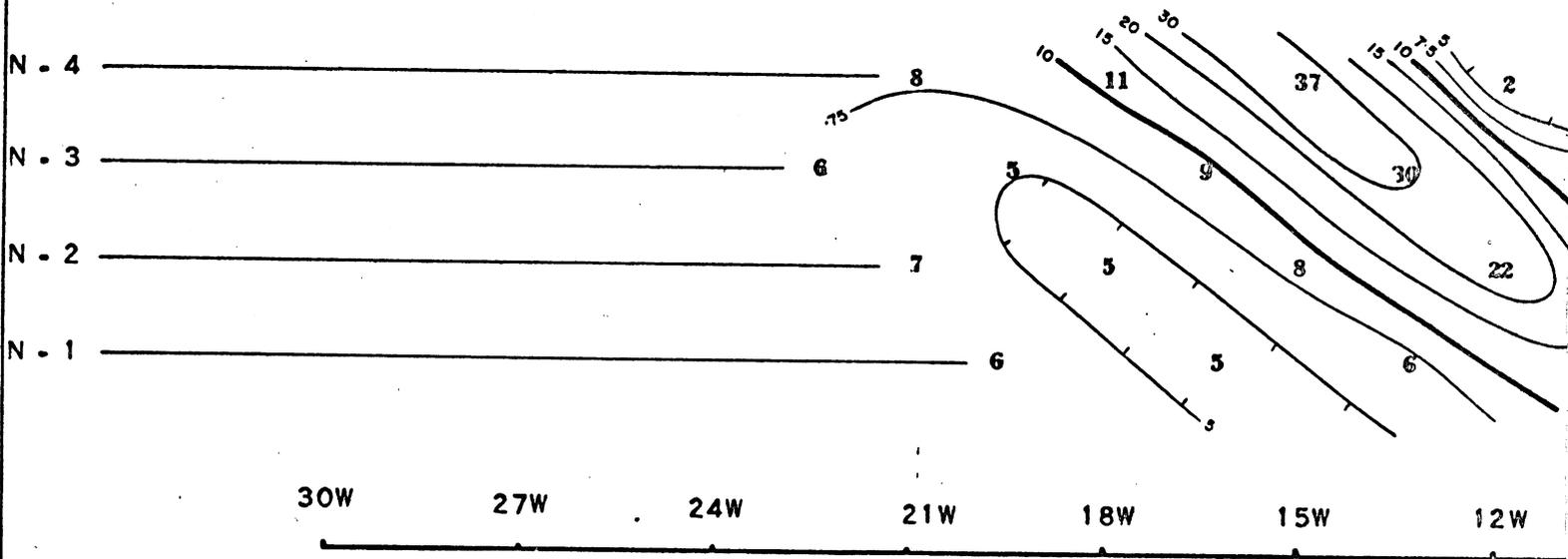
McPHAR GEOPHY

INDUCED POLARIZATION ANI



ELECTRODE CONFIGURATION

X - 300



(10) DOUBTFUL READING
 N SIGNAL/NOISE TOO LOW

ANOMALOUS ZONE

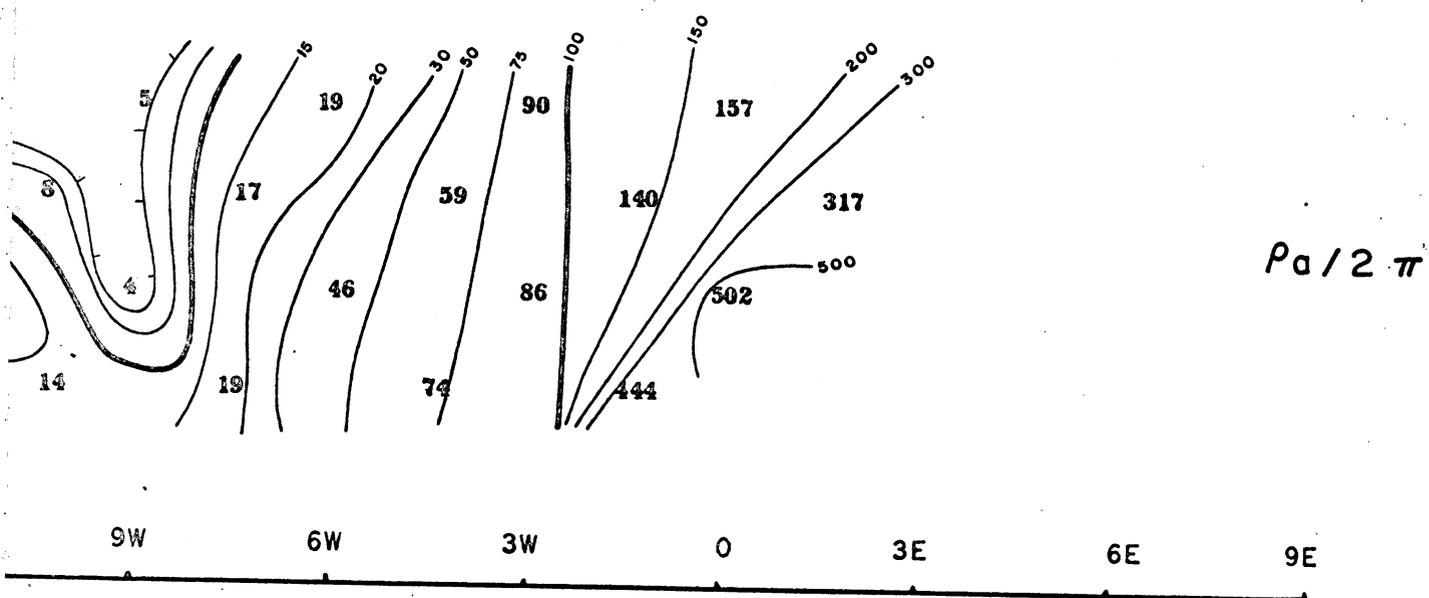
POSSIBLE ANOMALOUS ZONE

NOTE
 LOGARITHMIC CONTOUR INTERVAL

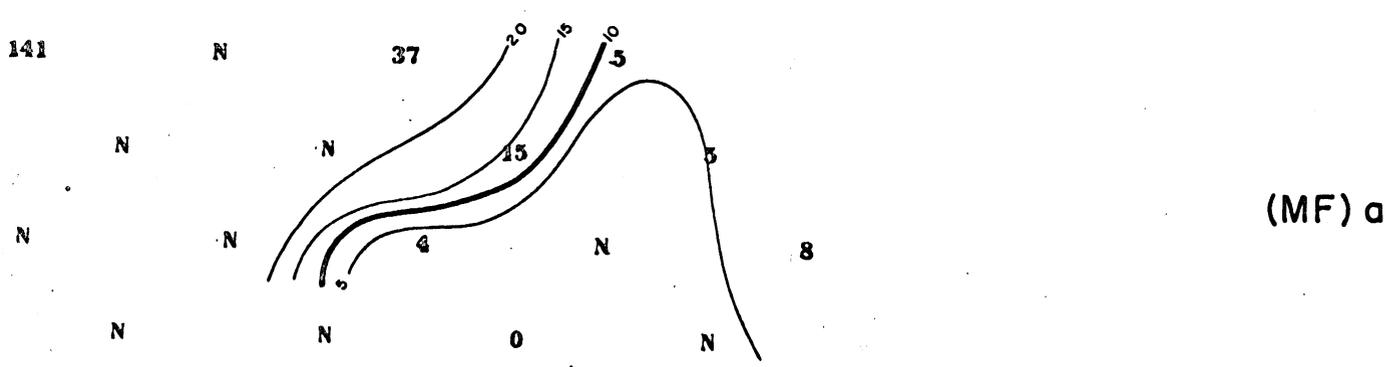
B.S. & K. MINING
 PIMA COUNTY
 Scale - One inch

PHYSICS LIMITED

D RESISTIVITY SURVEY



$\rho_a / 2\pi$



(MF) ρ_a

LINE NO. 2N

ING COMPANY.
-ARIZONA.
= 300 Feet

FREQUENCY 25 - 2.5 C.P.S.

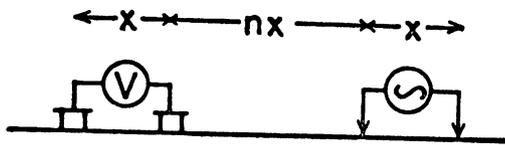
DATE SURVEYED JUNE/60

APPROVED R.A.H.

DATE Nov. 2/60

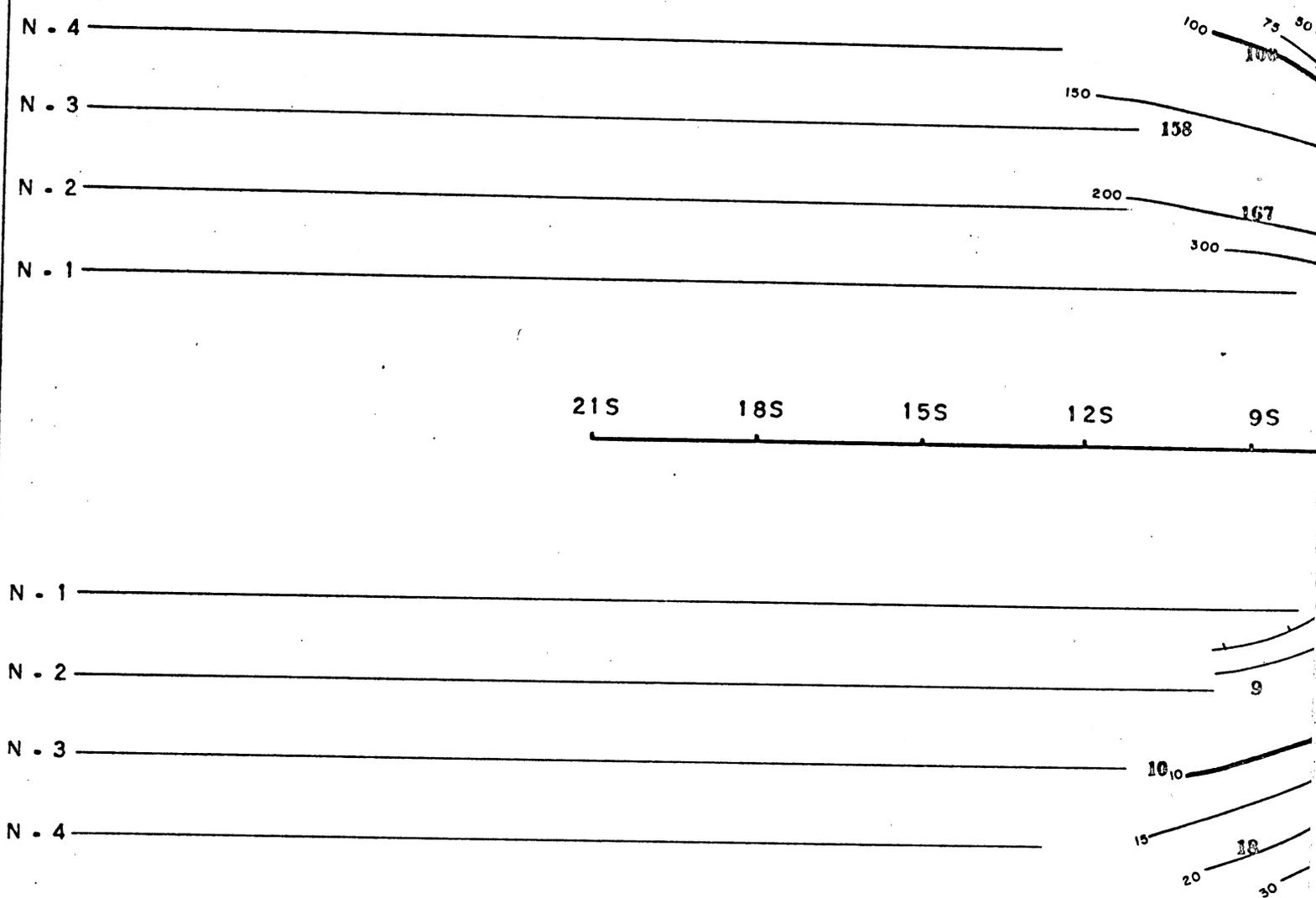
McPHAR GEOPHYSICAL

INDUCED POLARIZATION AND



ELECTRODE CONFIGURATION

X = 300



(10) DOUBTFUL READING

N SIGNAL/NOISE TOO LOW

ANOMALOUS ZONE

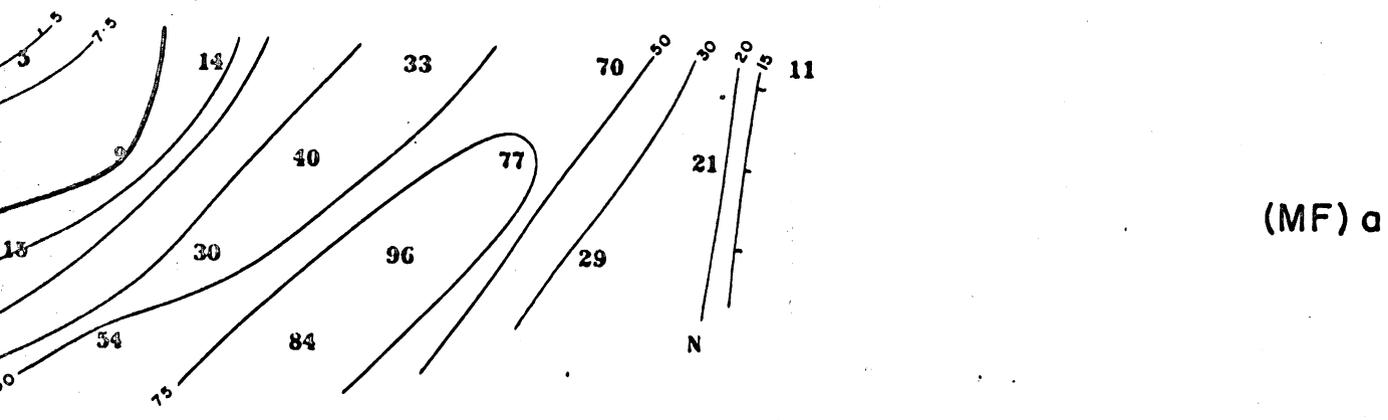
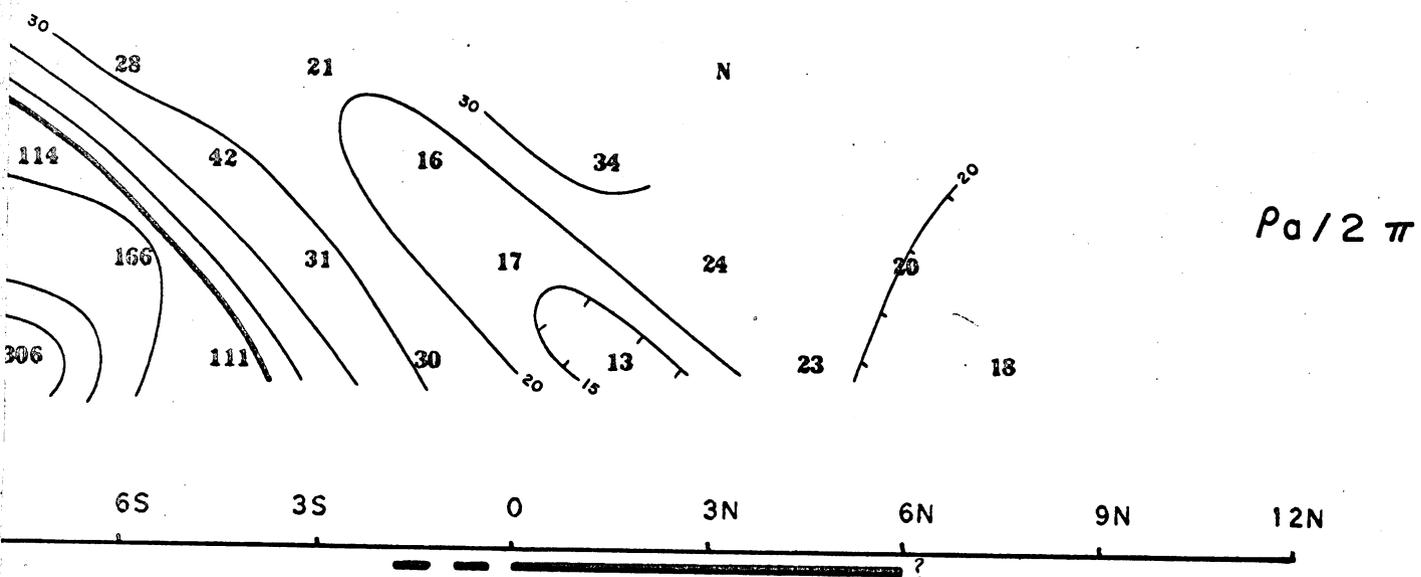
POSSIBLE ANOMALOUS ZONE

NOTE LOGARITHMIC CONTOUR INTERVAL

B.S. & K. MININ
 PIMA COUNTY
 Scale - One inch

SICS LIMITED

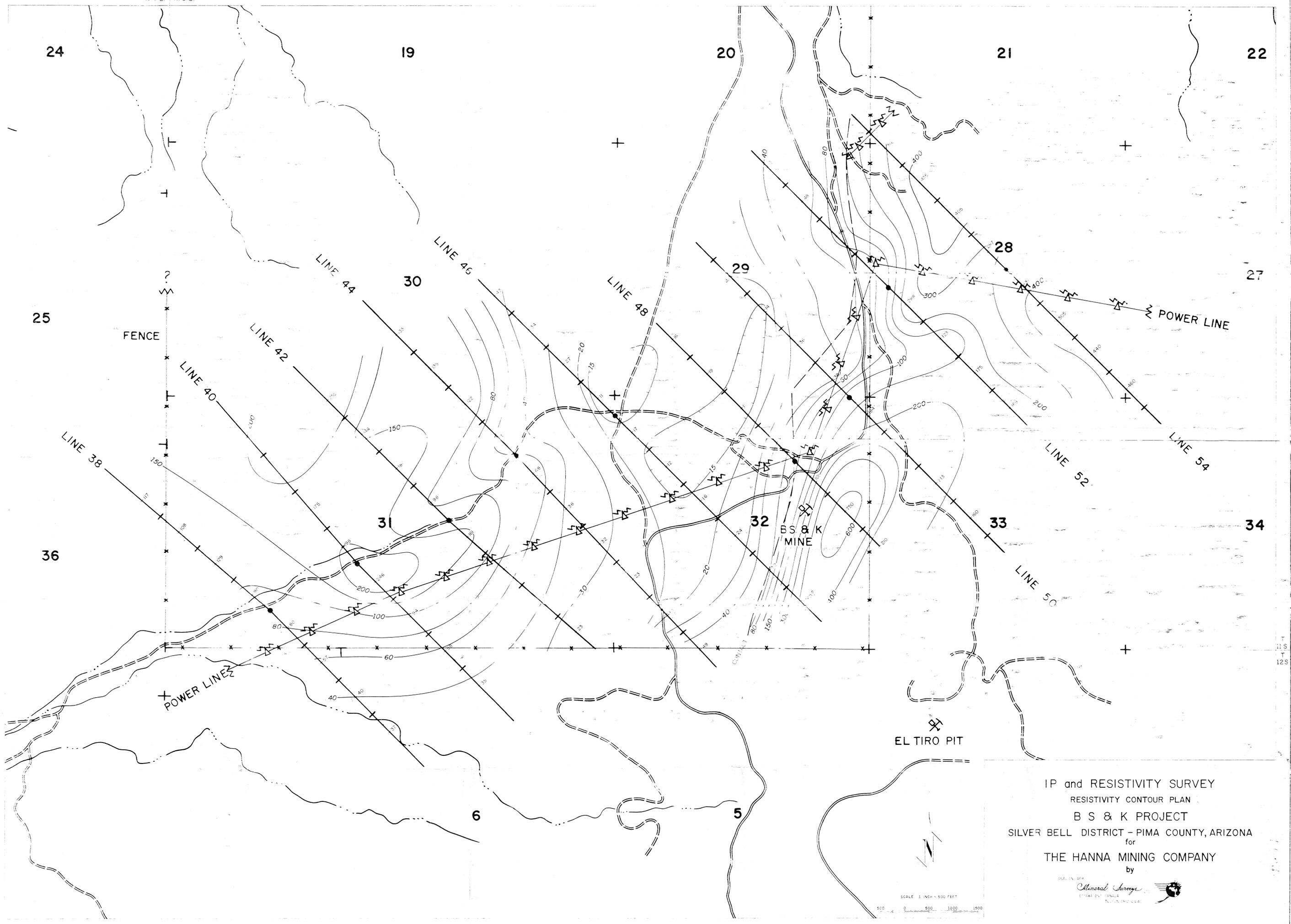
RESISTIVITY SURVEY



LINE NO.10W

ING COMPANY
-ARIZONA.
= 300 Feet

FREQUENCY 25 - 2.5 C.P.S.
DATE SURVEYED JUNE/60
APPROVED LAB.
DATE Nov. 2/60.

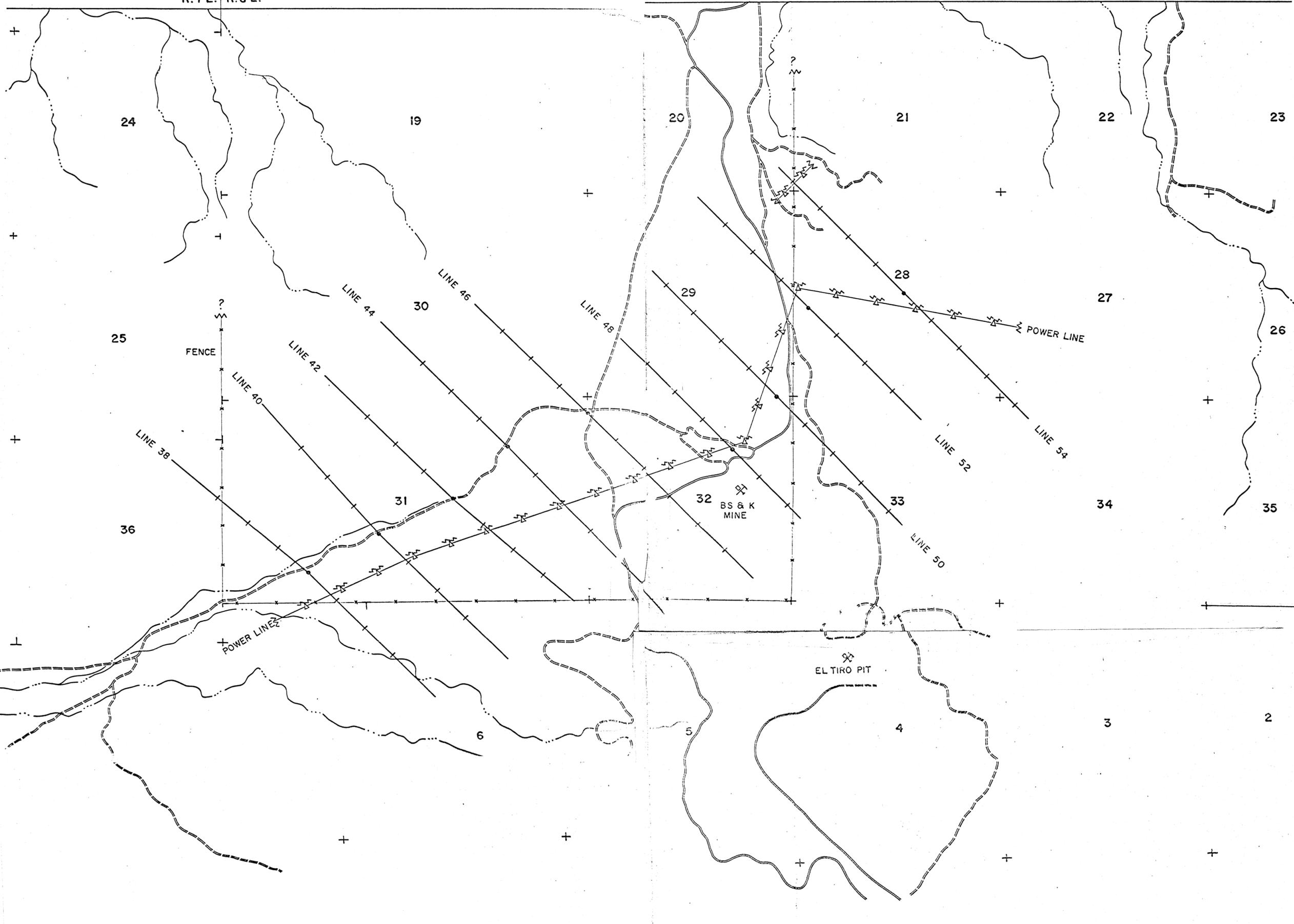


IP and RESISTIVITY SURVEY
 RESISTIVITY CONTOUR PLAN
 B S & K PROJECT
 SILVER BELL DISTRICT - PIMA COUNTY, ARIZONA
 for
 THE HANNA MINING COMPANY
 by

SCALE 1 INCH = 500 FEET

500 0 500 1000 1500

Mineral Surveys
 CONSULTING ENGINEERS
 TULSA, OKLA. U.S.A.



I.P. and RESISTIVITY SURVEY
 PLAN MAP
 B S AND K PROJECT
 SILVER BELL DISTRICT - PIMA COUNTY, ARIZONA
 for
 THE HANNA MINING COMPANY
 by

CANADIAN AERO
Mineral Surveys LTD.
 OTTAWA, ONT., CANADA
 TUCSON, ARIZONA, U.S.A.



INCH = 2000 FEET
 2000 4000

Samples collected from BS&K
Hole 302

| | | |
|---------|-------|--------|
| 95-100 | 0.71% | 88 PPM |
| 100-105 | 0.70% | 83 |
| 105-110 | 0.76 | 65 |
| 110-115 | 0.95 | 169 |
| 115-120 | 0.67 | 70 |
| 120-125 | 0.40 | 41 |
| 125-130 | 0.50 | 105 |
| 130-135 | 0.28 | 149 |

Hole 300

| | | | | | |
|---------|------|--------|-----------|------|-----|
| 1AK-300 | 0.38 | 117 | 170'-175' | Ca | mo |
| 2AK-300 | 0.78 | 0.035% | 175-182 | 0.62 | .01 |

| BS&K | Hole 302 | Our Samples | BS&K |
|--------|----------|-------------|------|
| (.001) | 95 | .71 | .66 |
| (.005) | 100 | .70 | .61 |
| (.013) | 105 | .76 | .44 |
| (.006) | 110 | .95 | .57 |
| (.004) | 115 | .67 | .54 |
| (.005) | 120 | .40 | .32 |
| (.009) | 125 | .50 | .43 |
| (.009) | 130 | .28 | .40 |
| (.009) | 135 | | |

BS&K
40

BS&K
Ca

ASSAY—GEOLOGY COMPOSITE LOG

Sheet of

| | | | |
|---------|------------|--------------|-----|
| BEARING | Coord. : N | HOLE N° | 300 |
| INCL. | E | COLLAR ELEV. | |
| | | DEPTH | |

| DESCRIPTION | Geo | Asy | INT. | C.R. | % Cu | % As Cu | % Mo | % As Mo | % EQIV | | | GROUPING—RMKS. |
|---|-----|-----|------|------|------|---------|------|---------|--------|--|--|----------------|
| | | | | | | | | | | | | |
| 0-92 (could not find boxes of this?) | | | | | | | | | | | | |
| Pink qtz - greenish diabase por w/ thin sand very fine filled w/ brn limonite (from soil). All. w/ to strong very fine beds some scale to quartz. Thin sandstone. Siltstone are common. upward between some pale green stains pass from 2000s. The core is broken in many places (good core remains) | | | | | | | | | | | | |
| 92-100 (missing) | | | | | | | | | | | | |
| 100-110 (missing) | | | | | | | | | | | | |
| 110-120 (missing) | | | | | | | | | | | | |
| 120-130 (missing) | | | | | | | | | | | | |
| 130-140 (missing) | | | | | | | | | | | | |
| 140-150 (missing) | | | | | | | | | | | | |
| 150-160 (missing) | | | | | | | | | | | | |
| 160-170 (missing) | | | | | | | | | | | | |
| 170-180 (missing) | | | | | | | | | | | | |
| 180-190 (missing) | | | | | | | | | | | | |
| 190-200 (missing) | | | | | | | | | | | | |
| 200-210 (missing) | | | | | | | | | | | | |
| 210-220 (missing) | | | | | | | | | | | | |
| 220-230 (missing) | | | | | | | | | | | | |
| 230-240 (missing) | | | | | | | | | | | | |
| 240-250 (missing) | | | | | | | | | | | | |
| 250-260 (missing) | | | | | | | | | | | | |
| 260-270 (missing) | | | | | | | | | | | | |
| 270-280 (missing) | | | | | | | | | | | | |
| 280-290 (missing) | | | | | | | | | | | | |
| 290-300 (missing) | | | | | | | | | | | | |
| 300-310 (missing) | | | | | | | | | | | | |
| 310-320 (missing) | | | | | | | | | | | | |
| 320-330 (missing) | | | | | | | | | | | | |
| 330-340 (missing) | | | | | | | | | | | | |
| 340-350 (missing) | | | | | | | | | | | | |
| 350-360 (missing) | | | | | | | | | | | | |
| 360-370 (missing) | | | | | | | | | | | | |
| 370-380 (missing) | | | | | | | | | | | | |
| 380-390 (missing) | | | | | | | | | | | | |
| 390-400 (missing) | | | | | | | | | | | | |
| 400-410 (missing) | | | | | | | | | | | | |
| 410-420 (missing) | | | | | | | | | | | | |
| 420-430 (missing) | | | | | | | | | | | | |
| 430-440 (missing) | | | | | | | | | | | | |
| 440-450 (missing) | | | | | | | | | | | | |
| 450-460 (missing) | | | | | | | | | | | | |
| 460-470 (missing) | | | | | | | | | | | | |
| 470-480 (missing) | | | | | | | | | | | | |
| 480-490 (missing) | | | | | | | | | | | | |
| 490-500 (missing) | | | | | | | | | | | | |
| 500-510 (missing) | | | | | | | | | | | | |
| 510-520 (missing) | | | | | | | | | | | | |
| 520-530 (missing) | | | | | | | | | | | | |
| 530-540 (missing) | | | | | | | | | | | | |
| 540-550 (missing) | | | | | | | | | | | | |
| 550-560 (missing) | | | | | | | | | | | | |
| 560-570 (missing) | | | | | | | | | | | | |
| 570-580 (missing) | | | | | | | | | | | | |
| 580-590 (missing) | | | | | | | | | | | | |
| 590-600 (missing) | | | | | | | | | | | | |
| 600-610 (missing) | | | | | | | | | | | | |
| 610-620 (missing) | | | | | | | | | | | | |
| 620-630 (missing) | | | | | | | | | | | | |
| 630-640 (missing) | | | | | | | | | | | | |
| 640-650 (missing) | | | | | | | | | | | | |
| 650-660 (missing) | | | | | | | | | | | | |
| 660-670 (missing) | | | | | | | | | | | | |
| 670-680 (missing) | | | | | | | | | | | | |
| 680-690 (missing) | | | | | | | | | | | | |
| 690-700 (missing) | | | | | | | | | | | | |
| 700-710 (missing) | | | | | | | | | | | | |
| 710-720 (missing) | | | | | | | | | | | | |
| 720-730 (missing) | | | | | | | | | | | | |
| 730-740 (missing) | | | | | | | | | | | | |
| 740-750 (missing) | | | | | | | | | | | | |
| 750-760 (missing) | | | | | | | | | | | | |
| 760-770 (missing) | | | | | | | | | | | | |
| 770-780 (missing) | | | | | | | | | | | | |
| 780-790 (missing) | | | | | | | | | | | | |
| 790-800 (missing) | | | | | | | | | | | | |
| 800-810 (missing) | | | | | | | | | | | | |
| 810-820 (missing) | | | | | | | | | | | | |
| 820-830 (missing) | | | | | | | | | | | | |
| 830-840 (missing) | | | | | | | | | | | | |
| 840-850 (missing) | | | | | | | | | | | | |
| 850-860 (missing) | | | | | | | | | | | | |
| 860-870 (missing) | | | | | | | | | | | | |
| 870-880 (missing) | | | | | | | | | | | | |
| 880-890 (missing) | | | | | | | | | | | | |
| 890-900 (missing) | | | | | | | | | | | | |
| 900-910 (missing) | | | | | | | | | | | | |
| 910-920 (missing) | | | | | | | | | | | | |
| 920-930 (missing) | | | | | | | | | | | | |
| 930-940 (missing) | | | | | | | | | | | | |
| 940-950 (missing) | | | | | | | | | | | | |
| 950-960 (missing) | | | | | | | | | | | | |
| 960-970 (missing) | | | | | | | | | | | | |
| 970-980 (missing) | | | | | | | | | | | | |
| 980-990 (missing) | | | | | | | | | | | | |
| 990-1000 (missing) | | | | | | | | | | | | |
| 1000-1010 (missing) | | | | | | | | | | | | |
| 1010-1020 (missing) | | | | | | | | | | | | |
| 1020-1030 (missing) | | | | | | | | | | | | |
| 1030-1040 (missing) | | | | | | | | | | | | |
| 1040-1050 (missing) | | | | | | | | | | | | |
| 1050-1060 (missing) | | | | | | | | | | | | |
| 1060-1070 (missing) | | | | | | | | | | | | |
| 1070-1080 (missing) | | | | | | | | | | | | |
| 1080-1090 (missing) | | | | | | | | | | | | |
| 1090-1100 (missing) | | | | | | | | | | | | |
| 1100-1110 (missing) | | | | | | | | | | | | |
| 1110-1120 (missing) | | | | | | | | | | | | |
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| 1160-1170 (missing) | | | | | | | | | | | | |
| 1170-1180 (missing) | | | | | | | | | | | | |
| 1180-1190 (missing) | | | | | | | | | | | | |
| 1190-1200 (missing) | | | | | | | | | | | | |
| 1200-1210 (missing) | | | | | | | | | | | | |
| 1210-1220 (missing) | | | | | | | | | | | | |
| 1220-1230 (missing) | | | | | | | | | | | | |
| 1230-1240 (missing) | | | | | | | | | | | | |
| 1240-1250 (missing) | | | | | | | | | | | | |
| 1250-1260 (missing) | | | | | | | | | | | | |
| 1260-1270 (missing) | | | | | | | | | | | | |
| 1270-1280 (missing) | | | | | | | | | | | | |
| 1280-1290 (missing) | | | | | | | | | | | | |
| 1290-1300 (missing) | | | | | | | | | | | | |
| 1300-1310 (missing) | | | | | | | | | | | | |
| 1310-1320 (missing) | | | | | | | | | | | | |
| 1320-1330 (missing) | | | | | | | | | | | | |
| 1330-1340 (missing) | | | | | | | | | | | | |
| 1340-1350 (missing) | | | | | | | | | | | | |
| 1350-1360 (missing) | | | | | | | | | | | | |
| 1360-1370 (missing) | | | | | | | | | | | | |
| 1370-1380 (missing) | | | | | | | | | | | | |
| 1380-1390 (missing) | | | | | | | | | | | | |
| 1390-1400 (missing) | | | | | | | | | | | | |
| 1400-1410 (missing) | | | | | | | | | | | | |
| 1410-1420 (missing) | | | | | | | | | | | | |
| 1420-1430 (missing) | | | | | | | | | | | | |
| 1430-1440 (missing) | | | | | | | | | | | | |
| 1440-1450 (missing) | | | | | | | | | | | | |
| 1450-1460 (missing) | | | | | | | | | | | | |
| 1460-1470 (missing) | | | | | | | | | | | | |
| 1470-1480 (missing) | | | | | | | | | | | | |
| 1480-1490 (missing) | | | | | | | | | | | | |
| 1490-1500 (missing) | | | | | | | | | | | | |
| 1500-1510 (missing) | | | | | | | | | | | | |

ASSAY-GEOLOGY COMPOSITE DRILL LOG

PROJECT Atlas Mine, Drill Hole for Nevada Claim

| | | |
|---------------|----------------|--------------|
| Coörd. : N | BEARING Vert | HOLE N° 305 |
| E | INCL. Vert | COLLAR ELEV. |
| START 8-19-65 | COMPL. 8-20-65 | DEPTH 109 |

| DESCRIPTION | Geol. | Assay | INT. | C/R | % Cu | % Mo | % | % | oz. | oz. % | EQUV. | GROUPING — RMKS. |
|--|-------|-------|------|-----|------|------|---|---|-----|-------|-------|------------------|
| <u>0-15 Dacite Porphyry.</u> Brown. Oxide zone, soft, Porphyritic, fine grained. Original sulfide content was 4%. Strong Arg. Alt.; tr ser. | | | | | | | | | | | | |
| | 0 | | | | | | | | | | | |
| | 10 | 40 | | | .02 | .021 | | | | | | |
| | 10 | 20 | 70 | | .02 | .017 | | | | | | |
| <u>15-25 Quartz Monzonite</u> Brown, oxide zone, soft Holocrystalline, Est. 2% Original sulfide. Wk Arg. Alteration. | | | | | | | | | | | | |
| | 20 | 25 | 80 | | .04 | .009 | | | | | | |
| | 25 | 30 | 90 | | .09 | .001 | | | | | | |
| | 30 | 40 | 78 | | .28 | .001 | | | | | | |
| <u>25-60 Quartz Monzonite</u> Gray. Supergene zone Holocrystalline. Est 2% Sulfide. Chalcocite occurs on fractures. Weak Arg. Alt. No sericite. | | | | | | | | | | | | |
| | 40 | 50 | 85 | | .29 | .009 | | | | | | |
| | 50 | 60 | 90 | | .16 | .005 | | | | | | |
| | 60 | 70 | 90 | | .13 | .015 | | | | | | |
| <u>60-109 Quartz Monzonite</u> Gray as above. Hypogene zone. Est 2% sulfide, in fractures. Trace of chalcopyrite. | | | | | | | | | | | | |
| | 70 | 80 | 90 | | .11 | .003 | | | | | | |
| | 80 | 90 | 90 | | .12 | .003 | | | | | | |
| | 90 | 100 | 90 | | .07 | .007 | | | | | | |
| | 100 | 109 | 95 | | .001 | | | | | | | |

Average from
 30 to 50 is
 .28% Cu,
 .005 Mo.

ASSAY-GEOLOGY COMPOSITE DRILL LOG

PROJECT Atlas Mine, BS&K Mining Co., Hole for BS&K No. 1

| | | |
|---------------|------------------|--------------|
| Coörd. : N | BEARING Vertical | HOLE N° 306 |
| E | INCL. Vertical | COLLAR ELEV. |
| START 8-21-65 | COMPL. 8-22-65 | DEPTH 100 |

| DESCRIPTION | Elev. | Dip | INT. | C/R | % Cu | % Mo | % | % | oz' | oz' | % EQUV. | GROUPING - RMKS. |
|--|-------|-----|------|-----|------|------|---|---|-----|-----|---------|------------------|
| | | | | | | | | | | | | |
| <u>0-30 Dacite Porphyry</u> Brown, fine grained, soft. Original sulfide now entirely oxidized. Original sulfide was 3% of rock. It occurred entirely in fractures. Arg AH., No Sericite | 0 | | | | | | | | | | | |
| | 10 | 30 | | | .04 | .007 | | | | | | |
| | 10 | | | | | | | | | | | |
| | 20 | 45 | | | .05 | .004 | | | | | | |
| | 20 | | | | | | | | | | | |
| | 30 | 55 | | | .10 | .070 | | | | | | |
| <u>30-50 Dacite Porphyry</u> Mixed Oxide and sulfide zone Fe Ox and Pyrite, with traces of chalcocite. Rock as above. | 30 | | | | | | | | | | | |
| | 40 | 75 | | | .20 | .030 | | | | | | |
| | 40 | | | | | | | | | | | |
| | 50 | 90 | | | .34 | .009 | | | | | | |
| | 50 | | | | | | | | | | | |
| | 60 | 90 | | | .38 | .009 | | | | | | |
| <u>50-60 Dacite Porphyry</u> Supergene zone Chalcoite coatings on pyrite. Rock as above. | 60 | | | | | | | | | | | |
| | 70 | 85 | | | .23 | .011 | | | | | | |
| | 70 | | | | | | | | | | | |
| | 80 | 90 | | | .21 | .016 | | | | | | |
| <u>60-100 Dacite Porphyry</u> Hypogene zone. No chalcocite. Rock as above. | 80 | | | | | | | | | | | |
| | 90 | 90 | | | .16 | .002 | | | | | | |
| | 90 | | | | | | | | | | | |
| | 100 | 85 | | | .10 | .006 | | | | | | |

Average from 0'-30'
.06 Cu,
.027 Mo

Average from 30' to 70' is
.29% Cu,
.015 Mo.

ASSAY-GEOLOGY COMPOSITE DRILL LOG

PROJECT _____

| | | |
|------------|---------|--------------|
| Coord. : N | BEARING | HOLE NO. 200 |
| E | INCL. | COLLAR ELEV. |
| START | COMPL. | DEPTH |

| DESCRIPTION | COR. | ASSAY | INT. | C/R | % Cu | % Mo | % | % | OZ. | OZ. | % EQUV. | GROUPING - RMKS. |
|---|-------------------------------|-------|------|-----|------|---------------------------------|------|------|-----|-----|---------|---|
| | | | | | | | | | | | | |
| <p>125-170 Dacite Porphyry</p> <p>Hypogene zone, Gray, soft, porphyritic. Copper occurs in seams and veinlets as crushed chalcopryite, with pyrite. Numerous qtz veinlets. Much pyrite in seams is crushed and black. Total sulfide is 47%. Sulfide is 90% in seams, 10% in diss. We see on seams.</p> | 125 | | | | | | | | | | | <p>Average Hypogene grade is .18 Cu .015 Mo</p> |
| | 125 | | | | 82 | .18 | .015 | | | | | |
| | 130 | | | | 80 | .14 | .028 | | | | | |
| | 135 | | | | 80 | .12 ² / ₃ | .011 | | | | | |
| | 140 | | | | 76 | .11 | .01 | | | | | |
| | 145 | | | | 70 | .11 | .010 | | | | | |
| | 150 | | | | 75 | .12 | .015 | | | | | |
| | 155 | | | | 80 | .16 ² / ₃ | .015 | | | | | |
| | 160 | | | | 85 | .12 | .008 | | | | | |
| | 170-182 Dacite Porphyry, Gray | 165 | | | | 70 | .15 | .031 | | | | |
| <p>Hypogene zone soft, fine gr. porphyritic. Copper occurs as chalcopryite with pyrite. Total sulfide is 37%. Sulfide is 80% in seams and gangues and 20% as diss. Much qtz veinlets. Pyrite is frequently crushed. We see on seams, with Molybdenite visible in quartz veinlets. Largest veinlet is 2" qtz-pyrite - chalcopryite at 177'. This veinlet also has trace of chalcocite.</p> | 170 | | | | 75 | .30 | .011 | | | | | |
| | 175 | | | | 75 | .16 ² / ₃ | .017 | | | | | |
| | 180 | | | | | | | | | | | |
| | 182 | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |

ASSAY-GEOLOGY COMPOSITE DRILL LOG

PROJECT Atlas Mine, BS&K Mining Co., BS&K No 3 Claim

| | | |
|--|----------------------|-----------------------|
| Coörd. : N | BEARING <u>Vert</u> | HOLE NO: <u>300</u> |
| E | INCL. <u>Vert</u> | COLLAR ELEV. |
| START <u>8-6-65</u> COMPL. <u>8-8-65</u> | <u>No. core size</u> | DEPTH <u>187 feet</u> |

| DESCRIPTION | Geol. | Assay | INT. | C/R | % Cu | % Mo | % | % | oz. | oz. | % | EQUV. | GROUPING—RMKS. |
|---|-------|------------------|------------------|------|------|------|---|---|-----|-----|---|-------|---|
| | | | | | | | | | | | | | |
| 0-90 Dacite Porphyry, Brown fine grained, soft, porphyritic, highly fractured, numerous qtz veinlets, Arg. Alteration, Original Sulfide was ± 3%, entirely in fractures. Core very badly broken. No green or blue copper minerals visible, though entire section is oxide. | 0 | | | | | | | | | | | | |
| | 10 | 56 | .08 | .002 | | | | | | | | | |
| | 10 | | | | | | | | | | | | |
| | 20 | 70 | .05 ⁷ | .002 | | | | | | | | | |
| | 20 | | | | | | | | | | | | |
| | 30 | 68 | .09 | .002 | | | | | | | | | |
| | 30 | | | | | | | | | | | | |
| | 40 | 76 | .14 ⁷ | .001 | | | | | | | | | |
| | 40 | | | | | | | | | | | | |
| | 50 | 86 | .14 | .005 | | | | | | | | | |
| 50 | | | | | | | | | | | | | |
| 50 | 90 | .16 ⁷ | .004 | | | | | | | | | | |
| 60 | | | | | | | | | | | | | |
| 60 | 78 | .15 | .009 | | | | | | | | | | |
| 70 | | | | | | | | | | | | | |
| 70 | 85 | .16 ⁷ | .006 | | | | | | | | | | |
| 80 | | | | | | | | | | | | | |
| 80 | 87 | .17 | .009 | | | | | | | | | | |
| 90-95 Dacite Porphyry, Gray Mixed oxide and sulfide. Soft, porphyritic, strong arg. Alt., numerous qtz veinlets. Copper occurs as oxide and chalcocite. | 90 | | | | | | | | | | | | |
| 90 | 90 | .94 | .025 | | | | | | | | | | oxide Mixed |
| 95 | | | | | | | | | | | | | |
| 95 | 86 | .79 ² | .015 | | | | | | | | | | Supergene Sulfide |
| 100 | | | | | | | | | | | | | |
| 100 | 83 | .51 | .010 | | | | | | | | | | |
| 105 | | | | | | | | | | | | | |
| 105 | 80 | .60 | .009 | | | | | | | | | | Average grade of Mixed and supergene is 35 feet |
| 110 | | | | | | | | | | | | | |
| 110 | 87 | .24 | .005 | | | | | | | | | | |
| 115 | | | | | | | | | | | | | |
| 115 | 80 | .12 ² | .011 | | | | | | | | | | .47 Cu .013 Mo |
| 120 | | | | | | | | | | | | | |
| 120 | 82 | .11 | .013 | | | | | | | | | | |

Average
oxide
is
.13 Cu
.005 Mo
for
90 feet

oxide
Mixed
Supergene
Sulfide
Average grade of
Mixed and supergene
is 35 feet
.47 Cu
.013 Mo

ASSAY-GEOLOGY COMPOSITE DRILL LOG

PROJECT Atlas Mine

| | | |
|------------|---------|--------------|
| Coörd. : N | BEARING | HOLE N° 300 |
| E | INCL. | COLLAR ELEV. |
| START | COMPL. | DEPTH 206 |

| DESCRIPTION | Geol. | Assay | INT. | C/R | % Cu | % Mo | % | % | oz. | oz. | % | EQUIV. | GROUPING — RMKS. | |
|--|-------|-------|------|-------------------------------------|-----------------------------------|------|---|---|-----|-----|---|--------|------------------|--|
| 125-206 Dacite Porphyry Supergene zone as above | | | | | | | | | | | | | | |
| | | | | | 1.21 | .006 | | | | | | | 125'-150' | |
| | | | | | | | | | | | | | .74 | |
| | | | | | .70 | .008 | | | | | | | .009 Mo | |
| | | | | | .65 | .009 | | | | | | | | |
| | | | | | .39 | .015 | | | | | | | | |
| | | | | | .76 | .009 | | | | | | | | |
| | | | | | .47 | .013 | | | | | | | | |
| | | | | | .38 | .043 | | | | | | | | |
| | | | | | .36 | .024 | | | | | | | | |
| | | | | | .51 | .040 | | | | | | | | |
| | | | | | .72 | .014 | | | | | | | | |
| | | | | | .50 | .010 | | | | | | | | |
| | | | | | .57 | .052 | | | | | | | | |
| | | | | | .88 | .011 | | | | | | | | |
| | | | | | 1.12 | .013 | | | | | | | | |
| | | | | | .40 | .004 | | | | | | | | |
| | | | | | .19 | .006 | | | | | | | | |
| | | | | | End of hole | | | | | | | | | |
| | | | | | Average Mo for Hole is 0.0158 Mo. | | | | | | | | | |
| | | | | Average from 105 to 200' is .72% Cu | | | | | | | | | | |
| | | | | | | | | | | | | | .018 Mo | |

DUVAL CORPORATION
 COPPER DIVISION — ESPERANZA PROPERTY
 SAHUARITA, ARIZONA

CERTIFICATE OF ASSAY

August 13, 1965

BS&K Drills

| BEAKER NOS. | MARKS, ETC. | SAMPLE | % Total | % Mo | | | | |
|-------------|-------------|--------|---------|------|--|-----------|--|--|
| | | GMS. | Cu | | | | | |
| | # 301-0-10' | | .12 | .006 | | | | |
| | 20' | | .20 | .012 | | | | |
| | 30' | | .17 | .010 | | | | |
| | 40' | | .18 | .009 | | | | |
| | 50' | | .16 | .014 | | | | |
| | 60' | | .11 | .016 | | | | |
| | 70' | | .12 | .016 | | | | |
| | 80' | | .13 | .017 | | | | |
| | 90' | | .24 | .010 | | | | |
| | 100' | | .10 | .009 | | | | |
| | 105' | | .15 | .013 | | | | |
| | 110' | | 1.31 | .040 | | | | |
| | 115' | | 1.74 | .019 | | | | |
| | 120' | | .49 | .008 | | | | |
| | 125' | | .45 | .013 | | | | |
| | 130' | | 1.21 | .006 | | | | |
| | 135' | | .70 | .008 | | .72 % Cu, | | |
| | 140' | | .65 | .009 | | .018 Mo | | |
| | 145' | | .39 | .015 | | | | |
| | 150' | | .76 | .009 | | | | |
| | 155' | | .47 | .013 | | | | |
| | 160' | | .38 | .043 | | | | |
| | 165' | | .36 | .024 | | | | |
| | 170' | | .51 | .040 | | | | |
| | 175' | | .72 | .014 | | | | |
| | 180' | | .50 | .010 | | | | |
| | 185' | | .57 | .052 | | | | |
| | 190' | | .88 | .011 | | | | |
| | 195' | | 1.12 | .013 | | | | |
| | 200' | | .40 | .004 | | | | |
| | 206' | | .19 | .006 | | | | |

AEB

W. J. RICHMOND
AMIL J. AJAMIE
RICHARD E. FAY
ALAN L. HAMMOND

HAL Miller
of General Electric

LAW OFFICES

264-2786

RICHMOND, AJAMIE & FAY

SUITE 705 UNITED BANK BUILDING
3550 NORTH CENTRAL AVENUE
PHOENIX, ARIZONA 85012

*Proved reserves
28,000,000 - 40,000,000
A8802
Abe's ground
as of 5-12-71*

February 5, 1970

**Mr. Jerome M. Willis
Director of Natural Resources Division
Essex International, Inc.
5315 E. Broadway - 104
Tucson, Arizona 85711**

Re: B. S. & K. Mining Company

Dear Mr. Willis:

I have been commissioned by Mr. Abe M. Kalaf, President of B. S. & K., to articulate his thinking.

First, it must be made clear that he does not intend for this letter to be considered an agreement; nor should anyone rely upon it, except to the extent that it is merely indicative of his present thinking. B. S. & K. Mining Company is not committed to anyone; and, until a formal, written agreement is fully executed, my client is free to negotiate and contract with anyone it chooses.

C
O
P
Y

100,000

1. B. S. & K. is to be paid an initial payment of \$200,000.00 upon signing of a formal agreement; thereafter, it is to be paid \$300,000.00 in monthly installments of \$8,333.33 for 36 months, or less, as hereinafter appears.

REVISIO

2. Within said 36 months, a copper processing plant must be placed on the premises and in operation. It must be capable of producing 30,000 pounds of electrolytically refined copper, or its equivalent, per day; and it must be operating on 300 business day year.

RETAIN

3. If the plant is not in and operating per paragraph 2, the \$500,000.00 is forfeited, as

Mr. Jerome M. Willis
Page 2
February 5, 1970

liquidated damages; and the developer forfeits any and all interest in and to the B. S. & K. property.

\$250,000

4. Once the plant is in and operating per paragraph 2, the monthly installments of \$8,333.33 are to cease; and the unpaid balance of the \$300,000.00 is not to be paid. Thereafter, however, the following conditions shall obtain: The developer gets a 51% interest in the B. S. & K. property, B. S. & K. retaining 49%; and all profits from the operation of the property and any other property within one mile of its boundaries, adjusted per paragraph 6, infra, are to be divided between the developer and B. S. & K. in the same ratios.

RETAIN
SUBJECT TO
NEGOTIATION

5. The developer must finance the entire operation and any future expansion, and "no lien" notices are to be conspicuously posted per law.

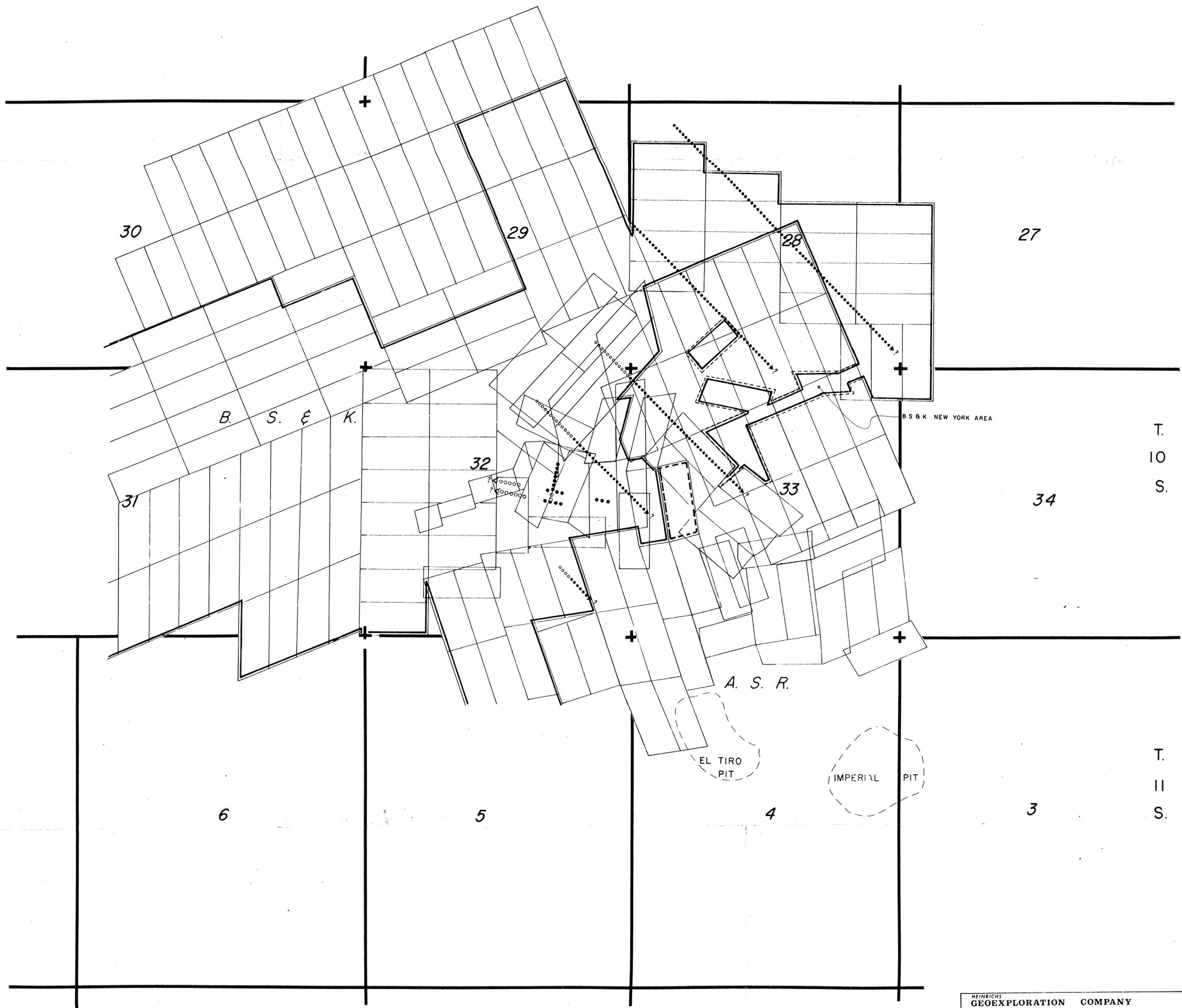
REVISED

6. That portion of the \$500,000.00, called for in paragraphs 1 and 2, supra, which has been paid to B. S. & K. and the capital invested in putting in the copper refining plant and in putting it into operation is to be recovered by the developer from profits, amortized on a monthly basis over the estimated life of the operation on a ratio satisfactory to the Internal Revenue Service of the United States of America. B. S. & K. Mining Company shall be entitled to an equity accumulation in said capital investment in direct proportion to its share of the amounts amortized and as those amounts are charged off.

Respectfully,

Anil J. Ajanie

AJA:ah

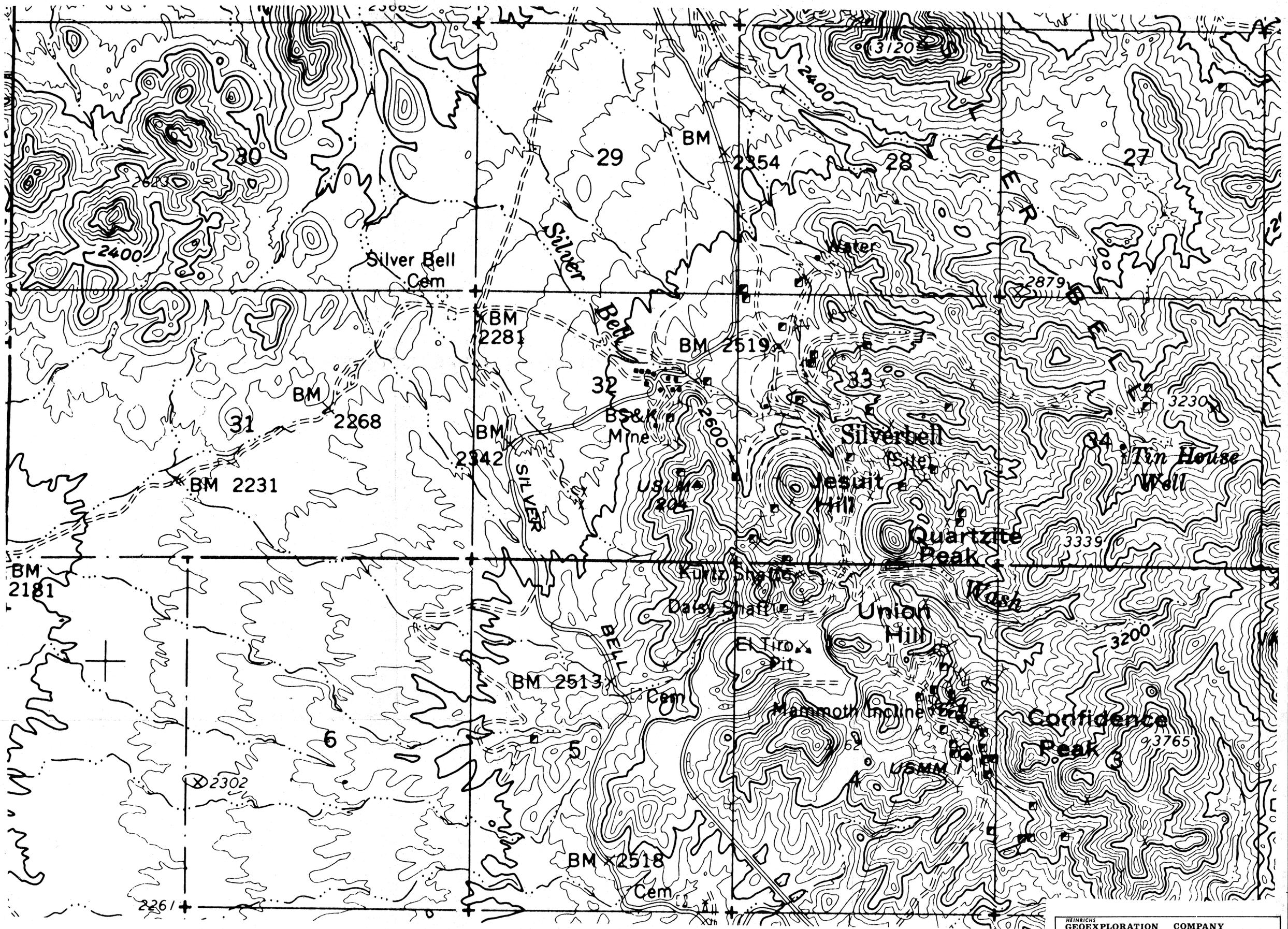


WEAK STRONG
 I.P. ANOMALISM (GEOEX, CANADIAN AERO & MCPHAR)

R. 8 E.

————— B. S. & K. BOUNDARY

| | |
|--|--|
| HEINRICHS GEOEXPLORATION COMPANY <small>POST OFFICE BOX 5071, TUCSON, ARIZONA 85703</small> <small>Phone: 602/623-0578 Cable: GEOEX, Tucson</small> <small>vancouver sydney</small> | |
| B. S. & K. MINING CO. ATLAS MINE & VICINITY PIMA COUNTY, ARIZONA OWNERSHIP | |
| FOR ESSEX INTERNATIONAL INC. | |
| <small>SCALE 1" = 1000' DRAWN BY EGH & JCO DATE MARCH 1970</small> | |



R. 8 E.

HEINRICHS
GEOEXPLORATION COMPANY
 POST OFFICE BOX 5671, TUCSON, ARIZONA, 85703
 Phone: 602/623-0578 Cable: GEOEX, Tucson
 geophysical engineers vancouver sydney 511-70

TOPOGRAPHIC MAP
B. S. & K. MINING CO. AREA
PIMA COUNTY, ARIZONA

FOR
ESSEX INTERNATIONAL INC.

SCALE: 1" = 1000' DRAWN BY: EGN-JD DATE: MAR 1970