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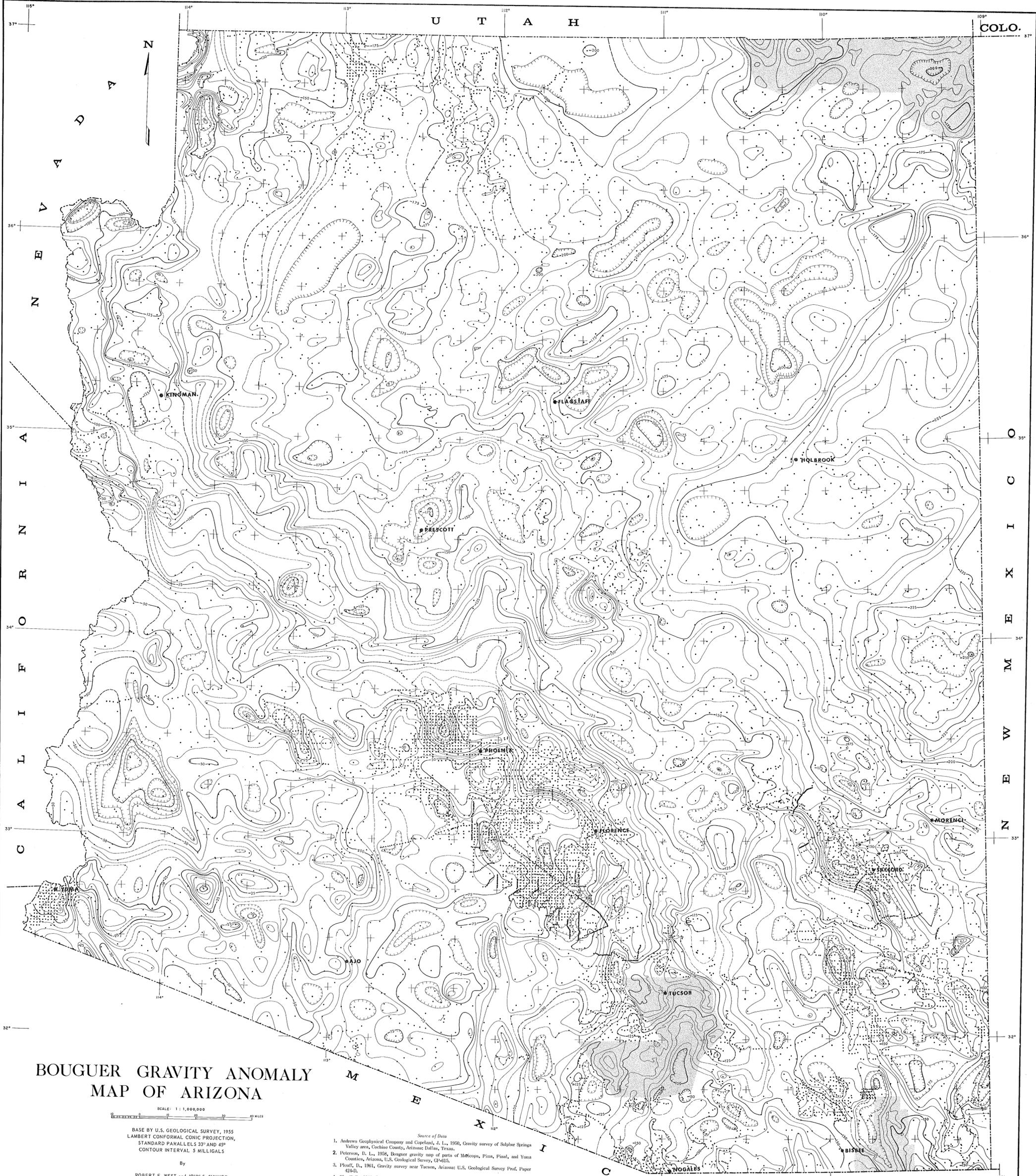
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# BOUGUER GRAVITY ANOMALY MAP OF ARIZONA

SCALE: 1 : 1,000,000  
0 10 20 30 40 50 MILES

BASE BY U.S. GEOLOGICAL SURVEY, 1955  
LAMBERT CONFORMAL CONIC PROJECTION,  
STANDARD PARALLELS 33° AND 45°  
CONTOUR INTERVAL 5 MILLIGALS

By  
ROBERT E. WEST and JOHN S. SUMNER  
1973

Revision of "Regional Bouguer Gravity Anomaly Map of Arizona," 1972

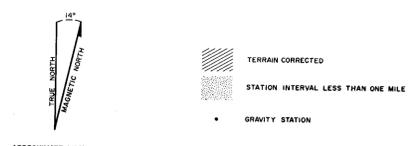
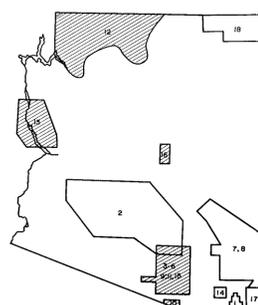
Gravity data were obtained from surveys by the Laboratory of Geophysics of The University of Arizona, U.S. Defense Mapping Agency, U.S. Geological Survey, Exxon Corporation, and mining companies and contractors. The index map gives the primary sources of data for particular areas. A density of 2.67 gm/cm<sup>3</sup> was used for the Bouguer corrections. Terrain corrections are not included except where they were calculated by the original source of the data; these areas are indicated on the index map. The station interval ranges from approximately one to five miles; a stippled pattern indicates where the station interval is less than one mile. Elsewhere the contours are dashed. In the Grand Canyon area and the Santa Catalina and Pinaleno Mountains, Bouguer anomaly values with large terrain effects were not used in contouring.

University of Arizona personnel who participated in regional gravity surveys to obtain data for this map include, in addition to the authors, Jerry Golden, William Johnson, Stephen Hench, Clifford Dewey, Robert Staley, Brian Hogan, Gene Rietz, Jonathan Earl, Carlos Aiken, James Schmidt, and Gary Young. Other University of Arizona gravity data used in this map are from M.S. and Ph.D. theses and dissertations, as noted on the index map.

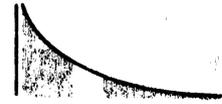
U.S. Geological Survey data used in this map are from the surveys also noted on the index map. U.S. Defense Mapping Agency gravity survey field crews were directed by R. Iverson, P. B. Benuff, and C. H. Marcan.

Financial assistance for production of this map was provided by the National Science Foundation, AMAX Exploration Company, Exxon Corporation, The University of Arizona, the Arizona Water Resources Research Center, the U.S. Defense Mapping Agency, the State of Arizona Oil and Gas Conservation Commission, and the Four Corners Regional Commission.

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mining  
geophysical surveys



2400 EAST GRANT ROAD - TUCSON, ARIZONA 85719

TELEPHONE - 602 326-8619

September 12, 1972

Mr. E. Grover Heinrichs  
Essex International, Inc.  
1704 West Grant Road  
Tucson, Arizona 85705

Project 0237

Dear Grover;

Rock and core samples from your Safford Project were lab tested for magnetic susceptibility and IP response. The results are as follows:

<u>SAMPLE</u>	<u>MAGNETIC SUSCEPTIBILITY</u> in $10^{-6}$ cgs units	<u>IP RESPONSE</u> (time domain) in millivolt seconds per volt
Basalt 1	0	-
2	720	- not required
3	2010	-
Core A-1	0	12.2
2	0	12.2
3	60	0.7
4	910	3.5
5	880	9.2
6	2120	21.4
7	2200	141.0
8	2540	383.0
9	1820	6.5
10	0	1.2

} electrode effects  
not valid response

11	0	-6.6 fracture problem
12	1650	6.8 not valid response
13	1710	7.3
14	540	7.8
15	370	1.7
16	3210	11.4
17	0	3.6
18	220	1.3
19	0	0.5
20	0	2.4
21	2320	25.7
22	7880	16.6
23	6400	17.3
24	10400	50.7

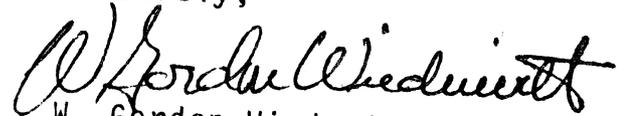
The magnetic susceptibility and induced polarization measurements were obtained by conventional laboratory techniques. Core samples were taken from the basalt surface specimens for the magnetic susceptibility tests, and where core samples were provided the specimen ends were cut to accommodate plate electrodes for the electrical measurements.

There are inherent limitations in extrapolating the data between surface and core specimens, and measurements obtained in the field. One obvious limitation is in the gross difference in the volume of rock tested in the laboratory and that sampled in the field. That difference alone is significant and merits a degree of caution in formulating interpretative ideas from lab data.

As noted certain specimens had characteristics that prevented a valid test of their electrical properties. Continuous veins of sulfides, or fractures from end to end in the specimen generally cause problems in the electrical measurements.

Let us know of any questions you may have.

Sincerely,

  
W. Gordon Wieduwilt

# CORE SAMPLES FOR I.P.

LONGKATE ES-1	833'	Box 10	A-1
"	1358'	" 69	A-2
"	1986'	" 140	A-3
"	2309'	" 176	A-4
ANDESITE	2493'	" 198	A-5
"	2689'	" 218	A-6
"	2902'	" 242	A-7
"	3129'	" 266	A-8
AGGLOMERATE ES-2	2079'	" 111	A-9
"	2120'	" 116	A-10
"	2179'	" 122	A-11
"	2242'	" 129	A-12
ANDESITE	2455'	" 152	A-13
"	2707'	" 180	A-14
"	2912'	" 202	A-15
"	3096'	" 220	A-16
AGGLOMERATE ES-3	2152'	" 1	A-17
"	2234'	" 9	A-18
"	2295'	" 16	A-19
"	2340'	" 21	A-20
ANDESITE	2509'	" 40	A-21
"	3058'	" 101	A-22
"	3522'	" 151	A-23
"	3989'	" 200	A-24

Sum + 392pg

SAFFORD

914 Industrial Ave.,  
Palo Alto, California  
94303  
April 17, 1972.

Mr. J. K. Jones,  
Essex International,  
1704 W. Grant Road,  
Tucson, Arizona, 85705

APR 19 1972  
RECEIVED  
D-11-11

Dear Ken,

Enclosed is a sketch of the magnetic map for the San Juan area. You will note that I have smoothed the data, and it now begins to resemble an aeromagnetic map. I have kept the original data, as well as a copy of this map; I would like to try applying some of the high powered interpretation techniques that we use here. There isn't a great deal that can be gotten out of this limited area, but I think the map, along with the one over the Winkler - Faulkner ground, does illustrate what could be accomplished on a district scale.

While applying only a qualitative interpretation, the main Butte fault is quite clear. The basalts to the south - west are easily identified. The two areas of different background in the north - east, and east central portions probably represent two types of volcanics.

The magnetic highs which surround the nonmagnetic intrusive area, - the San Juan intrusive, should be checked on the ground. The magnetic gap, or window coincides with a window in the pyrite halo, and it is quite possible that an alteration zone is being defined. I realize that there is an access problem, but the possibility of mapping an alteration trend through the destruction of magnetite is quite intriguing, and should be followed up.

In the past, the interpretation of magnetic maps has been limited by the immense amount of data processing involved. Geometrics has solved many of these problems, and offer interpretation services using their proprietary techniques. I'm sure that you would be impressed by what could be done at Safford, and I think it would be well worth your while to come out and have a look at what is being done elsewhere. The rocks at San Juan have such characteristic magnetic signatures, that I'm sure the magnetics could map various rock types, even at different levels. I know you're flat out every minute but it would be well worth it for you and Paul to see what can be done. It's much easier to show you, than to merely talk or write about the program. There is a clear application of the method to your program, and I would like to see you investigate it further.

Regards to you and Paul,

Dave

*Dave*

To: P. I. Eimon  
From: H. David Mac Lean

Subject: REview of Geophysical Data in Essex Files for the  
Safford Area, Graham County, Arizona.

March 28, 1972

General Remarks;

A quantity of geophysical data taken in the vicinity of the San Juan prospect, near Safford Arizona, has been made available to ESSEX INTERNATIONAL. A review of this data has been undertaken while visiting the property March thirteenth to sixteenth, for the purpose of assembling, organizing and reinterpreting the data, and to make recommendations as to how this and simaliar work could further contribute to the geological understanding of the area. The geophysical data available consists of ground magnetics and IP-RESistivity for two properties which adjoin the ground in which Essex has an interest. Unfortunately, this data was collected at different times for very restricted purposes and does not provide district wide information. However, it does provide and indication of the type of information which could be extracted from similar surveys elsewhere in the district.

The location of the properties for which information is available is shown in Fig. 1A, which is a compilation of two of the seven and one half minute quadrangles in the Safford Area ( see Fig. 1.) This figure also shows in rough outline the location of the San Juan and Winkler- Fauldkner properties for which geophysical information herein discussed is available. The property boundaries shown are diagramatic; no attempt has been made to outline the property with any degree of precision. The survey grids which are shown on the figure are also approximate. The grid locations have been scaled onto this figure from other sources, but no information was available by which grid stations could be tied to specific topographic features or reference points.

Any description of topographic or geological features, such matters as access, water supply and other factors not directly related to , or bearing on the geophysical matters, is beyond the scope of these notes. These topics are either self evident, well known, or adequately discussed elsewhere in the Essex files.

A very preliminary examination of the available geophysical data indicates that the material is of little use for purposes of direct exploration in the classic sense of an orebody possessing certain physical properties which will permit its detection by surface measurement of these properties. Rather, the exploration problem here is one of projecting geological conditions from known to covered areas. Nevertheless, certain geological features do lend themselves to detection and mapping by geophysical methods and it is possible that these, or similar surveys might provide a guide to an understanding

of the geology of the area, and thus indirectly to an understanding of potential ore locations.

#### Geophysical Data Examined.

Data available consisted of ground magnetic and VIPS on the Winkler - Faulkner and San Juan properties. The magnetic surveys are both vertical intensity variations, measured by an Askania ground magnetometer in the case of the W.-F. ground, and presumably by a hand held fluxgate magnetometer in the case of the San Juan survey. Accordingly, the accuracy of the latter survey would be somewhat less than that of the former, but such a consideration is more or less irrelevant, since no information is available in either case which describes the method of drift recognition and removal, or the tolerances of magnetic tie points. For the purposes of this discussion one can do nothing else but assume that all procedures were carried out in a professional manner by competent and qualified personnel.

The posted magnetic values show a high level of noise, which is probably due to the presence of magnetic boulders (of basalts). The magnetic data for the W. F. ground has been smoothed using a simple averaging technique; i.e. each point has been averaged with all neighbouring points within a radius of five hundred feet, with unit weight applied to each point. A description of the method used is not available, but this scheme appears to duplicate most of the smoothed data values. Similarly, the magnetic data from the San Juan property should be filtered either by this scheme or by a more advanced band pass filter operator before comparisons or interpretations are attempted. Magnetic data appears on Plates 1 & 1A.

The IP - Resistivity surveys in the two areas utilized quite different techniques. The survey on the W.-F. ground was run with conventional frequency domain gear, using the expanding Eltran array. All of this data is available in the Essex files (Heinrichs, 1970), and is presented on a line by line basis in pseudo-section format. The work on the San Juan property was run by the Anaconda company, using a variation of the three electrode array, with measurement of the IP effect made in terms of phase angles. The data is presented as a plan for two separate spacings, and is bound herewith as plates 2 & 2A (IP) and plates 2R & 2A(R) (Resistivity).

A few "rule of thumb" calculations will permit the conversion of data from one system to another:

$$\text{PFE} = \text{phase angle (minutes)} \cdot \frac{3.2}{60}$$

$$\text{Chargeability (milliseconds)} \approx \text{PFE} \cdot 5 \approx \text{phase angle} \cdot 4$$

Though a report is available for the IP work done on the W. F. ground, there is not any similar technical information

regarding the work which Anaconda did in the San Juan area . Again it must be assumed that in general the work was conducted in accordance with generally accepted procedures. Where discrepancies appear, they will be dealt with individually.

#### Discussion of Results.

##### IP- Resistivity. San Juan Area.

The strong IP response on Plates 2 sheets 1 & 2 is indicative of a strong mineralized zone. Reliable depths to the mineralization cannot be made since only two relatively wide spacings have been used for the measurements, but depth to source ( sulfide material) is probably less than 400 feet. The strong responses are suggestive of heavy pyrite mineralization of about five to fifteen percent. The zone of mineralization has been outlined on Plate 3, which is a general interpretation map, and on Fig. 1A. The pattern is indicative of a mineralized halo which surrounds a weakly mineralized core. Since this core represents the ore of the San Juan mine, detection of this halo may be a guide to the location of ore on the hanging wall of the Butte fault, - the mineralized or anomalous zone terminates against the fault, indicating that there may be a continuation to the south west. The gap in the mineralized halo may be significant in that it may reflect a mineralization trend which should be followed during the course of exploration.

The halo could be significant in the exploration of the Essex ground. The idealized section, presented in Fig. 2 shows that the ore zone which Phelps-Dodge is now developing could extend onto the Essex ground. The halo could be traced to a depth of fifteen hundred feet, and possibly deeper by IP methods. Whether or not the delineation of this halo would constitute a material contribution to the geological understanding of the area is a question for the project geologist to answer, and the nature of this answer would dictate whether or not the survey would be justified.

It is interesting to note that the mineralized halo probably does not extend as far as the W.- F. ground to the south. The IP pseudo- sections show no evidence of mineralization except at the extreme south end. In Fig. 3 the source of the IP anomaly has been interpreted as a buried layer, at a depth of about 1,500 feet. This interpretation is reasonable, in that the resistivity interpretation indicates about 1,000 feet to bedrock. The mineralized layer should be somewhat deeper, due to weathering.

The two solutions in the figure are consistent between 1,000 and 1,500 feet. More spacings with different electrode separations would be required to obtain a more accurate interpretation. The geological significance of sulfided at 1,000 feet at the south end of the W.-F. property, and their complete absence, or at least burial in excess of 1,500 or 2,000 feet is not immediately apparent, but is duly observed, and may have

relevance to the future development of geological thinking in the area.

Elsewhere on the W.-F. ground, the resistivity data would indicate that overburden is somewhat thinner. At Line 5 there is only about three hundred feet of gravel if it is assumed that the bedrock is the higher resistivity material, and the solution of the resistivity case in Line 3 would indicate about five hundred feet or so. Clearly, any mineralization would be much deeper, since there does not appear to have been a problem in getting current into the bedrock material.. In the event that mineralization were much deeper than 1,500 feet, it could probably not be detected by this survey, since the response would likely fall within the noise level.

It may be useful to trace the pyrite halo south west of the Butte fault. This could be accomplished by surveying the grid of five lines, spaced at 2,000 foot intervals which is shown on Plate 3, and on Fig. 1A. These lines, each of which are about three miles long, could be surveyed with dipoles of five hundred or one thousand feet in length, - depending on the depth to sulfides, or responsive material, - at a cost of about seven thousand five hundred dollars. The proposed grid has been laid out so that the material could be traced onto the W.-F. ground so that the previous survey could be used to further extend the data..

The two magnetic surveys indicate that the various rock types in the area have quite characteristic magnetic properties.. The vertical component data is amenable to various interpretation procedures, and once the data has been collected on a district basis, it should be useful for purposes of projecting the various geological units. On plate 3 a few of the relatively obvious interpretations have been shown, and this plate illustrates what might be attempted on a district wide scale.

Provided that this information is useful, the magnetic survey should be continued onto the Essex property, and then tied into the San Juan and W. - F. surveys. Once the data is smoothed and filtered, it should be possible to determine the position and depth of the Lone Star Granite, and other geological units. The inferred fault, which parallels the Butte fault near the North Eastern boundary of the W. F ground may also show up, as well as other structural features. The basalts will certainly interfere with the interpretation of the magnetics, but features from this source should be easily identifiable..

A complete reprocessing, filtering and re interpretation of the magnetics from the San Juan area would require about ten days using hand methods. The small amount of material would not justify processing by automatic methods. This work is being undertaken on a time available basis to demonstrate the applicability of the technique.

Even without filtering, the magnetics show a number of

features. For instance the Butte fault marks the transition from high frequency to lower frequency magnetics.. A frequency analysis would enable this feature to be traced in covered areas. The broad highs,- not the isolated single point anomalies in the south east corner co-incide with the location of basalts. However, the high north of this feature is as yet unexplained, and one would be obliged to search for an intrusive rock or other magnetite bearing unit to account for this anomaly. In addition, the north west trending anomaly in the northwest corner of the property may reflect the trend of the San Juan Intrusive. Some filtering, and a much more detailed treatment of the map would be required to affix the boundaries of the feature, but even these unprocessed results may reflect some general trends..

The magnetic survey on the W.-F. ground has been employed to trace the Lone Star granite south west from its outcrop position onto the W.-F. ground. In addition other occurrences have been inferred, and a northwest trending fault has been identified. This information could be projected onto the Essex ground if the survey were continued.

#### Conclusions and Recommendations.

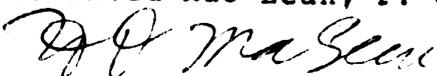
The IP data on the San Juan property indicates that the ore zone is surrounded by a halo of mineralization. Though this halo may not be everywhere visible, its presence is unmistakable. The halo has been truncated by the Butte fault but could easily be traced in the hanging wall. The proposed grid shown in Fig. 1A and in Plate 3 would permit the detection and delineation of this halo in the event that such an action would be of benefit to the development of geological information in the area.

The intrusive rock, the Lone Star granite, has an anomalously high magnetic susceptibility. The location,- position and depth,- of this unit could be approximated in many instances from the results of a magnetic survey. A ground magnetic survey which would tie into the previous work on the W.-F. and San Juan properties along the proposed grid shown in Fig. 1A and Plate 3 is recommended.

Considering the problem of access in this area the benefits which could derive from a low altitude magnetic survey should be given serious attention. The various rock types could be identified by their susceptibilities, and thus could be mapped without regard to trespass considerations. The area to be covered is shown on Fig. 1A. Cost of flying the 410 line miles,- quarter mile line spacing, would be about eight thousand dollars. This survey is not recommended at this time, but is suggested as a means of expanding the area in which geological mapping is available.

Respectfully submitted,

H. David Mac Lean, P. Geoph.



## References;

Bell, J. D. ; "Exploration summary report,  
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Mining District." Graham County, Arizona.

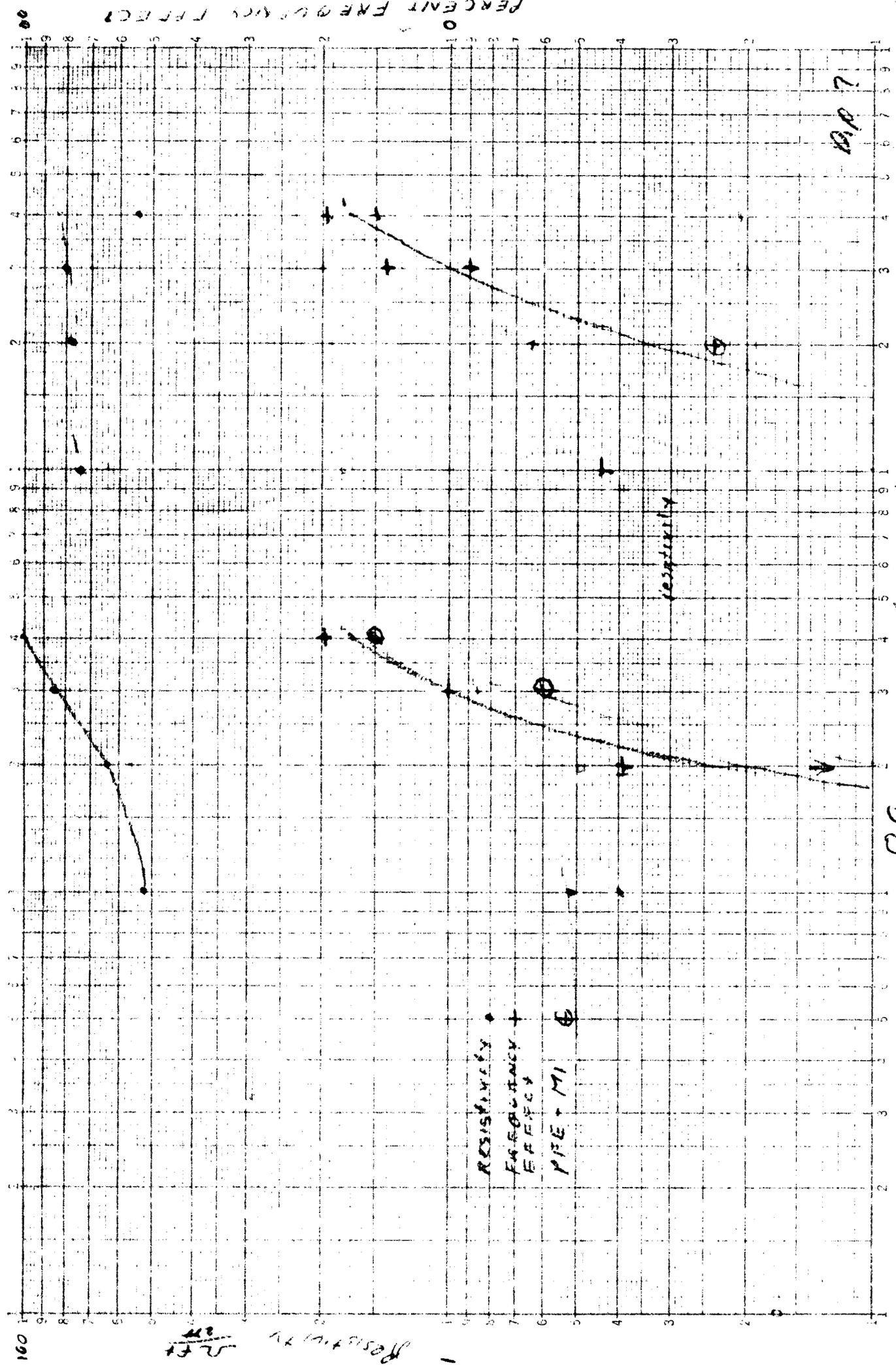
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Rodriguez, R. G.;" IP Resistivity & Magnetic Surveys,  
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Arizona," April 1968. Maps only  
Essex files.

## Summary of maps and figures accompanying this report.

Fig. 1.	Location map.	page 7
Fig. 1A	Detailed location map	pocket 1
Fig. 2	Idealized section through the P.D. orebody and projected onto Essex property by J. K. Jones.	page 8
Fig. 3	Depth sounder on Line 1 W.-F. property at station o, and 20 West.	9
Plate 1.	Vertical intensity magnetic survey W. - F ground	pocket 2
Plate 1A	Vertical Intensity magnetic survey, San Juan property	" 2
Plate 2 & 2R	IP Resistivity of San Juan sheets 1&2	pocket 3
Plate 3	Compilation of IP and magnetic features, and grid location for proposed IP and magnetic surveys in the area	pocket 4.

Time  $t = 8$



LINE 1.  $t_R = 1000'$   
 $t_{100} = 1500'$   
 LINE 2.  $t_R = 1000'$   
 $t_{100} = 1500'$

Fig 3



# **Kennecott Exploration, Inc.**

**Exploration  
Services  
Department**

February 8, 1974

Mr. Paul I. Eimon  
Manager of Exploration  
Essex International, Inc.  
1704 West Grant Road  
Tucson, Arizona 85705

**SXM**  
**FEB 11 1974**  
**RECEIVED**

Dear Paul:

The data collected by Phil Nelson on KCC property with a transmitter located on Essex claims are attached. Phil describes the work as follows:

"We spent January 4-7 attempting to map the Butte Fault with an EM method. To do so, we located an 8000-foot grounded dipole parallel to the fault and placed about a mile to the southwest. We read vertical and horizontal magnetic field amplitudes at 1740 Hertz which gave the highest sensitivity with the available coils.

"A vertical or near-vertical conductor should exhibit a vertical field null directly above it providing that the primary vertical field is very small. However, if the primary field is large compared to the secondary, then the conductor will lie below the point of maximum slope of the total vertical field. We have assumed that the former condition holds, that our transmitter is sufficiently far removed from the fault that the primary field is virtually horizontal and that the conductor lies below a null in the vertical field. On the best nulls, an increase in the horizontal field was also discernible (data not shown) and the direction of the polarization ellipse minor axis also changed in crossing the conductor.

"The vertical magnetic field data in Figure 2 exhibit nulls which are generally 20% or less than the adjacent maxima. Note that two nulls appear on Lines BF-1, BF-2, and BF3. On Lines BF-7 and BF-8 the null disappears and the tilt of the polarization ellipse remained more or less uniform along the line. Since these lines are entirely over gravel, we cannot say whether the conductor has terminated or is at a depth greater than detection capability. On the map in Figure 1 are plotted the locations of the nulls. The darkened squares are subjectively picked as being more definitive nulls than the undarkened."

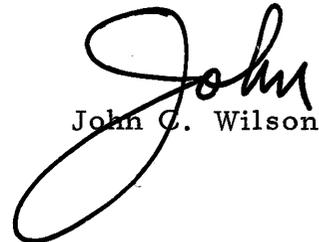
Paul I. Eimon

-2-

February 8, 1974

I hope these data are of some use to you.

Sincerely yours,

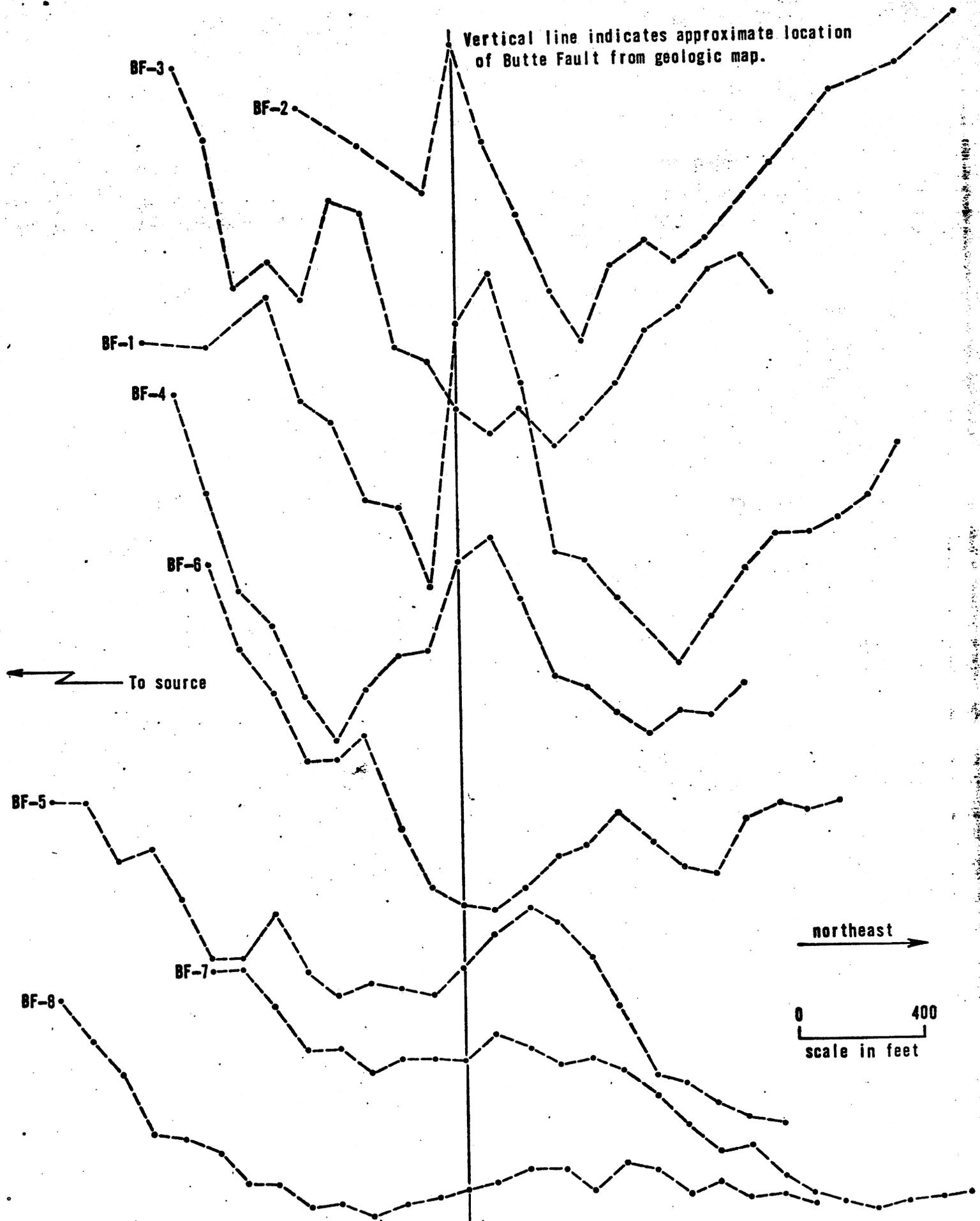
A handwritten signature in cursive script that reads "John C. Wilson". The signature is written in black ink and is positioned above the printed name.

John C. Wilson

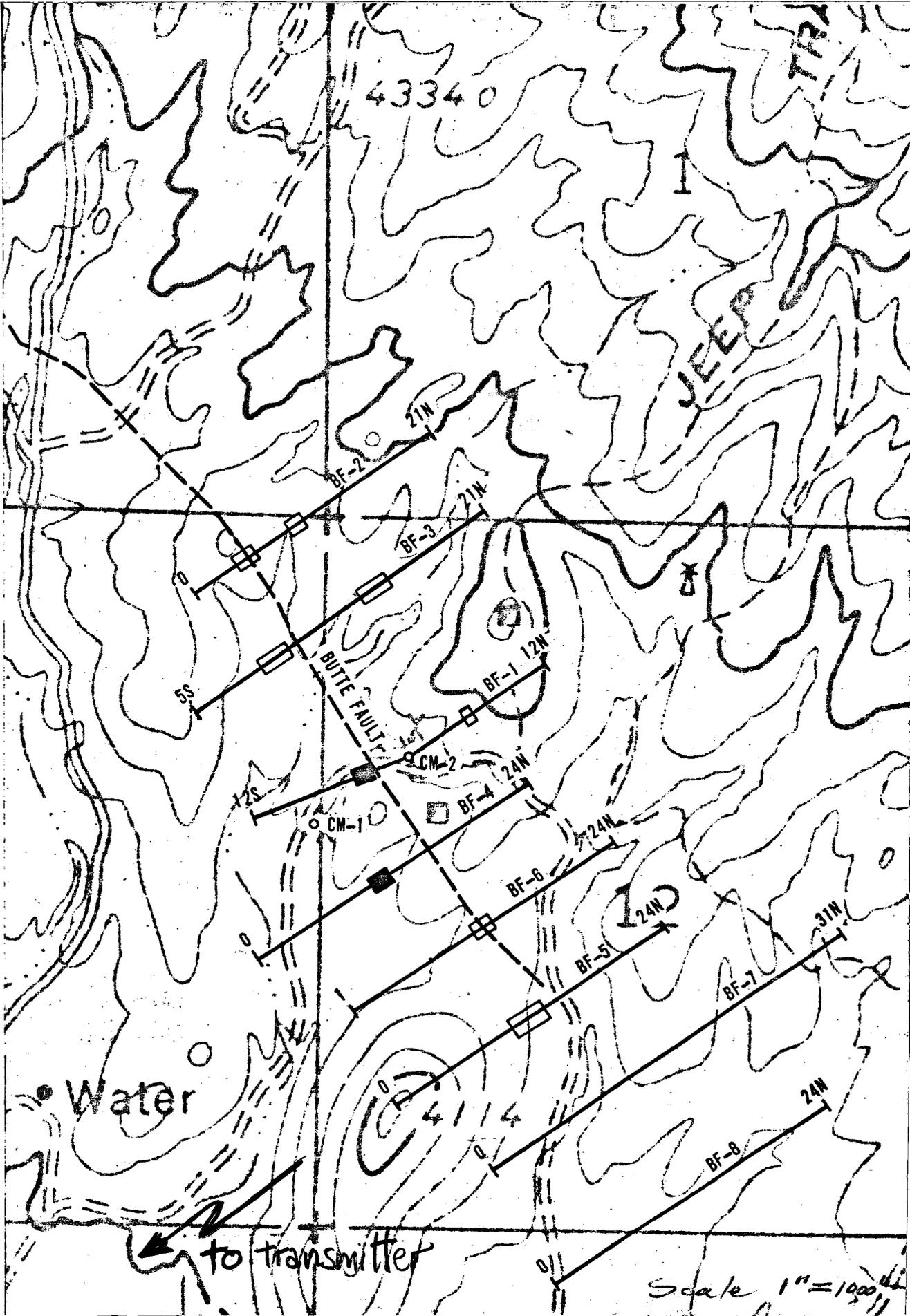
JCW/ac

Enclosure

cc: H. L. Bauer  
N. Gambell



**FIGURE 2.** Vertical magnetic field amplitude at 1740 Hz across the Butte Fault at Safford. Vertical scale is about 32 microvolts (coil output) or 0.5 microamps/meter (field strength) per inch. The line spacing ranges between 700 and 1100 feet.





250  
14  
236 38 | 550  
38  
170  
132  
18

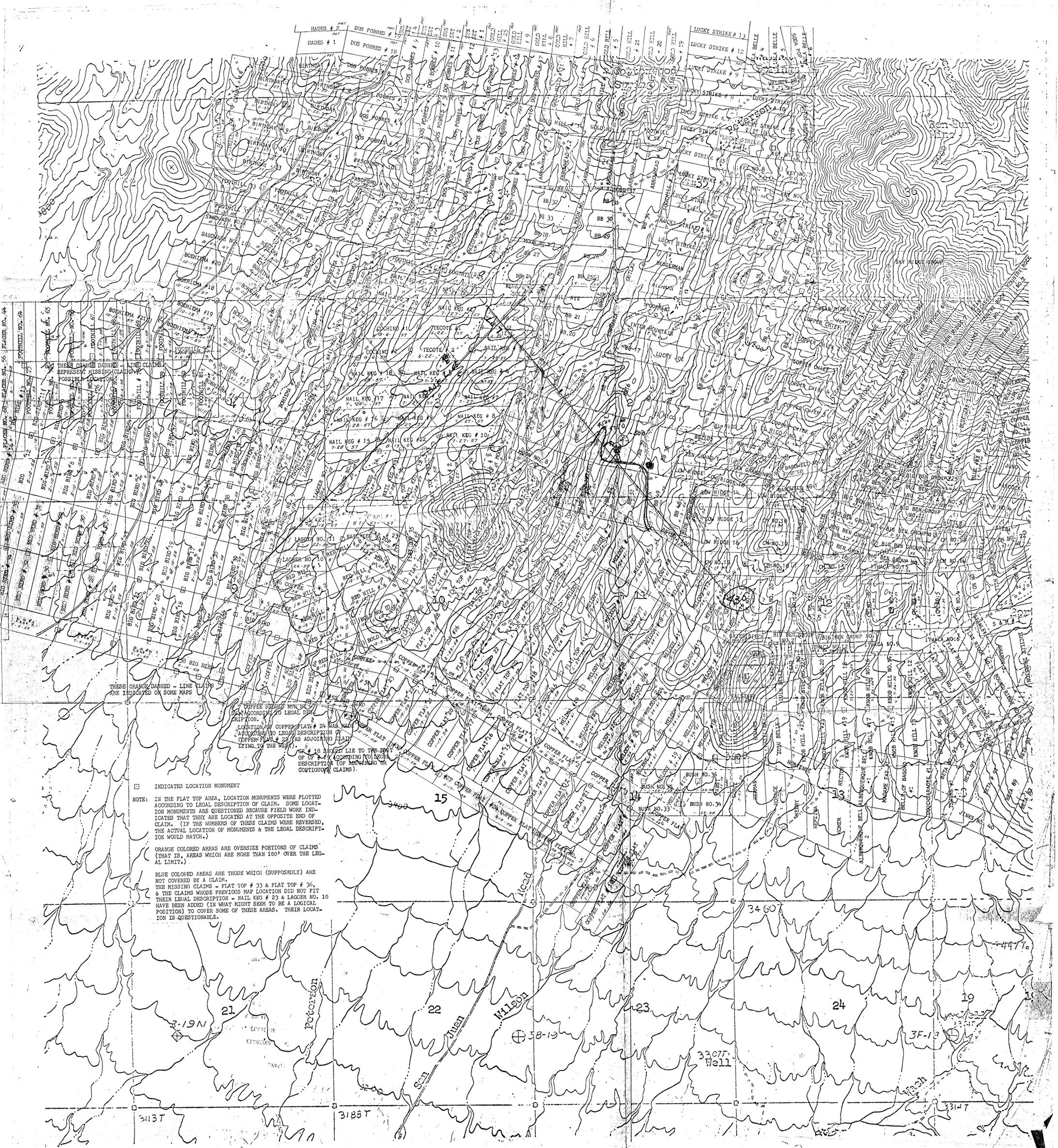
9500  
8550  
4550

Valley

Cottonwood

RED HILL 1  
RED HILL 2  
RED HILL 3  
RED HILL 4  
RED HILL 5  
RED HILL 6  
RED HILL 7

10



THESE ORANGE DASHED - LINE CLAIMS ARE INDICATED ON SOME MAPS

NOTE: IN THE FLAT TOP AREA, LOCATION MONUMENTS WERE PLOTTED ACCORDING TO LEGAL DESCRIPTION OF CLAIM. SOME LOCATION MONUMENTS ARE QUESTIONED BECAUSE FIELD WORK INDICATES THAT THEY ARE LOCATED AT THE OPPOSITE END OF CLAIM. (IF THE NUMBERS OF THESE CLAIMS WERE REVERSED, THE ACTUAL LOCATION OF MONUMENTS & THE LEGAL DESCRIPTION WOULD MATCH.)

ORANGE COLORED AREAS ARE OVERSIZE PORTIONS OF CLAIMS (THAT IS, AREAS WHICH ARE MORE THAN 100' OVER THE LEGAL LIMITS.)

BLUE COLORED AREAS ARE THOSE WHICH (SUPPOSEDLY) ARE NOT COVERED BY A CLAIM. THE MISSING CLAIMS - FLAT TOP # 33 & FLAT TOP # 36, & THE CLAIMS WHOSE PREVIOUS MAP LOCATION DID NOT FIT THEIR LEGAL DESCRIPTION - NAIL KEG # 23 & LAGGER NO. 10 HAVE BEEN ADDED (IN WHAT MIGHT SEEM TO BE A LOGICAL POSITION) TO COVER SOME OF THESE AREAS. THEIR LOCATION IS QUESTIONABLE.

NOTE: DATES ARE DATE OF LOCATION OF CLAIM

- |    |  |    |   |   |  |
|----|--|----|---|---|--|
| 1  | <input type="checkbox"/> NAIL KEG GROUP (1-19), A. CLARIDGE ET AL                                    | 13 | <input type="checkbox"/> MESQUITE, B. JOHN                                      | <input type="checkbox"/> HORSESHOE PATENTED CLAIMS (LONE STAR MINE), G. ANDERSON ET AL (under option to PRODUCERS MINERALS CORP.) | <input type="checkbox"/> CENTER-WINKLER FAULKNER (BIG BIRD & COPPER FLAT GROUPS), WINKLER & FAULKNER ET AL |
| 2  | <input type="checkbox"/> NAIL KEG GROUP (20-24), A. CLARIDGE ET AL                                   | 14 | <input type="checkbox"/> COPPER CHIEF GROUP (& EL RICO 3), P. LINES ET AL       | <input type="checkbox"/> BLUE BIRD GROUP (KNOX HILL CLAIMS), L. WEST ET AL (under option to PRODUCERS MINERALS CORP.)             | <input type="checkbox"/> EAST-WINKLER FAULKNER, WINKLER & FAULKNER ET AL                                   |
| 3  | <input type="checkbox"/> REDHILL GROUP, A. CLARIDGE ET AL  | 15 | <input type="checkbox"/> SANDMASH GROUP, D. HAWKINS ET AL                       | <input type="checkbox"/> PHILIPS DODGE GROUP, PHILIPS DODGE   | <input type="checkbox"/> WEST-WINKLER FAULKNER, WINKLER & FAULKNER ET AL                                   |
| 4  | <input type="checkbox"/> BOHEMIA GROUP (1-24), (TECOTE 1, 2 & FOOT-HILL 39, 40) V. HOUSEHOLDER ET AL | 16 | <input type="checkbox"/> PICKUP, L. WEST ET AL                                  | <input type="checkbox"/> KENROTT GROUP (BEAR CREEK MINING CO.)  |  |
| 5  | <input type="checkbox"/> COFFEE & COCHINO GROUP, V. HOUSEHOLDER                                      | 17 | <input type="checkbox"/> SOTO STATE LEASE, H. GREEN                             | <input type="checkbox"/> SAN JUAN GROUP, ETC., PRODUCERS MINERALS CORP.   |  |
| 6  | <input type="checkbox"/> FLAT TOP GROUP, A. CLARIDGE ET AL   | 18 | <input type="checkbox"/> BOLD GROUP, R. CARRASCO ET AL                          | <input type="checkbox"/> HARPON GROUP, ETC., SANCHEZ & CARRASCO ET AL (leased to INSPIRATION CONSOLIDATED CORP.)                  |  |
| 7  | <input type="checkbox"/> MELODY GROUP, CARRASCO & BELLMAN ET AL                                      | 19 | <input type="checkbox"/> BIG BIRD GROUP (1-24, 49, 50), V. HOUSE - HOLDER ET AL | <input type="checkbox"/> BEN HUR GROUP, L. WEST ET AL (leased to INSPIRATION CONSOLIDATED CORP.)                                  |  |
| 8  | <input type="checkbox"/> LAGGER GROUP, M. GREEN  | 20 | <input type="checkbox"/> BIG BIRD 51, V. HOUSEHOLDER ET AL                      |   |  |
| 9  | <input type="checkbox"/> BIG BEN GROUP, A. CLARIDGE ET AL  | 21 | <input type="checkbox"/> COPPER FLAT (11-23), V. HOUSEHOLDER ET AL              |   |  |
| 10 | <input type="checkbox"/> BARDWELL GROUP, A. CLARIDGE ET AL   |    |   |   |  |
| 11 | <input type="checkbox"/> LEAD HILL GROUP, A. CLARIDGE ET AL  |    |   |   |  |
| 12 | <input type="checkbox"/> KEY GROUP, A. CLARIDGE ET AL  |    |   |   |  |

REVISED 11/18/71

REVISED 12/15/71

CLAIM MAP

SAFFORD

ACIPSO - 771

GRAHAM, ARIZ.

SECTION 66, 27S

SCALE 1:100,000

DATE 11/10/71

PREPARED BY G.H. A.T.C.

**CONFIDENTIAL**

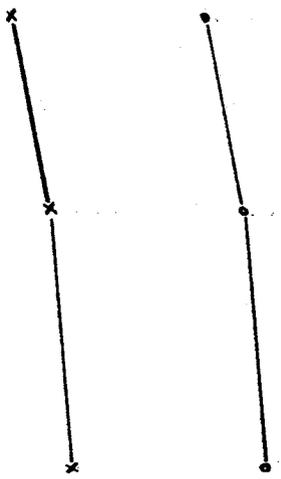
FIELD WORK MAP

REVISED 12/15/71

DUAL GRAVITY CURVE  
 O BEARING: BASE STA  
 X ADJUSTED VALUES  
 1" = 20 GAMMAS

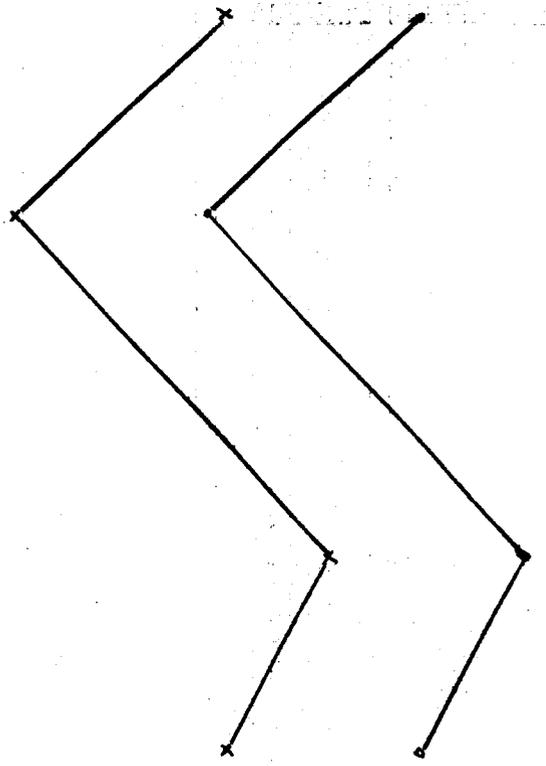
LINE 135  
 BASE 135, 4SW  
 61.172

4160  
 4140  
 4120  
 4100  
 4080  
 4160



LINE 138  
 BASE 135, 4SW  
 61.172

4140  
 4120  
 4100  
 4080  
 4160  
 4140  
 4120  
 4100  
 4080



THIS AREA IS FOR POSITION  
 (VERTICAL INTERFERE)  
 SCALE CORRECTION- 215.5 / HOURS DIV.  
 ALL VALUES ARE CORRECTED FOR  
 DIURNAL DRIFT & PLOTTED IN GAMMAS

DIURNAL CORRECTION CURVE  
 O READING : BASE STA  
 X ADJUSTED VALUES  
 1" = 20 GAMMAS

LINE 147  
 BASE 141, 35W  
 6/2/72

LINE 150  
 BASE 149, 45W  
 6/5/72

INST: ASKANIA GFZ TORSION  
 (VERTICAL INTENSITY)  
 SCALE CONSTANT = 215.5 / SCALE DIV.  
 ARBITRARY MAGNETIC BASE  
 ALL VALUES ARE CORRECTED FOR  
 DIURNAL DRIFT & PLOTTED IN GAMMAS

3820

3800

3780

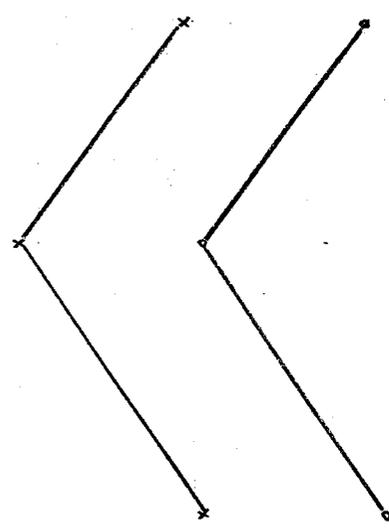
3760  
 3680

3660

3640

3620

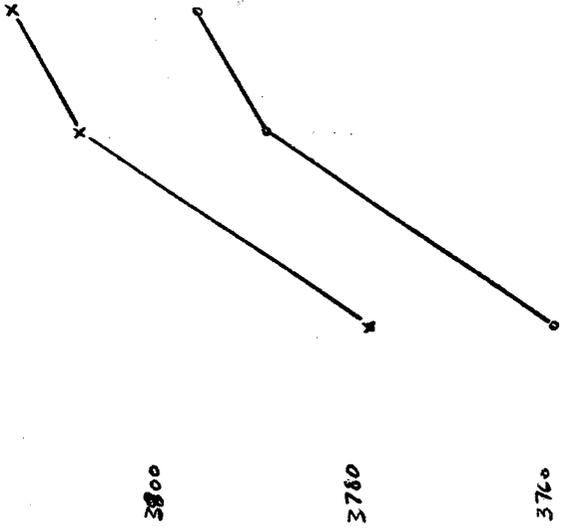
3600



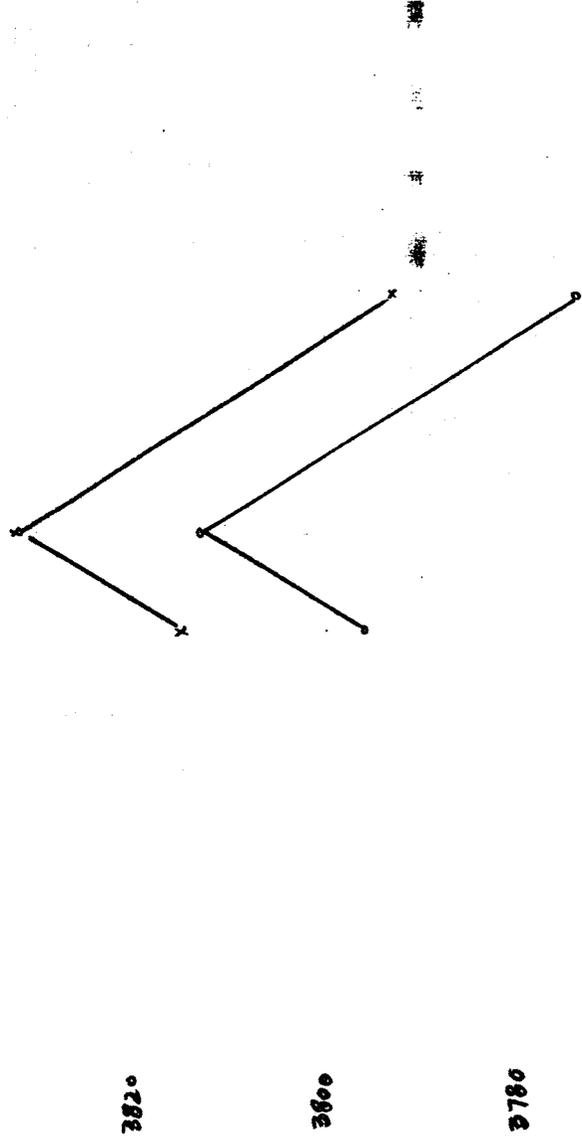
9:00 10:00 11:00 12:00 1:00 2:00 3:00 4:00 5:00

DIURNAL CORRECTION CURVE  
 O READING: BASE STA  
 X ADJUSTED VALUES  
 1" = 20 GAMMAS

LINE 141  
 BASE 141 3, SW  
 6/2/72



LINE 144  
 BASE 141 3, SW  
 6/2/72



EMP: AERIAL GPS POSITION  
 (VERTICAL ILLUMINATION)  
 SCALE CORRECTED - 215.9 / SCALE DIV.  
 APPROPRIATE MAGNETIC DATA  
 ALL VALUES ARE CORRECTED FOR  
 DIURNAL DRIFT & PLOTTED IN GREEN

STA	1ST READING	2ND READING	AVG. E & S	TIME OF DAY	REMARKS
-----	----------------	----------------	---------------	----------------	---------

SAFFORD PROJ.  
 VERTICAL Intensity  
 Magnetometer Notes

INST. ASKANIA GFZ  
 601378

Scale Const. 238.5

Instrument Read by B.B.

4/25 STA	1st Read	2nd Read	Aug.	0/5.0 FACTOR	Time
STA.	is Located		Joo'S.	±185'	west
LINE 5	of $\frac{54}{89}$		T.	R.	
5000 W					
Mag. Base	97.62	97.62			11 <sup>05</sup>
	<del>95.45</del>	97.60	97.61		11 <sup>15</sup>
4750 W	97.67	97.73			
	97.70	97.72	97.71		11 <sup>20</sup>
4500 W	97.45	97.40	97.42		
	97.41				
4250 W	97.40	97.44	97.40		11 <sup>30</sup>
	97.38	97.38			
4000 W	97.25	97.25	97.25		
3750 W	97.00	96.90	96.99		11 <sup>40</sup>
3500 W	97.16	97.18	97.17		
3250 W	97.15	97.12	97.12		11 <sup>45</sup>
	97.10	97.12			
3000 W	96.94	96.94	96.94		11 <sup>50</sup>
Base					
5000 W	97.70	<del>97.60</del>			12 <sup>03</sup>
	97 <sup>55</sup>	97 <sup>55</sup>			
	97 <sup>56</sup>	97 <sup>57</sup>			
	97 <sup>57</sup>	97 <sup>56</sup>			

DIURNAL  
CORR

$\delta$   
Reading

REMARKS  
(See Note  
Below)

$\delta$  bearing

S. 62 E.

-.11

23,254  
1379

Base correction  
97.50

Rotate 90°

97.61

-.10

23280  
1405

67

97.32

-.09

23210  
1335

73

70

43

97.31

-.09

23208  
1333

MAIN RD.  
EAST Side of

~~97.30~~ ~~08~~

97.17

-.08

1300

West Side of  
WASH

96.92

-.07

1240

IN WASH

97.10

-.07

1253

97.05

-.07

1271

49.2

96.88

-.06

1231

Return to base

To compute value multiply Avg.  
reading by scale constant (238.5)

then subtract 21875 to correct  
to an arbitrary base

1/25 W <sup>5</sup> STA	151 READ	200 READ	Avg	S.D FACTOR	TIME
BASE 5000W	97 <sup>57</sup>	97 <sup>57</sup>			1:55
3000 W	96 <sup>95</sup>	97 <sup>00</sup>	96 <sup>97</sup>		2:39
2750 W	95 <sup>96</sup>	95 <sup>94</sup>	95 <sup>95</sup>		2:40
2500 W	96 <sup>95</sup>	96 <sup>95</sup>	96 <sup>95</sup>		2:47
2250 W	96 <sup>85</sup>	96 <sup>87</sup>	96 <sup>86</sup>		2:54
2000 W	96 <sup>90</sup>	96 <sup>90</sup>	96 <sup>90</sup>		2:59
1750 W	96 <sup>75</sup>	96 <sup>77</sup>	96 <sup>76</sup>		3:04
1500 W	96 <sup>94</sup>	96 <sup>94</sup>	96 <sup>94</sup>		3:11
1250 W	96 <sup>80</sup>	96 <sup>82</sup>	96 <sup>81</sup>		3:16
1000 W	96 <sup>88</sup>	96 <sup>86</sup>	96 <sup>87</sup>		3:25
750 W	96 <sup>95</sup>	96 <sup>95</sup>	96 <sup>95</sup>		3:36
500 W	97 <sup>07</sup>	97 <sup>05</sup>	97 <sup>06</sup>		3:42
250 W	96 <sup>80</sup>	96 <sup>82</sup>	96 <sup>81</sup>		3:50
STATION 0 E/W	97 <sup>05</sup>	97 <sup>03</sup>	97 <sup>04</sup>		3:57
250 E	96 <sup>96</sup>	96 <sup>94</sup>	96 <sup>96</sup>		4:03
BASE 5000 W	97 <sup>78</sup>	97 <sup>80</sup>	97 <sup>79</sup>		4:40

	DIRIAL CORR	δ READING	δ	REMARKS
				BASE
	-.10	96.87	1231 1228	FLAT
	-.11	95.84	983	"
	-.12	96.83	1219	"
	-.13	96.83	1195	"
	-.13	96.77	1205	WASH
	-.14	96.62	1169	E OF WASH
	-.15	96.79	1209	FLAT
	-.15	96.66	1178	EDGE OF WASH
	-.17	96.80	1212	
	-.18	96.77	1205	
	-.19	96.87	1229	Slope OF RIDGE
	-.19	96.62	1169	BIG WASH
	-.20	96.84	1221	FLAT
	-.22	96.74	1197	430' x 40' W IS A WASH H2 RED. 1.20
	-.29			BASE

4124 W5 STA	1ST READ	2ND READ	AVG.	J.F.S.O EARTH	TIME
BASE 5000 W	9772	9774	9773		9:07
500E	9718	9720	9719		10:05
750E	9722	9718	9719		10:15
1000E	9613	9613	9613		10:37
STAKE 1250E	9715	9715	9715		10:45
1500E	9716	9716	9716		10:50
1750	9732	9732	9732		10:55
2000	9710	9712	9711		
2250	9515	9517	9516		
STAKE 2500E	9733	9736	9734		11:24
2750	9660	9660	9660		
3000	9630	9630	9630		
3250	9720	9720	9720		
3500	9708	9710	9709		11:52
STAKE 3750	9727	9729	9728		
4000 E	9724	9724	9724		12:07

DRUM #	CORR	READING		REMARKS
				BASE
	-.22	96 <sup>97</sup> <sub>-</sub>	1252	FLAT
	-.22	96 <sup>97</sup> <sub>-</sub>	1252	
	-.22	95 <sup>91</sup> <sub>-</sub>	1000	1/4 COR SEC 9
	-.22	96 <sup>93</sup> <sub>-</sub>	1243	200' N 35 E
	-.22	96 <sup>94</sup> <sub>-</sub>	1245	FENCE 100' EAST
	-.22	97 <sup>10</sup> <sub>-</sub>	1283	
	-.22	96 <sup>89</sup> <sub>-</sub>	1233	EDGE OF WASH
	-.22	94 <sup>94</sup> <sub>-</sub>	768	? SCOPE OF BASALT HILL
	-.22	97 <sup>12</sup> <sub>-</sub>	1288	"
	-.21	96 <sup>39</sup> <sub>-</sub>	1114	"
	-.21	96 <sup>09</sup> <sub>-</sub>	1042	BASE OF BASALT HILL
	-.21	96 <sup>99</sup> <sub>-</sub>	1257	WASH
	-.21	96 <sup>88</sup> <sub>-</sub>	1231	ROAD 4' WASH
	-.21	97 <sup>03</sup> <sub>-</sub>	1276	SE COR FT 28 SE COR 26
	-.21	97 <sup>03</sup> <sub>-</sub>	1267	150' 80 E ↙

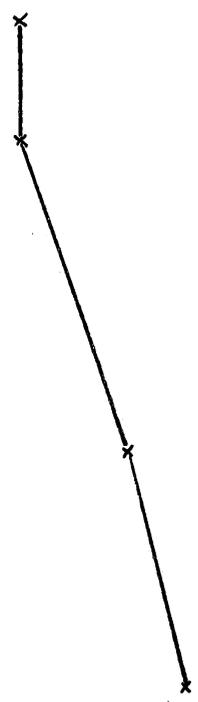
4/24 LW6 STA	1ST READ	2ND READ	AUG	TIME
STAKE 4000 E	9780	9778	9779	12:32
3750 E	9730	9730	9730	
3500 E	9730	9730	9730	
3250 E	9750	9748	9749	12:49
3000 E	9745	9743	9744	
STAKE 2750 E	9757	9757	9757	
2500 E	9775	9777	9775	
BASE 5000 W	9770	9768	9769	1:46
2250	9755	9756	9753	2:32
4/25 5000 W BASE	LINE 6 9784	9784	9781	8:47
2000 E	9805	9807	9806	9:17
1750 E	9771	9773	9772	
STAKE 1500 E	9760	9762	9761	
1250	9755	9753	9754	
1200	9748	9748	9748	9:39

DIURNAL CORAL	♂ HEAD		REMARKS
-.21	97 <sup>58</sup>		
-.21	97 <sup>59</sup>		
-.21	97 <sup>09</sup>		
-.21	97 <sup>28</sup>		WASH
-.21	97 <sup>23</sup>		
-.20	97 <sup>37</sup>		EDGE OF WASH
-.20	97 <sup>06</sup>		
-.20	97 <sup>36</sup>		
			100 ft OF FENCE
			150 ft OF FENCE

3720

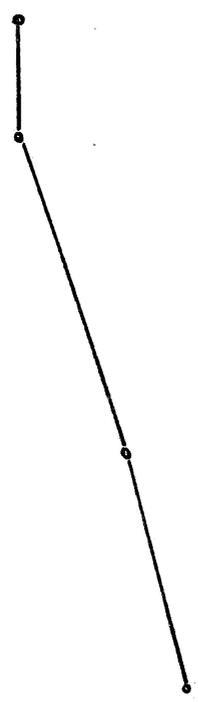
DIURNAL CORRECTION CURVE  
O READING: BASE STA  
X ADJUSTED VALUES

3700



LINE 38N  
BASE 41,010  
6/6/72

3680



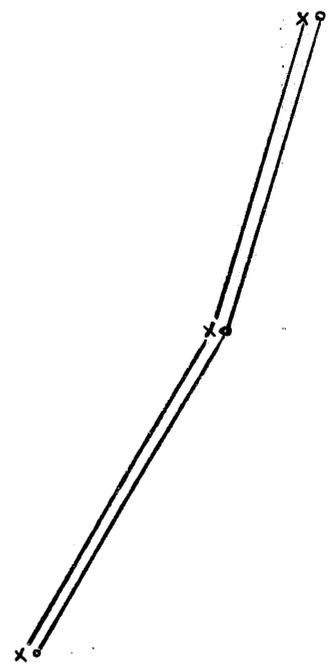
LINE 35N  
BASE 35N, 7W  
6/8/72

3660

3640

3620

3600



3780

INST: ASKANIA GFZ TORSION  
(VERTICAL INTENSITY)  
SCALE CONSTANT= 215.5 /SCALE DIV.  
ARBITRARY MAGNETIC BASE  
ALL VALUES ARE CORRECTED FOR  
DIURNAL DRIFT & PLOTTED IN GAMMAS

3760

9:00 10:00 11:00 12:00 1:00 2:00 3:00 4:00 5:00

3840

3820

3800

3780

3760  
3840

3820

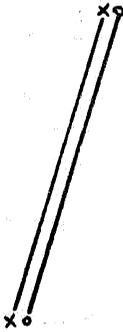
3800

3780

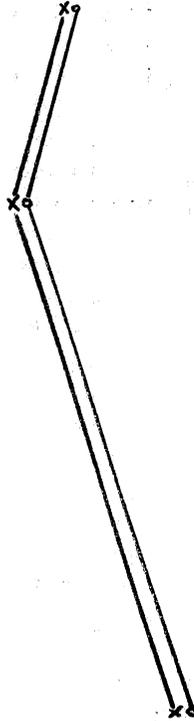
3760

DIURNAL CORRECTION CURVE  
O READING: BASE STA  
X ADJUSTED VALUES  
1" = 20 GAMMAS

LINE 32 N  
BASE 35N, 7W  
6/18/72



LINE 29 N, 26N, 23N  
BASE 35N, 7W  
6/18/72



INST: ASKANIA GFZ TORSION  
(VERTICAL INTENSITY)  
SCALE CONSTANT = 215.5 / SCALE DIV.  
ARBITRARY MAGNETIC BASE  
ALL VALUES ARE CORRECTED FOR  
DIURNAL DRIFT & PLOTTED IN GAMMAS

9:00

10:00

11:00

12:00

1:00

2:00

3:00

4:00

5:00

DIURNAL CORRECTION CURVE  
O READING : BASE STA  
X ADJUSTED VALUES  
1" = 20 GAMMAS

LINE 53 N, 56 N  
BASE 530, 11E  
619172

LINE 102  
BASE 53 N, 11E  
619172

INST: ASKANIA GFZ TORSION  
(VERTICAL INTENSITY)  
SCALE CONSTANT = 215.5 / SCALE DIV.  
ARBITRARY MAGNETIC BASE  
ALL VALUES ARE CORRECTED FOR  
DIURNAL DRIFT & PLOTTED IN GAMMAS

3740

3720

3700

3680

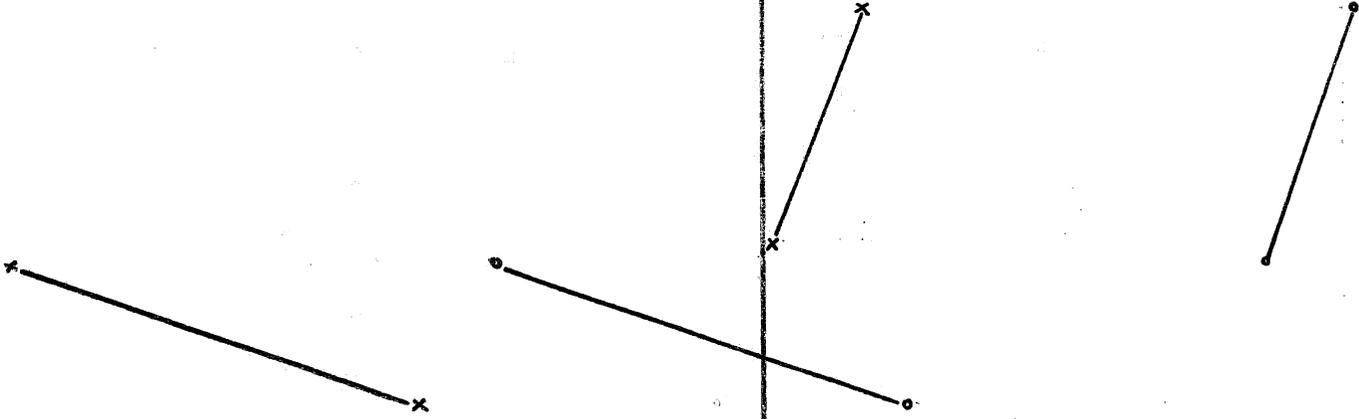
3660  
3740

3720

3700

3680

3660

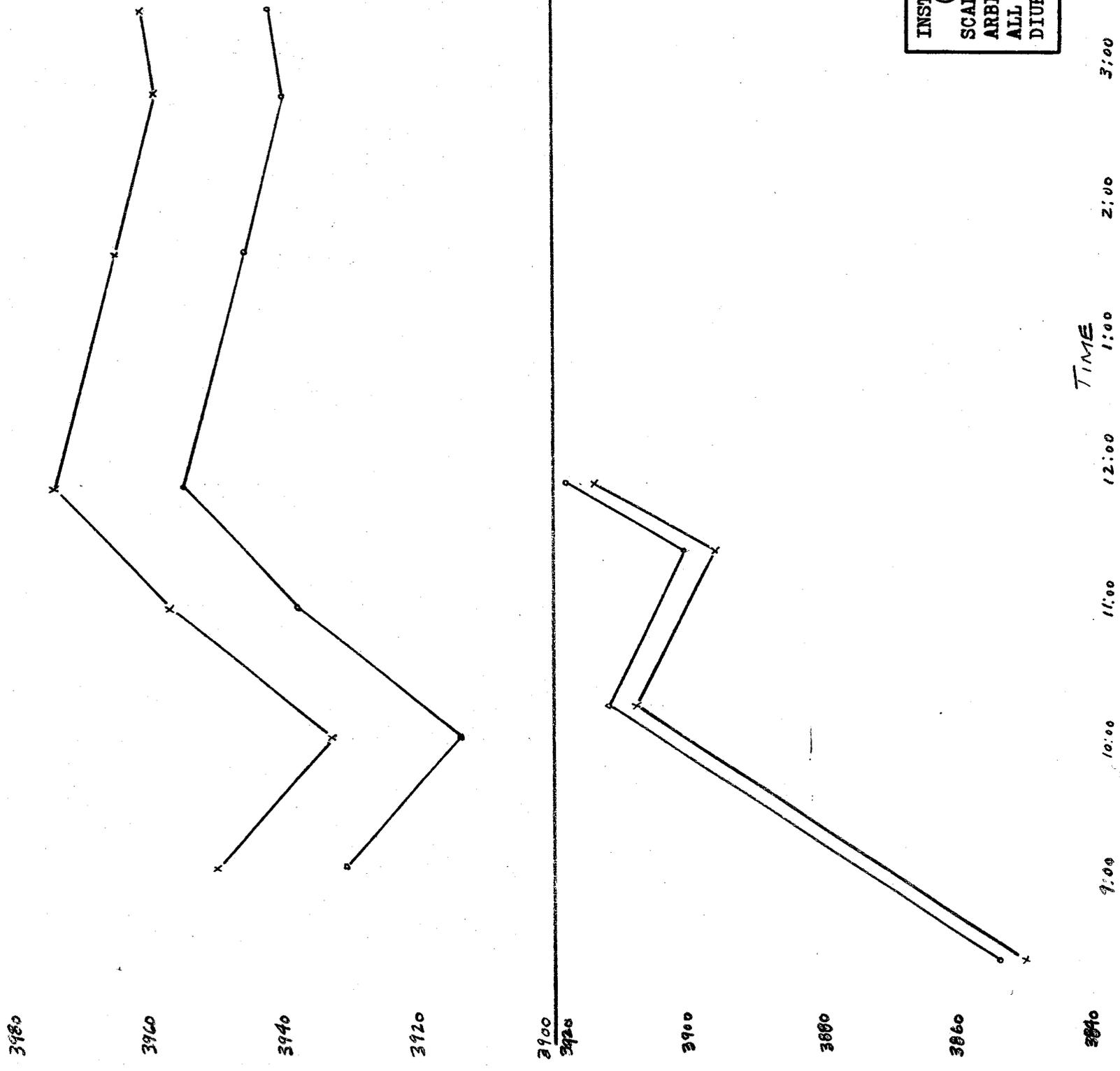


DIURNAL CORRECTION CURVE  
 O READING: BASE STA  
 X ADJUSTED VALUES  
 1" = 20 GAMMAS

LINES 12SE, 9SE, 6SE  
 15SE, 18SE, 21SE  
 BASE 12SE, 35W  
 6/13/72

LINES 59N, 62N, 68N  
 71N, 74N, 77N  
 BASE 73N 6E  
 6/19/72

INST: ASKANIA GFZ TORSION  
 (VERTICAL INTENSITY)  
 SCALE CONSTANT = 215.5 / SCALE DIV.  
 ARBITRARY MAGNETIC BASE  
 ALL VALUES ARE CORRECTED FOR  
 DIURNAL DRIFT & PLOTTED IN GAMMAS



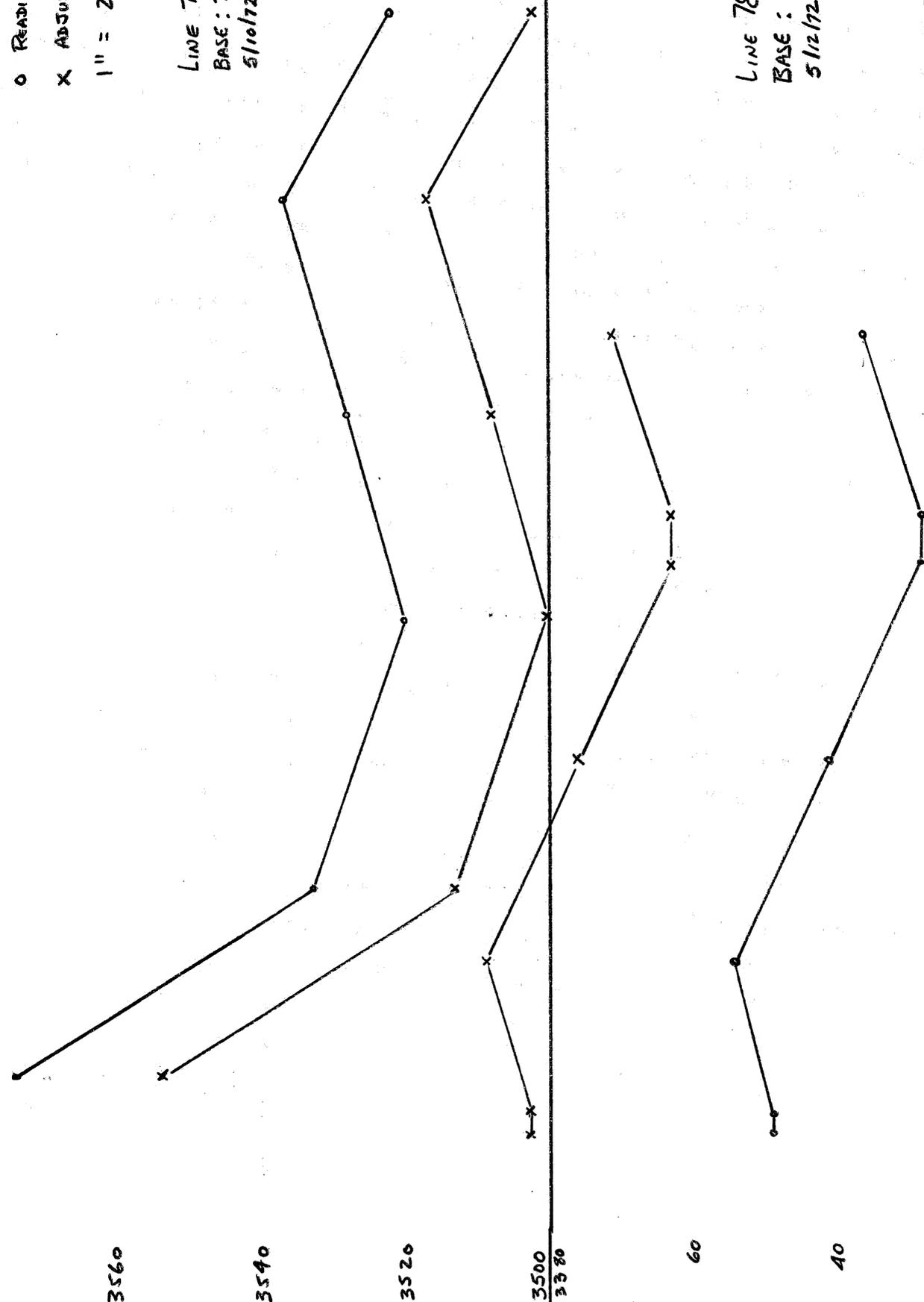
3:50 4:00 4:10 4:20 4:30 4:40 4:50 5:00

DIURNAL CORRECTION CURVE  
O READING: BASE STA VALUES  
X ADJUSTED VALUES  
1" = 20 GAMMAS

LINE 75  
BASE: 75 0/0  
5/10/72 MFB

LINE 78  
BASE: 78,3 S/W  
5/12/72

INST: ASKANIA GFZ TORSION  
(VERTICAL INTENSITY)  
SCALE CONSTANT= 215.5 /SCALE DIV.  
ARBITRARY MAGNETIC BASE  
ALL VALUES ARE CORRECTED FOR  
DIURNAL DRIFT & PLOTTED IN GAMMAS

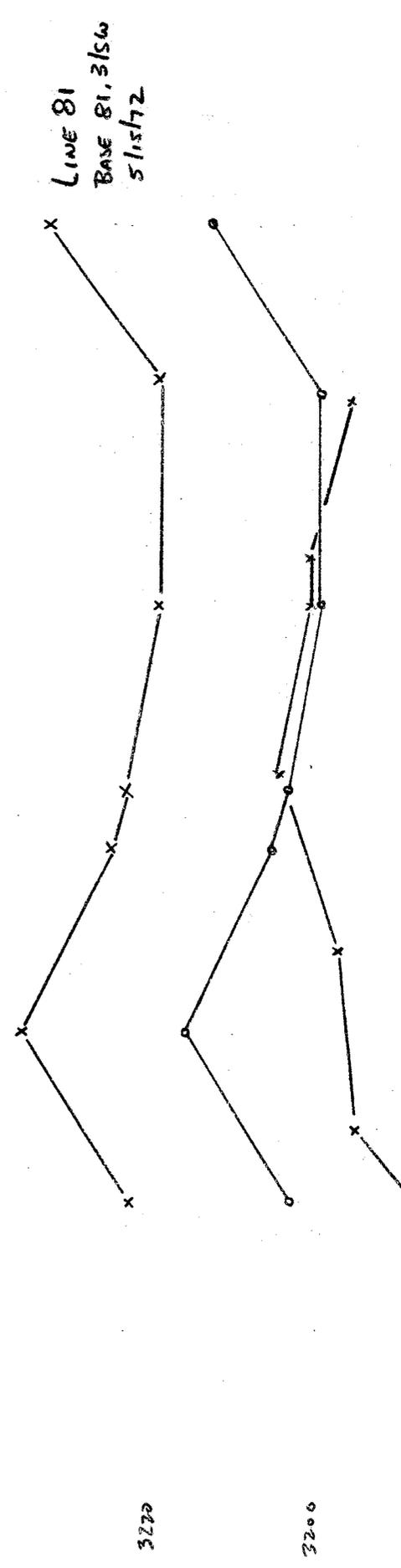


3:50 4:00 4:10 4:20 4:30 4:40 4:50 5:00

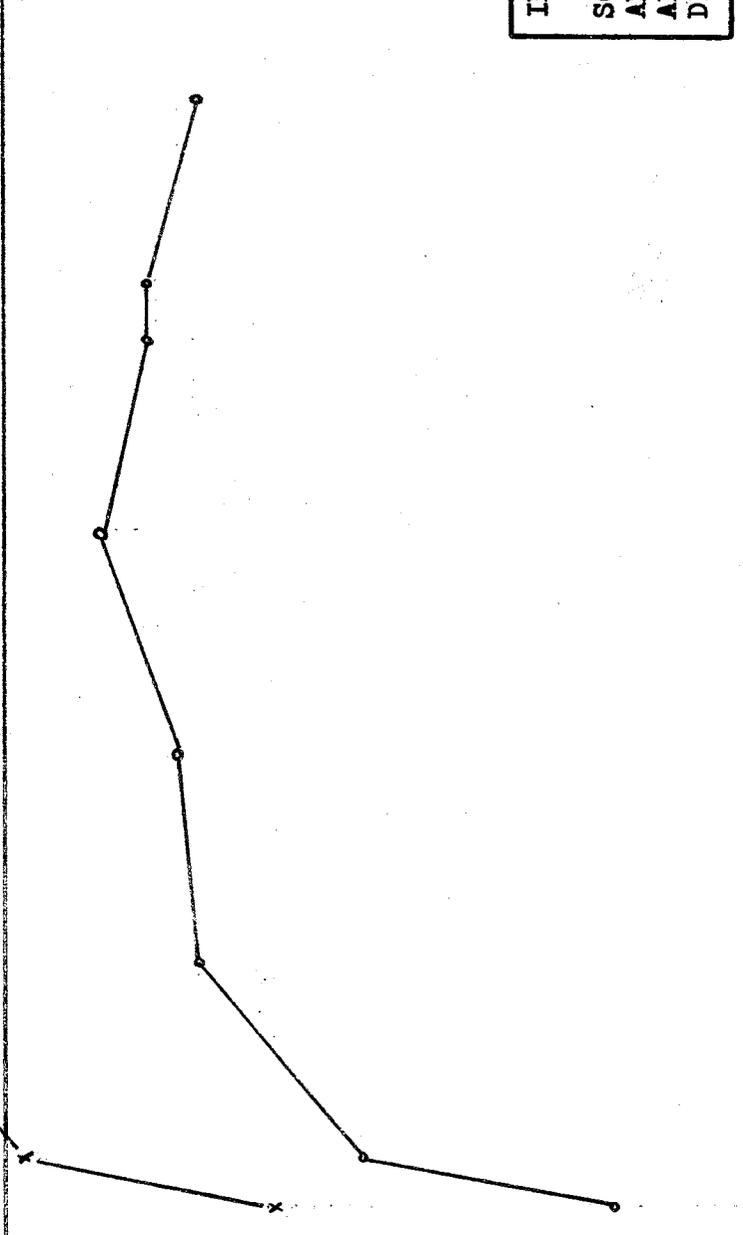
DIURNAL CORRECTION CURVE  
 O READING: BASE STA VALUES  
 X ADJUSTED VALUES  
 1" = 20 GAMMAS

4.00  
 3.00  
 2.00  
 1.00  
 12.00  
 11.00  
 10.00  
 9.00

3260  
 3240  
 3220  
 3200  
 3180  
 3160  
 3140  
 3120



LINE 89  
 BASE: 89, 2SW  
 5/16/72



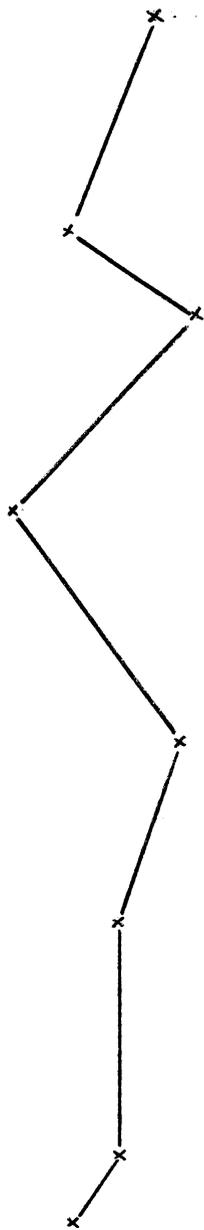
INST: ASKANIA GFZ TORSION  
 (VERTICAL INTENSITY)  
 SCALE CONSTANT= 215.5 / SCALE DIV.  
 ARBITRARY MAGNETIC BASE  
 ALL VALUES ARE CORRECTED FOR  
 DIURNAL DRIFT & PLOTTED IN GAMMAS

4.00  
 3.00  
 2.00  
 1.00  
 12.00  
 11.00  
 10.00  
 9.00

3260  
 3240  
 3220  
 3200  
 3180  
 3160  
 3140  
 3120

DIURNAL CORRECTION CURVE  
 O READING BASE STA  
 X ADJUSTED VALUES  
 1" = 20 GAMMAS

LINE 87  
 BASE 27,010  
 5/17/72



3460

3440

3420

3400  
3480

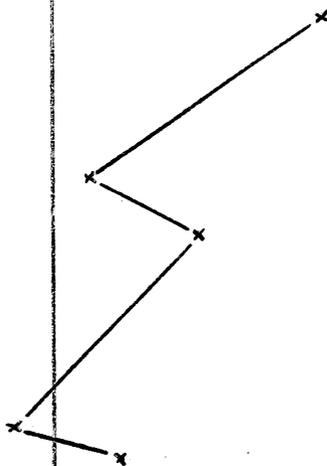
3460

3440

3420

3400

LINE 90  
 BASE 90,010  
 5/18/72



INST: ASKANIA GFZ TORSION  
 (VERTICAL INTENSITY)  
 SCALE CONSTANT = 215.5 / SCALE DIV.  
 ARBITRARY MAGNETIC BASE  
 ALL VALUES ARE CORRECTED FOR  
 DIURNAL DRIFT & PLOTTED IN GAMMAS

9:00 10:00 11:00 12:00 1:00 2:00 3:00 4:00

3460

DIURNAL CORRECTION CURVE  
O READING BASE STA  
X ADJUSTED VALUES  
1" = 20 GAMMAS



3440

3420

LINE 93  
BASE 90,010  
5/18/72



3400

3380  
3280

3260

LINE 96  
BASE 97,450  
5/19/72



3240

3220



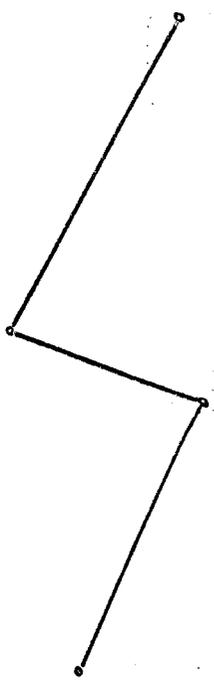
3200

INST: ASKANIA GFZ TORSION  
(VERTICAL INTENSITY)  
SCALE CONSTANT = 215.5 / SCALE DIV.  
ARBITRARY MAGNETIC BASE  
ALL VALUES ARE CORRECTED FOR  
DIURNAL DRIFT & PLOTTED IN GAMMAS

9:00 10:00 11:00 12:00 1:00 2:00 3:00 4:00 5:00

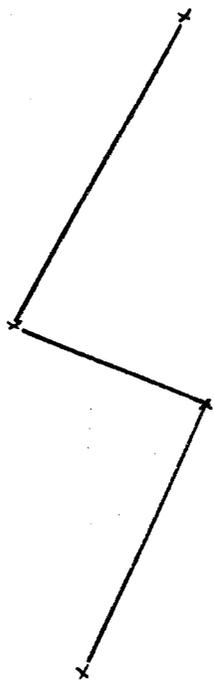
326°

DIURNAL CORRECTION CURVE  
O READING: BASE STA  
X ADJUSTED VALUES  
1" = 200 GAMMAS



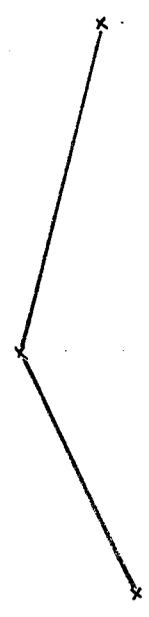
329°

LINE 99  
BASE 97, 4SW  
5/19/72



322°

320°  
310°



338°

336°

334°

332°



330°

LINE 102  
BASE 97, 4SW  
5/23/72

INST: ASKANIA GFZ TORSION  
(VERTICAL INTENSITY)  
SCALE CONSTANT = 215.5 / SCALE DIV.  
ARBITRARY MAGNETIC BASE  
ALL VALUES ARE CORRECTED FOR  
DIURNAL DRIFT & PLOTTED IN GAMMAS

9:00 10:00 11:00 12:00 1:00 2:00 3:00 4:00 5:00

DIURNAL CORRECTION CURVE  
 O READING: BASE STA  
 X ADJUSTED VALUES  
 1" = 20 GAMMAS

LINE 105  
 BASE 97,4SW  
 5/22/72

3420

3400

3380

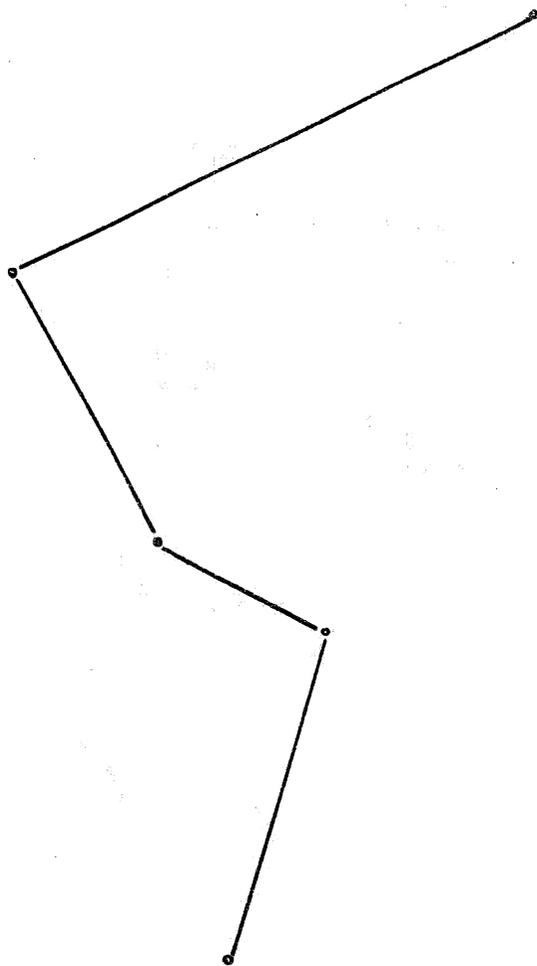
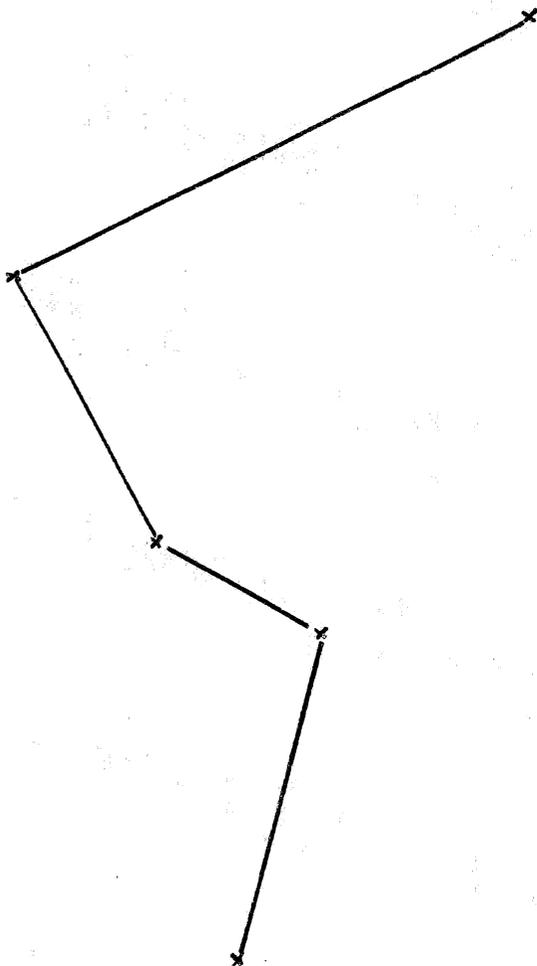
3360

3340

3320

3300

3280



INST: ASKANIA GFZ TORSION  
 (VERTICAL INTENSITY)  
 SCALE CONSTANT = 215.5 / SCALE DIV.  
 ARBITRARY MAGNETIC BASE  
 ALL VALUES ARE CORRECTED FOR  
 DIURNAL DRIFT & PLOTTED IN GAMMAS

9:00 10:00 11:00 12:00 1:00 2:00 3:00 4:00

DIURNAL CORRECTION CURVE  
O READING: BASE STA  
X ADJUSTED VALUES  
1" = 20 GAMMAS

LINE 108  
BASE 9745W  
5/23/72

INST: ASKANIA GFZ TORSION  
(VERTICAL INTENSITY)  
SCALE CONSTANT = 215.5 / SCALE DIV.  
ARBITRARY MAGNETIC BASE  
ALL VALUES ARE CORRECTED FOR  
DIURNAL DRIFT & PLOTTED IN GAMMAS

3420

3400

3380

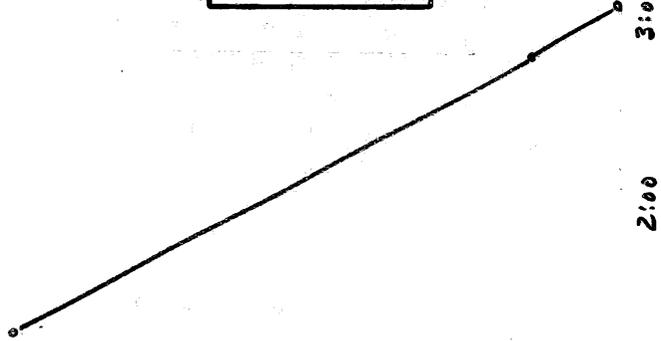
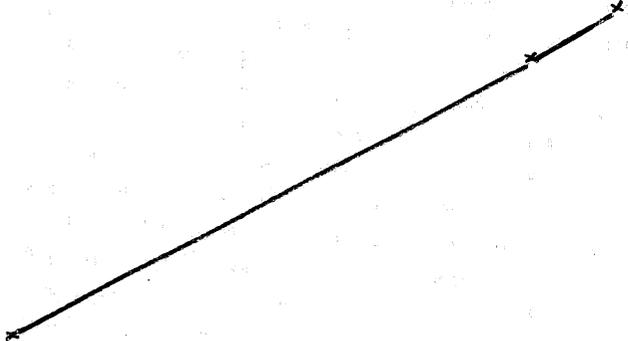
3360

3340

3320

3300

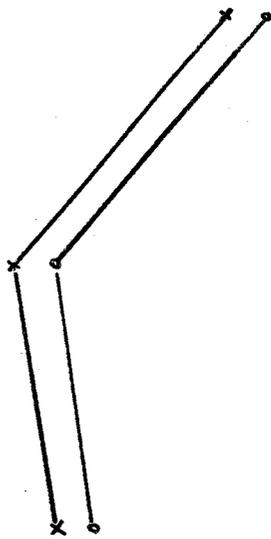
3280



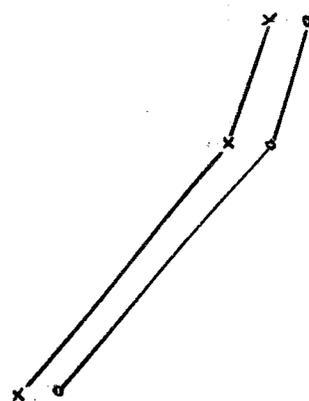
9:00 10:00 11:00 12:00 1:00 2:00 3:00 4:00 5:00

DIURNAL CORRECTION CURVE  
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X ADJUSTED VALUES  
1" = 20 GAMMAS

LINE 111  
BASE 116,350  
512472



LINE 114  
BASE 116,350  
512472



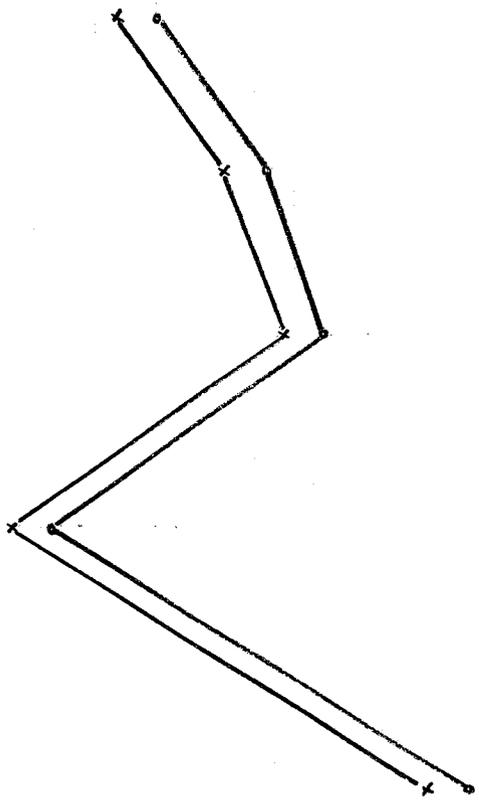
INST: ASKANIA GFZ TORSION  
(VERTICAL INTENSITY)  
SCALE CONSTANT = 215.5 / SCALE DIV.  
ARBITRARY MAGNETIC BASE  
ALL VALUES ARE CORRECTED FOR  
DIURNAL DRIFT & PLOTTED IN GAMMAS

3880  
3860  
3840  
3820  
9:00  
10:00  
11:00  
12:00  
1:00  
2:00  
3:00  
4:00  
5:00

3880

DIURNAL CORRECTION CURVE  
O READING: BASE STA  
X ADJUSTED VALUES  
1" = 20 GAMMAS

3860



LINE 117  
BASE 116,35W  
5/29/72

3840

3820

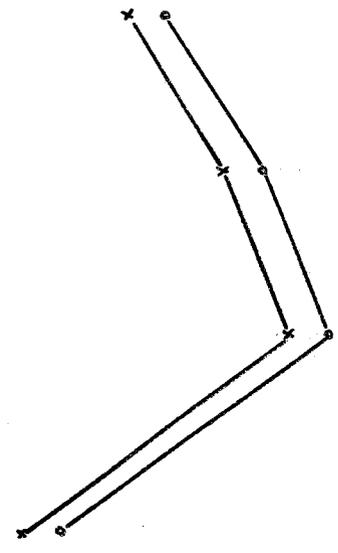
3800

3860

LINE 120  
BASE 116,35W  
5/29/72

3840

3820



INST: ASKANIA GFZ TORSION  
(VERTICAL INTENSITY)  
SCALE CONSTANT= 215.5 / SCALE DIV.  
ARBITRARY MAGNETIC BASE  
ALL VALUES ARE CORRECTED FOR  
DIURNAL DRIFT & PLOTTED IN GAMMAS

3800

9:00 10:00 11:00 12:00 1:00 2:00 3:00 4:00 5:00

DIURNAL CORRECTION CURVE  
 O READING: BASE STA  
 X ADJUSTED VALUES  
 1" = 20 GAMMAS

LINE 123  
 BASE 123,010  
 5/25/72

3700

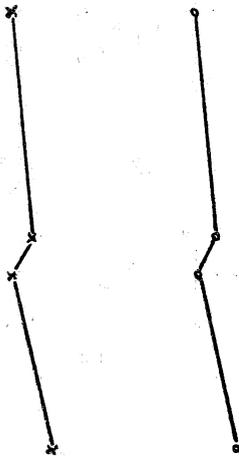
3680

3660

3640

3620

3600



9:00

10:00

11:00

12:00

1:00

2:00

3:00

4:00

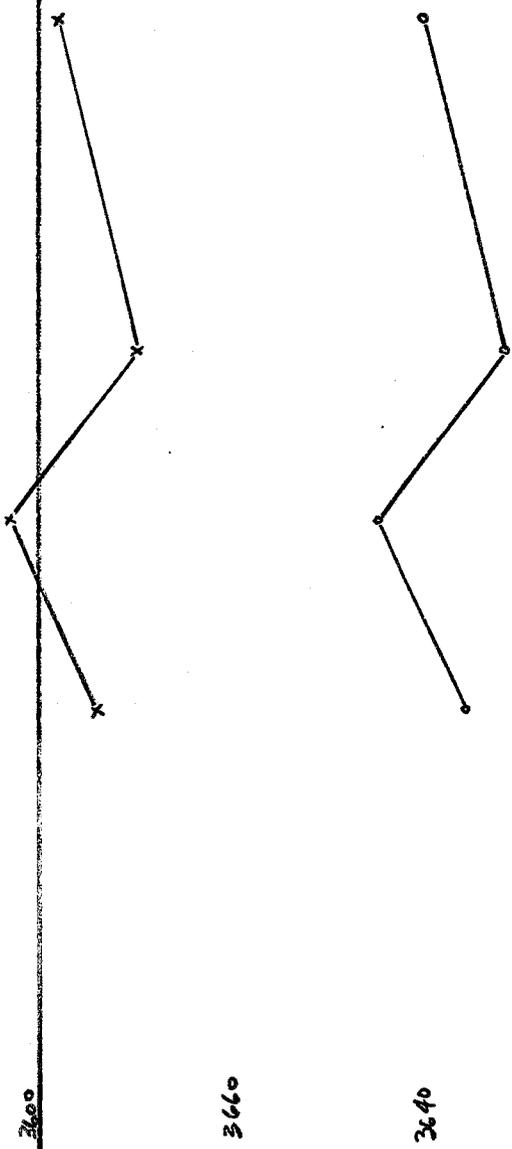
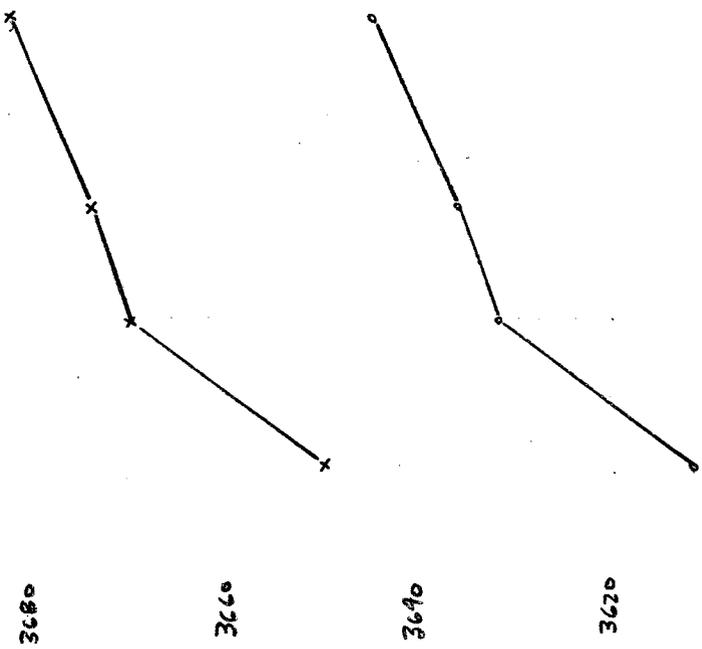
INST: ASKANIA GFZ TORSION  
 (VERTICAL INTENSITY)  
 SCALE CONSTANT = 215.5 / SCALE DIV.  
 ARBITRARY MAGNETIC BASE  
 ALL VALUES ARE CORRECTED FOR  
 DIURNAL DRIFT & PLOTTED IN GAMMAS

DIURNAL CORRECTION CURVE  
 O READING: BASE STA  
 X ADJUSTED VALUES  
 1" = 20 GAMMAS

LINE 124  
 BASE 126,010  
 5/30/72

LINE 129  
 BASE 126,010  
 5/30/72

INST: ASKANIA GFZ TORSION  
 (VERTICAL INTENSITY)  
 SCALE CONSTANT = 215.5 / SCALE DIV.  
 ARBITRARY MAGNETIC BASE  
 ALL VALUES ARE CORRECTED FOR  
 DIURNAL DRIFT & PLOTTED IN GAMMAS



3580  
 3600  
 3640  
 3620  
 3600  
 3660  
 3640  
 3620  
 3600

9:00 10:00 11:00 12:00 1:00 2:00 3:00 4:00

3680

DIURNAL CORRECTION CURVE  
O READING: BASE STA  
X ADJUSTED VALUES  
1" = 20 GAMMAS



3660

LINE 132  
BASE 120, 310  
5/30/72



3640

3620

3600

3600

3600

3620

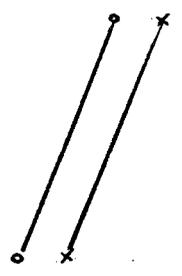
3600

INST: ASKANIA GFZ TORSION  
(VERTICAL INTENSITY)  
SCALE CONSTANT= 215.5 /SCALE DIV.  
ARBITRARY MAGNETIC BASE  
ALL VALUES ARE CORRECTED FOR  
DIURNAL DRIFT & PLOTTED IN GAMMAS

9'00 10'00 11'00 12'00 1'00 2'00 3'00 4'00

DIURNAL CORRECTION CURVE  
 O READING: BASE STA  
 X ADJUSTED VALUES  
 1" = 20 GAMMAS

LINE 50 N  
 BASE 149, 45W  
 6/5/72



3690

3620

3600

3580

3560  
3690

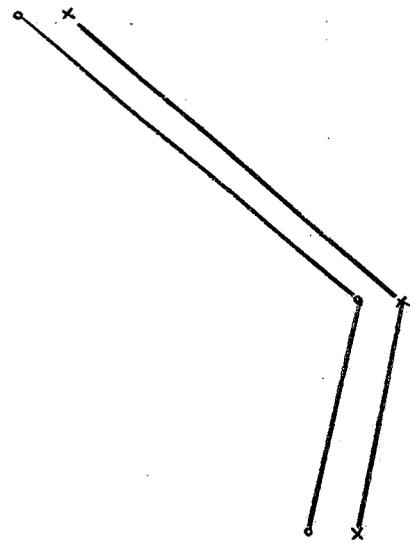
3620

3600

3580

3560

LINE 47 N  
 BASE 149, 45W  
 6/5/72



INST: ASKANIA GFZ TORSION  
 (VERTICAL INTENSITY)  
 SCALE CONSTANT = 215.5 / SCALE DIV.  
 ARBITRARY MAGNETIC BASE  
 ALL VALUES ARE CORRECTED FOR  
 DIURNAL DRIFT & PLOTTED IN GAMMAS

4.00 5.00

3.00

2.00

1.00

12.00

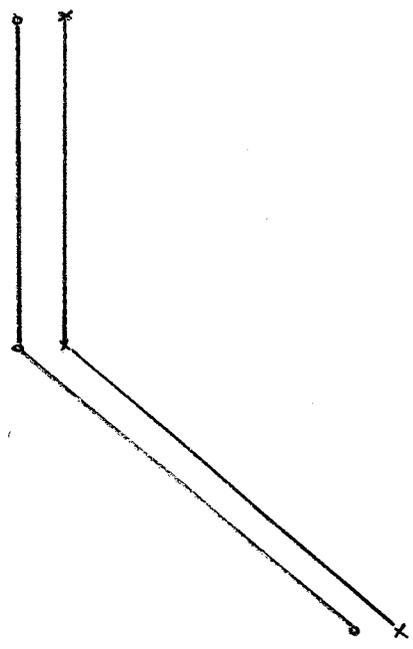
11.00

10.00

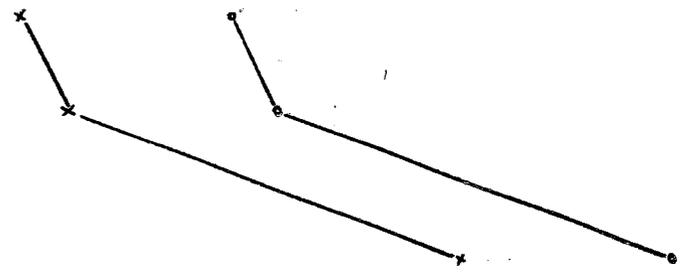
9.00

DIURNAL CORRECTION CURVE  
 O READING: BASE STA  
 X ADJUSTED VALUES  
 1" = 20 GAMMAS

LINE 44 N  
 BASE 149,450  
 6/5/72



LINE 41 N  
 BASE 41,010  
 6/6/72



INST: ASKANIA GFZ TORSION  
 (VERTICAL INTENSITY)  
 SCALE CONSTANT = 215.5 / SCALE DIV.  
 ARBITRARY MAGNETIC BASE  
 ALL VALUES ARE CORRECTED FOR  
 DIURNAL DRIFT & PLOTTED IN GAMMAS

3640

3620

3600

3580

3560  
 3700

3680

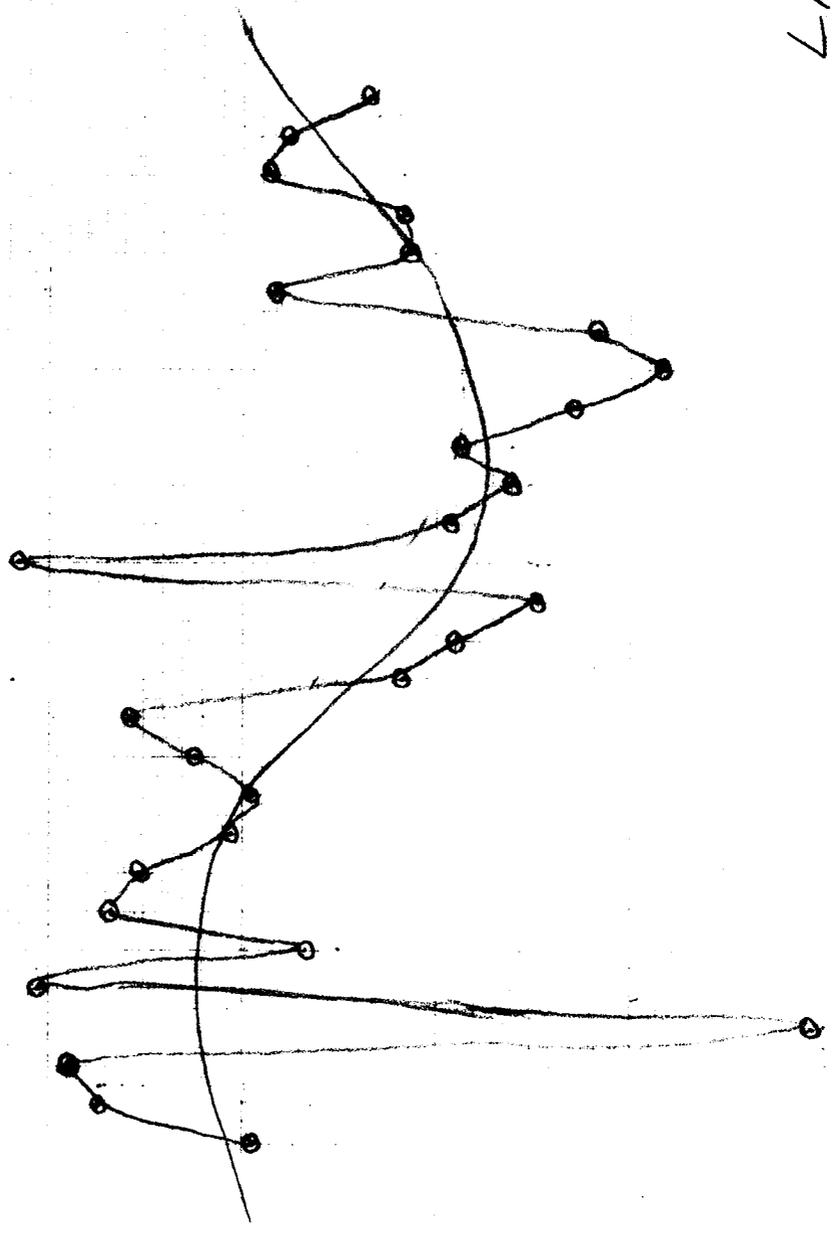
3660

3640

3620

9:00 10:00 11:00 12:00 1:00 2:00 3:00 4:00 5:00

Safford Proj:  
Asxnum 620263  
215.58 Scale  
Constant



4400  
— 4200  
— 4000  
— 3800  
— 3600  
gammmas

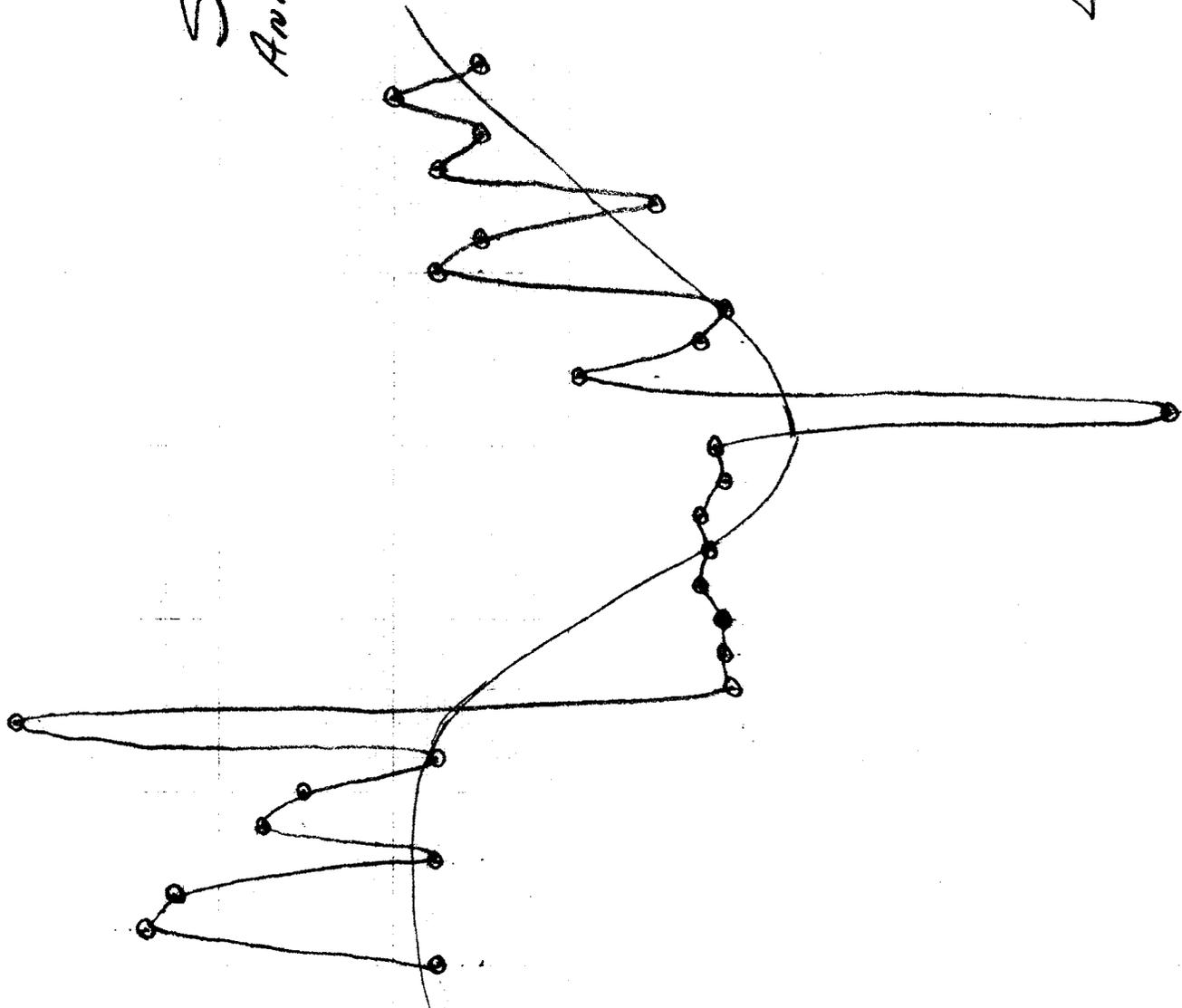
LINE 48+00 E  
Scale H 1"=500'  
U 1"=200'

STATION

— 18+00

Safford Proj.  
Anaconda flux gate

Smooth  
Curve



Line 48 to 0 E  
Scale H  $1\frac{1}{2}$ " = 500'  
V 1" = 200'

1600

1400

1200

1000

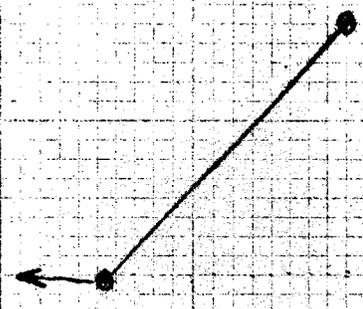
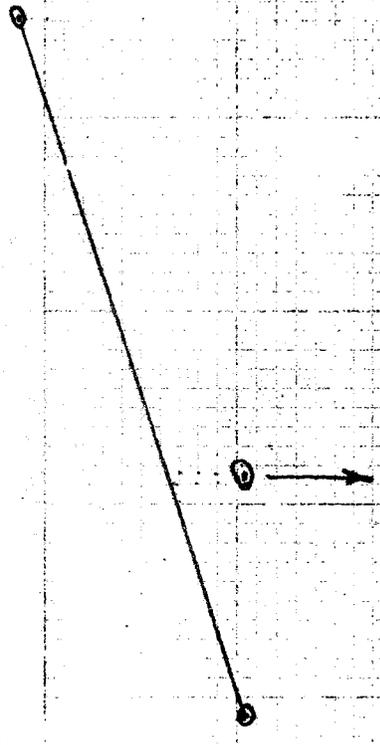
800

600

400

200

Safford Proj.  
Diurnal Correction  
7-12-72



3900

3880

4190

4180

4180

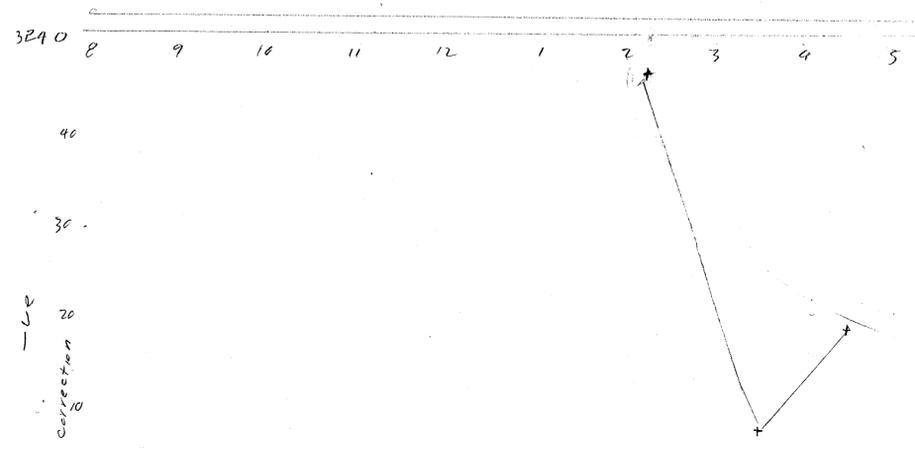
1 2 3 4 5

3290

+ Reading BASELO,00  
x Adjuster Value.

Vertical Component  
Note: Reading at bas. - 20,000

May 5 1972



1" = 200'

May 20

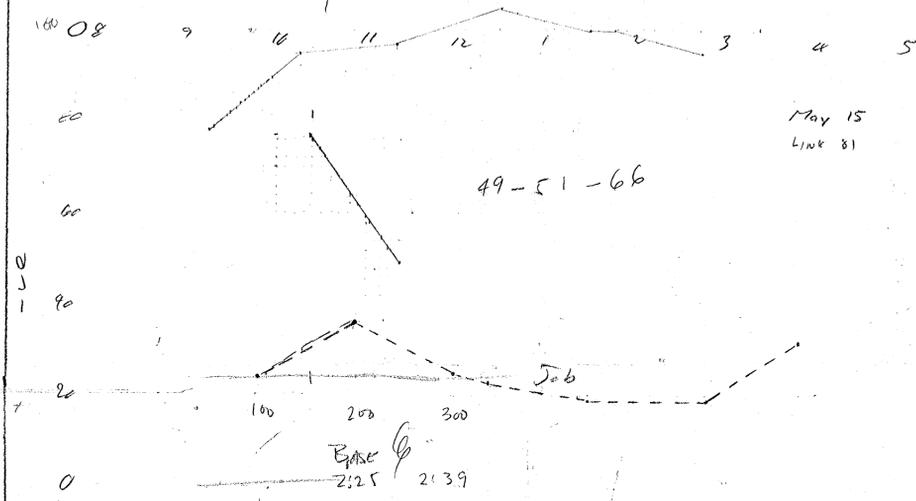
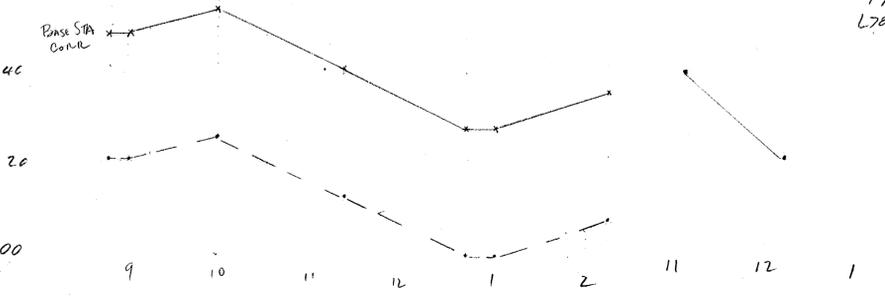
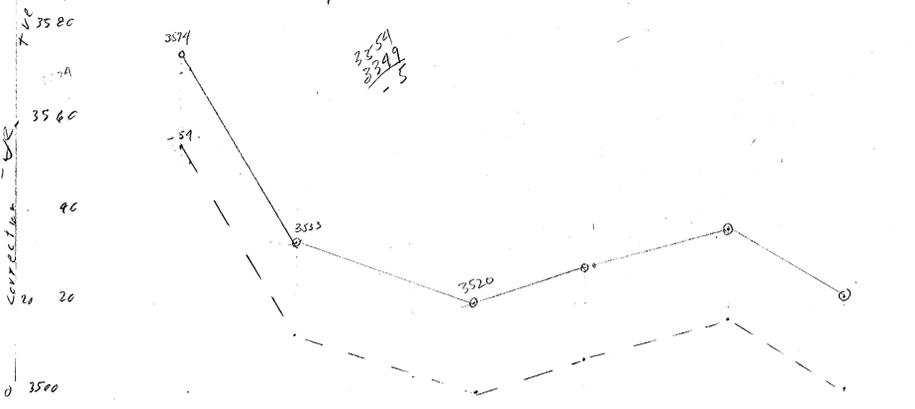
x 72.35  
+ 75.0  
Δ 81  
o 84  
□ 87

Correction Curve

Correction Curve  
- LE

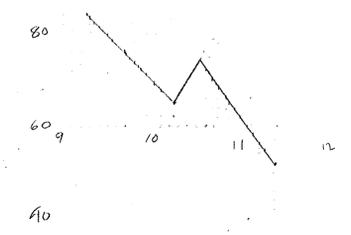
May 10

Base L75 N4,00



49-51-66

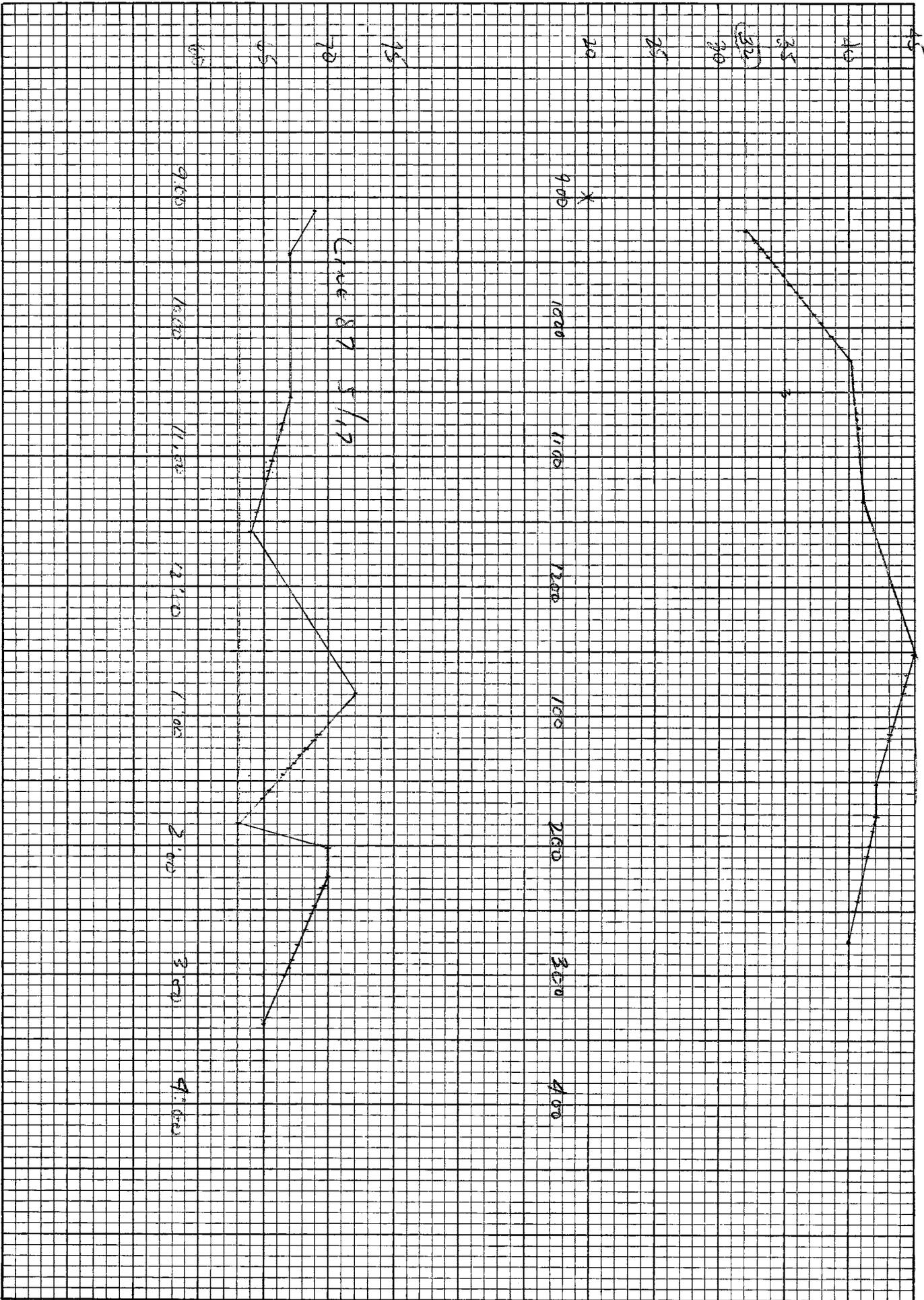
May 15  
Line 81



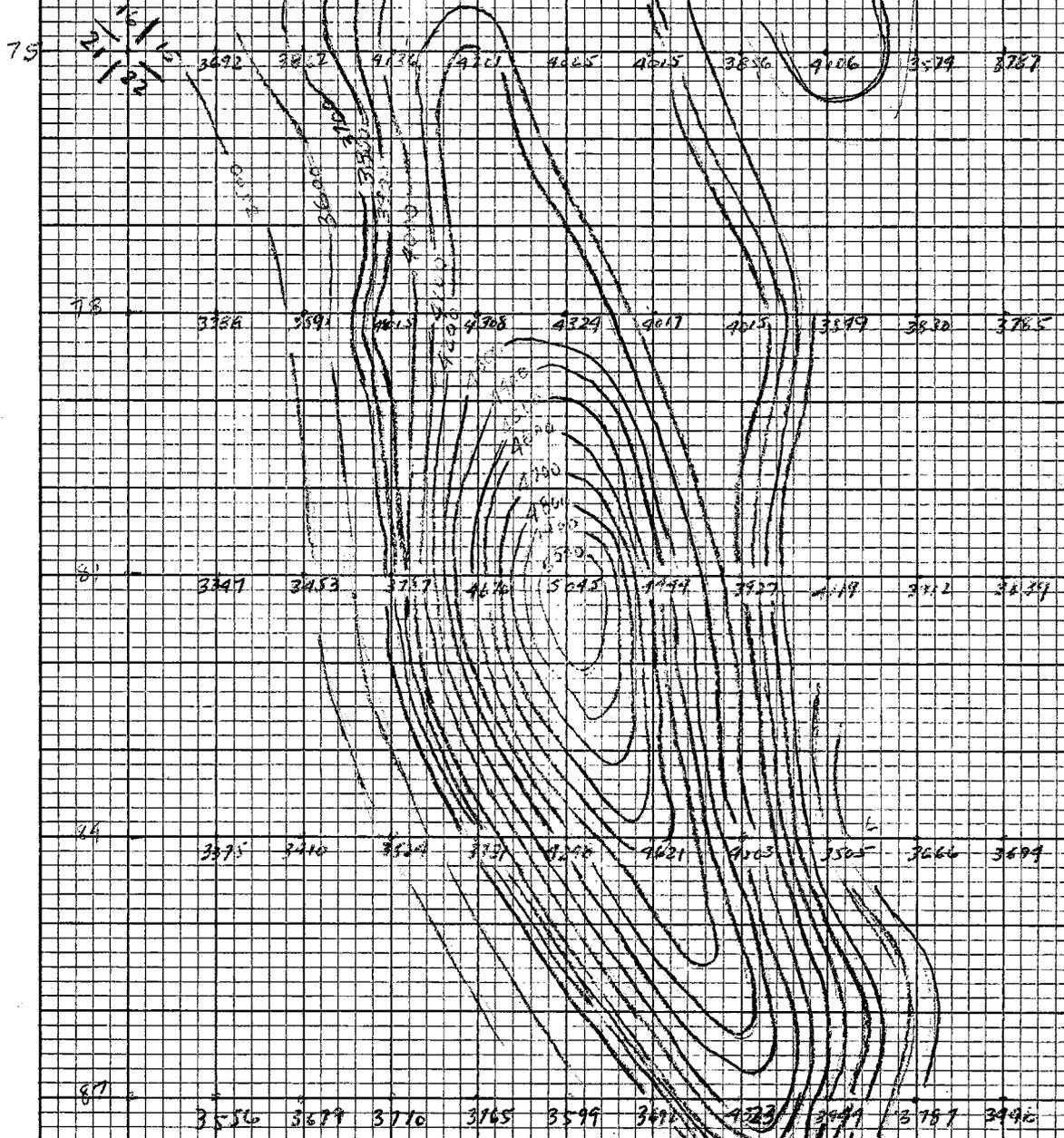
Base  
2125 2139

3414  
11  
3358  
56  
3414

LINE 84 S116



1" = 200'



10 X 12 TO THE INCH 46 1933  
7 X 10 INCHES  
MADE IN U.S.A.  
KEUFFEL & ESSER CO.

0 10 INE 2 3 4 5 6 7 8 9 10 11 NE

KE 10 X 12 TO THE INCH 46 1933  
7 X 10 INCHES  
KEUFFEL & ESSER CO.  
MADE IN U. S. A.

109.10

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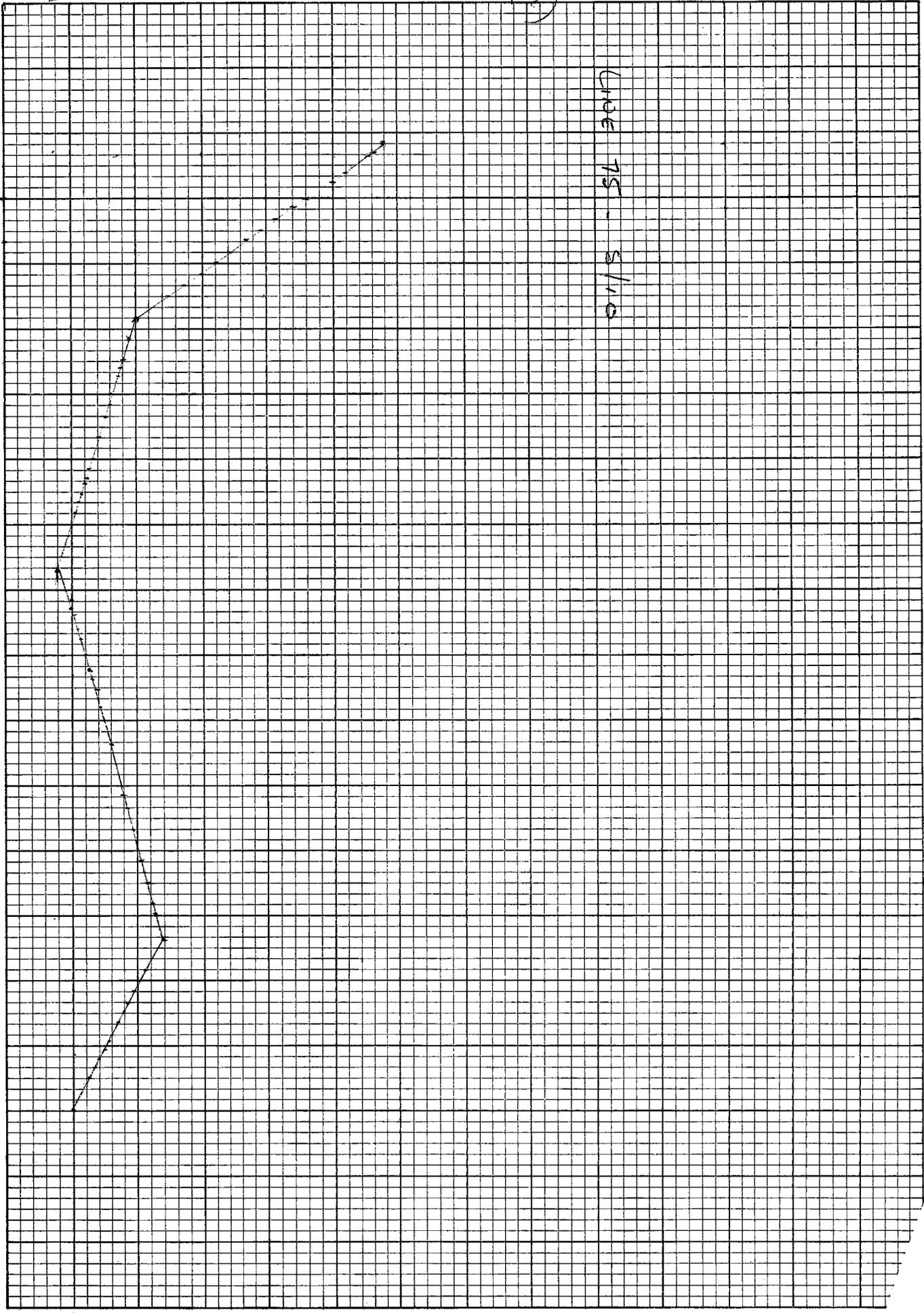
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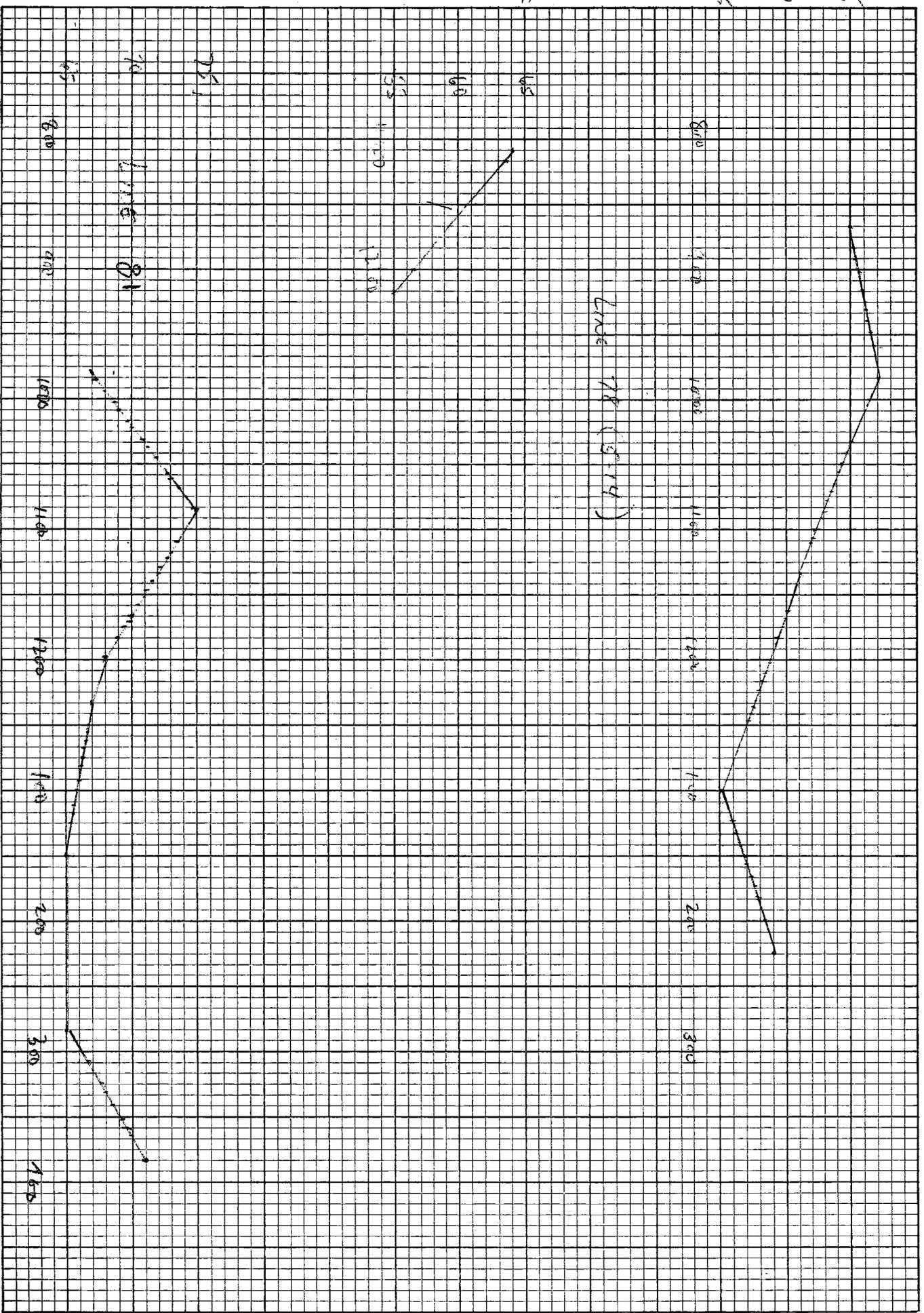
40

26 2/1000  
DIP

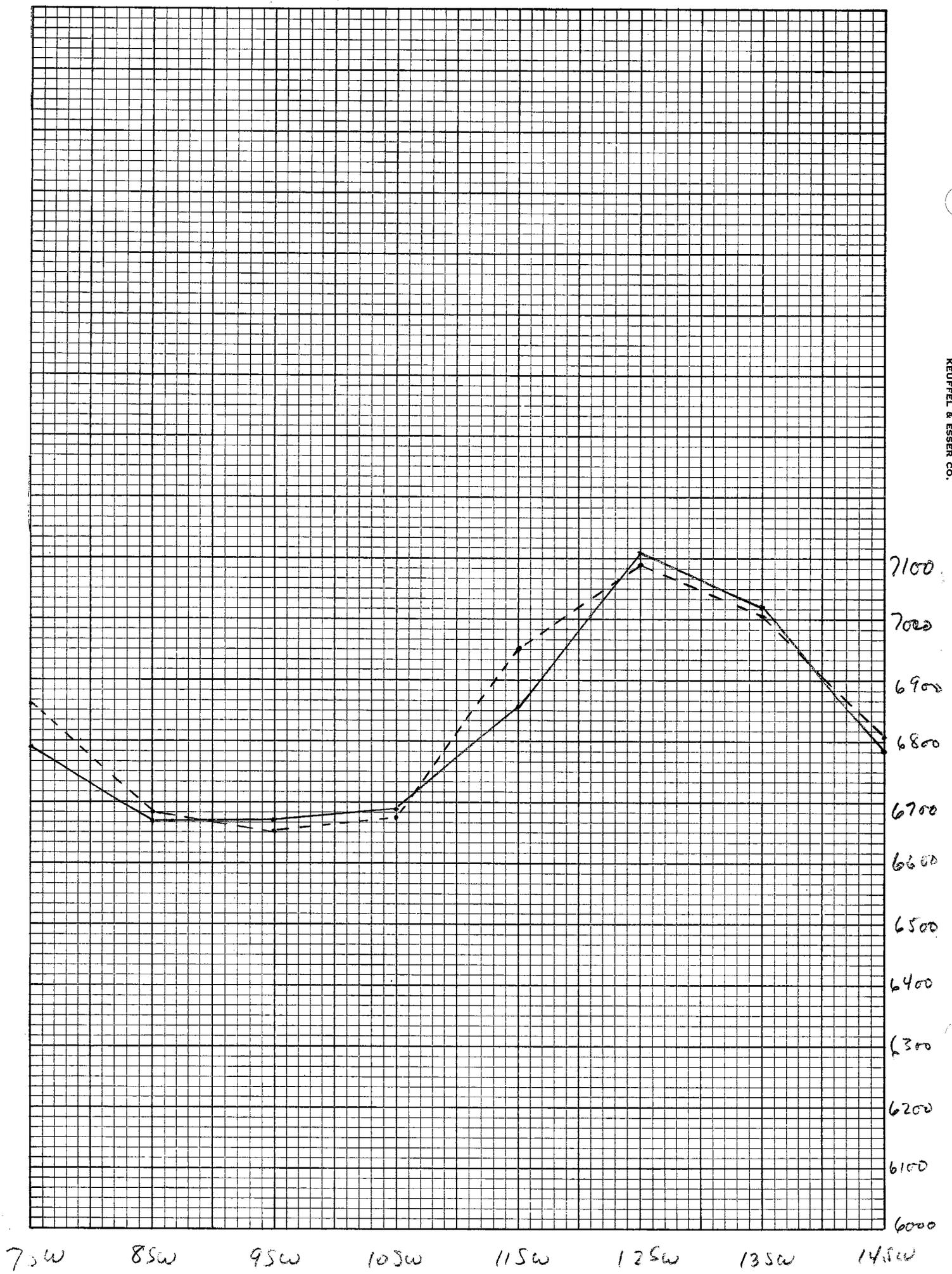
LINE 75 - S/10

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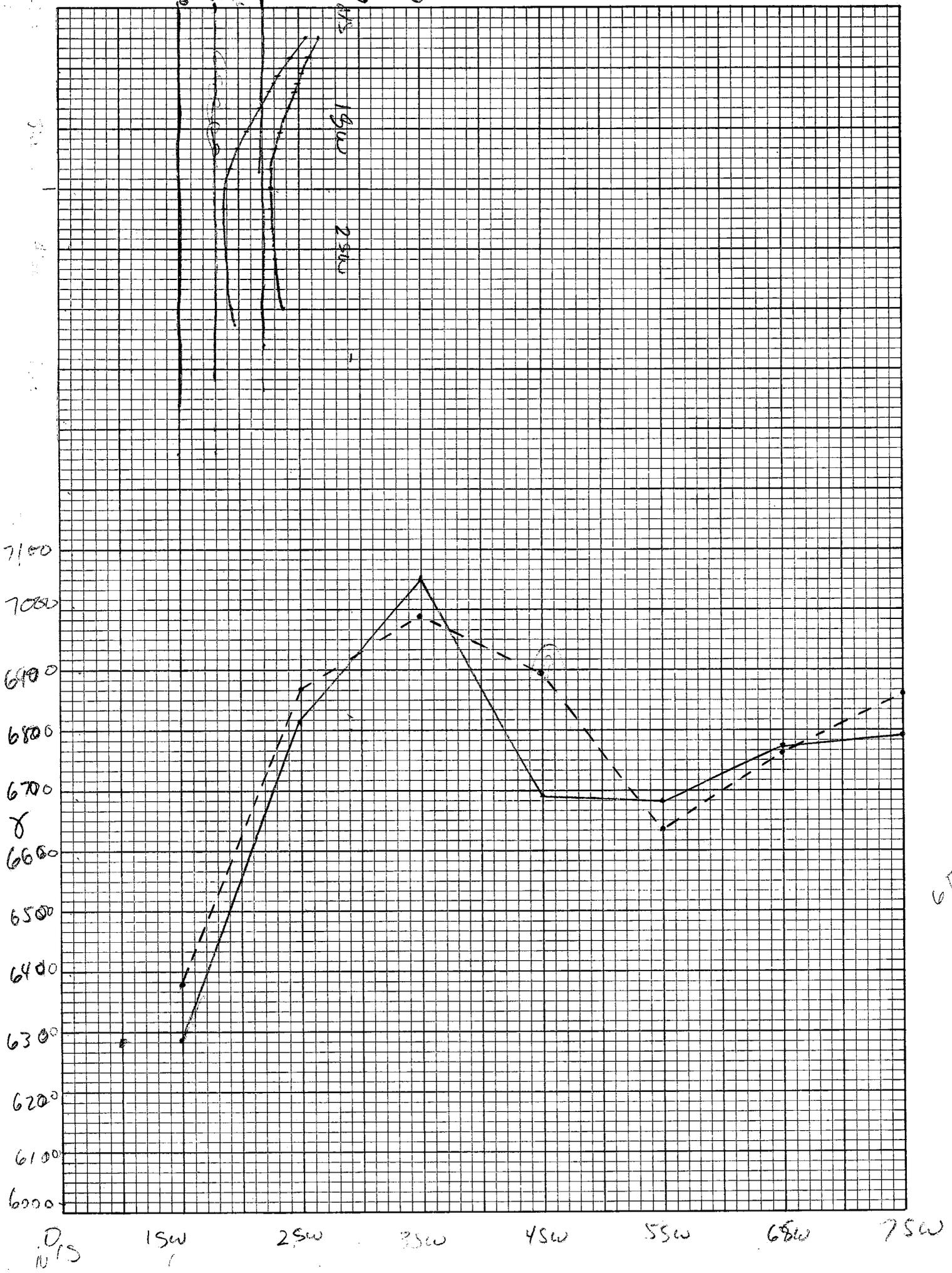




35  
 30  
 25  
 5/14



8



6700  
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 6400  
 6300

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