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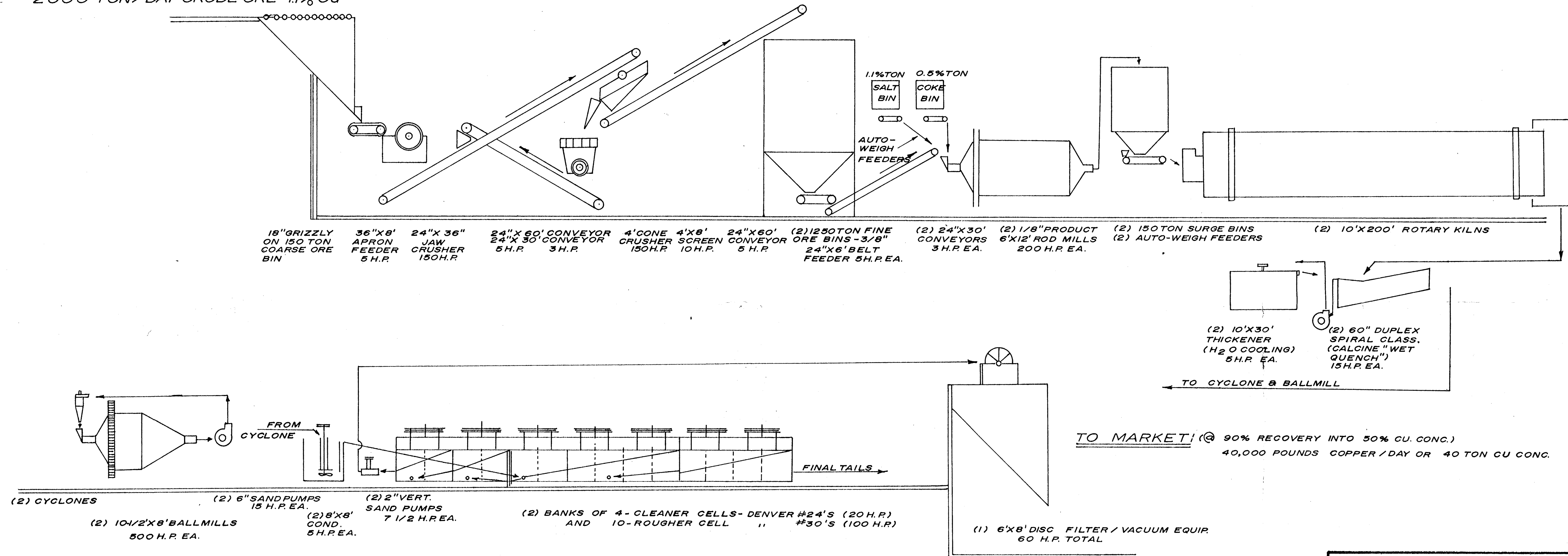
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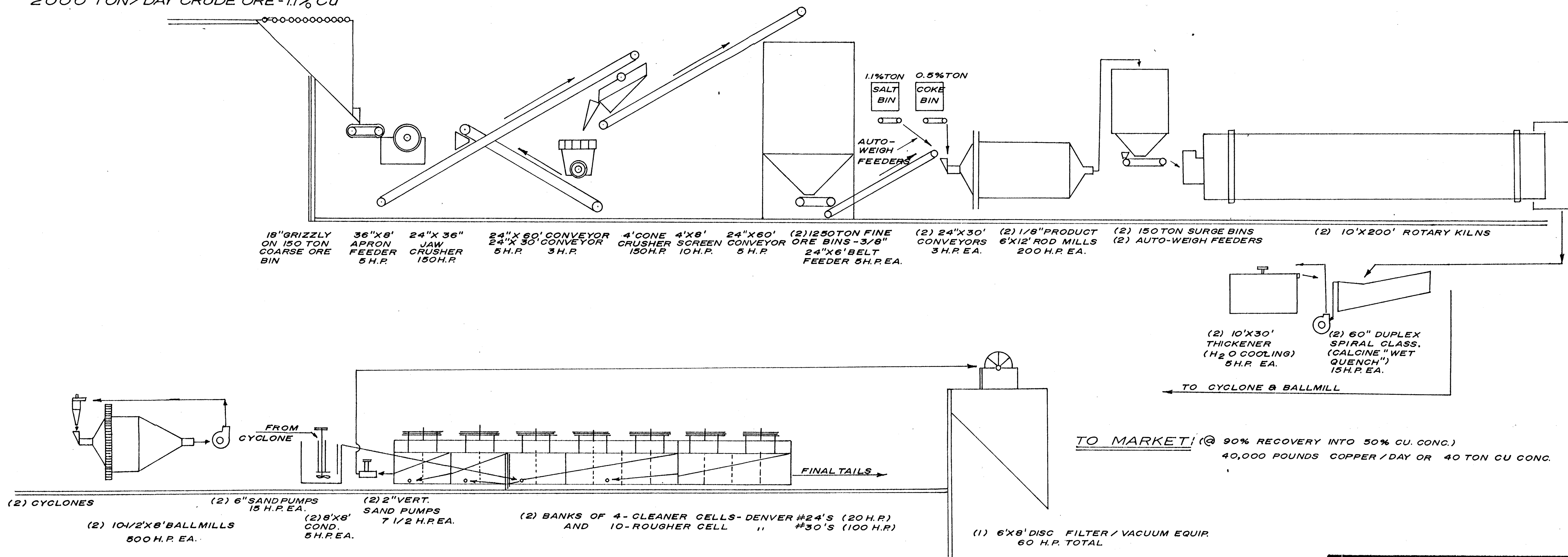
INPUT:
2000 TON/DAY CRUDE ORE - 1.1% CU



CARLOTA MINE
 DIAGRAMMATIC PRELIMINARY FLOWSHEET
 2000 TON/DAY
 SALT-COKE SEGREGATION PLANT AND
 FLOTATION
 G.A.F. 4/25/69

TRAIN LINE

INPUT:
2000 TON/DAY CRUDE ORE - 1.1% CU



18" GRIZZLY ON 150 TON COARSE ORE BIN 36"X36" APRON FEEDER 5 H.P. 24"X36" JAW CRUSHER 150 H.P. 24"X60' CONVEYOR 5 H.P. 24"X30' CONVEYOR 3 H.P. 4' CONE CRUSHER 150 H.P. 4'X8' SCREEN 10 H.P. 24"X60' CONVEYOR 5 H.P. (2) 1250 TON FINE ORE BINS - 3/8" 24"X6' BELT FEEDER 5 H.P. EA. (2) 24"X30' CONVEYORS 3 H.P. EA. (2) 1/8" PRODUCT 6'X12' ROD MILLS 200 H.P. EA. (2) 150 TON SURGE BINS (2) AUTO-WEIGH FEEDERS (2) 10'X200' ROTARY KILNS

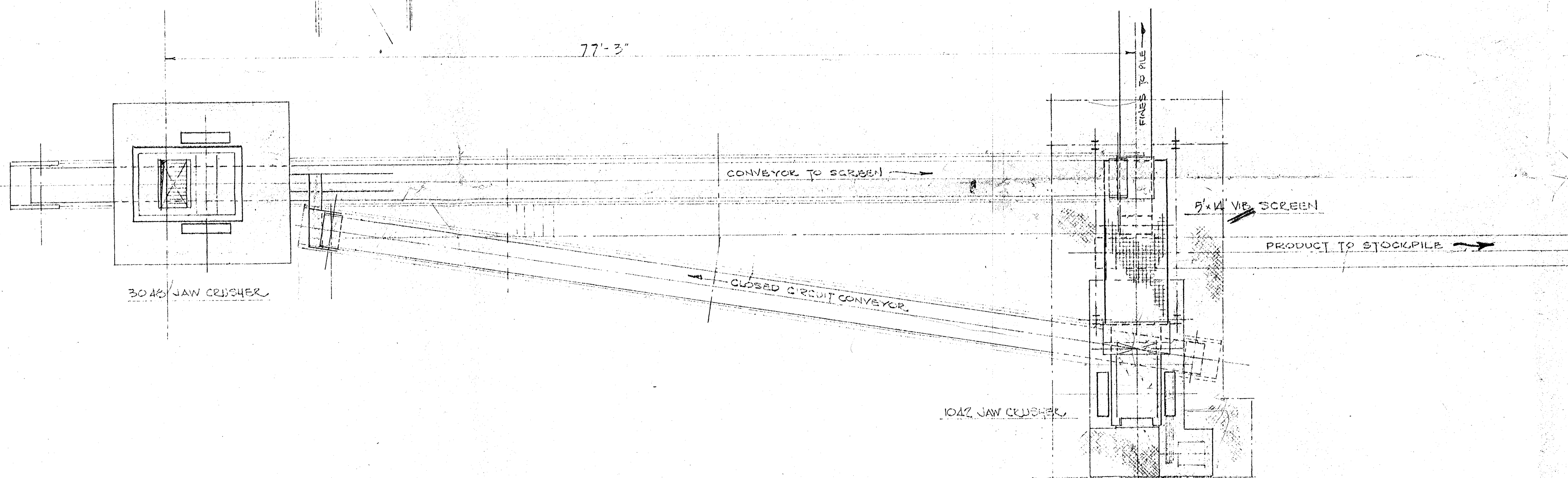
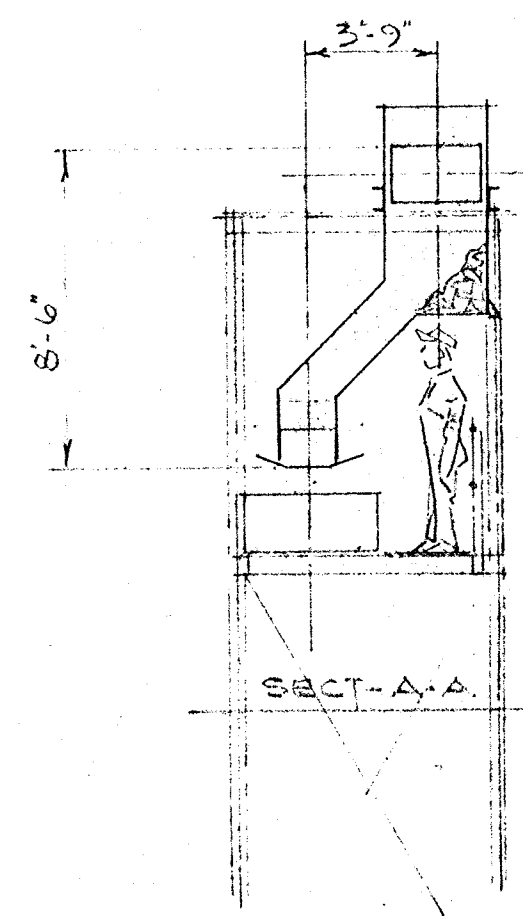
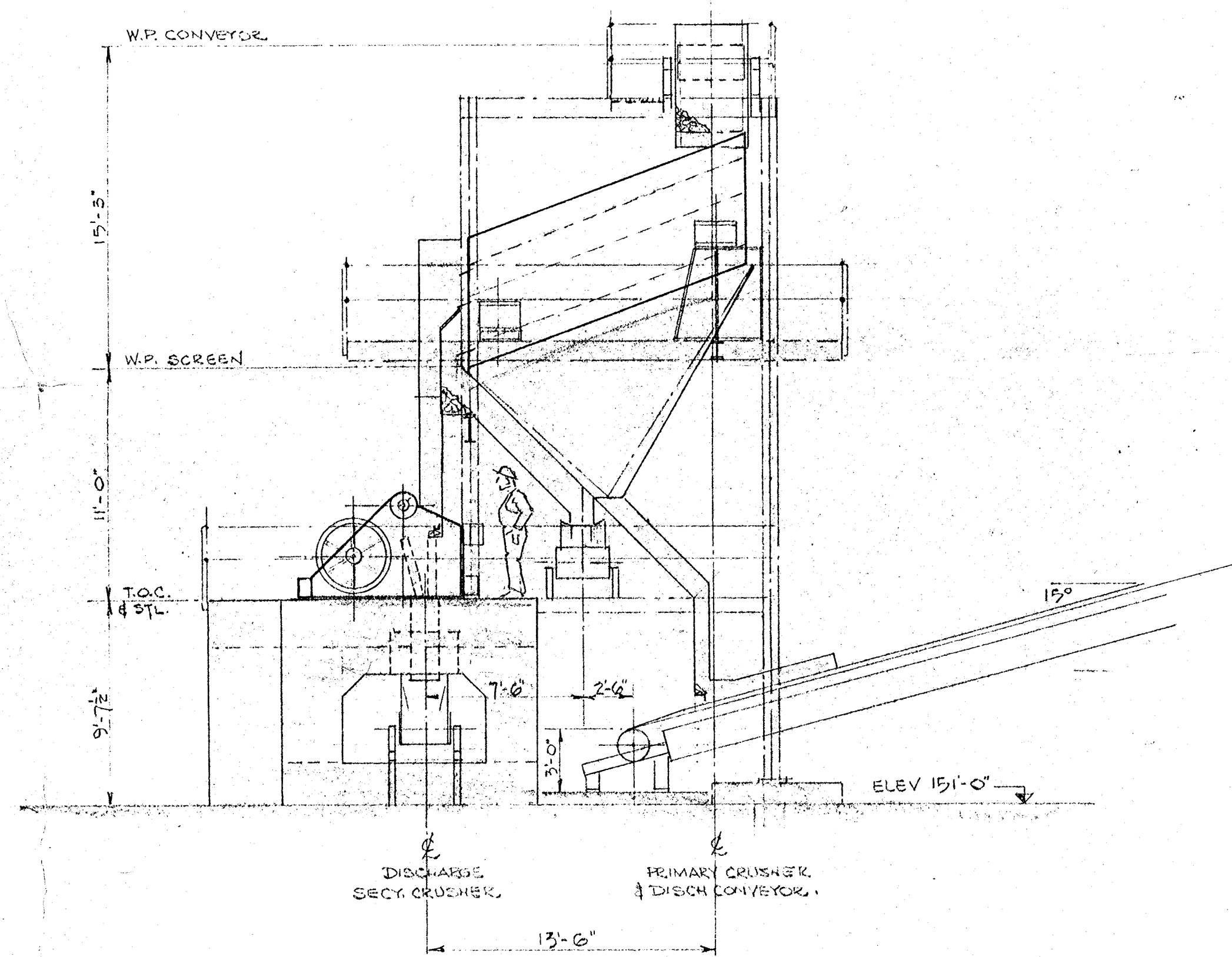
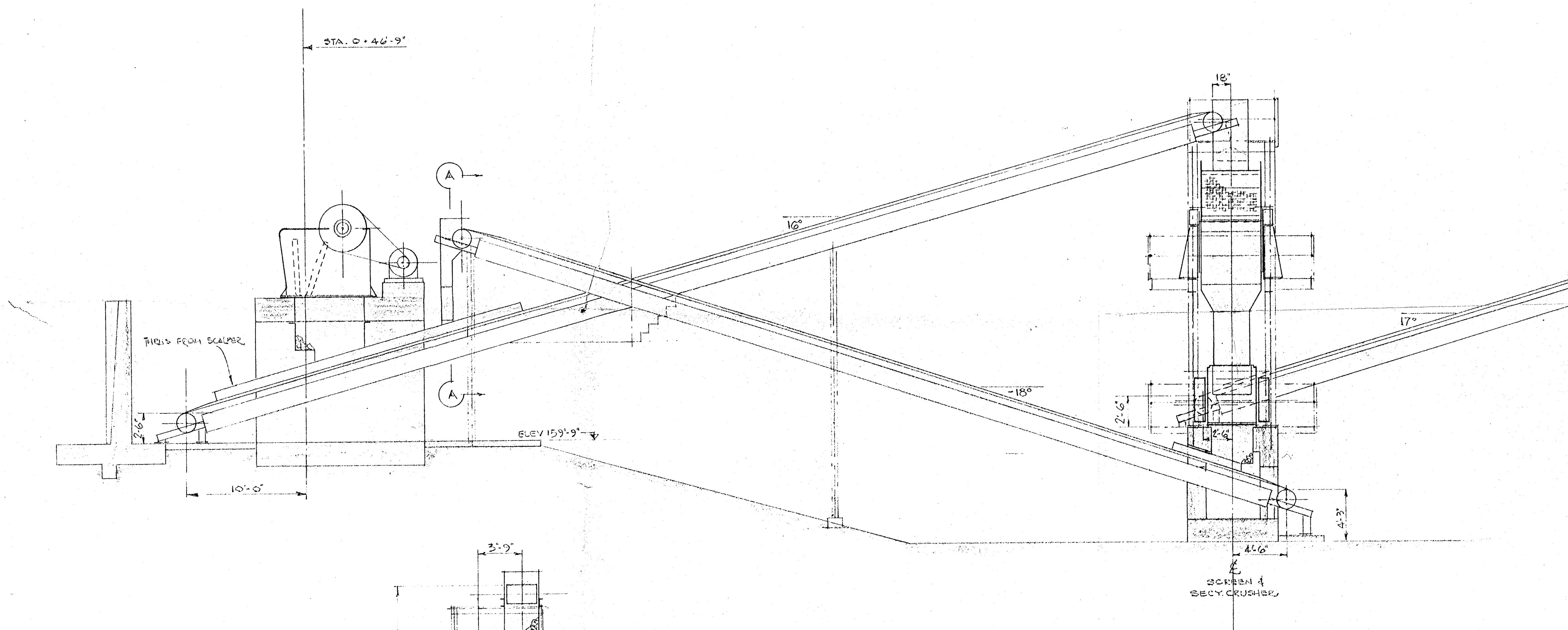
(2) 10'X30' THICKENER (H₂O COOLING) 5 H.P. EA. (2) 60" DUPLEX SPIRAL CLASS. (CALCINE "WET QUENCH") 15 H.P. EA.
TO CYCLONE & BALLMILL

TO MARKET! (@ 90% RECOVERY INTO 50% CU. CONC.)
40,000 POUNDS COPPER / DAY OR 40 TON CU CONC.

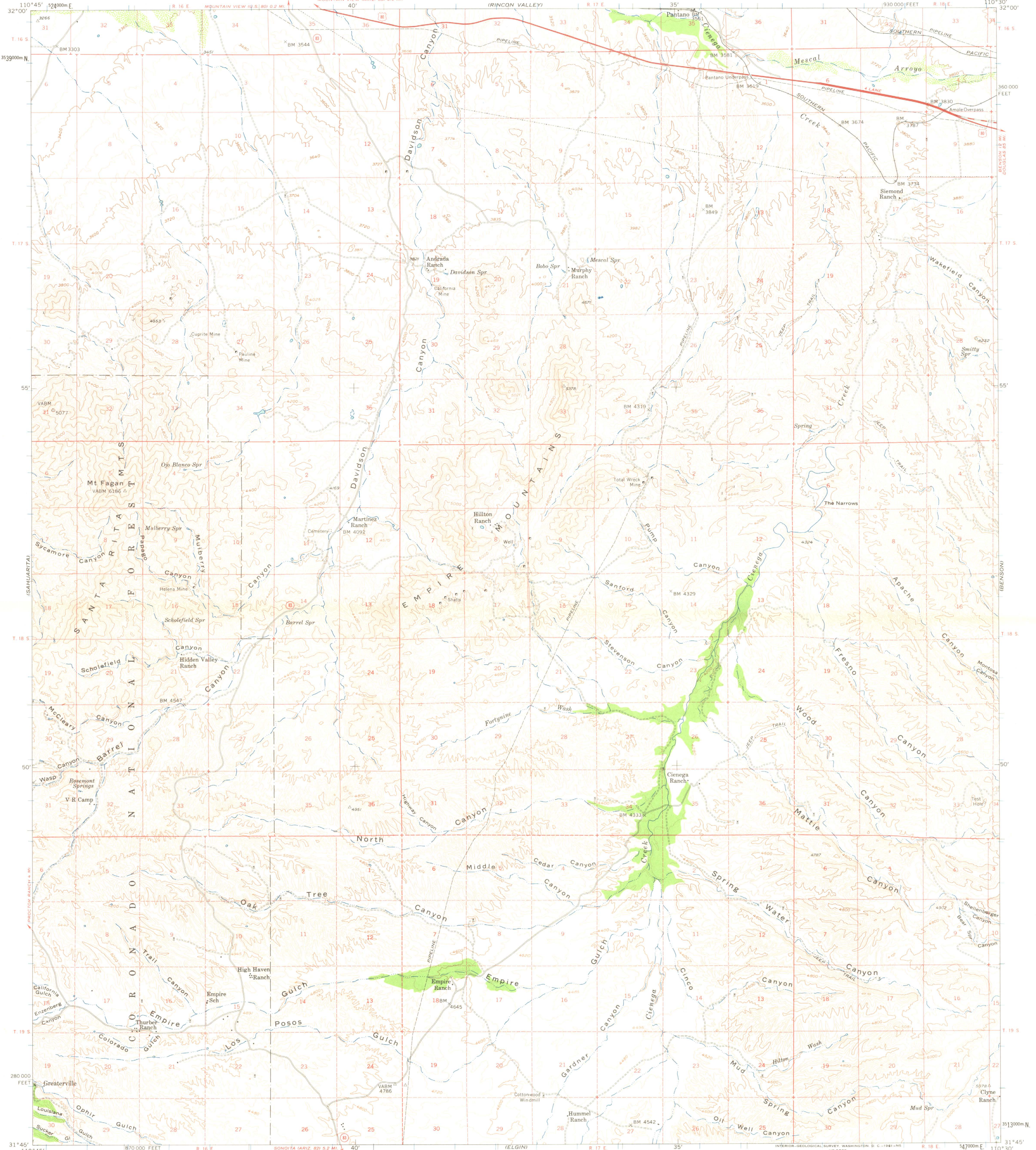
(2) CYCLONES (2) 10 1/2'X8' BALLMILLS 500 H.P. EA. (2) 6" SAND PUMPS 15 H.P. EA. (2) 8'X8' COND. 5 H.P. EA. (2) 2" VERT. SAND PUMPS 7 1/2 H.P. EA. (2) BANKS OF 4-CLEANER CELLS-DENVER #24'S (20 H.P.) AND 10-ROUGHER CELL " #30'S (100 H.P.) (1) 6'X8' DISC FILTER / VACUUM EQUIP. 60 H.P. TOTAL

CARLOTA MINE
DIAGRAMMATIC PRELIMINARY FLOWSHEET
2000 TON/DAY
SALT-COKE SEGREGATION PLANT AND FLOTATION
G.A.F. 4/25/69

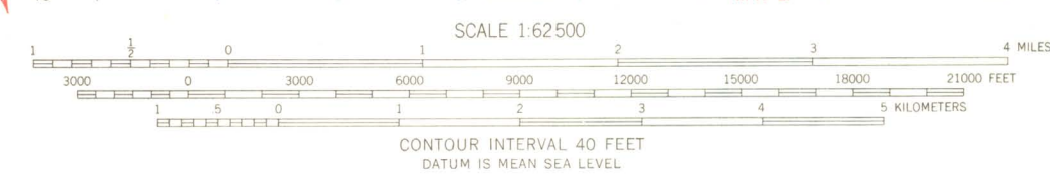
T.M. LINDSAY



PROPOSED LAYOUT OF
PRIMARY & SECONDARY CRUSHERS.



Mapped, edited, and published by the Geological Survey
Control by USGS, USC&GS and USCE
Topography from aerial photographs by ER-55 plottter
Aerial photographs taken 1955. Field check 1958
Polyconic projection. 1927 North American datum
10,000-foot grid based on Arizona coordinate system, central zone
1000-meter Universal Transverse Mercator grid ticks,
zone 12, shown in blue
Dashed line indicates approximate locations
Unchecked elevations are shown in brown



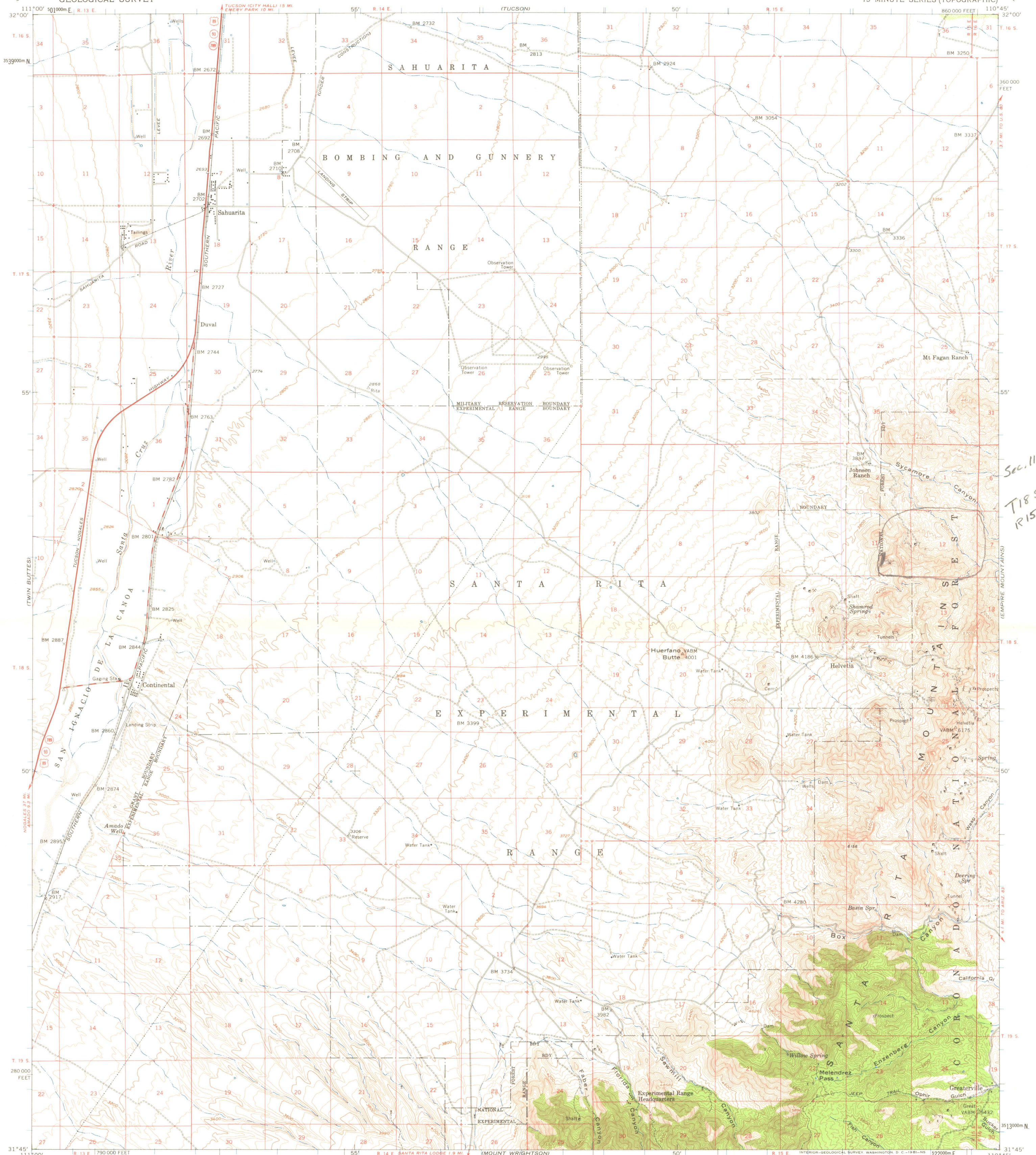
ROAD CLASSIFICATION

Heavy-duty	Light-duty
Medium-duty	Unimproved dirt
U.S. Route	State Route

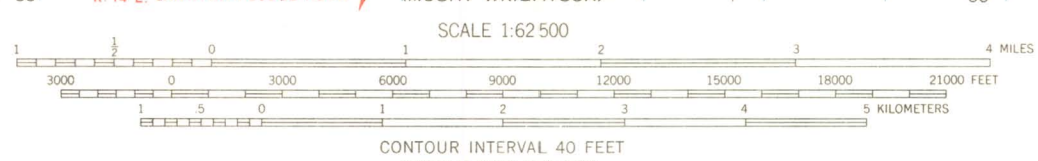


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A FOLDER DESCRIBING TOPOGRAPHIC MAPS AND SYMBOLS IS AVAILABLE ON REQUEST

EMPIRE MOUNTAINS, ARIZ.
N3145-W1030/15
1958



Mapped, edited, and published by the Geological Survey
Control by USGS and USC&GS
Topography from aerial photographs by ER-55 plottter
Aerial photographs taken 1955-1956. Field check 1958
Polyconic projection. 1927 North American datum
10,000-foot grid based on Arizona coordinate system, central zone
1000-meter Universal Transverse Mercator grid ticks,
zone 12, shown in blue
Dashed land lines indicate approximate locations
Unchecked elevations are shown in brown



ROAD CLASSIFICATION

Heavy-duty	Light-duty
Medium-duty	Unimproved dirt
U.S. Route	State Route



THIS MAP COMPLIES WITH NATIONAL MAP ACCURACY STANDARDS
FOR SALE BY U. S. GEOLOGICAL SURVEY, DENVER 25, COLORADO OR WASHINGTON 25, D. C.
A FOLDER DESCRIBING TOPOGRAPHIC MAPS AND SYMBOLS IS AVAILABLE ON REQUEST

SAHUARITA, ARIZ.
N3145-W11045/15
1958

① Yamapai
schist - sch - 45°
to core axis.

oxidized ^{leucite} &
② malachite

Schistosity 80° to
core axis - mod
③ oxidized

Schistosity 50°
④ some diss -
mal.

Schistosity 45° &
⑤ some blebs
of calcite.
mal.
Some flow structure
to breccia

⑥ flow str. 45° to
axis

Same as prior

①

Schint with
some q/t_3

②

50° to core
axis

③

Schint

④

Stop Sch

60% c.n.

⑤

OXid. +
mal. +

⑥

q/t_3 +

Schint

13

fresh shirt

14

fresh.
shirt
sweat

15

shirt
60%

16-17

shirt
mol.

GEOLOGY AND ORE DEPOSITS OF THE GLOBE-MIAMI DISTRICT, ARIZONA

By N. P. PETERSON

ABSTRACT

The rocks of the Globe-Miami district range from lower Precambrian to Recent. The oldest formation, the Pinal schist, comprises several varieties of schist formed by dynamic and thermal metamorphism of shale and feldspathic sandstone during the early Precambrian Mazatzal revolution. During the later stages of this revolution, the schist was intruded by a complex of dioritic rocks and by plutons of granite and quartz monzonite. There were extensive intrusions of a biotite-quartz diorite, known as the Madera diorite, mainly south of the district. In the northern part of the mapped area, the schist was invaded by an extensive mass, the Ruin granite, which is a coarse-grained rock most commonly of quartz monzonitic composition. There are also smaller sill-like masses of slightly gneissic muscovite granite.

Upper Precambrian sedimentary rocks of the Apache group rest unconformably on the deeply eroded surface of the Pinal schist and intruded igneous rocks. The group consists of the very thin Scanlan conglomerate at the base, Pioneer formation, Barnes conglomerate, Dripping Spring quartzite, Mescal limestone, and one or more thin flows of olivine basalt at the top.

The Apache group is separated from the Troy quartzite (Middle Cambrian) by an erosional disconformity; and the Troy was completely removed by erosion from a large part of the district before the Martin limestone of Devonian age was deposited. The younger Paleozoic rocks are represented by the Escabrosa limestone (Mississippian) and the lower part of the Naco limestone (Pennsylvanian).

There are no sedimentary rocks representing the Mesozoic era, but igneous activity probably began in Late Cretaceous time and continued into the early part of the Tertiary period. The Solitude granite, Willow Spring granodiorite, and the granodiorite in Gold Gulch have been tentatively assigned to this interval, but they intrude only the Pinal schist, and their ages are therefore uncertain. They may be older than Cretaceous and may even be early Precambrian. Of more certain age are the Lost Gulch quartz monzonite, extensive sills and dikes of diabase intruded mainly into the formations of the Apache group, many small dikes and sills of diorite porphyry, the Schultze granite with its granite porphyry facies, and many small isolated bodies of granite porphyry which probably were about contemporaneous with and related to the Schultze granite.

Local accumulations of erosional detritus known as the Whitetail conglomerate and an overlying thick sheet of dacitic volcanic rocks, probably Tertiary in age, rest unconformably on the extensively faulted and deeply eroded older formations. A thick blanket of the Gila conglomerate of Pliocene and early Pleistocene age, locally intercalated with thin flows of olivine basalt, filled the valley between the Pinal Mountains and Apache Peaks. In places the conglomerate is more than 4,000

feet thick and at one time, it probably mantled the entire district, but it is now being rapidly worn away by erosion.

There are strong angular unconformities at the bases of the Apache group, the Whitetail conglomerate and associated dacite, and the Gila conglomerate, and erosional disconformities occur at the bases of the Troy quartzite, the Martin limestone, and probably at the base of the Naco limestone, but the strata of the Apache group and those of Paleozoic age are essentially conformable.

The structural features of the upper Precambrian and younger formations are predominantly the results of block faulting and other displacements during the intrusion of thick dikes and sills of diabase magma. The earliest recognized faulting began at some time later than the Pennsylvanian period, and the fundamental fault pattern probably had formed by the time the diabase was intruded. Faulting continued into Quaternary time with recurrent movements on many of the major faults.

Parts of three major structural blocks are in the mapped area: the Globe Hills block, the Globe Valley block, and the Inspiration block. The Globe Hills block includes the northeastern half of the Globe quadrangle. It is bounded on the southwest side by the Pinal Creek fault system, a broad zone of step faults. Some faults in the block are older and some are younger than the diabase; the largest are the northeastward-trending faults of the Old Dominion system and the Copper Gulch, Cuprite, Budget, and McGaw faults, which strike north to northwest.

The Globe Valley block is a graben inset between the Globe Hills block to the northeast and the Inspiration block to the west. The west boundary is clearly defined by the Miami fault, which is known to have a throw of about 1,500 feet at the east end of the Miami-Inspiration ore body. Little is known concerning the structural details of the bedrock in the block, for the structural basin was filled with Gila conglomerate. The basin provides most of the water supply for domestic and industrial use in the district.

The Inspiration block includes the part of the district west of the Miami fault. The Schultze granite is the principal rock in the southern part of the block, and near it are grouped the large disseminated-copper deposits of the district. Relatively few faults have been recognized in this area, and most of the larger ones trend north to northwest. The Castle Dome and Copper Cities horsts are the most prominent structural features. In the northern part of the block, faults with northwest strikes are most numerous, and their net effect has been to depress blocks progressively to the northeast so as to repeat outcrops of rocks of similar age from southwest to northeast. The boundary between the northern and southern parts of the block, though poorly defined, appears to be a zone of major vertical displacement, probably along an intrusive contact between the Pinal schist and Ruin granite.

Mining in the Globe-Miami district began after the Globe claim was located on the Old Dominion vein in 1874, but owing to the remoteness of the region, interest centered for a time on the many small silver and gold deposits of the area. The production of copper was insignificant until 1882, when active mining was started on the Old Dominion and Buffalo veins. Development of the large, low-grade, disseminated-copper deposits began in 1904 and large-scale production in 1911. At the end of 1953, the mines of the district had produced about 6,121 million pounds of copper and minor amounts of gold, silver, lead, and zinc, having a total value of more than \$1 billion.

Most of the productive deposits are of hydrothermal origin subsequently enriched by supergene processes; however, some with substantial yields of copper were deposited by cold meteoric solutions. The deposits of hydrothermal origin are of two main types: disseminated-copper or "porphyry-type" deposits and vein, or lode, deposits. There are several different kinds of vein and lode deposits, but only the simple copper-bearing veins are of major economic importance.

The large disseminated-copper deposits account for more than 80 percent of the total value of the metals credited to the district. The Miami-Inspiration ore body, by far the largest, is partly in the granite porphyry facies of the Schultze granite, but most of it is in the adjacent Pinal schist, whereas the Castle Dome and Copper Cities ore bodies are in the Lost Gulch quartz monzonite. The gangue is chiefly the original minerals of the host rocks and the minerals produced by their hydrothermal alteration, mainly quartz, sericite, and clay minerals. The protore consists chiefly of pyrite and chalcopyrite and very minor amounts of molybdenite, sphalerite, galena, and bornite. The ore bodies were formed by supergene replacement of chalcopyrite and pyrite by chalcocite and covellite. Most of the supergene enrichment in the Miami-Inspiration deposit occurred during a period of erosion and weathering that preceded the eruption of dacite. During the present cycle, erosion removed most of the cover of dacite and Gila conglomerate and also the leached capping from parts of the ore body. The copper sulfides have been extensively altered to carbonates and silicates in the exposed parts. The replacement of the Castle Dome and Copper Cities deposits has occurred during the present cycle of erosion, and the effects are not as complete as in the Miami-Inspiration deposit. The ore contains much unreplaced chalcopyrite and pyrite and very little copper in the form of oxidized minerals.

The largest vein deposits are along the Old Dominion vein system, from which metals, mainly copper, valued at about \$152 million have been produced. Other similar, but smaller, deposits are the Great Eastern, Buckeye-Black Oxide, Dime, Stonewall, Big Johnnie, Maggie, Josh Billing, and Buffalo veins. All were formed by replacement of breccia and wall rock along faults and fissures that cut the upper Precambrian and Paleozoic sedimentary rocks and intruded bodies of diabase. The principal hypogene vein minerals are quartz, pyrite, chalcopyrite, bornite, and specular hematite. The upper parts of all the veins have been enriched or altered by supergene processes and contain chalcocite, covellite, cuprite, and copper carbonates and silicates. Many of the near-surface ore bodies contained only oxidized minerals.

All other types of vein deposits are of minor commercial importance and are in the areas bordering the main centers of copper mineralization. They include several small zinc-lead veins, zinc-lead-vanadium-molybdenum veins, manganese-zinc-lead-silver veins, many narrow stringers containing native silver

and gold in their oxidized zones, and a group of small molybdenite-bearing veins.

Copper deposits formed by circulating ground-water include several ore bodies. The six major deposits of this type have produced copper valued at about \$7 million. The ore consists of copper carbonates and silicates that replaced tuffaceous conglomerate and dacite along fracture zones or filled interstices between breccia fragments along faults in schist, diabase, or granite.

All the productive mineral deposits of the Globe-Miami district, the Pioneer district, and several smaller nearby districts to the northeast and southwest, are in a northeastward-trending belt about 6 miles wide. Within the belt several large areas underlain by Tertiary(?), Tertiary, and Quaternary rocks, younger than the period of mineralization, may include other ore bodies in the underlying older rocks.

INTRODUCTION

LOCATION, CULTURE, AND ACCESSIBILITY

The Globe-Miami mining district, in the lower foothills of the Pinal and Apache Mountains, in Gila County, Ariz., is an area of indefinite extent, most of which is included in the Globe, Inspiration, and the northern part of the Pinal Ranch 7½-minute quadrangles, as mapped by the U.S. Geological Survey in 1945. The location of the mapped area is shown on figure 1.

Globe, the county seat, and Miami are the largest towns of the district. Their populations, according to the census of 1950, are 6,419 and 4,320 respectively. Globe, Miami, and the nearby smaller settlements of Claypool, Central Heights, Midland City, and Inspiration have a total population of about 18,000. They all depend largely on the copper-mining operations of the district, but also serve many outlying ranches and are the centers of an extensive cattle-raising industry.

Globe and Miami are the hub of several main highways. U.S. Highway 60-70 connects the district with Phoenix 86 miles to the west. Northeastward from Globe U.S. 60 crosses the Salt River to Show Low and Springerville, and southeastward U.S. 70 to Safford connects with U.S. 80 at Lordsburg, N. Mex. State Route 77 runs south to Winkelman and Tucson, and the Apache Trail (State Route 88) runs northwest to Roosevelt Dam and thence to Apache Junction where it joins U.S. 60-70.

The Gila Valley, Globe, and Northwestern Railroad, a branch of the Southern Pacific system, has its terminus at Globe and connects with the main line of the system at Bowie. From Globe a branch line serves the copper mines and smelter at Miami.

Electric power for domestic and commercial use is supplied by diesel plants of the Arizona Public Service Co., and power for industrial use is produced by steam plants of the Miami Copper Co. and the Inspiration Consolidated Copper Co. and by the hydroelectric plant

FIELDWORK AND ACKNOWLEDGMENTS

The fieldwork in the Globe-Miami district began in July 1943, when the Geological Survey undertook a detailed study of the Castle Dome area in connection with the development of the Castle Dome copper deposit. An area of about 6 square miles was mapped at a scale of 1:2,400 on a photogrammetric base map supplied by the Castle Dome Copper Co. The fieldwork was completed in September 1944, and maps and descriptions of the copper deposit were published in 1951 (Peterson, Gilbert, and Quick).

When this project had been completed, it was decided to extend the detailed study to include the entire Globe-Miami district. Areal mapping was done on a scale of 1:12,000 on a photogrammetric base prepared by the Geological Survey. Fieldwork continued at various intervals until June 1953. C. M. Gilbert, G. L. Quick, J. P. Albers, J. V. N. Dorr, 2d, Waldemere Bejnar, D. W. Peterson, Leonid Bryner, H. C. Rainey, and J. C. McKallor assisted with the fieldwork and preparation of reports at various times.

It is a pleasure to acknowledge the cordial cooperation of the local executives of the various operating companies and their technical staffs. Special acknowl-

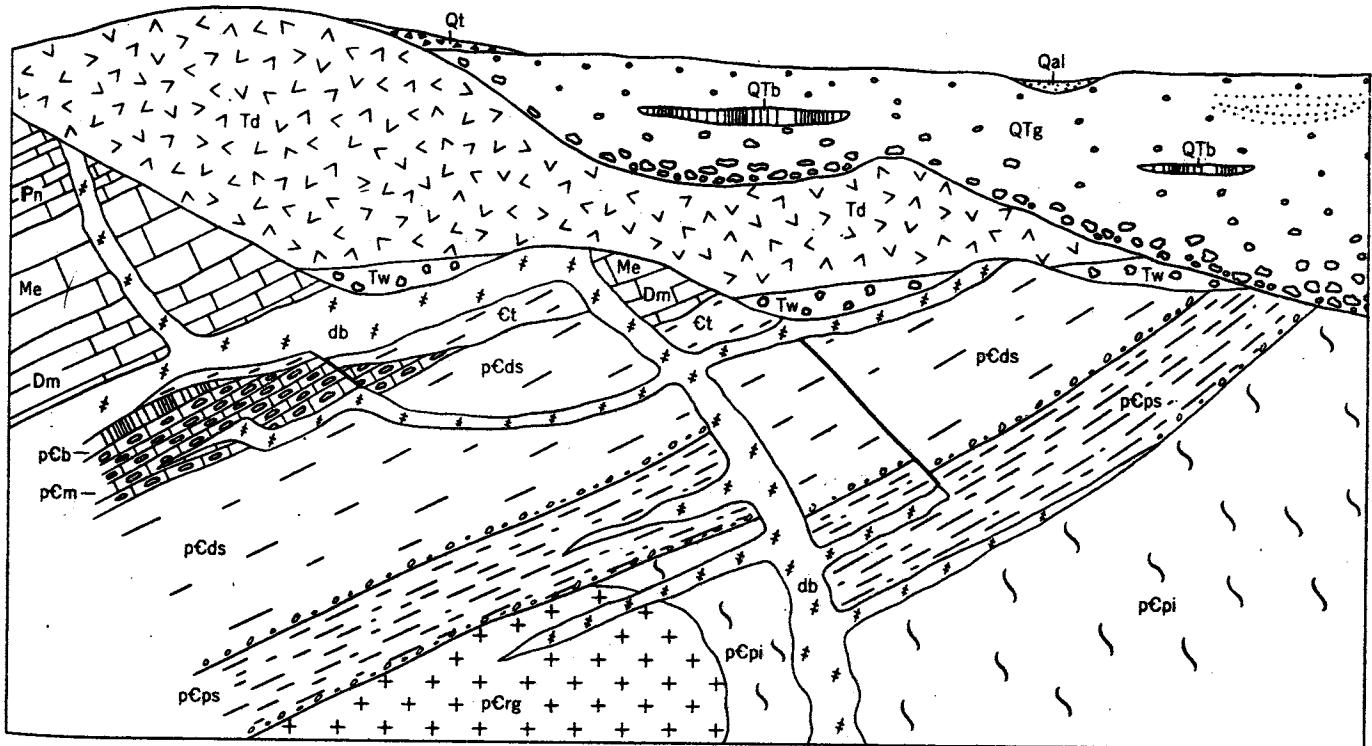
edgment is due Mr. R. W. Hughes, general manager, and Mr. B. R. Coil, assistant manager, of the Miami Copper Co.; Mr. P. D. I. Honeyman, general manager, Mr. H. C. Weed, general superintendent, and Mr. E. F. Reed, geologist, of the Inspiration Consolidated Copper Co.

The early work of F. L. Ransome, of the Geological Survey, was of great assistance, furnishing many data on mines and areas now inaccessible. The discussion of the Old Dominion property is based mainly on the meticulous detailed mapping of the underground workings by Guy N. Bjorge and A. H. Shoemaker. Maps and records of the Iron Cap mine were supplied by F. P. Knight and Sam Knight. Much of the history of mining development during the early days of the district was taken from unpublished notes compiled by J. B. Tenney, of the Arizona Bureau of Mines.

GENERAL GEOLOGY

PRELIMINARY SUMMARY

The rocks of the Globe-Miami district range from lower Precambrian to Recent. They are shown on the geologic map (pl. 1). Figure 3 is a diagram show-



EXPLANATION

Alluvium, Qal; talus, Qt; basalt, QTb; Gila conglomerate, QTg; dacite, Td; Whitetail conglomerate, Tw; diabase, db; Naco limestone, Pn; Escabrosa limestone, Me; Martin limestone, Dm; Troy quartzite, Ct; basalt, pCb; Mescal limestone, pCm; Dripping Spring quartzite, Barnes conglomerate at the base, pCds; Pioneer formation, Scanian conglomerate at the base, pCps; Ruin granite, pCrg; and Pinal schist, pCpi

FIGURE 3.—Diagram showing the hypothetical general relationships of the sedimentary and volcanic rocks and the intruded diabase.

ing the hypothetical general relationships of the sedimentary and volcanic rocks and the intruded diabase.

The oldest rocks are lower Precambrian crystalline schists, mainly of sedimentary origin, that had been highly deformed, invaded by various igneous rocks, and deeply eroded before the upper Precambrian sedimentary sequence known as the Apache group was deposited. The rocks of the Paleozoic era consist of the Troy quartzite of Cambrian age, the Martin limestone of Devonian age, the Escabrosa limestone of Mississippian age, and the Naco limestone of Pennsylvanian age. No sedimentary rocks of the Mesozoic era are represented, but a series of igneous intrusions probably began in Late Cretaceous and continued into early Tertiary time. The intrusions were accompanied by extensive faulting and deformation of the rocks and were climaxed by widespread copper mineralization in the district. Probably also in Tertiary time, the Whitetail conglomerate was deposited, and a vast sheet of tuff and dacite was erupted over the eroded surface of the fault-block mosaic of sedimentary and igneous rocks. Faulting continued and later in Pliocene and Pleistocene time, alluvial deposits that form the Gila conglomerate were laid down unconformably on the deeply eroded surface of dacite and older formations. Mild volcanic activity accompanied deposition of the Gila conglomerate, and further faulting and uplift followed, resulting in the current erosion cycle that is wearing away the conglomerate and depositing talus on the slopes and alluvium along the beds of intermittent streams.

LOWER PRECAMBRIAN ROCKS

PINAL SCHIST AND INTRUDED COMPLEX OF DIORITIC ROCKS

The Pinal schist and the large bodies of igneous rock intruded into it in early Precambrian time constitute the basement complex of the Globe-Miami district and surrounding region. Ransome's (1903, p. 23-28) type locality for the Pinal schist is in the Pinal Mountains south of Globe and Miami. Later he (1904b, p. 24) applied the name to the basal schistose rock of the Bisbee quadrangle near the southeastern corner of Arizona, and the name is now applied to the basal schists throughout the southeastern part of the state. The Pinal schist is generally correlated in age with the Yavapai series of central Arizona and with the Vishnu schist of the Grand Canyon Region of northern Arizona.

There are extensive outcrops of Pinal schist in the Pinal Mountains south of the Globe-Miami district, and the several relatively small outcrops in the southwestern part of the district are separated from the main outcrops in the Pinal Mountains by the extensive intrusive

body of Schultze granite. The largest outcrops within the mapped area are in the southeastern part of the Inspiration quadrangle from Bloody Tanks Wash northward to the mass of quartz monzonite south of Sleeping Beauty Peak. A large body crops out in the Castle Dome horst block south of Gold Gulch, and others crop out west of Pinto Creek near the southwest corner of the quadrangle.

In the Globe Hills area in the eastern part of the district, Pinal schist is reached by the bottom levels of the Old Dominion, Iron Cap, and Superior and Boston mines, but there is only one small outcrop, a mile north of Black Peak. Throughout the rest of the northern part of the district, the upper Precambrian and Paleozoic sedimentary rocks rest on the truncated surface of Ruin granite, which probably intruded the schist, although direct proof is lacking.

The Pinal schist exposed in the district comprises a gradational variety of rocks that range from very fine grained quartz-sericite schist to rather coarse feldspathic sandstone. A few small bodies of amphibolite are known, and in a few places the schist appears to have been formed from rhyolite or fine-grained granite. Most of the schist, however, was formed by dynamic and thermal metamorphism of interbedded shale and feldspathic sandstone. Relict bedding is recognizable in most outcrops and is generally parallel with the foliation.

In most of the larger outcrops, the schist can be divided into fairly distinct units that could be separately mapped. No detailed stratigraphic study of the schist has been undertaken, however because the results do not seem to justify the necessary time and labor. The outcrops within the mapped area are relatively small, and the units have been displaced by faults and igneous intrusions and are not sufficiently characteristic to permit correlation from one outcrop to another. The larger outcrops show that beds are lenticular and are interfingered on a relatively small scale.

The Pinal schist comprises such a wide range of gradational varieties of rocks whose stratigraphic relationships are not known that detailed descriptions would have little significance. The most common varieties have approximately the same mineral composition. They are essentially quartz and muscovite, which generally compose at least 75 percent of the rock. They range from fine-grained quartz-sericite-chlorite schist to coarse-grained quartz-muscovite schist. Nearly all contain some fine-grained flaky biotite or chlorite, or both. Magnetite and ilmenite are present in variable amounts, either as fine disseminated grains or segregated in thin layers with grains of quartz.

The schist ranges from a highly foliated rock to a

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tions of gouge or clay. This condition is in
g with the fact that no major faults other than
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the ore body. As would be expected, however,
ing operations revealed many small irregularities
boundary between capping and ore resulting from
ferences in permeability caused by minor faults and
ures.

AGE OF SUPERGENE ENRICHMENT

the western part of the quartz monzonite outcrop,
nts of the dacite lie directly on quartz monzonite
granite porphyry (pl. 7). Farther northeast, in
vicinity of the ore body, remnants of dacite over
e adjacent sedimentary rocks within 400 feet of
Sleeping Beauty fault, which forms the northwest
ary of the quartz monzonite mass. On the north-
margin of the quartz monzonite outcrop, near the
mi fault, a patch of dacite overlaps a small outcrop
abase that intrudes the quartz monzonite. These
relationships indicate that at least a part of the quartz
zonite mass had been uncovered before the erup-
of dacite, and they strongly suggest that the un-
red area may have been approximately equal to
of the present outcrop.

However, the chalcocite zone of the ore body is clearly
ed to the present topography carved during the
ent erosion cycle, and its relative youth is also
n by the superficial extent of the enriched zone
by the incomplete replacement of hypogene sulfides
chalcocite.

that the quartz monzonite outcrop stood relatively
during the interval of erosion that directly pre-
ed the eruption of dacite is shown by the absence of
etail conglomerate under the dacite in the vicinity
e copper deposit. It appears likely that the miner-
al quartz monzonite was undergoing too rapid
on during this interval of exposure to allow enrich-
to proceed.

Furthermore, there is nothing to indicate that the
artz monzonite was again uncovered during the
erval between the eruption of dacite and the depo-
n of the Gila conglomerate in this area. The
s of dacite that crop out along the Miami fault
and the outcrops of dacite that underlie the con-
erate along the west side of Pinal Creek farther
e east suggest that dacite underlies the Gila con-
erate east of the Miami fault.

Thus we may conclude that the enrichment that
duced the chalcocite ore of the Copper Cities de-
t occurred after the block containing the outcrop
artz monzonite had been elevated by displacement
g the Miami fault and after the cover of Gila

conglomerate and the dacite beneath the Gila had been
removed during the present cycle of erosion.

ORE BODY

The shape and size of the Copper Cities ore body
is determined to a large extent by economic factors;
that is, the tonnage of ore included within the planned
limits of the mine is that which can be profitably mined
and treated at certain anticipated costs and price of
copper. These factors arbitrarily determine the ulti-
mate limits of the mine illustrated on the cross sections
through the mine (pl. 8). The outline of the proposed
open-pit mine is shown in plates 7 and 8.

Excluding the leached capping, most of the rock
within the limits of the mine has been affected to some
extent by supergene enrichment, and therefore, the
mine limits roughly delineate the chalcocite ore. The
ore is thin in the granite porphyry bodies, where the
chalcocite zone is thin and the copper content of the
protore below the economic cut-off grade. The ore
is generally thick in the quartz monzonite adjacent to
the granite porphyry bodies, where the copper content
of the protore ranged from slightly below to well above
the cut-off grade and where the vertical range of super-
gene enrichment was much greater than in the granite
porphyry bodies. Some of the ore near the bottom
of the mine contains very little chalcocite or none at
all, it is ore because the primary copper content of the
rock made it ore grade or was so high that the rock
was raised to ore grade by very slight enrichment.

CACTUS DEPOSIT

The Cactus property on Pinto Creek near the south-
west corner of the Inspiration quadrangle contains a
relatively small disseminated-copper deposit that
attracted considerable attention as early as 1905.
From 1908 to 1910, Cactus Copper Co. sunk 15 churn-
drill holes ranging from 170 to 700 feet in depth.
The Pinto and Hamilton shafts were sunk, and about
6,500 feet of lateral workings were driven on the 300-
400-, and 500-foot levels of the Hamilton shaft. In
1921, Pinto Valley Co. took over the properties of
Cactus Copper Co. and during the ensuing years sunk
at least 15 churn-drill holes to further explore the
Cactus deposit and contiguous areas. As a result of
this exploration a small body of mineralized schist had
been blocked out. Work was discontinued in 1929 and
has never been resumed. The property was acquired
by Castle Dome Copper Co. in 1940.

The deposit is considered as too small and too low
in copper content to permit economic exploitation
under present conditions. All the underground work-
ings except a few shallow adits are now inaccessible.

The available records are lacking in firsthand descriptions but do give some information concerning the general structure of the deposit.

The copper deposit is in a mass of highly shattered and hydrothermally altered Pinal schist that crops out on the north side of Pinto Creek just west of Manitou Hill (pl. 7). The shafts and drill holes in the mineralized area are described as entering unaltered or "black" schist after passing through a fault zone that directly underlies the chalcocite deposit. This fault zone, known as the Cactus fault, dips 20° to 30° SW. The mineralized schist appears to have been a plate thrust over the normal schist on the Cactus fault, probably from the south or southwest (section *B-B'*, pl. 7). The deposit is a gently dipping, partly oxidized chalcocite blanket formed by supergene enrichment. On the west and north sides, its outcrop is overlapped by dacite and Gila conglomerate. The south boundary is formed by the Kelly fault along which the altered schist has been dropped into contact with an unaltered, coarse-grained quartz-sericite schist, Precambrian granite, and diabase in the south or footwall, side of the fault.

The chalcocite deposit is overlain by 100 to 300 feet of highly silicified schist from which all but a trace of copper has been leached.

The east boundary between mineralized and unmineralized schist is largely covered by talus, but in the few places where it can be seen, it is marked by a zone of intense brecciation that probably is the outcrop of the Cactus fault. The breccia fragments show random orientation as a result of rotation, and they are bound together by a matrix of finely ground rock that is firmly cemented by silica and limonite. Large and small fragments of apparently unaltered schist are common in the breccia. The best exposure is in an open-cut from which 50 to 100 tons of oxidized ore has been mined. At this point, the breccia zone appears to have a westward dip of 30° to 40°.

In the northern part of the schist outcrop, there is a small area of unmineralized schist that is bounded on the north, west, and south sides by steep faults. It apparently is the outcrop of an up-faulted block of the schist that underlies the Cactus fault. At the eastern side the block is overlapped by a mass of schist breccia that is no doubt a small remnant of the thrust plate.

A thrust fault that probably is an offset segment of the Cactus fault strikes north along the west side of Pinto Creek, 3,000 feet northwest of the Hamilton shaft. This fault is well exposed for about 2,000 feet, and strikes approximately north and dips 20°-30° W. The hanging-wall block is of unaltered schist which

has been thrust over the Whitetail conglomerate and the diabase. To the north, the outcrop of the fault is overlapped by dacite; and at the south, the fault is cut off by a normal fault, although the inferred intersection of the two faults is concealed by alluvium in the bed of Pinto Creek. The normal fault is roughly parallel with the Kelly fault, and the block between has been relatively depressed so as to bring dacite in contact with schist of the thrust plate above the Cactus fault.

The copper-bearing rock that forms the Cactus deposit is reported to contain chalcocite, a little pyrite, and copper carbonates and silicates. Some of the carbonates, particularly in the upper part of the deposit, undoubtedly were formed by alteration of chalcocite. The most metallized rock is generally in the lower part of the deposit, just above the Cactus fault, which itself is richly metallized with copper carbonates and silicates that coat breccia fragments or interstices between them. These minerals are regarded as a direct deposit from supergene solutions that percolated downward through the shattered mineralized schist into the gently-dipping fault zone where much of their dissolved copper was deposited.

The protore of the deposit has not been described and probably it was not found in the course of exploration. No doubt it is similar to that of the other disseminated deposits of the district, in which the hypogene sulfides consist mainly of pyrite and chalcopyrite.

The host rock, as seen in the outcrop, is highly silicified schist containing some sericite but generally much less than in most local varieties of unaltered Pinal schist. It is stained light brown by residual limonite; the color is generally a little deeper than the leached-schist capping that overlies the Miami Inspiration ore body. In the most highly altered schist all semblance of foliation has been destroyed.

The major brecciation clearly occurred after hypogene metallization. Veinlets have been offset by fractures; and where brecciation was most intense, fragments have been rotated and veinlets do not continue into the matrix. Fragments of relatively unaltered schist commonly are completely surrounded by fragments of altered rock.

It is uncertain whether the supergene enrichment of the deposit took place before or after the plate had been thrust into its present position. If, as appears probable, the Cactus fault and the fault that crops out west of Pinto Creek are one fault, its age can be established very closely. It is younger than the Whitetail conglomerate but is older than the dacite, and therefore was formed during the interval of erosion that pre-

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ruption of dacite. Much of the supergene enrichment in the district took place during this interval. The drilling logs record that altered schist underlies the depressed block in the hanging wall of the Kelly fault, but there is no mention that copper was present either as sulfide or carbonate in the altered schist. If copper is really absent, this condition suggests that the plate of altered schist had been at least partly leached and leached before it was thrust into its present position. However, the information contained in the report is too meager and incomplete to constitute more than suggestive evidence. Criteria based on the relationship of the top of the chalcocite zone to present topography or to that preceding the deposition of the schist are not conclusive. It is certain, however, that the process of the oxidation, leaching, and deposition of copper carbonates and silicates was accomplished during the present cycle of erosion after the plate had been thrust to its present position.

The source of the mineralized schist is purely a matter of speculation. If it can be assumed that the overlying plate has been thrust up the dip of the fault since the present attitude would indicate that the mineralized block had been thrust from the west or southwest; but the rocks in this general area have been faulted and tilted, and the present attitude does not necessarily represent the initial attitude of the schist. A possible source is suggested by a small body of altered schist having the characteristics of leached schist that crops out under the dacite cliffs on the west side of Powers Gulch $1\frac{1}{4}$ miles west-southwest of the copper deposit, but there is no direct evidence that the bodies of schist are in any way related (p. 140).

COPPER VEINS

The copper-bearing veins of the Globe Hills area yielded less than 20 percent of the total metal produced from the district, but nevertheless, their contribution amounts to nearly a billion pounds of copper and more than \$9 million in gold and silver. The major part of the production came from the Old Dominion, Globe, Arizona Commercial, and Iron Cap veins, all on the Old Dominion vein system. Similar veins of considerably less importance are the Great Western, Buckeye-Black Oxide, Dime-Stonewall, Big Maggie, Maggie, Josh Billings, Buffalo, Original Old Dominion, I.X.L., and Highline veins.

In all these veins, the principal hypogene minerals are pyrite, chalcopyrite, bornite, and specular cuprite. Cuprite that is intergrown with specular pyrite may also be hypogene. Sphalerite and galena occur locally in very small amounts, and a little tetrahedrite and enargite have been reported (Adams, S. F.,

written communication 1917), in the ores of the Old Dominion mine.

The veins were formed by replacement of breccia and wall rock along faults and fissures that cut upper Precambrian and Paleozoic sedimentary rocks and bodies of diabase intruded into them. Undoubtedly the veins continue downward into the underlying Pinal schist, but the few that have been followed down to the schist were found to be poorly mineralized. Some of the veins, the Old Dominion for example, are along faults that have displacements of several hundred feet, whereas others follow fissures with little or no displacement. The largest and most continuous ore bodies are along faults or segments of faults having relatively large displacements.

In general, the ore does not appear to be limited to definite shoots of great vertical extent but rather seems to be localized in areas of the fault zones that show a definite relationship to the formations traversed by the faults; that is, the character and volume of the vein matter differ from place to place, according to the type of wall rock. Except for limestones of the Paleozoic age, the differences are due mainly to the physical characteristics of the rocks that affect the permeability of the fault zones rather than to the chemical character of the rocks.

Very abrupt changes occur where veins pass from one type of rock to another. The Paleozoic limestones were the most readily replaced and commonly contain thick lenses of very rich ore. In some places, flat tabular ore bodies extend outward along certain especially favorable beds as far as a hundred feet from the vein fault. Extensive ore bodies have been mined between walls of Mescal limestone and between walls of the various quartzite and sandstone formations or any combination of these formations. Good ore bodies may be found also where diabase forms one wall and any of the sedimentary formations the other; but where both walls are of diabase, the vein fault is likely to be tight and poorly mineralized or entirely barren.

The productive parts of the veins in the Old Dominion and other mines have long been inaccessible for inspection, and no detailed descriptions of the veins are available. Ransome's (1903, p. 125-128) descriptions deal almost entirely with the highly oxidized, near-surface ore bodies. Apparently the veins pinch and swell and range from a single quartz stringer to broad zones of wholly or partly replaced breccia, or lodes comprised of several to many irregular, discontinuous stringers. The character of the vein changes abruptly with changes of wall rocks. Where the vein faults traverse quartzite, the veins are zones of loose, angular breccia in which the vein minerals occur as replacement

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terminated by the Van Dyke fault, which is coincident with the footwall of a granite porphyry dike. The fault and dike strike N. 70° W. and dip 70° NE.

The localization of the copper minerals appears to have been controlled by the intersection of the low-angle fault zone with the Van Dyke fault. The greatest amount of brecciation and the best ore occurred near the intersection, and the amount of brecciation and ore minerals decreases progressively southwestward. The Van Dyke fault clearly served as a barrier to the copper-bearing solutions that seeped into the low-angle fault zone.

The copper minerals in the ore consist entirely of azurite, malachite, chrysocolla, and tenorite. According to I. A. Ettliger (written communication, 1929):

These oxidized copper minerals are not the result of oxidation in place of a primary sulphide ore body which contained copper but were first deposited as carbonates and silicates by laterally moving or descending solutions either in a practically barren fault zone or at least a fault zone containing small amounts of pyrite and traces of chalcopyrite. This fact is clearly demonstrated by the oxidized copper minerals which are filling voids and act as a cementing material for irregular angular fragments of practically unaltered schist. The oxidized copper minerals in filling these voids between the schist fragments appear as crustations and in many places assume botryoidal form.

The deposition of the copper carbonates and silicate may have occurred while oxidation and leaching of the surrounding sparsely mineralized schist protore was in progress, probably before the Gila conglomerate was deposited and possibly before the eruption of dacite. The age of the faults has not been determined. The Van Dyke fault, if projected upward, would intersect the shaft near the point where it enters the schist; but whether the fault displaced the Gila is not known. At the time the shaft was sunk, the ground-water level was at 300 feet; that is, about 900 feet above the ore body. Most likely the ore body was formed before displacement occurred on the Miami fault, when the water table in the block now depressed was below the level of the ore body.

The mineralized zone cut by the second drill hole is about 670 feet lower in elevation than the ore body cut by the first hole, but its attitude is not known. The intersection of the faults, as seen in the mine workings, plunges southeastward with a dip and bearing that, if projected, would pass near the ore zone cut by the second hole. It is possible that the two bodies are along the same structure, and they may be connected.

CARLOTA DEPOSIT

Near the southwest corner of the Inspiration quadrangle, deposits of copper carbonates and silicates occur in shattered rock along the Kelly fault zone (pl. 7).

At two places the rock has been sufficiently mineralized to constitute ore; one is on the Carlota property, the other is 2,000 feet southeast of the Carlota mine near the old Arizona National shaft.

The Kelly fault zone has an average strike of N. 60° W., and it dips 60° to 70° NE. At the Carlota mine and northwestward to the edge of the quadrangle, a diabase sill intruded between Pinal schist and the base of the Apache group forms the footwall of the fault zone, and dacite forms the hanging wall. In the vicinity of the mine, the dacite is underlain by Whitetail conglomerate and hydrothermally altered Pinal schist; but farther westward, it probably is underlain by Whitetail conglomerate and Paleozoic limestone. The details of structural relationships as they were before the eruption of the dacite cannot be determined. Southeast of the Carlota mine a wedge of shattered but unaltered schist crops out within the fault zone; whereas just northwest of the mine the fault structure becomes complex, and lenticular blocks of Whitetail conglomerate, Paleozoic limestone, diabase, and altered schist crop out in the fault zone.

In the Carlota deposit, the copper minerals occur in brecciated diabase in the footwall of the fault zone. The ore body has no sharp boundaries but grades into low-grade material in which the mineralized fractures are too narrow and too widely spaced to make ore. Its maximum dimensions at the outcrop are about 250 feet long by 100 feet wide. The depth to which rock of ore grade extends is not known. On the deepest level of the mine, about 200 feet below the outcrop, the mineralized zone appears to have contracted to a few major fractures.

A small ore shoot 2,000 feet southeast of the Carlota mine occurs in schist breccia within the Kelly fault zone. At this point altered schist forms the hanging wall of the fault and unaltered, coarse-grained, quartz-sericite schist the footwall. About 1904, a shaft was sunk by the Arizona National Copper Co. to explore the fault zone in the vicinity of the ore body. According to the mine records, which are rather meager, the shaft was sunk about 250 feet in schist breccia, at which depth it entered diabase. A crosscut driven northeastward on the 280-foot level is reported to have intersected a zone of carbonate ore, but the extent of the ore and its location in relation to the shaft are not described. The shaft and a northeast crosscut on the 125-foot level should have intersected the ore zone, but the records do not show that they did. The shaft is now caved.

Some shipping ore was produced in 1943-45 from an open cut on the outcrop of the fault zone. The mineralized fault breccia is mainly of unaltered schist, but in places there is considerable admixture of frag-

ments of hydrothermally altered schist derived from the hanging-wall block. Except for the difference in host rock, the mineralization was of the same type as the Carlota deposit.

In both deposits the ore minerals are malachite, a little azurite, and various hydrated copper silicates. They occur in veinlets ranging from microscopic to as much as half an inch thick and also as crusts coating the breccia fragments. Where the breccia was especially open, the fragments are commonly covered by several superimposed, botryoidal crusts composed of radially oriented, fibrous silicates that differ in color, texture, and optical properties. Some of the silicates have vitreous luster and are so intimately fractured as to suggest solidification of a colloidal gel. Small botryoidal masses of black tenorite generally embedded in and veined by chrysocolla are present in many places. Silicate layers commonly are separated by thin black films that probably also are tenorite.

The copper minerals have clearly formed by direct deposition either from true or from colloidal solutions that contained copper not derived from minerals originally present in the immediate host rock. There is no evidence whatever that they have formed either by replacement or by alteration in place of older, hypogene, copper-bearing minerals.

The hydrothermally altered schist in the hanging wall of the Kelly fault zone is the host rock of the Cactus ore body. The rock in the outcrops has been thoroughly oxidized and leached, but underground development and exploratory drilling have disclosed a small chalcocite blanket formed by supergene enrichment (p. 95). The altered schist has been thrust over unaltered schist along the Cactus fault, a low-angle fault that dips southwestward and crops out about 900 feet southeast of the Hamilton shaft. This low-angle fault is cut off but the Kelly fault zone along that portion of it in which the deposits of copper carbonate and copper silicate occur. Copper-bearing supergene solutions drained into the Cactus fault zone and deposited large amounts of copper carbonates and silicates in the fault breccia. It is not difficult to imagine how these solutions could have percolated into the Kelly fault zone, whence they could have ascended along especially permeable channels. On the other hand, deposition by descending supergene solutions presents no serious problem of explanation.

In both of the developed deposits on the Kelly fault zone, the ore bodies decrease in size with increasing depth. It is not likely that deposits of this type would be formed below the zone of active ground-water circulation.

PORPHYRY RESERVE

In 1929 and 1930, the Porphyry Reserve Copper Co. produced 350,000 pounds of copper (Elsing and Heiman, 1936, p. 92) from terrace deposits of stream gravels along the sides of Tinhorn Wash east of the Copper Cities open-pit copper mine. The gravels are composed of detritus of local origin, mainly fragments of quartz monzonite, granite, porphyry, diabase, quartzite, and limestone. The fragments are firmly cemented by limonite and copper carbonates deposited by supergene solutions that carried iron and copper, probably as sulfates, leached from the nearby Copper Cities copper deposit. Much of the copper occurs as replacement shells of malachite coating fragments of limestone; the rest is partly in the matrix and partly in the diabase fragments, where it probably replaces carbonates formed by weathering of the diabase.

POWERS GULCH (64 GROUP)

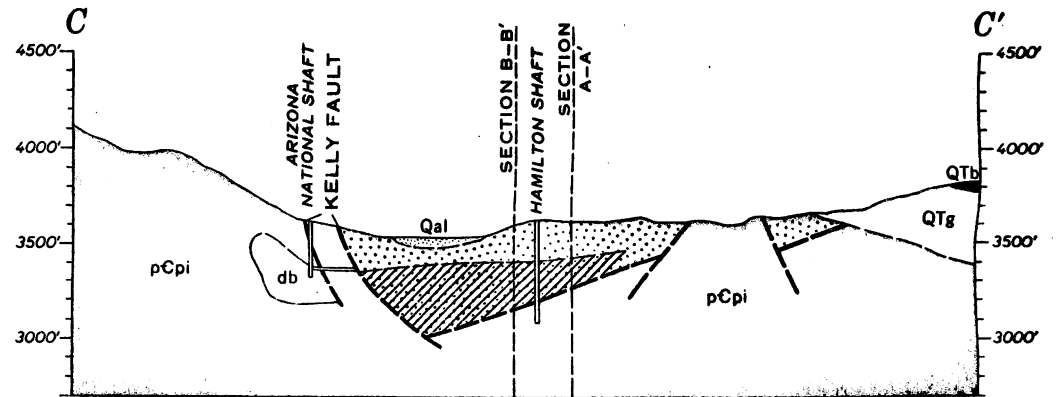
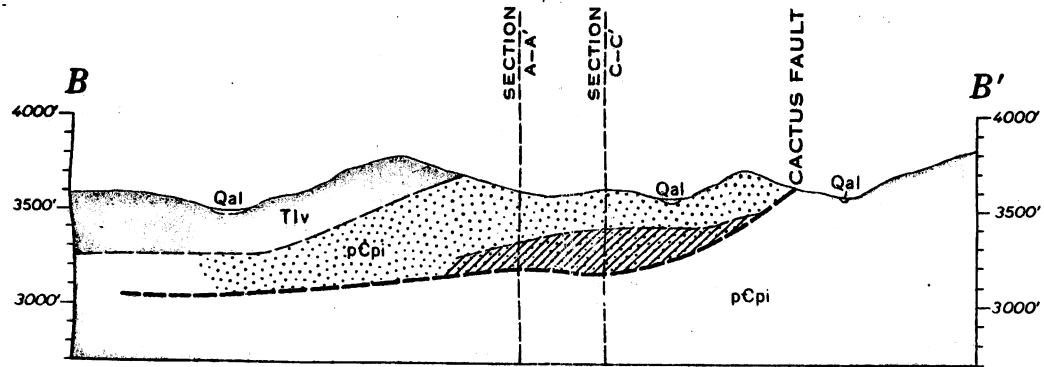
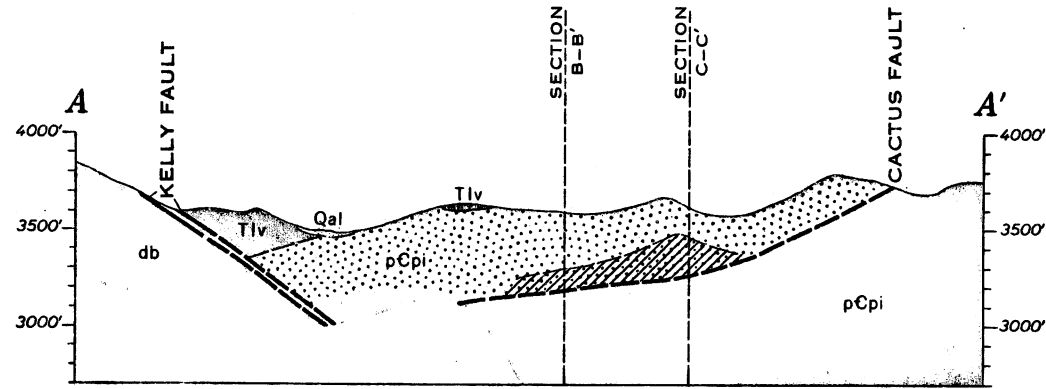
In the southwest corner of the Inspiration quadrangle and for 1½ miles southward in the Pinal Ranch quadrangle, the schist that crops out under the dacite on the west side of Powers Gulch contains small amounts of copper carbonates and silicates. The copper minerals occur as impregnations and veinlets that range in width from microscopic to nearly an inch. They are not evenly distributed, and bulk samples of the rock from various places would probably assay from 0.1 to 0.25 percent copper.

The copper-bearing schist shows no evidence of hydrothermal alteration or the former presence of sulfide minerals, except in a small area just north of the common corner of the quadrangles and also along the contact with a body of the granite porphyry facies of Schultze granite that crops out under the dacite 4,500 feet south in the Pinal Ranch quadrangle. The granite along the contact shows considerable sericitization and slight metallization by pyrite and chalcopyrite.

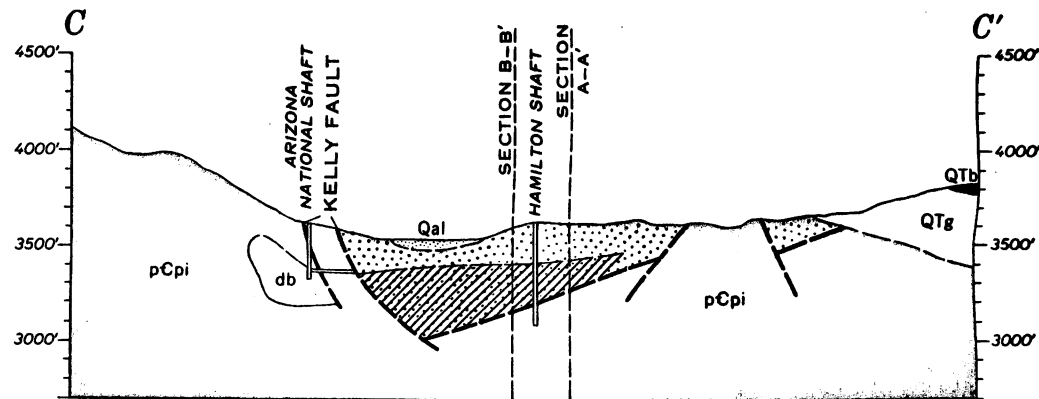
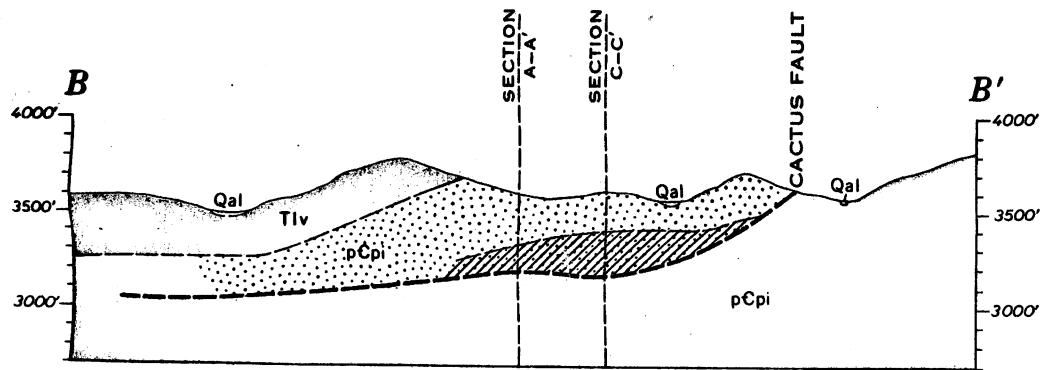
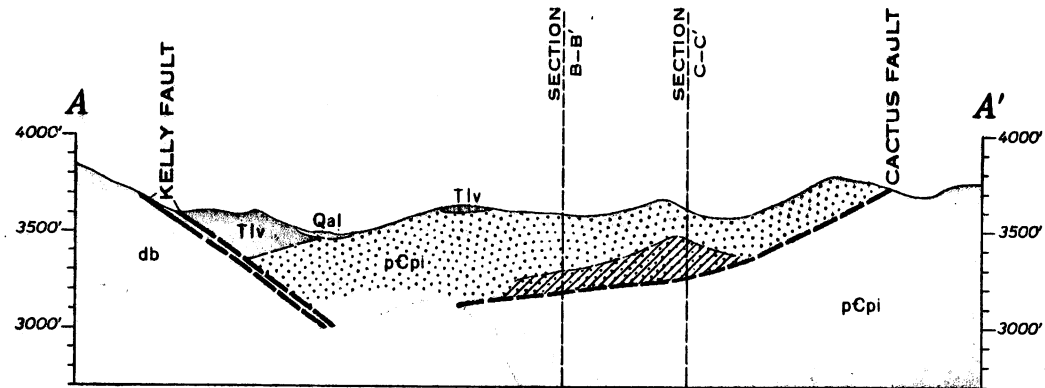
Although the copper content of the rock is too low to be of any economic importance, the total amount of copper in this area undoubtedly amounts to many millions of pounds; and it is significant as a possible indication of extensive hypogene copper metallization in the general vicinity of these outcrops. The copper carbonates and silicate undoubtedly were deposited by ground water; and, since no evidence has been found of any concentration of copper minerals in the tuff that underlies the dacite and which is normally a good precipitant of copper, it is probable that the deposition occurred before the eruption of the tuff and dacite.

The source of the copper is not known, but the wide distribution of the copper minerals suggests a source of considerable lateral extent, most likely a body of

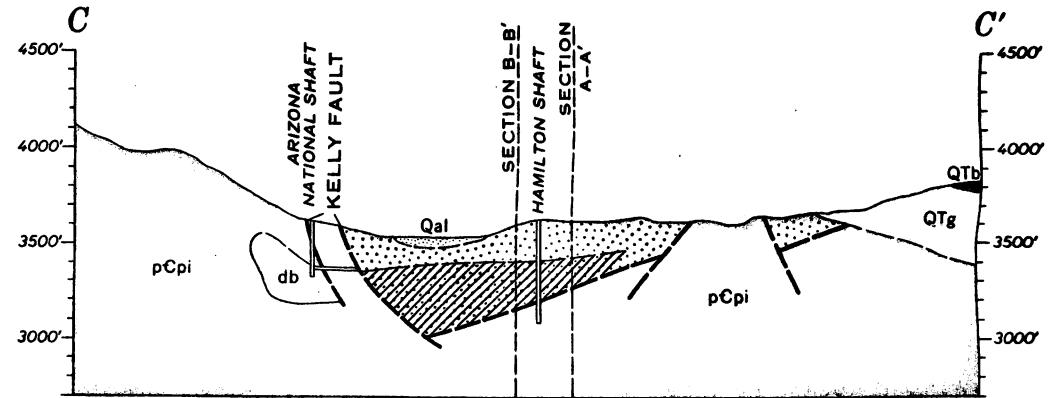
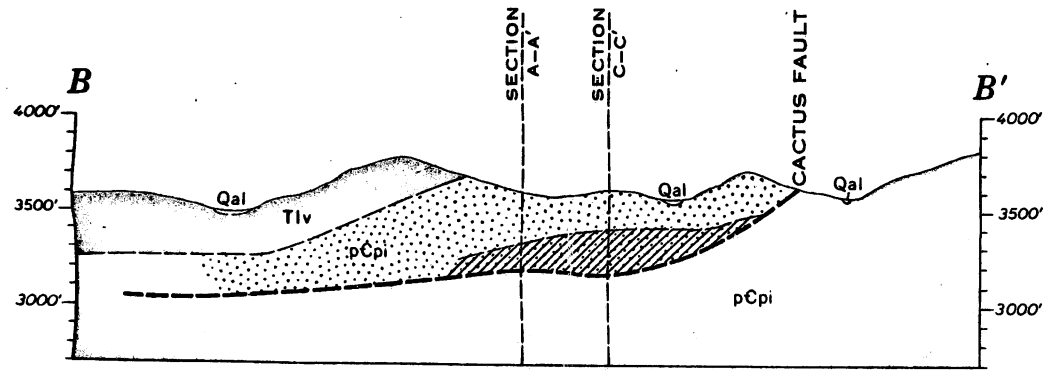
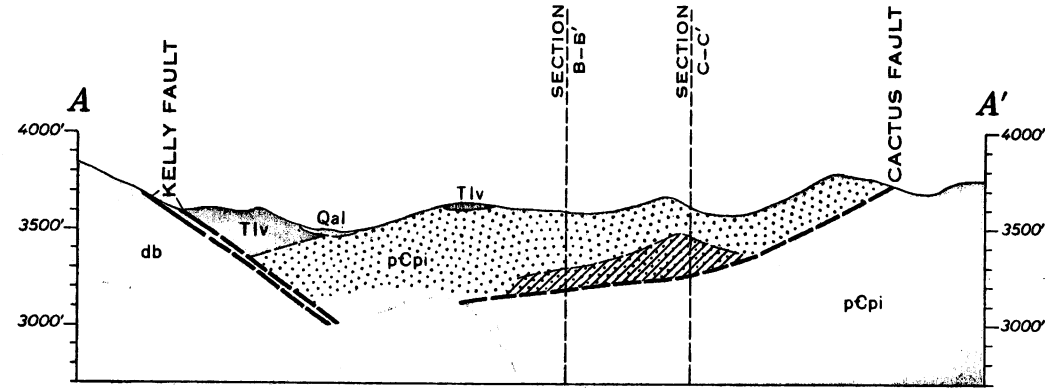
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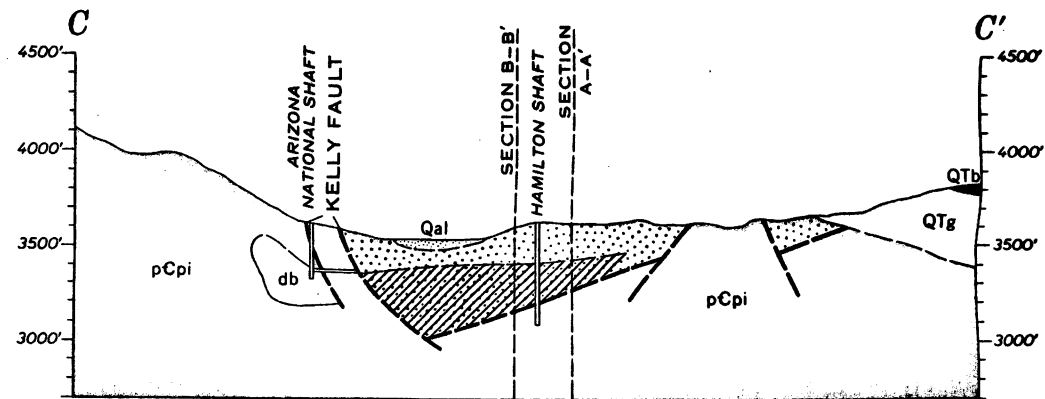
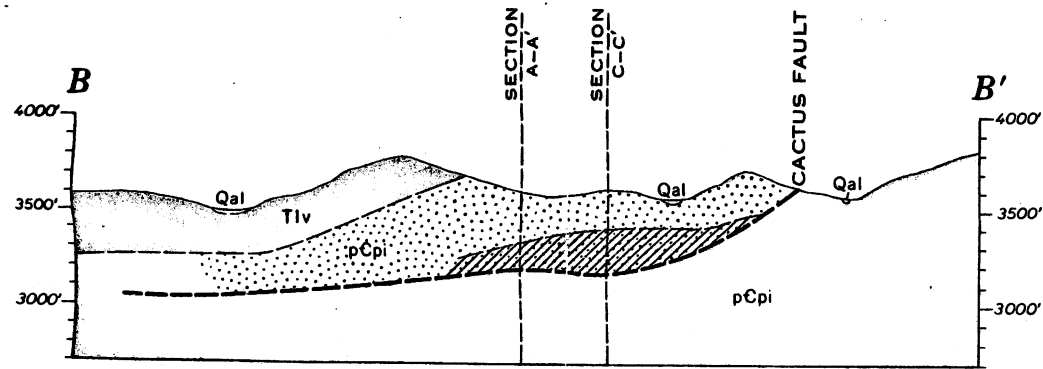
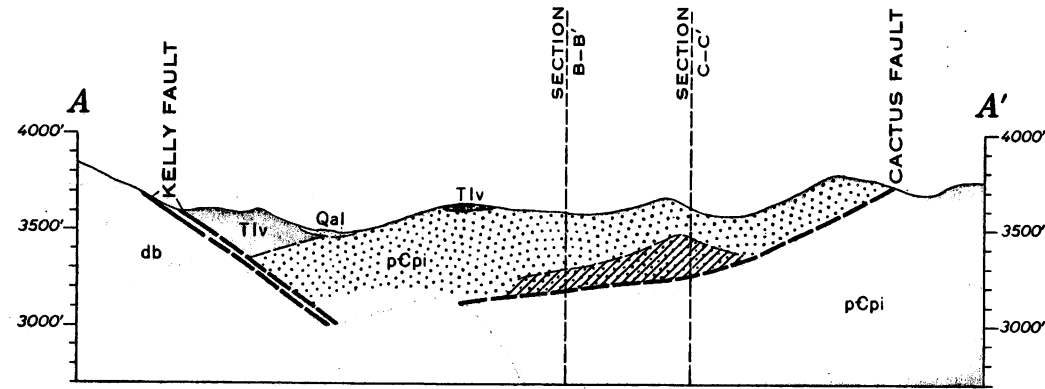
CACTUS-CARLOTA AREA



CACTUS-CARLOTA AREA



CACTUS-CARLOTA AREA



the most reactive rocks in the district, and it is inconceivable that the copper could have traveled through these rocks for more than a few hundred feet without being precipitated. The presence of Paleozoic limestones in the downfaulted block east of the Castle Dome ore body practically eliminates the possibility that ground water could have transported the copper from that deposit.

STRUCTURAL CONTROL

In the detailed study of the Globe-Miami district, one is greatly impressed by the prevalence of northeastward structural trends, particularly those related to such deep-seated phenomena as igneous intrusion and mineralization. All the productive mineral deposits of the district, as well as those of the Pioneer (Superior) district a few miles to the southwest, are distributed along a northeastward-trending belt about 6 miles wide (fig. 14). Within this narrow belt, there are 14 mines whose past production and known reserves are valued at more than \$1 million for each mine. Of this number,

2 of the mines have already produced more than \$300 million each, 4 have or will produce more than \$100 million each, and 2 others have produced more than \$10 million each. There are many smaller deposits that have yielded from a few thousand to several hundred thousand dollars in metals. The total production of the Globe-Miami district recently passed the billion-dollar mark, and the Pioneer district has produced about \$230 million in copper, silver, gold, and zinc.

The northeastward continuation of the belt includes the small but rich silver mines of the Richmond Basin district with a total production of a little more than \$1 million. The southwestward extension takes in several small silver, lead, and zinc deposits of the Reymert, Martinez Canyon, and Mineral Hill districts, which probably have a total production of about \$1 million.

The outcrop of the mineral belt is interrupted in the Globe Valley area between Globe and Miami by a thick cover of Gila conglomerate that is younger than the period of primary copper mineralization. Tertiary(?) volcanic rocks, which also are postmineralization

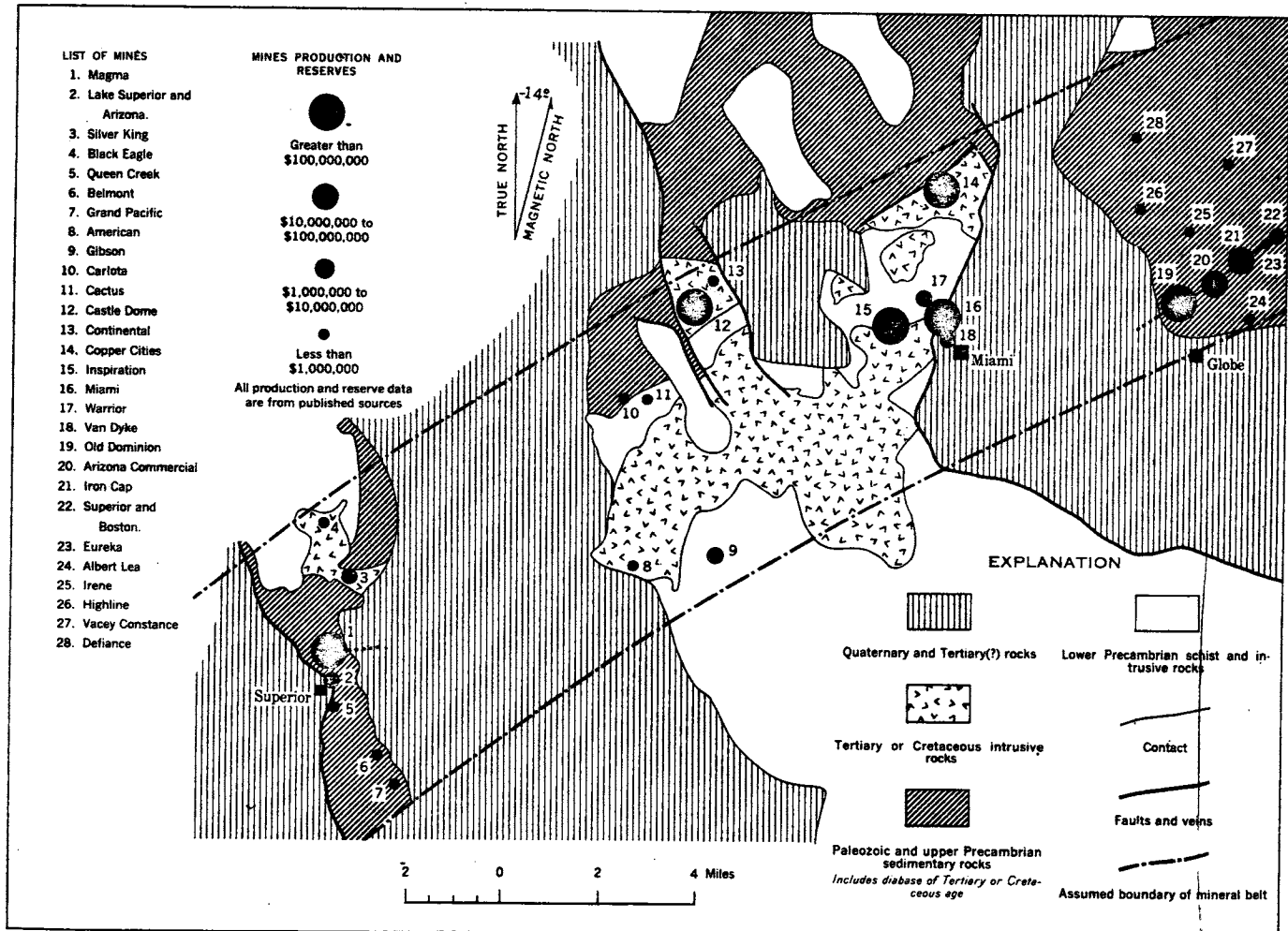


FIGURE 14.—Index map of the Globe-Miami and Pioneer districts showing assumed limits of the mineral belt and the location of the productive deposits.

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L. K. # 2

DEW

LAD

Clipper

Old Abe fraction
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ENTER ANGLE
71.0000*
3.0000*
56.0000*

TRIANGLE SUMMARY

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SIDE 2
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SIDE 3
1449.2124

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ANGLE 3
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TRIANGLE AREA
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Books

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✓ Docket 355 - 213, 214.

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416 + 417
418 ✓
419 + 420

✓112 - 399 -

✓11 - 286 ✓ X

X102 - 41 + 42 - -

✓40 - 357 + 358 X

✓237 - 636 + 635 -

✓OK6 - 356 - Surprise X

X Hope #14?

Carlota Mine Property
 Cooper ~~Abund~~ Survey
 Tucson
 (for Skelly)

10-7-68

Lad a Dow - purchase for surveying

Lost Knife - file an amended loc'n notice
 to 1150 NW 1/4 a 350' SE 1/4

Lad - 19⁶⁹~~47~~ - 1947 No
 1947 - 1956 No
 1956 - 1967 No
 1967 - 1974 ✓ a Dow

Moonrise 6-401 Feb 15/1899
 J.W. Gilmore et al.

Sun Rise F.W. Gilmore et al
 2/12/99 & 8/2/99 1900

6-356

213
 355 - 214

Mang Cap Amended 176 - 507
 230 - 419 420 ✓
 Golena Amended 176 - 508 a 230 - 416 417
 Lost Knife No. 1 Amended 100 - 416 a 230 - 418 ✓
 No. 2 Amended 108 - 133 - 230 - 415 ✓

Brewery 4-145
 Clipper 11-286 ✓
 Blue Jay FV 48-357 ✓
 Old Abe 48-70 (Amended) ✓
 Thomas Jefferson 48-71 ✓
 Vet 112-344 ✓

Check
 102-5944

Lad 237-636 ✓ Den 237-635
 write down data

12 ds

Globe
Court House - Loc'n Notices

Have Loc'n Notices
176/507

✓ Vat - loc'n 25/11/59 rec 25/2/60
H-23-59 112-344

1000' wt? Manganese Cap
230-419 Amended Mar. 17/68
May 6/65

No. ✓ Mad + Dew
loc 1/6/68 rec 21/7/68
2 1/6/68 11/7/68
237 - 636 & 635

— Galena
230-416 Amended Mar. 17/68
May 6/65

✓ Clippu - rec Jan, 20/1/06? loc'n 20/1/06
3-23-06 11-286

— Lost Knife No. 1
230-418 Amended Mar. 17/68
May 23/59

3 Browny - 7-19-32
BJ? 4-145

— Lost Knife No. 2
230-415 Amended Mar. 17/68
Oct. 28/59

3 Thomas Jefferson (Sunrise)
Book 356

✓ Old Abe (amended) loc rec 19/6/59? 102-41
48-70 Book 6-17-59

230-415 Amended Mar. 17/68

✓ Blue Jay Full loc'n rec 21/12/42
11-21-42 48-357 Book

(all Dickerson Lease)

✓ Amended - Lost Knife No. 1 & 2
Manganese Cap
Galena

* "Docket", unless noted as "Book"
LI-50

Mineral Surveys 2525, 2667, 2676, ~~2690~~, ~~2640~~, 3838
pinto? Crown pt

Attendant of Labour - 3 books - name of person who paid for work
(not by claim name): A B C D E F G H I J K L M N O P Q R S T U V W X Y Z

Costa, A.E. & M. - 4 Dickerson lvs - 1967
Carotta Mining Co - 1968 + B.F. vouchers
Home-State - 1969, 1973, Feb. 26/74 (Dickerson)
Dickerson - 1965, 1967, 1968, 1969,
Milca Mining Co & Kanestelce - 1969
Milca 1968 (min 31 - Old Abe)

Cities Service
Oct. 13/70
Old Mar, CA
No. 1 unit, etc.
1972, 1973
Tennessee Corp'n 1969
Drap'n - Moonrise
Ranbar, Stars &
Stripes

355-213 & 216
(over)
COPY

1. Loc'n monument
2. End centers
3. Corners

Laura Regis borrowing Min'l Rights
in Arizona, Phoenix

State Dept Min'l Res - 19th Hu & McDowell - Fair Grounds

176/500

LOCATION NOTICE

LODE MINING CLAIM

This mining claim, the name of which is the MANGANESE CAP
mining claim, was located by the undersigned ARNOLD W. DICHERSON AND ARTHUR E. COFF
on the 6TH day of MAY 19 65

This claim is 1500 feet long and 600 feet wide, and the point of
discovery is 500 feet from the NORTHEASTLY end and 7000 feet from the SOUTHEASTLY
end of this claim.

The general course of this claim is from NORTH to SOUTH

This claim is situated and located in the PINTO
Mining District, in GILA County, State of Arizona, about 3 MILES FROM PERREY HILL
in a SOUTH WESTERLY direction from PERREY HILL

ONE MILE WEST FROM CATYS MALNIN CAP. JOINING ON EAST OF ST. CHARLES WEST MINE
AND ON NORTH OF THE PINTO VALLEY MINING PROPERTY

SURFACE BOUNDARIES:

LOCATION MONUMENT 500 FT. TO THE NORTH THEN 300 FT. TO THE WEST 1500 FT. TO THE
SOUTH CORNER. THIS CLAIM BEING 600 FT. WIDE AND 1500 FT. LONG

Dated and posted on the ground the day and year first above written.

Witness: _____

LOCATION NOTICE

LODE MINING CLAIM

This mining claim, the name of which is the GALENA
mining claim, was located by the undersigned AROLD L. DICKERSON AND ANTHONY E. COSTA
on the 6TH day of MAY 19 65

This claim is 1500 feet long and 600 feet wide, and the point of
discovery is 300 feet from the NORTHERLY end and 1200 feet from the SOUTHERLY
end of this claim.

The general course of this claim is from SOUTHERLY to NORTHERLY

This claim is situated and located in the PINTO
Mining District, in GILA County, State of Arizona, about 3 MILES
in a SOUTHERLY direction from PEREY HILL ONE HALF MILE FROM
CACTUS MINE. AND JOINING ON THE EAST OF MARGARET CARL WEST MINE
SURFACE BOUNDARIES!
LOCATION MONUMENT IS 300 FT TO THE NORTH

Dated and posted on the ground the day and year first above written.

Witness: _____

LOCATION NOTICE

LODE MINING CLAIM

This mining claim, the name of which is the LOST KNIFE #1
mining claim, was located by the undersigned MR. ARNOLD L. DICKERSON AND MR. MERRILL J.
DICKERSON on the 23 day of MAY 19 59

This claim is 1500 feet long and 600 feet wide, and the point of
discovery is 600 feet from the NORTH-WESTERN end and 900 feet from the
SOUTH-EASTERN end of this claim.

The general course of this claim is from NORTH-WESTERN to SOUTH-EASTERN

This claim is situated and located in the MIAMI

Mining District, in GILA County, State of Arizona, about 1/4 MILE

in a SOUTHERLY direction from THE CAROLITA MINE IN PINTO CANYON,

PAUL'S GULCH - PINTO CANYON ROAD - APPROX. SOUTH END OF THE LOST KNIFE

CLAIM #1. THE LOST KNIFE CLAIM #1 JOINS THE MARGARET CLAIM ON THE

NORTH-WESTERN END, ALSO JOINS THE SAN CHARLES CLAIM, WHICH IS A

PATENTED CLAIM ON THE NORTH EAST SIDE OF THE LOST KNIFE CLAIM #1, RANGE 13,

EAST TOWNSHIP 1, NORTH

Dated and posted on the ground the day and year first above written.

Witness: _____

LOCATION NOTICE

LODE MINING CLAIM

This mining claim, the name of which is the LOST KNIFE #2
mining claim, was located by the undersigned ARNOLD L. DICKERSON AND A. F. COLE
on the 28TH day of OCTOBER 1959

This claim is 1500 feet long and 600 feet wide, and the point of
discovery is APPRX 400 feet from the NORTH WESTERLY end and APPRX 1100 feet from the SOUTH-EASTERLY
end of this claim.

The general course of this claim is from NORTH - WESTERLY to SOUTH EASTERLY

This claim is situated and located in the MIAMI

Mining District, in GILA County, State of Arizona, about 1/2 MILE

in a SOUTHERLY direction from THE CAROLITA MINE IN PINTO CANYON

PAUL'S GULCH - PINTO CANYON ROAD CROSSING SOUTH END OF LOST KNIFE #2 CLAIM

THE LOST KNIFE #2 CLAIM JOINS MANGANESE CAP CLAIM ON THE NORTH WESTERLY

END, ALSO JOINS THE LOST KNIFE #1 CLAIM ON THE NORTHEAST SIDE OF THE LOST

KNIFE #2 CLAIM.

RANGE 13, EAST, TOWNSHIP 1, NORTH

Dated and posted on the ground the day and year first above written.

Witness: _____

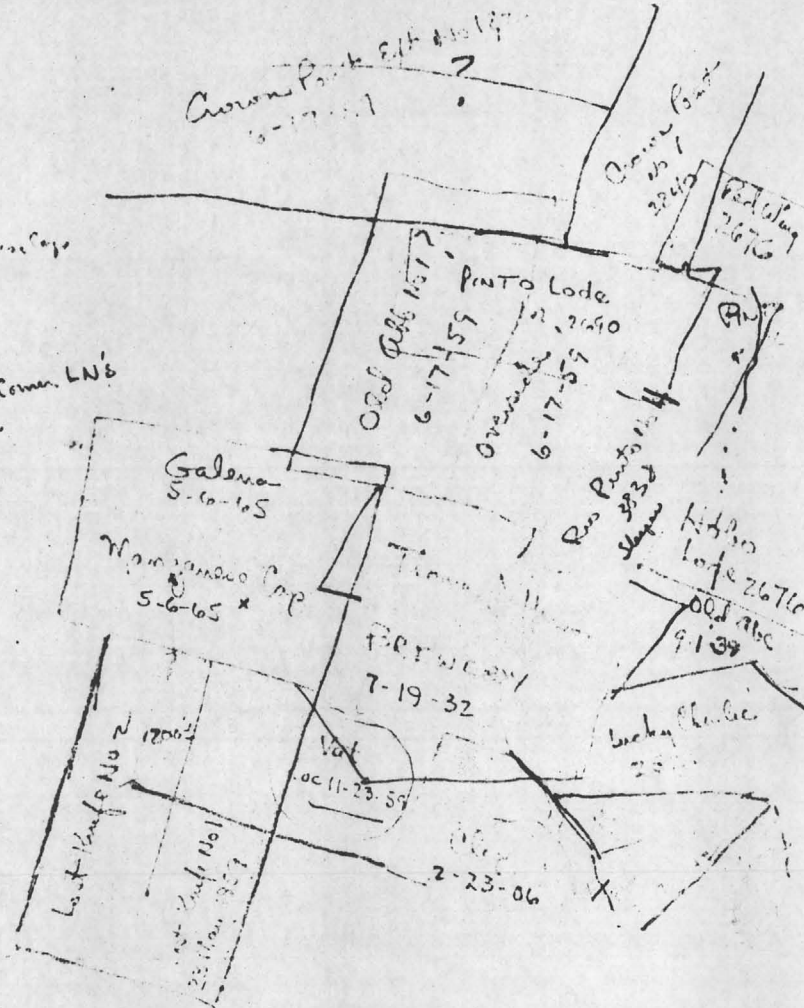
MEMO...

2667	7690
2525	2840
3838	

*Mineral
Surveys*

*N 55° W 350'
Galena & Mangrove Cops*

*N 35° E Common Corner LNE
& Wc Man Cops*



EVANS-HARBOR PRODUCTS CO.

A SUBSIDIARY OF .

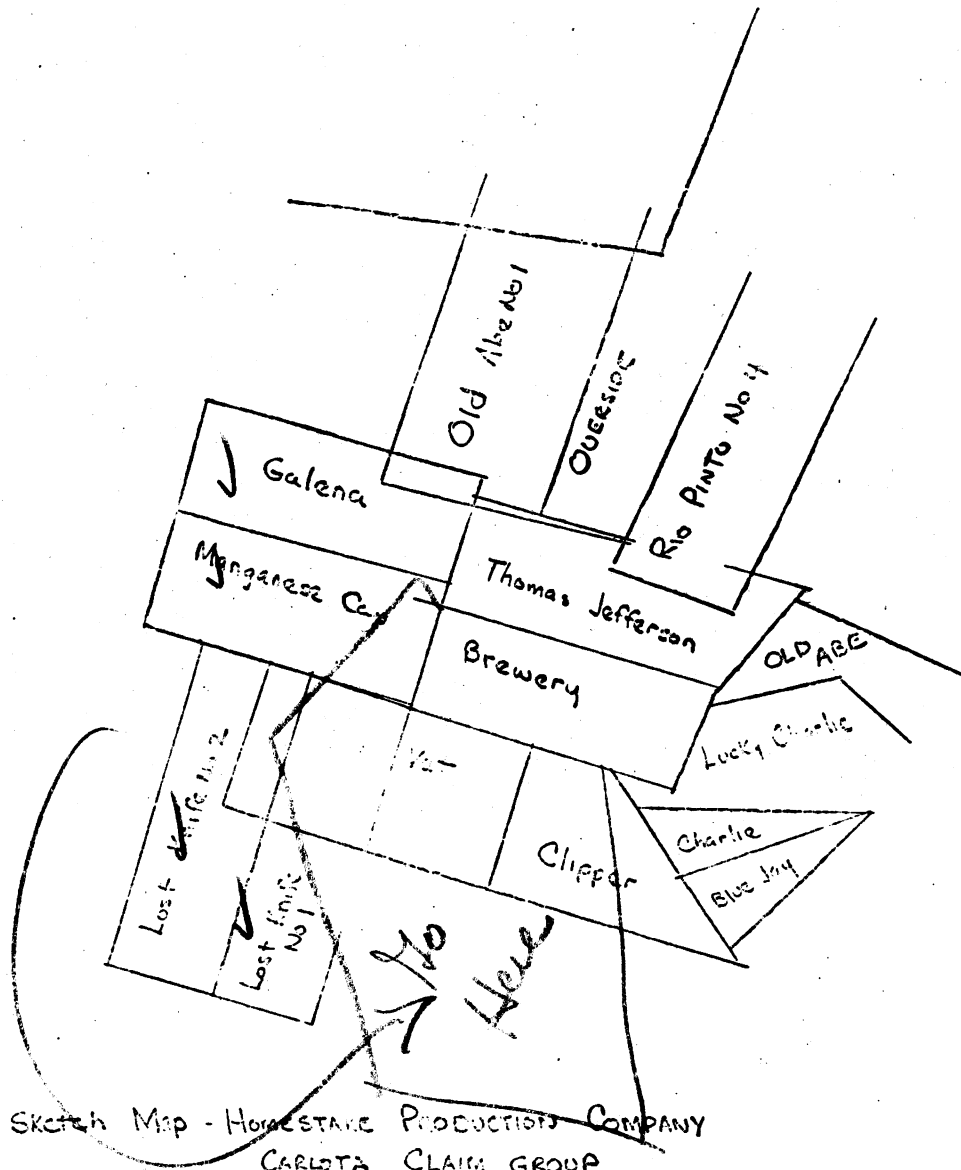


Street Address:
1838 N. 23rd Ave.
Phoenix 9, Ariz.

PHONE
254-6311

Mailing Address:
P. O. Box 6662
Phoenix 5, Ariz.

Evanite
BUILDING
MATERIALS



Sketch Map - Homestake Production Company
 CARLOTA CLAIM GROUP

Property of A.L. Dickerson - suppose to show relation of Dickerson's claims
 to Carlota Group as identified by Homestake's engineer

Cary -

Carlota Ept No 1

No 2

No 3

237

461

8th July 1968
3/4 mile N westerly from Pinto Creek & Coates Mine
50' Easterly 1450' westerly
General Course East to West

462

Same as above
50' westerly, 1450' Easterly 11/2 mile N westerly

463

3/4 mile N westerly Pinto Creek & Coates Mine
50' westerly, 1000' Easterly

(See back p. 46)

6-390, 6-401, 27-149

Thur
Jul. 11/74

Carlota Claims

1881-1901	Sunrise	4-12-81	1-94		7-15-98	6-312	Schasse
		5-18-81	1-117		12-4-00	5-637	McAfee
		12-15-81	1-340				
		12-27-84	2-339				

Sun Rise	9-11-95	5-249	Coleman				
	12-21-99 ⁸	6-356	Gilmo		Description good - N side Brewery		
"Sun Rise"	(index)? 3-1-99	6-390	Gilmo		Rising Sun Miller's Well		
					NE side Brewery Mine		

similar

1881-1901	"Moon Rise"	2-15-99	6-401	Gilmo	W.E. of the Brewery Mine (no others).		
-----------	-------------	---------	-------	-------	--	--	--

1881-1901	(pre 7-10-09) Lost Dollar	None	1901-1910	None	1910-1919	9-15-13	25-69
(from survey 2676)		1881-1901	None				
	Lost Dollar	No 1, 2, 3	1901-1910	4-6-09	19-227, 228, 229.		

This old
low probably
would precede
Sun Rise &
Rio Pinto No. 4
indentation
possibly ok.

		1919-1947	1910-1919	1901-1910	1881-1901
Old Crow				1-5-04 9-215 11-6-01 7-434	Work at D.M. Bremen 2-3-99 5-428
Rio Pinto No. 4	None	✓	Kelly 1-1-15	Nothing re re-loc'n 27-149	None
Trackite		2		2-7-06 11-130 P.M.L. Amended 10-27-09 16-32	None
Filicite				Pinto Cop Min Co 10-27-09 20-141	None

Lookout 1-8-98 6-269 5-3-99 7-70 1-29-08 17-22
Look Out 5-6-99 6-925 3-20-09 18-954

Lulita 5-19-09 8-628 Cactus Dev Co

TRAVIS L. GANT & ASSOCIATES

PROFESSIONAL ENGINEERS & SURVEYORS

**110 BLAZER DRIVE
GLOBE, ARIZONA**

**TRAVIS L. GANT, P.E.
REG. CIVIL ENGINEER
AND LAND SURVEYOR
U.S. MINERAL SURVEYOR**

**P.O. BOX 943
GLOBE, ARIZONA
PHONE 425-6131**

June 25/74

Ted Gunt has copies of all

Carlota location notices, plus mineral
survey plats for adjacent patented ground, etc.



P.S. Ted's in Alaska for 3 weeks, or so. Get
any data from his wife Joyce.

Party chief - Earl Harman - 425-6525

Bernie Stannus

Jun. 18/74

PINE TREE #4, CM Medlock JR. Dec 18 1973.

1500 x 600 - Discovery is 10' from SW end & 1490' from NE

Course - SW - NE.

13,130' S-34°16'W from center of Pinto Valley Mine.

PINE TREE #1 CM Medlock JR Dec 18/73

1500 x 600 Discovery is 10' from NE end & 1490' from SW end.

Course is NE to SW

13,200 ft S31°-51'W from " " " " "

Witness D.R. Norman.

from Lad location to Pine Tree 4 - bearing 302° (compass)

Rock Mnd #1 - bearing 298° (compass).

Rock Mnd #2 - bearing 248° (compass).

from Rock Mnd 2 to Lad Loc - bearing 70° compass.

Rock Mnd 2 to Rock Mnd 1 - bearing 16° compass - 350'

Rock Mnd

Sun.

Jul. 21/74

Claim corners for 50-scale plan.

- Rio Pinto No. 4 - SW & S corners
- Thomas Jefferson - E, SE, NW, & W
- Moon Rise - E, SE, W
- Stars and Stripes - E, SE, W
- Brewery - SE, E, W, NW
- Lucky (the one with house) - W, SW, NE
- Old Abe - split with Miami.

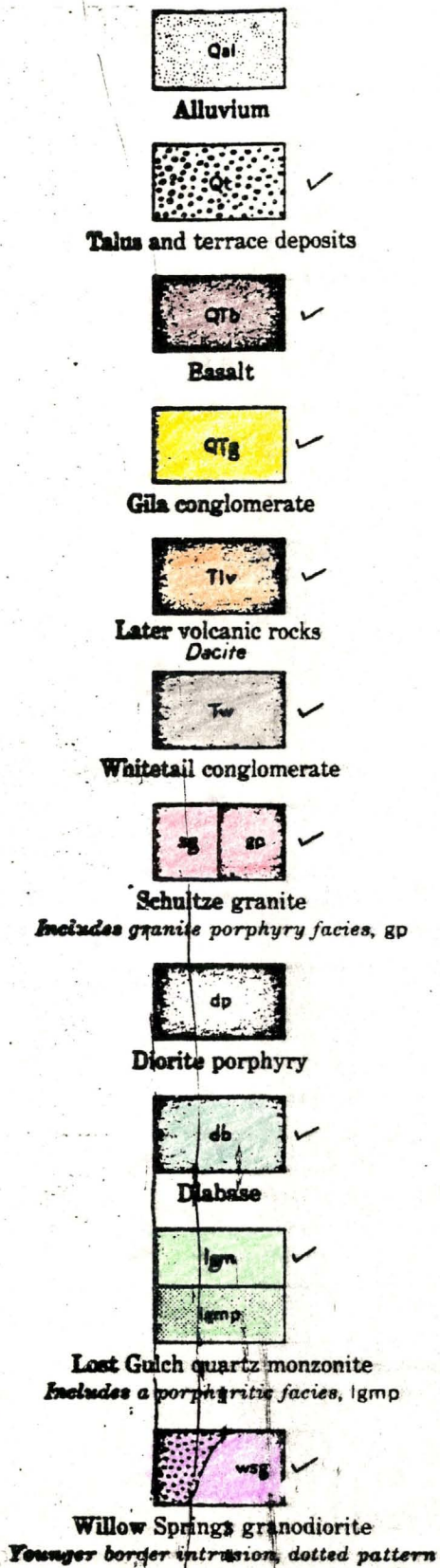
✓ Moved to Ted Grant
 Mon. Jul. 22/74
 12:00pm
 (work on tomorrow)
 vs Sunrise

Tue
Jul. 23/74

(from
 work files
 packet 355
 page 214)

<u>Claim</u>	<u>Book or Docket</u>	<u>Page</u>
Brewery	4	145
Clipper	11	286
Old Abe	48	70
	See also Quit Claim Deed	May 7/47
	(102	39 Miami?)
Thomas Jefferson	48	71 (Sun Rise BK 6 - p. 356)
Blue Jay Fraction	48	357 & 358 (BK 6 - p. 300)
Lost Knife #1	100	416
Amended	230	418
Lost Knife #2	108	133
Amended	230	415
Vat	112	344
Manganese Cap	176	507
Amended	230	419 & 420
Galena	176	508
Amended	230	416 & 417
Dew	237	635
Lad	237	636

LEGEND

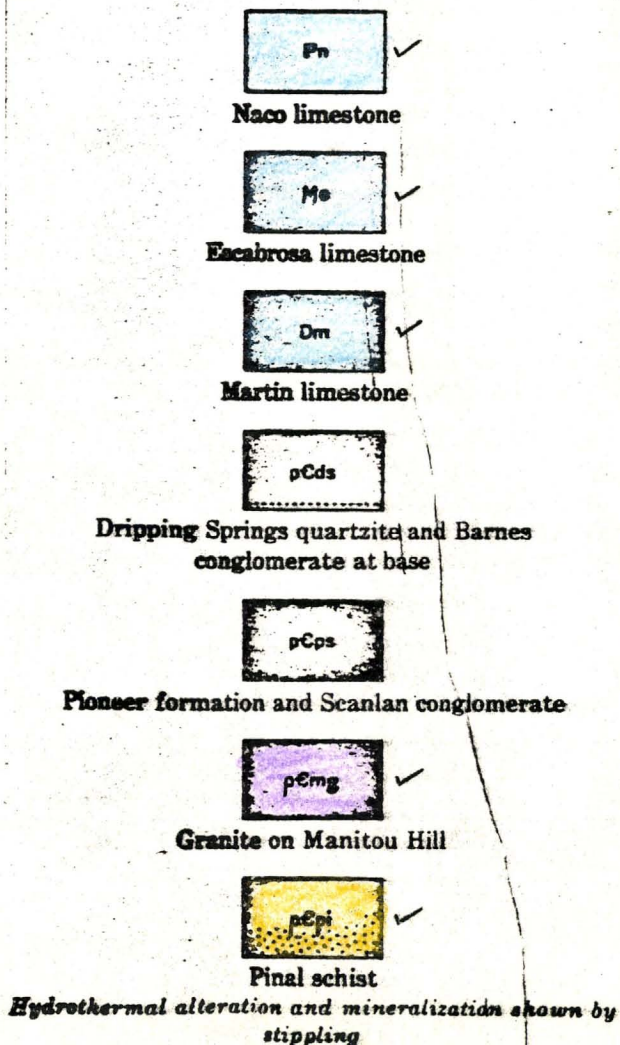


QUATERNARY

TERTIARY AND QUATERNARY

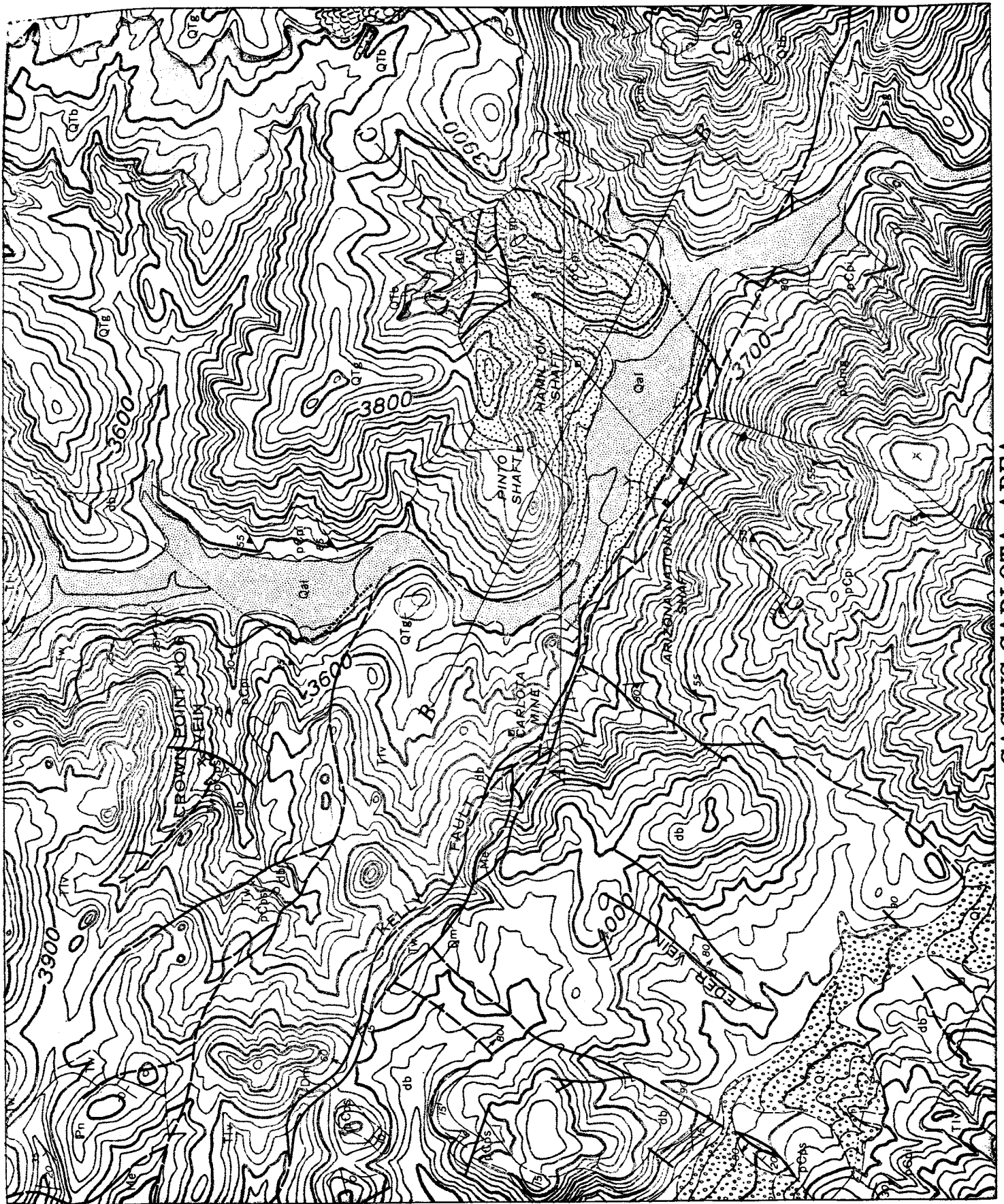
TERTIARY(?)

CRETACEOUS OR TERTIARY



PENNSYLVANIAN
MISSISSIPPIAN
DEVONIAN
PRECAMBRIAN

CARBONIFEROUS



CACTUS-CARLOTA AREA

"DON'T SAY IT--
WRITE IT"

INTER-OFFICE MEMORANDUM

Truman

HOME-STAKE PRODUCTION COMPANY

TO Mr. R. S. Trippat
FROM Dennis K. Pickens

DATE December 11, 1968

SUBJECT Comparison Sulphur Processes

- 1) Attached you will find a comparison of our process with four other processes which Benguet Consolidated considers as workable and technically sound. The Potosi process is too crude and too expensive to be considered. We have not included the following:
 - a) Dibrox Process - this is a solvent extraction system using methyl isobutyl carbinol and a plant is being built using this process in Nevada, but Mr. Davidson of Benguet says it is too expensive.
 - b) Catalano or CH/ process (see my memo of November 26) which is essentially the same as the Thermochem process (comparison attached) in that it is a solvent extraction process said to use trimethyl chloride. Mr. Davidson had visited the alleged pilot plant at Sakersfield on two occasions and in neither case was it running and he has concluded that it is strictly a promotion, although if the patenters got their number 739230 application in ahead of the Vancouver Thermochem group there may be a conflict.
 - c) Elkor - because it is based upon treating the gypsum normally associated with elemental sulphur and the economics are based upon the sale of the by-product calcium oxide.
- 2) Mr. Davidson claims that his modified Manza process which he has piloted both in the Philippines and at the Colorado School of Mines Research Foundation comes the closest to the simplicity of our two systems. However, when he claims costs of \$9.82 I am sure he is bargaining because he said they "hoped" to cut the retention time (3 hours to 15 minutes) but admitted this had not been accomplished yet. We conclude that the Manza process is the closest to competing with ours on the basis of Mr. Davidson's figures.
- 3) We may hear of other processes from time to time because American Ingenuity invariably attacks any shortage problem with great intensity. I feel we are ten years ahead and that the simple comparison of the process steps as given in the attached where we eliminate fine grinding and preliminary flotation show that our process will be difficult, if

December 11, 1968

not impossible, to beat both as regards to capital and operating costs.

The comparison, incidentally, is made adjusted to Benguet's proposed size plant so that each of the processes is properly compared as to starting volume and quality of ore feed even though one ore is Philippine and the other Costa Rican.

- 4) We are still testing Philippine ores for the best combination of steps as well as retention time, pressure, etc. So far it looks as though the Benz modification may be the best.

DKP:hj

Enclosure



cc: Mr. Frank Sims
Mr. John Long
Mr. Herbert Dahlman
Mr. George Freeman
Mr. Percy Coe

P. S. We will add to this comparison the consumption of water, steam and electricity for each process shown as soon as this data can be checked out.

COMPARISON KNOWN PROVEN PROCESSES - EXTRACTION SURFACE SULPHUR

(Prepared by D. K. Pickens from Files and from Data Supplied by Benguet Consolidated)

All figures adjusted to 2000 TPD - 30% Ore - 500 Tons Day Sulphur
(Omitting Mining Costs)

ITEM	HOME-STAKE	HOME-STAKE (Benz Modification)	MANZA	CHEMICO (Manza Modifi- cation) (Colo. Found.)	POTOSI	THERMACHEM (Pilot Plant at Colo. Found.)
<u>Capital Costs</u>	\$1,250,000	\$1,350,000	\$3,000,000	\$2,250,000	NA	\$3,000,000
<u>Direct Operating Costs</u>	\$4.94	\$5.49	\$8.00	\$7.00	\$20.00	\$8.00
Depreciation/10 yr.	.83	.90	2.00	1.82	NA	2.00
Total	\$5.77	\$6.39	\$10.00	\$8.82	NA	\$10.00 (claimed)
<u>Process Steps</u>						
1) Crushing	to ½"	to ½"	to ½"	to 10 mesh	no crushing	to ¼"
2) Fine Grinding	none	none	65% -200	all -48 mesh	finest screened out	-100 mesh
3) Flotation (Raise grade to 50% sulphur)	none	none	88% recovery	none	none	none
4) Autoclaving (or melting)	15 min. 30 psi	15 min. 30 psi	3 hours 30 psi	15 min. 30 psi	3 hours steam only	Pressure leaching w/chlorinated hydrocarbon
5) Pressure Screening	Removes 50% barren material 94% recovery	Removes 50% barren material 94% recovery	none	none	none	none
6) Flotation (after autoclaving)	none	50% of material	50% refloated 88% recovery	50% refloated 90% recovery	none	none
7) Pressure Centrifugation	87% recovery 10 min. cycle	95% recovery 10 min. cycle on 80% concentrate	none	none	none	none
8) Filtration	None	None	98% to 99.7%	90% to 99.6%	95% to 99.6%	not required
9) Solvent Recovery	None	None	None	None	None	System not disclosed
<u>Overall Recovery</u>						
a) Costa Rican	87½%	92%		(Under test)	NA	95%(claimed)
b) Philippine	(Under test)	(Under test)	88½%	90%		95%(claimed)

SUMMARY OF HOME-STAKE
1968 PROGRAM

1. Home-Stake is an established corporation of many years standing. We conduct our operations on properties with large known oil reserves rather than by wildcatting. Because of the conservatism of secondary recovery from these known reserves your profit on money invested in Home-Stake is calculated at about 300% disregarding taxes, and at over 700% considering tax advantages for those in the higher brackets. (You will note on Page 14, of the Budget Section that these calculations are based on a 55% bracket. Of course the higher your tax bracket the greater your profit.)

2. You can deduct 106% of your investment in Home-Stake from your taxable income.

3. Also, 27 1/2% of your gross oil income is tax free.

4. Home-Stake operates on a fixed price contract with you, and there are no over-calls.

5. The reversionary interest of Home-Stake is only 20%, which takes effect only after a participant's gross investment is returned to him. Consequently Home-Stake must prudently operate your properties in order to secure and maximize its own interest.

6. The Company has an outstanding staff of over 250 highly qualified people and some of the leading experts in secondary recovery who have come to us from the major oil companies.

You may want to peruse the first two sections of the Program Book and particularly the last page of the second section which gives the calculated income per unit each year. The other sections indicate how thoroughly Home-Stake analyzes its separate properties.

With the progress of the Company, we are having a larger program this year and we are inviting additional investors to join us. Home-Stake's programs are usually subscribed by mid-summer; if you wish, a participation can be reserved. Payments will not be due until the last half of this year and the first half of next year.

All in all, Home-Stake offers a valuable way of converting tax dollars into an oil equity, and hence into a second income.

Jesse G. Wolf
450 N. Devereaux St.
Globe, Arizona 85501
August 10, 1968

Dennis Pickins
Homestake Productions
55 E. Thomas
Room 103
Phoenix, Arizona

Dear Sir:

My partner, Henry F. Huffman and I are aware that your Company is drilling the area of the old Carlotta Mine in Pinto Creek.

We have a group of mining claims in that immediate area, and thought that you would like to inspect or examine them in the hope that you would be interested in some sort of agreement to drill them.

We have good indications of mineral on the surface and from reports of geologists who have prospected them, there should be an ore body of commercial value below the surface.

If you or your geologist should care to look these over please let me know and I will make the necessary arrangements.

Sincerely yours

Jesse G. Wolf
Jesse G. Wolf

JOHN L. ALEXANDER

QUIROZ Y MORA NO. 93 - TELEFONOS 9 Y 183

APARTADO POSTAL NO. 54

CABORCA, SONORA, MEXICO

8 / 12 / 66

Mr. Sherwood B. Owens
Box 769
Tucson, Arizona.
U S A

Dear Mr. Owens;

Referring to our conversation the other day at lunch, I think you have a very good chance to develop a worth while mine at the Carlota.

As you know my Father and I owned the property since about 1920, having bought it from the original locator. Practically all the development work shown on the Composite Map which you have was done by us. My Father had the original 300 Level driven on the Hanging Wall Vein before I took over. This caved and I never saw all of it. It went father into the hill than any of the workings I made.

He drove a crosscut to the North from some point near the face of this drift and cut what he described as probably the upward continuation of the silicious ore opened up in the old 400' shaft. I dont recall the copper content of the ore he encountered here but it was possibly around two or three percent.

Ore outcrops on surface some 150' West of the underground workings and no work was ever done to develop ore at this point.

Going East no work was done, except the start of the 300 drift level, from the Vertical Section shown as D - D' to the end line of the claim. Both ore in place and float is found across this entire distance. I intended to sink a new shaft here about the end of the War, but due to the impending stoppage of the Bonus Price on copper, did not do so.

I think that development work on this East end would show up a continuation of both Foot Wall and Hanging Wall Ore Bodies. The same is probably true on the West end, where surface outcrops are seen.

Getting back to this East end, I did not look for the downward continuation of the ore on the 300 Level, shown on Section D - D', as the grade of ore shown above was a little low for the price I was recieving for copper then. I did find about a

ten foot width of 6% copper on the Hanging Wall Vein at this point, which I figured as the top of a new ore chute on this vein.

Again I did no work on this as there was only about 40' of backs and I was working on a fifty foot width of 5% ore at the time. This should certainly be explored at depth. There should be a nice ore body here on both the Foot and Hanging Wall occurrences.

The ore body which the old maps showed as being opened up on the 400' level of the old shaft should by all means be prospected at depth. Probably drilling would be the most practical method on the start to get some new information. The 60' of 3.4% copper reported here could be the making of a big mine. This should be drilled both above and below this level and at the same time the holes should be drilled far enough to cut both the Foot Wall and the Hanging Wall ore bodies, below the present mine workings, which more or less parallel each other.

The property needs some systematic development work both laterally and in depth. I only tried to open up ore of shipping grade and made no attempt to block out ore for the future.

The ore bodies on this Carlota property lay along the Kelly Fault, which extends for at least a mile to the East cutting across several claims of the Miami Copper Co. This Fault shows ore along its entire length across these claims.

I leased on a portion of this area on the Miami ground and found very good ore. I had some old maps made by the people who did all the development in this area about 1912. One of these I had occasion to check out in my development work there and found it as represented. Another map of a portion of this ground, by these same people, shows a shaft on the Kelly Fault to the South side of Pinto Creek, some 300' deep. From this shaft crosscuts were run both North and South. In the crosscut to the North the map shows a 40' width of 8% oxide copper, just about under Pinto Creek. This would be about the same depth as the 400' level of the old shaft on the Carlota.

Two or three years back the Miami Company did a lot of drilling in this section and I was told encountered some very good ore.

The same cemented breccia found in the Cactus Mine of the Miami Copper occurs along side the Kelly Fault, to the South side of the old 400' shaft, on the Carlota property.

This breccia, carrying copper, occurs almost parallel to the Hanging Wall Vein. Without doubt this is connected with the Cactus ore body and probably a part of same, apexing along side the Fault on Carlota ground.

Should the Miami ever mine the Cactus ore body or the ore occurring along the Kelly Fault to the South of Pinto Creek, they will almost be forced to buy the Carlota for protection, in my opinion.

On top of the Carlota hill above the mine there is an outcrop that was never investigated beyond two or three surface diggings in which a little gold was reported. This is quite wide as I recall and strikes N - S. Some drilling at depth should be done here also. This shows up to the South of the Kelly Fault and its known ore bodies.

If it should ever be of help to you I would be pleased to meet you on the ground and go over some of these possibilities there, showing what I recall of the occurrences and structures.

Wishing you every success on the development of this property, I am.

Sincerely yours



John L. Alexander

Travis L. Gant & Associates

PROFESSIONAL ENGINEERS & SURVEYORS

MAILING ADDRESS:
P. O. BOX 943
GLOBE, ARIZONA 85501

PHONE: 425-6131 • 110 BLAZER DR., GLOBE, ARIZONA

August 12, 1974

Aerial Mapping Co.
2958 W. Clarendon Ave.
Phoenix, Arizona 85017

RE: CARLOTA MINE
Crown King Investment Co.
Aerial Mapping, between
Miami and Pinal Ranch

Attn: Mr. Ken Donley, Pres.

Dear Ken:

We are now submitting the information you need for proceeding with Jim Simpson's aerial mapping project for your client, Crown King Investment Co. This flight was made August 1, 1974. We have been taking our instructions here from Chris Armstrong who represents the Consolidated Fortune Channel Mines, Inc., of Prescott, Ariz., address 202-117 E. Gurley Street, whose legal counsel is Donald Head of Head and Toci, P.C., P.O. Box 591, Prescott, Ariz., 86301. The results of our survey are as follows:

Panel	Designation	N. Coord.	E. Coord.	Grd. Elev.
	"B"	7723.39	14288.00	4581.6
	"Y"	11093.26	18103.56	4470.6
	"Z"	8152.26	19675.68	4587.5
	"T"	17966.64	15460.75	3533.7
	"U"	18761.60	15177.46	3763.4
	"V"	20001.50	13929.11	3657.9
	"AA"	20832.26	20265.13	3976.8
	"BB"	17371.30	18722.74	4198.5
	PG-12	19629.68	11723.29	3968.4
	PG-13	18143.05	12272.11	4061.6
	PG-14	17360.00	12860.00	4110.6
	PG-37	16674.39	14692.01	4146.1
	PG-40	14180.46	15669.16	4530.3
	PG-49	18503.64	14258.29	3641.6
	Carlota B.M.	18506.04	14254.95	3642.23 (C&GS)

I don't know whether you can incorporate any of the info which I sent you on 5/10/74 into this new work; if so, you would probably need to know that Target "A" was destroyed. Target "L" is probably also gone, although I didn't check it. If there is any further information you need, please call.

Sincerely yours,

Travis L. Gant

Travis L. Gant, P.E.

TLG/lag



Exploration Department • P. O. Box 426, Boulder City, Nevada 89005 • (702) 293-2817

August 8, 1974

Mr. Chris Armstrong
c/o Copper Hills Motel
Miami, Arizona

Dear Chris,

Enclosed are the typed results from Cutlass' DDH- C-21.

We didn't mean to run off with them--sorry. Thanks very much for showing us around the property. Good luck.

Regards,

A handwritten signature in cursive script that reads "Bruce".

Bruce A. Bouley

/b

enclosures

SAM J. HEAD (1907-1968)
DONALD R. HEAD
PHILIP E. TOCI
JAMES B. MUSGROVE
MICHAEL R. MURPHY

HEAD & TOCI, P. C.
ATTORNEYS AT LAW
117 EAST GURLEY STREET
PRESCOTT, ARIZONA 86301

MAILING ADDRESS
POST OFFICE Box 591
TELEPHONE [602] 445-6860

August 1, 1974

Mr. James Simpson
Post Office Box "L"
Miami, Arizona 85539

Dear Jim:

Enclosed herewith is another bill from Longyear Company. Would you please review same and, if in order, indicate your approval thereon and return the same to us for payment.

Sincerely yours,

HEAD & TOCI, p.c.

By *Don*

DRH:jmw
Encl:

Jul. 1-15

*OK'd
Aug. 2/24
MLL
(mailed Aug. 3)
Requested Don send
us an Xerox copy-*

SAM J. HEAD (1907-1968)
DONALD R. HEAD
PHILIP E. TOCI
JAMES B. MUSGROVE
MICHAEL R. MURPHY

HEAD & TOCI, P. C.
ATTORNEYS AT LAW
117 EAST GURLEY STREET
PRESCOTT, ARIZONA 86301

MAILING ADDRESS
POST OFFICE BOX 591
TELEPHONE [602] 445-6860

July 26, 1974

Mr. Christopher Armstrong
Post Office Box "L"
Miami, Arizona 85539

Dear Mr. Armstrong:

Enclosed herewith please find the original and one copy of invoices from Longyear Company concerning Consolidated Fortune Channel Mines, Inc.

Please review them and if in order, please indicate your approval thereon and return to this office for payment.

Sincerely,

HEAD & TOCI, p. c.

BY *Donald R. Head /chm*

/chm

*OK'd a mailed original
Jul. 30/74
MR*

May 29, 1974

MEMO

TO: Paul Sawyer

FROM: Consolidated Fortune Channel Mines

Enclosed is a copy of our contract for drilling with Longyear Company at Carlota Mine per your request.

I am also enclosing 2 W-4 forms for possible future use.

Regarding your expenses, please submit a statement periodically to:

Head & Toci, p.c.

P. O. Box 591

Prescott, AZ 86301

ATTN: Mrs. Bertha Elwing

This should show your professional fee as well as necessary expenses, receipts attached, for period statement is submitted for.

A handwritten signature in cursive script, appearing to read "Robin".

MAILING ADDRESS:
P. O. BOX 943
GLOBE, ARIZONA 85501

PHONE: 425-6131 • 110 BLAZER DR., GLOBE, ARIZONA

FEE SCHEDULE FOR PROFESSIONAL ENGINEERING
AND SURVEYING SERVICES

Effective March 1, 1974

Hourly Rates:

Field Services:

Basic 3-man Survey Crew:	28.00
4-man Survey Crew: (E.D.M. & Theodolite)	36.00
2-man Survey Crew:	20.00

Note: Rates for crews engaged in monumenting shall be @ \$3.00/hr. less than rates shown above.

Field-man, working alone:	7.50
Field services by Prof. Engineer:	12.50

Office Services:

Professional Engineering: Consultation or Design:	25.00
Computing	12.50
Engineering Technician:	10.00
Office Aide:	5.50
Electronic Computer Time:	6.00

NOTE: All the above rates are for regular 8-hour days.

When it is requested by the Client, or deemed to be in the Client's best interest, overtime will be worked; the rate charged shall be regular rate + a 30% surcharge. All Saturday, Sunday, or holiday time shall be overtime, as well as any time worked over 8 hours in a regular day.

It is our policy to charge to the Client daily travel time from our office to the job site. At the end of the work-day, we pay return trip time if less than one hour; travel time in excess of one hour is charged at regular rates listed above.

Transportation: Four-wheel-drive vehicles are used exclusively. Rates are 20¢ per mile, on or off highway. Minimum daily charge is \$5.

Special Equipment: Whenever, in our opinion, the use of electronic distance measuring equipment (EDM) will enhance the performance of a survey project, such equipment will be used and the rate will be \$15 per hour; however, daily maximum for EDM will be \$75.

Materials: Reimbursement, plus cost of acquisition. For Clients' printing: blue-line and black-line, reg., @10¢ /S.F.; slower papers, 12¢ / s.f.; sepias, 25¢ /s.f.

Out-of-Town Expenses, including Room and Board:

2-man Crew	35.00/day
3-man Crew:	50.00/day
4-man Crew:	60.00/day

CARLOTTA PROJECT

AS AT

JANUARY 10, 1969

H. W. VAN LOO
P. E. COE

COE AND VAN LOO
CONSULTING ENGINEERS, INC.
4831 NORTH 11TH STREET, SUITE 1
PHOENIX, ARIZONA 85014

TELEPHONE
279-7391

January 13, 1969

Homestake Production Company
P. O. Box 7277
Phoenix, Arizona 85012

Attn: Dennis Pickens

Re: Ore Reserves, Carlotta Mine

Gentlemen:

At your request computations have been made of the oxide ore reserves, both proven and probable, at the Carlotta Mine. In making these computations assay data, obtained from samples taken by exploratory drilling done by your firm, were used.

In determining proven ore reserves, the area of influence of each drill hole was assumed to extend 100 feet to each side in accordance with procedures frequently followed in computing reserves in western copper mines. A further assumption made was that ore in the Kelly fault would average 60 feet in width with an average grade of 1%. Since in many places this fault is known to be 120 feet wide and ore grades run between 2% copper on the surface to 3½% underground, this assumption can be considered conservative. Actually we have been informed that shipping records are available showing that 14,000 tons of ore averaging 3½% in copper have been mined and sent to the smelter in the past.

On the foregoing basis, the double-average end area method was used with vertical cross-sections to compute ore volumes. These volumes were then converted to tonnages by using a unit weight of 160 pounds per cubic foot of ore. This conversion factor has been found to accurately represent the average weight of oxide copper ores in the Miami, Arizona area.

In determining average ore grades, the standard assumption was made that values between sample points in the drill holes will vary at a uniform rate. On this basis, the longitudinal area of influence of each drill hole was established so that every point within that area of influence was nearer the hole involved than it was to any other hole. Assays were weighted on the basis of ore volumes within these respective areas of influence to give a weighted average assay for the entire ore-body.

Probable or inferred ore reserves were determined by using the same basic methods as were used for proven ore. This probable ore includes an inferred lateral extension of the ore horizons beyond the 100 foot distance from each drill hole to the Kelly fault on one side of each hole and an extension beyond the 100 foot limit to the property line on the otherside. Since known ore exists in the fault and ore has been reported at the same level in the adjoining property, this inference is logical and reasonable. Grade of probable ore is assumed to be the same as that computed for proven ore.

In computing the amount of waste excavation required to make mining physically possible, the necessity of following safe, practicable and feasible mining methods was considered. Excavation side slopes were set at 1:1 in conformance with standard design procedures and the normal requirements for benching and haul roads would be met. On this basis, it is estimated that the ratio of waste to ore mined would be 4 to 1, i.e., 4 tons of waste would have to be removed per ton of ore recovered.

In summary, computed and probable ore reserves and grades have been computed to be as follows:

<u>Classification</u>	<u>Tons</u>	<u>Grade, Percent, Copper as Oxide</u>
Proven ore	3,175,000	0.9
Probable ore	2,600,000	0.9
Total	5,775,000	0.9

On the 4:1 rates basic total waste removal requirements would be 23,100,000 tons.

All known underground workings have been plotted on a plan map of the mine within a vertical accuracy of \pm 10 feet using data obtained from various older maps of the property. Vertical sections at 100 foot intervals have also been prepared and we are in the process of completing mass overlays of ore outlines on lucite sheets, which will be assembled in the form of a 3-dimensional model of the mine. All this material can be made available to you at your convenience.

It is hoped that the foregoing data will be of assistance to you in your development of future plans for the Carlota Mine. Should further studies or data be desired, we will be pleased to provide them.

Very truly yours,
COE & VAN LOO
Consulting Engineers, Inc.



P. E. Coe

HOME-STAKE PRODUCTION COMPANY

TO Mr. R. S. Trippet
FROM Dennis K. Pickens
DATE January 10, 1969
SUBJECT Carlotta Project as at
January 10, 1969

SUMMARY

As a result of drilling, assaying, surveying, contouring and cross-section analysis, Carlotta now has 3,250,000 tons of proven ore averaging 0.93% oxide copper. In addition, probable (semi-proven) ore is estimated at 3,000,000 tons of the same grade.

If mining were to commence on this block of proven ore, the stripping ratio to obtain this ore is 4 tons to 1 ton of ore (12,800,000 tons) of which an estimated 3,000,000 tons of low grade ore would be piled separately for future heap leaching. As and when additional ore is developed contiguously, the stripping ratio will drop and the economics again improve.

It is not practical to estimate the ultimate, possible, maximum ore body except to say that it could be very large especially if massive sulphides are found under the oxide body or the oxide body persists, or both. We have explored 6 out of 180 acres.

The Carlotta project now appears to meet the low risk, good return criteria generally associated with Home-Stake projects without regard to tax implications.

Applying pricing factors recently used in other copper transactions involving sale of property, adjusted to Carlotta tonnage and grade, the property could be properly and presently valued for sale to third parties at about \$1,250,000 and value will rise rapidly with each additional 500,000 tons proven.

RECOMMENDATIONS

a) Further Drilling

Mr. Freeman and I, after consulting with others skilled in this field, recommend the following:

- 1) A minimum of 10 holes, totaling approximately 7500 feet to fill in areas of probable ore. This drilling is development drilling, is essential, and, we believe, will represent a low risk, very high return expenditure.
- 2) A minimum of one hole (extend #13) to penetrate the schist underlying the oxide at least 400 feet to determine if sul-

phides are present as they are less than 300 feet away from Hole #13 on Miami Copper ground.

- 3) At least one hole each 200 feet apart on the north side of the Kelly Fault. This would involve up to 8 holes, totaling approximately 4500 feet and would be exploratory.
- 4) At least one hole on each claim on the south side of the Kelly Fault for an estimated total of 3000 feet of drilling - this would also be exploratory.

Note: We estimate the cost of this program at \$200,000 maximum, but it could be less if ore body delineates with less footage or it could be more if sulphides are hit, and/or oxides persist beyond probable estimates. Under the latter circumstance, Home-Stake would have a mine of very high value indeed.

b) Open Ore Body

- 5) When the above drilling is completed, or even before completion if thought desirable, the ore body should be opened up to obtain large scale samples for further testing to establish final plant design and most effective mining methods and machines. This could involve approximately \$250,000 to move about 1,000,000 tons of waste.

c) Water Well Test

- 6) Well drilling and testing contract should be let as soon as possible even though there appears little doubt that adequate water is available. This should cost about \$20,000 including casing and pump for first well.

d) Acquisition of Property

- 7) Although the Milca option has lapsed, it would be desirable to purchase their interest. The first offer should be \$100,000 (\$80,000 Milca and \$20,000 Weathers) vs. \$175,000 in option which just expired for Milca (including Weathers). It is believed that Milca will insist on at least \$115,000 because of a bank loan. Weathers will accept \$20,000 for a total of \$135,000 may have to be paid to buy out Milca.
- 8) Dew and Lad claims should be optioned (see memo to RST of December 3, 1968).
- 9) Requirement to build plant should be negotiated out of contract if possible.

- 10) Consideration should be given to buying out Owens and Dickerson before too long.

CONCLUSION

A participation program for this project can now be considered and, I believe, justified. (See Economics - Schedules I, II, III & IV). If a system permitting a high write-off can be perfected, anyone in the 50% or higher bracket should find the project attractive on present proven ore and extremely attractive on proven plus probable ore.

In any participation program, Home-Stake should not include sulphide ores or low grade oxides placed out for future heap leaching.

Respectfully submitted,

Dennis K. Pickens

ORE RESERVES, CROSS-SECTIONS, MAPS, VISUAL AIDS
AND LUCITE MODEL WILL BE BROUGHT BY HAND JANUARY 17, 1969.

COE AND VAN LOO LETTER ON ORE RESERVES BEING PREPARED.
WILL BE MAILED MONDAY, JANUARY 13, 1969.

COE WILL STATE AS FOLLOWS:

PROVEN ORE	3,175,000 tons
PROBABLE	2,600,000 tons
GRADE •	0.9%
WASTE RATIO	4 to 1

OR VERY CLOSE TO FIGURES USED HEREIN.

COE COULD NOT GET LETTER OUT TODAY

January 10, 1969

ORE RESERVES

In summary, the calculated ore reserves and waste ratio are as follows:

Proven Ore	- 3,457,000 tons	- 0.93% Cu
Probable Ore-	3,000,000 "	- 0.90% Cu
Waste	- 16,748,000 "	- Ratio 4:1 (approx.)

Separate are tabulation sheets showing the breakdown of ore reserves and waste tonnages. The "Summary - Proven Ore Calculations" shows the tonnages and weighted average grade in each section.

In determining "Proven Ore" reserve volumes, the double-average end area method was used with vertical cross-sections. Since we had such strong structures in the drill holes, we extended 100 feet to each side at each drill hole ore intersection. For computing from ore volumes to tons, we used a factor of 12 cu. ft./ton ore in place.

The 16,748,000 tons of waste shown includes approximately 2,500,000 tons of the "Probable Ore" reserves. If the Probable ends up being Proven ore, then the waste to ore ratio will improve considerably. Also, as can be seen in cross sections, the waste ratio will be decreased rapidly as the ore zone is extended to the west from Hole #16.

The "Proven Ore" reserves are actually contained in an area 400 ft. x 800 ft.; the 400 ft. being parallel to the Kelly Fault. Since there is a surface outcrop exposure of approximately 400 feet along the Kelly Fault of close to 2% Cu grade, I feel that the assumption of 1% Cu grade for the down dip tonnage of the Kelly Fault zone is very conservative. In addition, to the surface ore outcrop grade, there was 14,000 tons mined underground averaging plus 3% Cu, plus a number of short drill holes averaging over 2%. The crosscut from the bottom of the 400 ft. shaft was reported to have intersected 60 ft. of 3.4% Cu. I also feel that the 60 ft. width used in the calculations is conservative since there were zones mined underground that were over 100 feet wide.

I feel that the chances of extending the ore reserves to the west and down-dip of the Kelly Fault are good since drill hole #16 (furtherest to the west) showed good mineralization with strong structure. As a continuous block, there was 391 feet that averaged 0.60% Cu.

Some deep drilling for copper sulphides should be done in this area of Proven Reserves since I feel, together with several geologists, that we may be drilling in a down-thrust block from the Miami Copper Company's adjoining sulphide ore body; Pinto Creek probably being the fault. From the sections that we have seen of Miami's, they had 150 - 200 feet of schist above their sulphide ore body. Our drill holes #13, 14 and 16 bottomed in schist. Deepening of hole #13 would probably be the cheapest way of proving this since it was drilled to 811 feet and another 200 feet should intersect the sulphides if this theory is correct.

ORE RESERVES (cont'd.)

Vertical sections at 100 ft. intervals with a scale of 1" = 50' have been prepared by Coe and Van Loo, Engineering and Consultant firm, showing drill holes and ore intersections. Also being prepared is a three dimensional model of drilled area made up with lucite sheets.

SUMMARY PROVEN ORE CALCULATIONS - CARLOTTA MINE

Weighted Averages of Grade from Holes and Sections

<u>Section 0 + 00</u>	<u>Tons</u>	<u>Grade</u>	<u>Distribution Factor</u>
	132,000 tons	0.80% Cu	1056.0
	157,000 "	0.76% "	1193.2
	271,000 "	0.78% "	2113.8
	350,000 "	1.00% "	3500.0
Total	<u>910,000 "</u>	<u>0.86% Cu</u> <i>0.864</i>	<u>7863.0</u>
<u>Section 0 + 100</u>	Averaged Section 0 + 00 and 0 + 200		
	903,000 tons	0.93% Cu	
<u>Section 0 + 200</u>			
	357,000 tons	1.05% Cu	3748.5
	190,000 "	0.97% "	1843.0
	350,000 "	1.00% "	3500.0
Total	<u>897,000 tons</u>	<u>1.01% Cu</u> <i>1.014</i>	<u>9091.5</u>
<u>Section 0 + 300</u>			
	132,000 tons	1.11% Cu	1465.2
	215,000 "	0.70% "	1505.0
	400,000 "	1.0 % "	4000.0
Total	<u>747,000 tons</u>	<u>0.93% Cu</u> <i>0.933</i>	<u>6970.2</u>
<u>Total and Average</u>			
	910,000 tons	0.864	7826.0 <i>7863.0</i>
	903,000 "	0.930	8397.9 <i>8397.9</i>
	897,000 "	1.014	9059.7 <i>9091.5</i>
	<u>747,000 "</u>	<u>0.933</u>	<u>6947.1</u> <i>6970.2</i>
	3,457,000 tons	0.93% Cu <i>0.934</i>	32,230.7 <i>32,322.6</i>

J. C. Lerman
1/15/69

SUMMARY - WASTE CALCULATIONS

(To Vert. Boundary to North and Miami Property)

Section 0 + 00	2,392,000 tons
Section 0 + 100	2,171,000 "
Section 0 + 200	1,950,000 "
Section 0 + 300	<u>2,235,000 "</u>
	8,748,000 tons
Plus 50° pit slope to the West (assuming no ore extension to West)	<u>8,000,000 tons</u>
	16,748,000 total tons waste (including "probable ore")

NOTE: Included in the above 8,748,000 tons of waste within Sections 0 + 00 to 0 + 300 are 1,536,000 tons of "Probable Ore".

Of the 8,000,000 tons of waste as pit slope to the west is included an additional 1,000,000 tons of "Probable Ore".

CARLOTTA MINE

SUMMARY HOLE #11

<u>Depth</u>	<u>Footage</u>	<u>% Cu</u>	<u>Dist.</u>
546 - 555	9	0.35	3.15
555 - 65	10	0.39	3.90
565 - 74	9	0.36	3.24
574 - 82	8	0.31	2.48
582 - 85	3	0.26	0.78
585 - 95	10	0.43	4.30
595 - 604	9	0.72	6.48
604 - 14	10	0.26	2.60
614 - 25	11	0.52	5.72
625 - 37	12	0.44	5.28
637 - 47	10	0.75	7.50
647 - 55	8	0.67	5.36
	<u>109'</u>	<u>0.47%</u>	<u>60.79</u>
121 - 130	9	0.42	3.78
130 - 140	10	0.68	6.80
140 - 152	12	0.51	6.12
152 - 169	17	0.36	6.12
169 - 174	5	0.41	2.05
	<u>53'</u>	<u>0.47%</u>	<u>24.87</u>

Note: No ore calculations from this hole

Carlotta

ARC LABORATORIES

Division of Arizona Research Consultants, Inc.

9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-3573

FOR: Homestake Production Corp.
Box 7277
Phoenix, Arizona

DATE 11/5/68

LAB No. 10202

Carlotta

RESULTS

Hole #	Depth	Copper	Hole #	Depth	Copper
11	60-69	0.04 %	11	406-28	0.08 %
	69-79	0.06		428-41	0.06
	79-87	0.08		441-52	0.04
	87-97	0.09		452-67	0.05
	97-108	0.18		467-79	0.06
	108-21	0.19		479-89	0.04
	121-30	0.42		489-503	0.10
	140-52	0.51		503-19	xtrace
	152-69	0.36		676-85	trace
	174-92	0.13		685-94	"
	192-204	0.07	694-702	"	
	204-21	0.06	13	75261	"
	221-30	0.16		761-69	"
	230-39	0.17		769-78	"
	239-51	0.19		778-89	"
	251-59	0.23	789-98	"	
	259-69	0.21	14 S1	400-10	0.24
	269-85	0.40		410-20	0.22
	285-301	0.22			
	311-49	0.34			
349-76	0.14				
376-89	0.08				
389-406	0.06				

Respectfully submitted,
ARC LABORATORIES

John T. Long, Jr.
John T. Long, Jr.

ARC LABORATORIES

Division of Arizona Research Consultants, Inc.

9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-8573

FOR: Homestake Production Corp.
 Box 7277
 Phoenix, Arizona

DATE 10/3/68

LAB No. 10159

Carlotta

RESULTS

Sample # Hole	Depth	Copper	Silver	Gold
9	392-9 $\frac{1}{4}$	0.16 %	1.00	nil
11	301-11	1.32	0.50	nil
Lead				
9	392- $\frac{1}{4}$	0.20 %		

Respectfully submitted,
 ARC LABORATORIES

John T. Long, Jr.

CARLOTTA MINE

SUMMARY HOLE #13

<u>Depth</u>	<u>Footage</u>	<u>% Cu</u>	<u>Dist.</u>	
112 - 124	12	0.33	3.96	} 79' - 0.80 - 132,000 tons <u>200 x 100 x 79</u> 12
124 - 34	10	0.67	6.70	
134 - 44	10	0.83	8.30	
144 - 54	10	0.79	7.90	
154 - 64	10	0.37	3.70	
164 - 71	7	1.74	12.18	
171 - 77	7	0.94	6.58	
177 - 85	7	0.22	1.54	
185 - 91	6	1.77	10.62	
	<u>79'</u>	<u>0.80%</u>	<u>62.48</u>	
191 - 236	45	0.21	9.45	} Waste and Heap
236 - 259	23	0.10	2.30	
259 - 268	9	0.13	1.17	
268 - 84	16	0.28	4.48	
284 - 94	10	0.46	4.60	
294 - 304	10	0.48	4.80	
	<u>113'</u>	<u>0.24%</u>	<u>26.80</u>	
304 - 367	63	0.24	15.12	} 94' - 0.76 - 157,000 tons <u>200 x 100 x 94</u> 12
367 - 370	3	0.38	1.14	
370 - 375	5	0.21	1.05	
375 - 85	10	0.64	6.40	
385 - 97	12	0.62	7.44	
397 - 406	9	1.04	9.36	
306 - 13	7	0.81	5.67	
413 - 25	12	0.55	6.60	
425 - 34	9	0.63	5.67	
434 - 46	12	1.01	12.12	
446 - 56	10	1.03	10.30	
456 - 61	5	1.15	5.75	
	<u>94'</u>	<u>0.76%</u>	<u>71.50</u>	

OR: 346' - 0.52% Cu

ARC LABORATORIES

Division of Arizona Research Consultants, Inc.

9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-3573

FOR: Homestake Production Co.
Box 7277
Phoenix, Arizona

DATE 10/16/68

LAB No. 10172

Carlotta

RESULTS

Hole #	Depth	Copper
13	104-12 ft.	0.19%
	112-24	0.33
	124-34	0.67
	134-44	0.83
	144-54	0.79
	154-64	0.37
	164-71	1.74
	171-77	0.94
	177-85	0.22
	185-91	1.77
	191-231	0.21
	236-59	0.10
	259-63	0.13
	263-34	0.28
	284-94	0.46
	294-304	0.48
	sludge	211-21
221-31		0.03
231-37		0.03
237-46		0.03
253-66		0.04
	266-76	0.02

$$\begin{array}{r} 191 \\ 124 \\ \hline 67 \end{array}$$

733 = 0.91%

Respectfully submitted,
ARC LABORATORIES

John T. Long, Jr.

ARC LABORATORIES

Division of Arizona Research Consultants, Inc.

9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-3573

FOR: Homestake Production Corp.
 Box 7277
 Phoenix, Arizona

DATE 10/28/68

LAB No. 10190

Carlotta

RESULTS

Sample #	Depth	Copper
12	172-185	2.57 %
	sludge 172-85	0.42
13	304-23	0.44
	323-52	0.11
	370-75	0.21
	471-96	0.03
	496-526	0.02
	526-42	0.02
	542-57	0.05
	557-77	0.08
	577-95	0.11
	595-615	0.09
	615-40	0.20
	640-53	0.63
	653-64	0.44
	664-76	0.29
	676-85	0.32
	685-96	0.56
	696-705	0.08
	705-14	trace
702-11	"	
711-22	"	
714-23	"	
723-34	"	
734-43	"	
743-52	"	
798-306	"	
806-11	"	

Respectfully submitted,
 ARC LABORATORIES

John T. Long, Jr.
 John T. Long, Jr.

ARC LABORATORIES

Division of Arizona Research Consultants, Inc.

9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-3573

FOR: Homestake Production Corp.
 Box 7277
 Phoenix, Arizona

DATE 10/18/68

LAB No. 10182

RESULTS

Hole #	Depth	Copper
13	352-60 sludge	0.03 %
13	350-67 cores	0.13
	367-70	0.38
	375-85	0.64
	385-97	0.62
	397-406	1.04
	406-13	0.81
	413-25	0.55
	425-34	0.63
	434-46	1.01
	446-56	1.03
	456-61	1.15
	461-71	0.23

Respectfully submitted,
 ARC LABORATORIES

John T. Long, Jr.
 John T. Long, Jr.

CARLOTTA MINE

SUMMARY HOLE #14

<u>Depth</u>	<u>Footage</u>	<u>% Cu</u>	<u>Dist.</u>	
256 - 303	47	1.48	69.56	} 153' - 1.05% - 357,000 tons <u>280 x 100 x 153</u> 12
303 - 409	<u>106</u>	<u>0.86</u>	<u>91.16</u>	
	153'	1.05%	160.72	
409 - 441	32	0.43	13.76	} Waste & Heap
441 - 489	48	0.23	11.04	
489 - 519	30	0.52	15.60	
519 - 604	85	0.44	37.40	
604 - 708	<u>104</u>	<u>0.97</u>	<u>100.88</u>	} 104' - 0.97% - 190,000 tons <u>220 x 100 x 104</u> 12
	452'	0.75%	339.40	
	Average	0.75% Cu		
<u>Bottom 765'</u>				

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9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-3573

FOR: Homestake Production Corp.
Box 7277
Phoenix, Arizona

DATE 11/15/68

LAB No. 10226

Carlotta

RESULTS

Hole #	Depth	Copper
14	606-08	6.33 %
	604-19 minus	
	606-08	0.47
	619-44	0.59
	644-58	0.38
	658-84	0.83
	684-94	1.12
	694-708	2.10
	708-16	0.10
	716-26	0.13
	726-42	0.04

Respectfully submitted,
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John T. Long, Jr.



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9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-3573

FOR: Homestake Production Corp.
Box 7277
Phoenix, Arizona


DATE 11/19/68
LAB No. 10226

Carlotta

RESULTS

Hole #	Depth	Copper
14	742-52	0.04 %
	sluffge	
	623-33	0.10
	633-43	0.08
	654-62	0.27
	662-72	0.41
	672-82	0.44
	703-07	0.38
	726-36	0.03
	736-40	0.02

Respectfully submitted,
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9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-3573

FOR: Homestake Production Corp.
Box 7277
Phoenix, Arizona

DATE 11/12/63

LAB No. 10216

Carlotta

RESULTS

Hole #	Depth	Copper
14	519-28	0.46 %
	523-36	0.43
	536-45	0.36
	545-74	0.31
	574-86	0.54
	586-95	0.88
	595-604	0.31
sludge	520-30	0.12
	530-40	0.10

Respectfully submitted,
ARC LABORATORIES

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9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-3573

FOR: Homestake Production Corp.
 Box 7277
 Phoenix, Arizona

DATE 11/11/68

LAB No. 10212

Carlotta

RESULTS

Hole #	Depth	Copper
14	453-89	0.23 %
	489-96	0.46
	496-502	0.51
	502-19	0.59
	sludge	510-20
17	216-21	0.38
	221-26	7.06
	226-30	1.19

Respectfully submitted,
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John T. Long, Jr.

Dr. + the file - Gen. Lab. Copies

PRODUCT DEVELOPMENT

APPLIED RESEARCH



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PHOENIX, ARIZONA 85021

943-3573

FOR: Homestake Production Corp.
Box 7277
Phoenix, Arizona

DATE 11/7/68

LAB No. 10207

RESULTS

Hole #	Depth	Copper
14	409-32	0.43 %
	432-41	0.45
	441-53	0.22

Respectfully submitted,
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Division of Arizona Research Consultants, Inc.

9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-3573

FOR: Homestake Production Corp.
 Box 7277
 Phoenix, Arizona

DATE 10/31/68


LAB No. 10198

Carlotta

RESULTS

Hole #	Depth	Copper	
14	303-314	1.13 %	
	314-21	3.06	
	321-23	1.35	
	323-333	1.34	
	333-343	0.64	
	343-355	0.24	
	355-386	0.09	
	386-409	1.27	
	Sludge	360-70	0.28
		370-89	0.17
	380-90	0.13	
	390-400	0.16	

Respectfully submitted,
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Division of Arizona Research Consultants, Inc.

9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-3573

FOR: Homestake Production Corp.
 Box 7277
 Phoenix, Arizona

DATE 10/29/68

LAB No. 10195

Carlotta

RESULTS

Hole #	Depth	Copper
12	185-88	1.53 %
14	256-63	0.52
	263-71	0.46
	271-81	1.10
	281-92	1.59
	292-303	3.04

Respectfully submitted,
 ARC LABORATORIES



John T. Long, Jr.

CARLOTTA MINE

SUMMARY HOLE #15

<u>Depth</u>	<u>Footage</u>	<u>% Cu</u>	<u>Dist.</u>	
218 - 250	32	0.35	11.20	}
250 - 267	17	0.80	13.60	
267 - 295	28	0.17	4.76	
295 - 317	22	0.14	3.08	
317 - 356	39	0.14	5.46	
356 - 370	14	0.24	3.36	
370 - 380	10	0.09	.90	
380 - 392	12	0.08	.96	
392 - 412	20	0.14	2.80	
412 - 421	9	0.12	1.08	
421 - 430	9	0.08	.72	
430 - 442	<u>12</u>	<u>0.12</u>	<u>1.44</u>	
	224	0.22	49.36	
442 - 455	13	0.52	6.76	}
455 - 463	8	0.45	3.60	
463 - 471	8	0.32	2.56	
471 - 481	10	0.13	1.30	
481 - 491	10	0.14	1.40	
491 - 498	7	0.11	0.77	
498 - 507	9	0.16	1.44	
507 - 515	<u>8</u>	<u>0.22</u>	<u>1.76</u>	
	73'	0.27	19.59	
515 - 517	2	0.62	1.24	}
517 - 523	6	0.86	5.16	
523 - 534	11	0.12	1.32	
534 - 546	12	0.15	1.80	
546 - 558	12	0.35	4.20	
558 - 569	11	0.21	2.31	
569 - 604	35	0.50	17.50	
604 - 617	13	0.22	2.86	
617 - 639	22	1.26	27.72	
639 - 47	8	.44	3.52	
647 - 52	5	3.48	17.40	
652 - 66	14	.54	7.56	
666 - 72	6	5.19	31.14	
672 - 78	<u>6</u>	<u>0.50</u>	<u>3.00</u>	
	163'	0.78	126.73	

Waste

Waste

163' - 0.78 - 271,000 tons
 $\frac{200 \times 100 \times 163}{12}$

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9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-3573

FOR: Homestake Production Corp.
Box 7277
Phoenix, Arizona

DATE 11/27/68


LAB No. 10236

Carlotta

RESULTS

Hole #	Depth	Copper
14	752-65	trace
15	218-50	0.35 %
	250-67	0.30
	267-95	0.17
	295-317	0.14
	317-56	0.14
	Sludge 222-30	0.19
	260-70	0.46
	270-80	0.40
	280-90	0.10
	290-300	0.12
	300-10	0.11
	310-20	0.16
	320-30	0.14
	330-40	0.18
18	340-50	0.12
	350-60	0.13
	76-87	0.02
	87-98	0.02
	98-106	trace

Respectfully submitted,
ARC LABORATORIES



John T. Long, Jr.

ARC LABORATORIES

Division of Arizona Research Consultants, Inc.

9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-3573

FOR: Homestake Production Corp.
Box 7277
Phoenix, Arizona

DATE 11/27/68

LAB No. 10236

Carlotta

RESULTS

Hole #	Depth	Copper
14	752-65	trace
15	218-50	0.35 %
	250-67	0.80
	267-95	0.17
	295-317	0.14
	317-56	0.14
	Sludge 222-30	0.19
	260-70	0.46
	270-80	0.40
	280-90	0.10
	290-300	0.12
	300-10	0.11
	310-20	0.16
	320-30	0.14
	330-40	0.18
	340-50	0.12
18	350-60	0.13
	76-87	0.02
	87-98	0.02
	98-106	trace

Respectfully submitted,
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Division of Arizona Research Consultants, Inc.

9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-3573

FOR:

Homestake Production Corp.
Box 7277
Phoenix, Arizona

DATE

12/2/68

LAB No.

10248

Carlotta

RESULTS

Hole #	Depth	Copper
15	356-70	0.24 %
	370-80	0.09
	380-92	0.03
	392-412	0.14
	412-21	0.12
	421-30	0.03
	430-42	0.12
	442-55	0.52
	455-63	0.45
	463-71	0.32
	471-81	0.13
	481-91	0.14
	491-98	0.11
	498-507	0.16
	507-15	0.22
	515-17	0.62
	517-23	0.86
	523-34	0.12
	534-46	0.15
	546-58	0.35
	558-69	0.21
	569-604	0.50
	604-617	0.22

Respectfully submitted,
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John T. Long, Jr.



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Division of Arizona Research Consultants, Inc.

9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-3573

FOR: Homestake Production Corp.
 Box 7277
 Phoenix, Arizona

DATE 12/6/63

LAB No. 10257

Carlotta

RESULTS

Hole #	Depth	Copper
15	617-39	1.26 %
	639-47	0.44
	647-52	3.48
	652-61	0.54
	661-72	5.19
	672-78	0.50
Sludge	620-30	0.31
	630-40	0.64
	640-50	0.64
	650-60	0.42
	660-70	0.44

Respectfully submitted,
 ARC LABORATORIES

John T. Long, Jr.

CARLOTTA MINE

SUMMARY HOLE #16

<u>Depth</u>	<u>Footage</u>	<u>% Cu</u>	<u>Dist.</u>	
321 - 31	10	.53	5.30	} 79' - 1.11% - 132,000 tons <u>200 x 100 x 79</u> 12
331 - 41	10	.83	8.30	
341 - 50	9	.92	8.28	
350 - 64	14	.99	13.86	
364 - 71	7	1.97	13.79	
371 - 82	11	2.81	30.91	
382 - 93	11	.43	4.73	
393 - 400	7	.37	2.59	
	<u>79'</u>	<u>1.11%</u>	<u>87.76</u>	
400 - 426	26	.22	5.72	} Waste & Heap
426 - 47	21	.14	2.94	
447 - 57	10	.38	3.80	
457 - 65	8	.39	3.12	
465 - 75	10	.28	2.80	
475 - 83	8	.36	2.80	
483 - 92	9	.32	2.88	
492 - 503	11	.31	3.41	
503 - 13	10	.68	6.80	
513 - 24	11	.47	5.17	
524 - 33	9	.43	3.87	
533 - 45	12	.23	2.76	
545 - 54	9	.28	2.52	
554 - 63	9	.24	2.16	
563 - 73	10	.32	3.20	
573 - 83	10	.40	4.00	
	<u>201'</u>	<u>0.32</u>	<u>65.27</u>	
583 - 93	10	0.63	6.30	} 129' - 0.70 - 215,000 tons <u>200 x 100 x 129</u> 12
593 - 602	9	.37	3.33	
602 - 18	16	.28	4.48	
618 - 26	8	.62	4.96	
626 - 38	12	.41	4.92	
638 - 53	15	.21	3.15	
653 - 98	45	1.04	46.80	
698 - 712	14	1.07	14.98	
	<u>129'</u>	<u>0.70</u>	<u>89.92</u>	
712 - 724	12	0.08		
Average 391'		0.60%	234.63	



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Division of Arizona Research Consultants, Inc.

9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-3573

FOR: Homestake Production Corp.
Box 7277
Phoenix, Arizona

DATE 12/13/68

LAB No. 10264

Carlotta

RESULTS

Hole #	Depth	Copper
15	668-87	trace
16	321-31	0.53 %
	331-41	0.83
	341-50	0.92
	350-64	0.99
	364-71	1.97

Respectfully submitted,
ARC LABORATORIES

John T. Long, Jr.

ARC LABORATORIES

Division of Arizona Research Consultants, Inc.

9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-3573

FOR: Homestake Production Co.
 Box 7277
 Phoenix, Arizona

DATE 12/17/68

LAB No. 10271

Carlotta

RESULTS

Hole #	Depth	Copper
16	371-82	2.81 %
	382-93	0.43
	393-400	0.37
	400-26	0.22
	426-47	0.14
	447-57	0.38
	457-65	0.39
	465-75	0.28
	475-83	0.35
	483-92	0.32
	492-503	0.31
	503-13	0.68
	Sludge	370-80
380-90		0.28
390-400		0.21
400-10		0.14
410-20		0.16
420-30		0.11
430-40		0.07
10	636-46	trace
	646-50	trace

Respectfully submitted,
 ARC LABORATORIES

John T. Long, Jr.



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Division of Arizona Research Consultants, Inc.

9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-3573

FOR: Homestake Production Co.
 Box 7277
 Phoenix, Arizona

DATE 12/20/68

LAB No. 10275

Carlotta

RESULTS

Hole #	Depth	Copper
16	513-24	0.47 %
	524-33	0.43
	533-45	0.23
	545-54	0.28
	554-63	0.24
	563-73	0.32
	573-83	0.40
	583-93	0.63
	593-602	0.37
	602-18	0.28
	618-26	0.62
626-38	0.41	
638-53	0.21	

Respectfully submitted,
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John T. Long, Jr.

Handwritten initials: J.S. 3/26/69



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9236 NORTH 10TH AVE.

PHOENIX, ARIZONA 85021

943-3573

FOR: Homestake Production Co.
Box 7277
Phoenix, Arizona

DATE 12/26/68

LAB No. 10280

Carlotta

RESULTS

Hole #	Depth	Copper
16	653-98	1.04 %
	698-712	1.07
	712-24	0.08
sludge	643-53	0.16
	653-53	0.14
	663-73	0.17
	670-80	0.25
	680-90	0.26
	690-700	0.40
	700-10	0.18
	718-28	0.24

Respectfully submitted,
ARC LABORATORIES

John T. Long, Jr.

CARLOTTA PROJECT

MINING SYSTEM AND PROCESS DESCRIPTION

The mine will be open pit with material removed by rippers and scrapers (as at Bluebird Mine 5 miles away) or by conventional power shovel and 50 ton off-the-highway trucks. The selection of equipment will not be determined until ripping tests are made and dumping areas established. To be conservative, this report (See Schedule II - Economics) has assumed drilling, blasting, power shovel loading and trucking from actual experience and costs of Bagdad Copper Company.

Waste ore (copper ore below 0.3% copper) will be hauled to dumps with less than 1 mile average round trip (vs. two miles average for Bagdad). Heap leach material (.3% and higher outside proven ore body) will be piled separately for future heap leaching from which an additional 12,000,000# of copper (on present ore body) alone can be recovered at very low cost over a period of years. This procedure of mining and wasting is used throughout the industry and involves known factors.

The mine will be equipped to remove 10,300 tons of waste rock per five day week on two shifts. In addition, ore will be delivered to the crusher at approximately 3,000 tons per day, five days per week on one shift. The processing plant will operate seven days per week on three shifts.

The extraction plant will be the same as described in the Summary Report of October 2, 1968 except it will be equipped for 2,000 tons of ore per day, or four times larger than the previous presentation. The plant will require four times as much water in make-up but acid and iron are in direct proportion to pounds of copper produced. For ease of reference, we have again attached Plates A and B from the October 2, 1968 report.

SCHEDULE I

CARLOTTA MINE - SUMMARY OF CASH FLOW

0.9% CU ORE TO PRODUCE 32,000# CU/DAY (10,000,000#/yr) AS COPPER PRECIPITATES

		<u>Proven</u>	<u>Proven Plus Probable</u>
1) <u>Reserves (tons ore)</u> as at January 1, 1969		3,250,000 tons	6,250,000
<u>Extractable</u> copper contained in reserves/lbs.		52,000,000	100,000,000
2) <u>VALUE OF SALES</u>	<u>Per Year</u>	<u>Life of</u> <u>Proven Reserves</u>	<u>Life of Reserves</u> <u>Proven & Probable</u>
@ 32¢ Smelter Settle- ment #/Cu	3,200,000	\$16,664,000	\$32,000,000
3) <u>LESS COSTS</u> See Schedules II & III	<u>\$2,135,000</u>	<u>\$11,102,000</u>	<u>\$21,135,000</u>
4) <u>CASH FLOW</u>	<u>\$1,065,000</u>	<u>\$ 5,562,000</u>	<u>\$10,865,000</u>
5) <u>Return of Total</u> <u>Cash In</u> Schedule IV		<u>\$ 1,988,600</u>	<u>\$ 1,988,600</u>
6) <u>Cash Profit (before</u> <u>Taxes & Depletion</u>		<u>\$ 3,573,400</u>	<u>\$ 8,876,400</u>
7) <u>Life of Project</u>		<u>5.2 years</u>	<u>10 years</u>
8) <u>Return on Cash In</u> (average without regard to taxes or depletion)		<u>34% per year</u>	<u>42.5% per year</u>

SCHEDULE II

CARLOTTA MINE - CASH OPERATING COSTS

WASTE 7000 TONS PER DAY - TREATING 2000 TONS ORE PER DAY OF

0.9% CU ORE TO PRODUCE 32,000# CU/DAY (10,000,000#/yr) AS COPPER PRECIPITATES

<u>DIRECT COSTS (a)</u>	<u>Cost per ton Ore/¢</u>	<u>Cost/#Cu/¢</u>	<u>Cost/year/\$</u>
1) Waste to Dump or Heap Leach Piles (Ratio 4.8 to 1 19.7¢/ton)	78.8	4.92	492,000
2) Mining & Delivery to Plant	30.0	1.88	188,000
3) Grinding & Floatation	78.0	4.88	488,000
4) Acid @ 3#/#CU	56.0	3.50	350,000
5) Iron @ 1.6#/#CU	<u>73.6</u>	<u>4.60</u>	<u>460,000</u>
<u>TOTAL DIRECT COSTS</u>	<u>316.4</u>	<u>19.78</u>	<u>1,978,000</u>
 <u>INDIRECT COSTS (b)</u>			
6) Arizona "Sales" Tax 1½% Gross	7.5	.47	47,000
7) Local Taxes & Insurance (\$150.00 Day)	7.7	.48	48,000
8) General Administrative & Sales (200.00/day)	<u>9.9</u>	<u>.62</u>	<u>62,000</u>
<u>TOTAL INDIRECT CASH COSTS</u>	<u>25.1</u>	<u>1.57</u>	<u>157,000</u>
<u>TOTAL ALL CASH COSTS</u>	<u>341.5</u>	<u>21.35</u>	<u>2,135,000</u>

NOTES:

- (a) Direct Costs - The costs per ton of ore are actual costs experienced by Bagdad Copper Corporation for the past ten months adjusted to expected cost increases during 1969. We are indebted to Mr. David Lincoln, President of Bagdad Copper Corporation for permitting use of these figures.
- (b) Indirect Costs - Again these costs are directly from Bagdad Copper Corporation costs for 1968 adjusted to 10,000,000 lbs. annual sales and local taxes to Arizona rates.

SCHEDULE III

CAPITAL COST - CARLOTTA MINE

PLANT TO TREAT 2000 TONS PER DAY

0.9% COPPER OXIDE TO PRODUCE 32,000# COPPER IN PRECIPITATES PER DAY

A. Basic Equipment delivered and set on Foundations

Item No.		<u>Amount</u>	<u>Connected</u> <u>H. P.</u>
101	Crushing Plant - 250 TPH - <u>(Used)</u>	\$60,000	250
102	Conveyor 24" x 100'	3,000	15
103	Feeder & Automatic Weighing Device	6,500	10
104	Conveyor 18" x 50'	4,000	10
105	8' x 12' (2) Rod Mills <u>(Used)</u>	40,000	750
106	Krebs Cyclones (2)	5,000	
107	6" x 6" Denver Sand Pump (2)	5,000	40
108 abc	Agitated Leaching Vats (Standard Denver Equipment Co.)	40,000	90
109	Precipitation Tube (Iron Addition) <u>Used</u>	50,000	50
110	Magnetic Separator & Screen	10,000	5
111	20 - #24 Denver Float Cells (Roughers)	25,000	150
112	8 - #18 Denver " " (Cleaners)	10,000	20
113	Eimco 6' - 4 leaf vacuum filters	30,000	70
114 a&b	2 - 8" x 8" Denver Sand Pumps	5,000	40
115	Acid Storage Tanks <u>(Used)</u>	10,000	
116	60,000 gallon Water Storage - 4 tanks - Fiberglass	20,000	
117	Prefabricated & Erected Bulter Type Building with Lighting	25,000	
118	Fence	5,000	
119	Scale <u>(Used)</u>	5,000	

B. Other Items of Construction Cost not included above:

120	Water Well (or wells), Pump & Pipe Installed - contract	40,000	200
-----	--	--------	-----

SCHEDULE III (Cont'd)

<u>Item No.</u>		<u>Amount</u>	<u>Connected H.P.</u>
121	Tailings Pond Pump & Piping-contract	\$ 15,000	50
122	Reinforced Concrete Floors & Foundations - 400 cu. yd. @ \$30 cu. yd. in place	12,000	
123	Rental Equipment during Construction	40,000	
124	Instrumentation, Piping & Wiring - Subcontracts	75,000	
125	Engineering, Drafting Equipment Inspection, Travel & Misc.	25,000	
126	Advance to Arizona Public Service for Power Line to Transformers	30,000	(1)
127	Offsite - Preparation of Steel Scrap (Shredding & Handling Equipment)	30,000	(2)
		<hr/> \$585,500	1750
	Contingency - 20%	120,000	
	TOTAL	<hr/> <u>\$705,500</u>	<hr/> <u>1750</u>

(1) APS advance recovered over 5 years - assumes maximum 5 miles new line - alternate lease rental butane engine generator should be studied.

(2) Based on completed studies shredding Pittsburgh Steel copper clad (6%) waste steel.

SCHEDULE IV

ESTIMATE OF CASH REQUIREMENTS - CARLOTTA MINE - PROVEN PLUS PROBABLE RESERVES

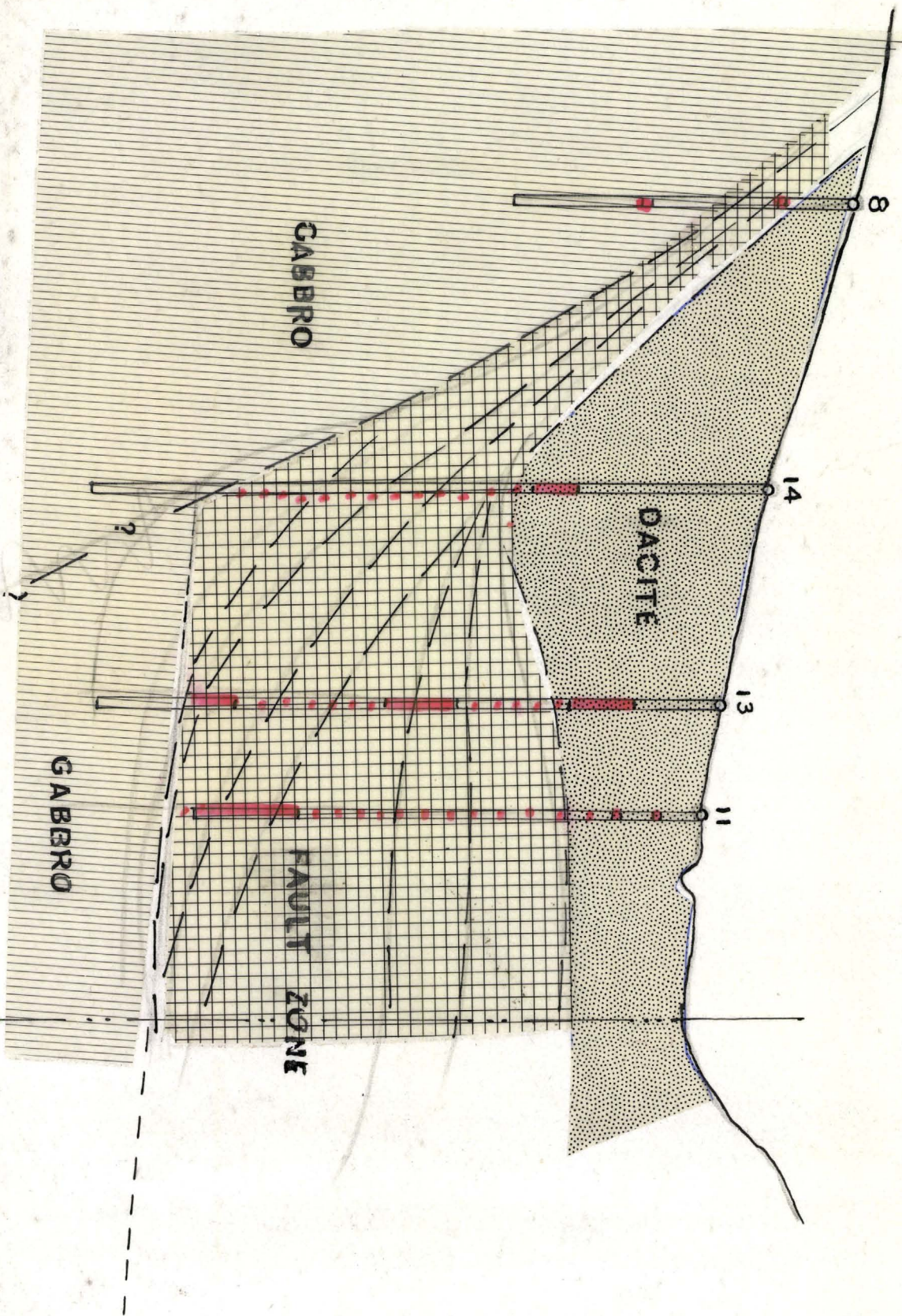
(Assumes Lease Purchase Mining Equipment or Contract Mining)

	<u>Spent To Date</u>	<u>Recommended 1969</u>	<u>Est. 1970</u>
Property Acquisition	\$190,000	\$135,000 (1)	\$200,000 (2)
Drilling & Engineering	100,000	200,000	
Property Options		8,600	
Open Up Property		250,000	
Water Well Test		20,000	
Start Construction of Plant		350,000	
Finish Construction of Plant			355,000
Other Expenses	<u>60,000</u>	<u>60,000</u>	<u>60,000</u>
	\$350,000	\$1,023,600	\$615,000
 <u>TOTAL CASH IN</u>			 <u>\$1,988,600</u>

(1) Assumes Purchase Milca

(2) Assumes Purchase Owens and Dickerson

CARLOTA



SECTION
Scale 1" = 200'

HOME-STAKE PRODUCTION COMPANY
CARLOTA COPPER PROPERTY

DIAMOND DRILL HOLE 13

LOCATION: Near Miami
Arizona.

ELEV. 3529'
LATITUDE: 5864 N
DEPARTURE: 7543 E

BEARING:
ANGLE DIP: - 90°

STARTED:
FINISHED:
LOGGED BY: C.W. Archibald

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH				
?	698.0	<p>FAULT ZONE</p> <p> ? - 599.0 some iron, copper oxides showing throughout</p> <p> 596.0 - 599.0 lost core</p> <p> 599.0 - 653.0 iron oxide and copper oxide decreasing to depth</p> <p> 672.0 - 687.0 slight copper oxide</p>						
698.0	774.0	<p>MICA SCHIST, slickensided throughout</p> <p> 736.0 - 738.0 <u>mud seam</u></p> <p> 772.0 - 774.0 <u>mud seam</u></p>						

DIAMOND DRILL HOLE 13

LOCATION: Near Miami
 Arizona.

ELEV. 3529'
 LATITUDE: 5864 N
 DEPARTURE: 7543 E

BEARING:
 ANGLE DIP: - 90°

STARTED:
 FINISHED:
 LOGGED BY: C.W.Archibald

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH				
?	698.0	FAULT ZONE ? - 599.0 some iron, copper oxides showing throughout 596.0 - 599.0 lost core 599.0 - 653.0 iron oxide and copper oxide decreasing to depth 672.0 - 687.0 slight copper oxide						
698.0	774.0	MICA SCHIST, slickensided throughout 736.0 - 738.0 <u>mud seam</u> 772.0 - 774.0 <u>mud seam</u>						

HOME-STAKE PRODUCTION COMPANY
CARLOTA COPPER PROPERTY

DIAMOND DRILL HOLE 13

LOCATION:

LATITUDE:
DEPARTURE:

BEARING:
ANGLE DIP:

STARTED:
FINISHED:
LOGGED BY: C.W.Archibald

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH				
774.0	811.0	GABBRO getting more broken and hematitic to depth.						

HOME-STAKE PRODUCTION COMPANY
CARLOTA COPPER PROPERTY

DIAMOND DRILL HOLE 14

Elev. 3590'

STARTED:

FINISHED:

LOCATION: Near Miami
Arizona

LATITUDE: 5710 N

BEARING:

DEPARTURE: 7300 E

ANGLE DIP: - 90°

LOGGED BY: C.W.Archibald

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH	% Cu			
0	323.0	Dacite 0 - 264.0 badly deteriorated, very little copper showing						
		256.0 - 263.0		7.0	0.52			
		263.0 - 271.0		8.0	0.46			
		264.0 - 284.0 massive						
		264.0 - 290.0 copper oxides showing along fracture planes		10.0	1.10			
		271.0 - 281.0		11.0	1.59			
		281.0 - 292.0		11.0	3.04			
		290.0 - 323.0 bleached, altered						
		292.0 - 303.0						
		290.0 - 321.0 copper stain		11.0	1.13			
		303.0 - 314.0		7.0	3.06			
		314.0 - 321.0		2.0	1.35			
		321.0 - 323.0 mud seam						
323.0	755.0	Fault zone - mostly gabbro						
		323.0 - 336.0 hard breccia, slight copper stain		10.0	1.34			
		323.0 - 333.0						
		333.0 - 336.0 more copper stain						
		336.0 - 405.0 slightly iron stained						
		336.0 - 343.0 heavy iron stain		10.0	0.64			
		333.0 - 343.0		12.0	0.24			
		343.0 - 355.0		31.0	0.09			
		355.0 - 386.0		23.0	1.27			
		386.0 - 409.0						
		405.0 - 412.0 brecciated, much less iron staining, slight copper stain						
		405.0 - 409.0 limonitic						

HOME-STAKE PRODUCTION COMPANY
CARLOTA COPPER PROPERTY

DIAMOND DRILL HOLE 14

LOCATION:

LATITUDE:
DEPARTURE:

BEARING:
ANGLE DIP:

STARTED:
FINISHED:
LOGGED BY: C.W. Archibald

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH	% Cu			
		566.0 - 568.0 more iron stain	574.0 - 586.0		12.0	0.54		
		580.0 - 582.5 sand seam						
		583.0 - 586.0 more copper stain	586.0 - 595.0		9.0	0.88		
		594.0 - 604.0 much iron stain	595.0 - 604.0		9.0	0.31		
		604.0 - 606.0 only very slight copper						
		606.0 quartzitic, high copper content						
		606.0 - 611.0 high copper stain	606.0 - 608.0		2.0	6.33		
		gradually lessening						
		604.0 - 619.0 less	606.0 - 608.0		13.0	0.47		
		611.0 - 648.0 less iron stain,	619.0 - 644.0		25.0	0.59		
		more copper oxides visible						
		648.0 - 691.0 iron stained, very slight						
		copper oxides	644.0 - 658.0		14.0	0.38		
			658.0 - 684.0		26.0	0.83		
		691.0 - 693.0 <u>mud seam</u>	684.0 - 694.0		10.0	1.12		
		693.0 - 698.5 hard, copper oxides						
		along fractures						
		698.5 - 707.0 high iron content as gossan	694.0 - 708.0		14.0	2.10		
		703.0 - 713.0 brecciated, slight jasper	708.0 - 716.0		8.0	0.10		

HOME-STAKE PRODUCTION COMPANY
CARLOTA COPPER PROPERTY

DIAMOND DRILL HOLE 14

LOCATION:

LATITUDE:
DEPARTURE:

BEARING:
ANGLE DIP:

STARTED:
FINISHED:
LOGGED BY: C.W.Archibald

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH	% Cu			
		703.0 - 707.0 1.0 core						
		707.0 - 708.0 0.5 "						
		713.0 - 720.0 brecciated, much jasper	716.0 - 726.0	10.0	0.13			
		720.0 - 723.0 <u>mud seam</u>						
		729.0 - 730.0 <u>mud seam</u>						
		731.0 - 755.0 much hematite	726.0 - 742.0	16.0	0.04			
			742.0 - 752.0	10.0	0.04			
755.0	765.0	Gabbro, broken siliceous.						
	765.0	END OF HOLE.						

HOME-STAKE PRODUCTION COMPANY
CARLOTA COPPER PROPERTY

DIAMOND DRILL HOLE 14

LOCATION:

LATITUDE:
DEPARTURE:

BEARING:
ANGLE DIP:

STARTED:
FINISHED:
LOGGED BY: C.W.Archibald

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH	% Cu			
		<u>SLUDGE ASSAYS</u>						
		360.0 - 370.0		10.0	0.28			
		370.0 - 380.0		10.0	0.17			
		380.0 - 390.0		10.0	0.13			
		390.0 - 400.0		10.0	0.16			
		510.0 - 520.0		10.0	0.30			
		520.0 - 530.0		10.0	0.12			
		530.0 - 540.0		10.0	0.10			
		623.0 - 633.0		10.0	0.10			
		633.0 - 643.0		10.0	0.08			
		654.0 - 662.0		8.0	0.27			
		662.0 - 672.0		10.0	0.41			
		672.0 - 682.0		10.0	0.44			
		703.0 - 707.0		4.0	0.38			
		726.0 - 736.0		10.0	0.03			
		736.0 - 740.0		4.0	0.02			

HOME-STAKE PRODUCTION COMPANY
CARLOTA COPPER PROPERTY

DIAMOND DRILL HOLE 14

Elev. 3590'

LOCATION: Near Miami
Arizona

LATITUDE: 5710 N

BEARING:

DEPARTURE: 7300 E

ANGLE DIP: - 90°

STARTED:
FINISHED:
LOGGED BY: C.W. Archibald

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH	% Cu
0	323.0	Basite 0 - 264.0 badly deteriorated, very little copper showing			
		256.0 - 263.0		7.0	0.52
		263.0 - 271.0		8.0	0.46
		264.0 - 284.0 massive 264.0 - 290.0 copper oxides showing along fracture planes		10.0	1.10
		281.0 - 292.0		11.0	1.59
		290.0 - 323.0 bleached, altered		11.0	3.04
		292.0 - 303.0			
		290.0 - 321.0 copper stain		11.0	1.13
		303.0 - 314.0		7.0	3.06
		314.0 - 321.0		2.0	1.35
		321.0 - 323.0 mud seam			
323.0	755.0	Fault zone - mostly gabbro 323.0 - 336.0 hard breccia, slight copper stain			
		323.0 - 333.0		10.0	1.34
		333.0 - 336.0 more copper stain			
		336.0 - 405.0 slightly iron stained			
		336.0 - 343.0 heavy iron stain		10.0	0.64
		333.0 - 343.0		12.0	0.24
		343.0 - 355.0		31.0	0.09
		355.0 - 386.0		23.0	1.27
		386.0 - 409.0			
		405.0 - 412.0 brecciated, much less iron staining, slight copper stain			
		405.0 - 409.0 limonitic			

DIAMOND DRILL HOLE 14

LOCATION:

LATITUDE:
DEPARTURE:

BEARING:
ANGLE DIP:

STARTED:
FINISHED:
LOGGED BY: C.W. Archibald

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH	% Cu			
		412.0 - 481.0 fairly heavy iron, hard, fine fragments						
		409.0 - 432.0		23.0	0.43			
		432.0 - 441.0		9.0	0.45			
		454.0 - 481.0 4.0 core		12.0	0.22			
		441.0 - 453.0		36.0	0.23			
		453.0 - 489.0						
		481.0 - 486.0 high iron, fine fragments						
		486.0 - 492.0 brecciated, slight iron						
		489.0 - 496.0		7.0	0.46			
		492.0 - 494.0 very high iron, <u>soft, muddy</u>						
		494.0 - 500.0 high iron						
		496.0 - 502.0		6.0	0.51			
		500.0 - 504.0 broken, no visible copper						
		504.0 - 534.0 much iron stain badly broken						
		502.0 - 519.0		17.0	0.59			
		519.0 - 528.0		9.0	0.46			
		528.0 - 536.0		8.0	0.43			
		534.0 - 543.0 brecciated, slight copper oxide visible						
		536.0 - 545.0		9.0	0.36			
		543.0 - 544.0 <u>sand seam</u>						
		566.0 - 698.5 fault breccia, fine fragments						
		545.0 - 574.0		29.0	0.31			

HOME-STAKE PRODUCTION COMPANY
CARLOTA COPPER PROPERTY

DIAMOND DRILL HOLE 14

LOCATION:

LATITUDE:
DEPARTURE:

BEARING:
ANGLE DIP:

STARTED:
FINISHED:
LOGGED BY: C.W.Archibald

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH	% Cu			
		703.0 - 707.0 1.0 core						
		707.0 - 708.0 0.5 "						
		713.0 - 720.0 brecciated, much jasper	716.0 - 726.0	10.0	0.13			
		720.0 - 723.0 <u>mud seam</u>						
		729.0 - 730.0 <u>mud seam</u>						
		731.0 - 755.0 much hematite	726.0 - 742.0	16.0	0.04			
			742.0 - 752.0	10.0	0.04			
755.0	765.0	Gabbro, broken siliceous.						
	765.0	END OF HOLE.						

HOME-STAKE PRODUCTION COMPANY
CARLOTA COPPER PROPERTY

DIAMOND DRILL HOLE 14

LOCATION:

LATITUDE:
DEPARTURE:

BEARING:
ANGLE DIP:

STARTED:
FINISHED: _____
LOGGED BY: C.W.Archibald

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH	% Cu			
		<u>SLUDGE ASSAYS</u>						
		360.0 - 370.0		10.0	0.28			
		370.0 - 380.0		10.0	0.17			
		380.0 - 390.0		10.0	0.13			
		390.0 - 400.0		10.0	0.16			
		510.0 - 520.0		10.0	0.30			
		520.0 - 530.0		10.0	0.12			
		530.0 - 540.0		10.0	0.10			
		623.0 - 633.0		10.0	0.10			
		633.0 - 643.0		10.0	0.08			
		654.0 - 662.0		8.0	0.27			
		662.0 - 672.0		10.0	0.41			
		672.0 - 682.0		10.0	0.44			
		703.0 - 707.0		4.0	0.38			
		726.0 - 736.0		10.0	0.03			
		736.0 - 740.0		4.0	0.02			

HOME-STAKE PRODUCTION COMPANY
 CARLOTA COPPER PROPERTY
DIAMOND DRILL HOLE 15

LOCATION: Near Miami Arizona
 LATITUDE: _____ BEARING: _____ STARTED: 1968
 DEPARTURE: _____ ANGLE DIP: - 90° FINISHED: 1968
 LOGGED BY: C.W.Archibald

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH				
0.0	245.0	DACITE, massive 0 - 215.0 weathered 215.0 - 245.0 altered, bleached						
245.0	672.0	FAULT ZONE 245.0 - 412.0 brecciated, hard, slight iron, siliceous 356.0 - 359.0 copper oxides in fractures 412.0 - 517.0 brecciated, badly broken, high iron content decreasing to depth 455.0 - 456.0 slightly more copper oxide 517.0 - 523.0 brecciated, kaolinized copper oxides, no iron 523.0 - 555.0 high iron, soft, no copper to odd copper oxides, fine fragmental 555.0 - 562.0 brecciated, hard, siliceous, slight copper oxides 562.0 - 576.0 high iron content, soft 576.0 - 605.0 siliceous, very slight copper oxides and iron 605.0 - 616.0 high iron content 616.0 - 632.0 brecciated, hard very slight copper oxides 623.0 - 632.0 1'.0 core 632.0 - 639.0 high iron content, slight copper oxides 639.0 - 647.0 mud, 4'.0 core 647.0 concentration of copper						

HOME-STAKE PRODUCTION COMPANY
 CARLOTA COPPER PROPERTY
DIAMOND DRILL HOLE 15

LOCATION:

LATITUDE:
 DEPARTURE:

BEARING:
 ANGLE DIP:

STARTED:
 FINISHED:
 LOGGED BY: C.W.Archibald

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH				
		647.0 - 648.5 hard, much copper oxide.						
		648.5 - 672.0 <u>mud seam</u>						
672.0	715.0	GABBRO (diorite?)						
	715.0	END OF HOLE.						

HOME-STAKE PRODUCTION COMPANY
CARLOTA COPPER PROPERTYDIAMOND DRILL HOLE 15

LOCATION: Near Miami Arizona
 LATITUDE: DEPARTURE:
 BEARING: ANGLE DIP: - 90°
 STARTED: 1968
 FINISHED: 1968
 LOGGED BY: C.W.Archibald

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH				
0.0	245.0	DACITE, massive 0 - 215.0 weathered 215.0 - 245.0 altered, bleached						
245.0	672.0	FAULT ZONE 245.0 - 412.0 brecciated, hard, slight iron, siliceous 356.0 - 359.0 copper oxides in fractures 412.0 - 517.0 brecciated, badly broken, high iron content decreasing to depth 455.0 - 456.0 slightly more copper oxide 517.0 - 523.0 brecciated, kaolinized copper oxides, no iron 523.0 - 555.0 high iron, soft, no copper to odd copper oxides, fine fragmental 555.0 - 562.0 brecciated, hard, siliceous, slight copper oxides 562.0 - 576.0 high iron content, soft 576.0 - 605.0 siliceous, very slight copper oxides and iron 605.0 - 616.0 high iron content 616.0 - 632.0 brecciated, hard very slight copper oxides 623.0 - 632.0 1'.0 core 632.0 - 639.0 high iron content, slight copper oxides 639.0 - 647.0 mud, 4'.0 core 647.0 concentration of copper						

DIAMOND DRILL HOLE 1

5650 N Elev. 3824
6375 E

STARTED: July, 1968

LATITUDE: 1100' W along BEARING:
Base line
LOCATION: CARLOTA PROPERTY, DEPARTURE 800 ft. N.E. ANGLE DIP: Vert.
Arizona

FINISHED:

LOGGED BY: E.A. Hart

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH				
0	15.0	CASING						
15.0	21.0	LIMESTONE - broken weathered.						
21.0	27.0	LIMESTONE - massive.						
27.0	31.0	LIMESTONE - fault zone, gouge.						
31.0	55.5	LIMESTONE - dense, massive.						
55.5	99.0	FAULT ZONE - gouge, red oxide staining fractured limestone.						
		75.0 - 79.0 mud gouge						
99.0	128.0	GABBRO - fractured, not mineralized.						
128.0	133.0	GABBRO - lightly fractured, carbonate stringers.						
133.0	149.0	FAULT ZONE - gouge, breccia, angular limestone fragments, red oxides.						
149.0	728.0	GABBRO 204.0 - 207.0 fault gouge 355.0 - 357.0 " " 568.0 - 575.0 " "						
		Increase to coarse grained from 602 to end of hole.						
		652.0 - 728.0 chloritic						
	728.0	END OF HOLE.						

PAGE:

DIAMOND DRILL HOLE 2

5560 N Elev. 3841

6600 E

LATITUDE: 820 W. along Base line BEARING:

STARTED: July, 1968

FINISHED:

LOCATION: Carlota Property
Arizona

DEPARTURE: 50 Ft. N.E. ANGLE DIP: Vertical

LOGGED BY: E.A.Hart

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH				
0	20.0	CASING						
20.0	50.0	LIMESTONE - fractured						
50.0	129.0	FAULT ZONE - gouge, with limestone fragments red oxides, agate pebbles 109-112						
129.0	141.5	LIMESTONE - fractured, locally brecciated						
141.5	145.0	MUD SEAM - gouge, oxides of iron						
145.0	157.0	CONGLOMERATE - red jasper, granite, agate & sedimentary pebbles, mud seams.						
157.0	361.0	GABBRO - fractured, some 25° slips.						
		164 - 166 fault						
	361.0	END OF HOLE.						

DIAMOND DRILL HOLE 35620 N
6400 E

Elev. 3825

CARLOTA PROPERTY LATITUDE: 1040 W. along BEARING: 198°
 LOCATION: Arizona DEPARTURE: 70 Ft. N.E. Base line ANGLE DIP: - 45°

STARTED: July 30, 1968

FINISHED: Aug. 5, 1968

LOGGED BY: E.A. Hart

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH				
0	10.0	OVERBURDEN						
10.0	15.0	LIMESTONE - fractured						
15.0	21.0	FAULT GOUGE, with limestone fragments @ 30° to C.A.						
24.0	25.5	FAULT GOUGE in limestone						
34.0	36.0	" " " "						
38.0	56.0	" " " "						
56.0	57.0	CONGLOMERATE - variety of pebbles						
57.0	87.0	GABBRO - fault zone, pebbles of conglomerate in gouge areas.						
87.0	205.0	GABBRO - fractured						
	205.0	END OF HOLE.						

PAGE:

CARLOTA PROPERTY, ARIZONA

DIAMOND DRILL HOLE #4

Elev. 3688

STARTED: Aug. 8, 1968

 LOCATION: 680' W along base
 390' N.E.

(line LATITUDE: 5830 N

BEARING: 190°

DEPARTURE: 6815 E

ANGLE DIP: - 45

FINISHED:

LOGGED BY:

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH		% cu
0	10.0	CASING				
10.0	278.0	DACITE - dull red, massive			286.0	304.0 0.04
278.0	331.0	FAULT ZONE - breccia, gouge and limestone fragments			304.0	321.0 0.03
		302 - 305 qtzite, agate pebbles			321.0	324.0 0.04
		321 conglomerate section ground up, lost core				
331.0	346.0	GABBRO - fractured				
346.0	502.0	GABBRO - massive, chloritic - some fractures				
	502.0	END OF HOLE.				

PAGE:

CARLOTA PROPERTY, ARIZONA
DIAMOND DRILL HOLE #5

Elev. 3713

STARTED: Aug. 10, 1968

FINISHED:

LOGGED BY: E.A. Hart

LOCATION: 590' along
base line
280' N.E.

LATITUDE: 5700 N

BEARING: -

DEPARTURE: 6850 E

ANGLE DIP: - 90°

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH			% cu
0	10.0	CASING					
10.0	265.0	DACITE - deep red, some fracturing					
		245 - 265.5 fracturing			278	289	0.08
					289	301	0.84
					301	313	0.09
265.0	485.0	FAULT ZONE - red oxides, breccia, gouge			313	324	0.02
					324	338	0.03
		293 - 301 copper staining, weak					
		376 - 401 gouge, red oxides mostly limestone					
		401 - 414 gabbro breccia					
		414 - 445 carbonate stringers					
		445 - 485 gouge, red oxides					
					<u>SLUDGE</u>		
					283	292	0.03
					292	300	0.28
485.0	758.5	GABBRO - dense massive, fine grained to 530			300	314	0.06
					331	340	0.06
		530 - 650 coarse grained					
		707 - 710 light coloured pyrite, chloritic			632	642	0.06
					642	651	0.04
758.5	791.0	QUARTZITE - light red, weakly bedded @ 60° to C.A.			651	659	0.02
		green areas upper contact @ 80° to C.A.			659	669	0.02
		resembles quartzite on south side of property					
	791.0	END OF HOLE.					

PAGE:

CARLOTA PROPERTY, ARIZONA
DIAMOND DRILL HOLE #6

Elev. 3688

STARTED: Aug. 24, 1968

Same Location

LATITUDE: 5830 N

BEARING: 170°

FINISHED:

LOCATION: as # 4

DEPARTURE: 6816 E

ANGLE DIP: -45

LOGGED BY: E.A. Hart

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH				
0	10.0	CASING						
10.0	60.0	DACITE - dull red, massive.						
	60.0	END OF HOLE.						

PAGE:

CAROLTA PROPERTY, ARIZONA
DIAMOND DRILL HOLE #7

Elev. 3701

STARTED: Aug. 28, 1968

LOCATION:

LATITUDE: 5550 N

BEARING: 210°

FINISHED:

DEPARTURE: 6980 E

ANGLE DIP: -45

LOGGED BY: E.A. Hart

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH		cu %	
0	104.0	DACITE - light red deepens to dark red near fault.			171	176	2.52
104.0	145.0	FAULT ZONE - breccia, limestone and pinal schist fragments.			176	183	0.43
					183	189	0.27
					189	194	1.19
145.0	171.0	GABBRO - fractured, rusty seams.			194	204	1.08
					204	207	0.37
171.0	215.0	GABBRO - fractured, with copper staining also silica seams and manganese.			207	214.5	1.12
					214.5	221.0	0.62
215.0	256.0	GABBRO - fractured, carbonate seams, fine grained to massive.			221.0	230.0	Nil
					<u>SLUDGE</u>		
	256.0	END OF HOLE.			171	176	0.14
					176	186	0.03
					186	196	0.13
					196	206	0.31
					206	214	0.44
					214	226	0.26

PAGE:

CARLOTA PROPERTY, ARIZONA
DIAMOND DRILL HOLE #8

Elev. 3699

STARTED: Sept. 6, 1968

LOCATION:

LATITUDE: 5450 N
 DEPARTURE: 7025 E

BEARING: -
 ANGLE DIP: -90°

FINISHED:
 LOGGED BY: E.A. Hart

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH			Cu %
0	60.0	CASING					
60.0	65.0	FAULT - gouge, grey.			86.0	88.0	2.98
					88.0	97.0	2.41
65.0	86.0	FAULT - gouge, red oxides, limestone fragments, with quartzite pebbles @ 65.0'.			97.0	107.0	0.06
					107.0	116.0	Nil
86.0	95.0	FAULT - rusty seams and copper staining.					
95.0	111.0	FAULT - gabbro breccia, rusty.					
111.0	166.0	GABBRO - fractured, carbonate stringers.			269.0	273.0	0.10
					273.0	280.0	1.66
166.0	252.0	GABBRO - fractured, chloritic, medium grained.			280.0	284.0	0.08
252.0	258.0	FAULT ZONE - white carbonate stringers.					
258.0	272.0	GABBRO - fractured, rusty seams.					
272.0	280.0	FAULT - at 20° to C.A. rusty.					
		273 - 280 copper staining on fractures.					
280.0	446.0	GABBRO - MASSIVE, FINE GRAINED, CHLORITIC.					
	446.0	END OF HOLE.					

PAGE:

CARLOTA PROPERTY, ARIZONA

DIAMOND DRILL HOLE 9

Elev. 3630

STARTED: Sept. 8, 1968

LOCATION:

LATITUDE: 5455 N

BEARING: S 40° W

FINISHED:

DEPARTURE: 7370 E

ANGLE DIP: - 45

LOGGED BY: E.A. Hart

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH				
0	80.0	DACITE - pale red, massive.						
80.0	122.0	DACITE - fractured, some fault breccia.						
122.0	178.0	FAULT ZONE - in dacite.						
178.0	480.0	GABBRO - fractured, chloritic medium to fine grained.						

PAGE:

**CARLOTA PROPERTY, ARIZONA
DIAMOND DRILL HOLE #10**

Elev. 3654

STARTED: Sept. 16, 1968

LOCATION:

LATITUDE: 5390 N

BEARING: -

FINISHED:

DEPARTURE: 7140 E

ANGLE DIP: - 90°

LOGGED BY: E.A. Hart

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH			cu %
0	50.0	CASING					
50.0	78.0	FAULT ZONE - rusty, gouge, with some massive sections of silicified fault breccia of syenite.			66.0	74.0	0.62
					74.0	85.0	3.83
					85.0	90.0	0.05
78.0	86.0	FAULT ZONE - with copper staining.					
86.0	97.0	FAULT ZONE - red oxides, and gabbro fragments.					
97.0	231.0	GABBRO - fractured.					
	231.0	END OF HOLE.					

PAGE:

CARLOTA PROPERTY, ARIZONA
DIAMOND DRILL HOLE #11

Elev. 3505

STARTED: Sept. 23, 1968

LOCATION:

LATITUDE: 5840 N

BEARING:

FINISHED:

DEPARTURE: 7700 E

ANGLE DIP: - 90°

LOGGED BY: E.A. Hart

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH			Cu%
0	60.0	CASING			130.0	140.0	0.68
60.0	91.0	DACITE - dull red, massive.			169.0	174.0	0.41
91.0	104.0	RHYOLITE FLOW - black glassy matrix with angular fragments, fractured from 102.0 - 104.0			519.0	546.0	0.08
					546.0	555.0	0.35
					555.0	565.0	0.39
104.0	702.0	FAULT ZONE - red oxides gouge, chert fragments, some fracturing at 55° to C.A.			565.0	574.0	0.36
					574.0	582.0	0.31
					582.0	585.0	0.26
		Limestone fragments 251.0 - 269.0			585.0	595.0	0.43
		Copper staining 301.0 - 311.0			595.0	604.0	0.72
		" " 519.0 - 563.0			604.0	614.0	0.26
					615.0	625.0	0.52
702.0	722.0	QUARTZITE - altered, fractured			625.0	637.0	0.44
					637.0	647.0	0.75
	722.0	END OF HOLE.			647.0	655.0	0.67
			SLUDGE				
					311	327	0.09
					333	338	0.10
					350	360	0.11
					360	366	0.07
					429	435	0.03
					638	642	0.16

PAGE:

CARLOTA PROPERTY, ARIZONA
DIAMOND DRILL HOLE W-1

LOCATION:

LATITUDE: 5465N
 DEPARTURE: 6525 E

Elev. 3890
 BEARING: 160°
 ANGLE DIP: - 45

STARTED: Sept.11,1968
 FINISHED:
 LOGGED BY: E.A. Hart

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH			Cu %
0	10.0	CASING					
10.0	78.0	GABBRO - coarse grained, well weathered, rusty.			0	24	0.65
					24	57	0.06
	78.0	END OF HOLE.			57	70	Tr.
					70	78	0.06
			<u>SLUDGE</u>				
					40	45	0.02
					45	50	0.04
					50	55	0.01
					55	60	Nil
					60	70	"

PAGE:

**CARLOTA PROPERTY, ARIZONA
DIAMOND DRILL HOLE W-2**

Elev. 3909

STARTED: Sept. 14, 1968

LOCATION:

LATITUDE: 5475 N

BEARING: 165°

FINISHED:

DEPARTURE: 6450 E

ANGLE DIP: -45

LOGGED BY: E.A. Hart

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH			Cu %
0	10.0	CASING					
10.0	91.0	GABBRO - fractured, fine grained. No alteration or mineralization lost core 20%			0	20	Tr
	91.0	END OF HOLE.		<u>SLUDGE</u>	0	20	Tr

PAGE:

CARLOTA PROPERTY, ARIZONA
DIAMOND DRILL HOLE W-3

Elev. 3750

STARTED: Sept. 19, 1968

LOCATION: Pit Floor

LATITUDE: 5400 N

BEARING: N 25° W

FINISHED:

DEPARTURE: 6865 E

ANGLE DIP: - 45°

LOGGED BY: E.A. Hart

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH				
0	47.0	GABBRO - fine fractures with copper silicates coating spaced about 8" apart.						
	47.0	END OF HOLE. Broke through to open stope. 4' lost in 0 - 10 4' " " 10 - 20 11.0' " " 20 - 47.0						

PAGE:

CARLOTA PROPERTY, ARIZONA
DIAMOND DRILL HOLE W-4

			Elev.	3747		STARTED: Sept. 21, 1968
LOCATION: Pit Floor	LATITUDE: 5380 N	BEARING: N 20° W				FINISHED:
	DEPARTURE: 6900 E	ANGLE DIP: - 45°				LOGGED BY: E.A. Hart

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH			Cu%
0	50.0	GABBRO - fractured, weathered with chrysocolla and malachite seams and fracture fillings.			0	13.5	1.21
					13.5	50.0	1.79
	50.0	END OF HOLE IN TIMER. 3'.0 lost 0-10' 35'.0 " 13-50'					

PAGE:

CARLOTA PROPERTY, ARIZONA
DIAMOND DRILL HOLE W-5

LOCATION: Pit Floor Elev. 3753
 LATITUDE: 5410 N BEARING: N 20° W
 DEPARTURE: 6855 E ANGLE DIP: -45°

STARTED: Sept. 25, 1968
 FINISHED: Sept. 26, 1968
 LOGGED BY: E. A. Hart

FROM	TO	REMARKS	SAMPLE NO	SAMPLE LENGTH			Cu %
0	30.0	GABBRO - fractured, with copper secondary mineral.			0	12.5	1.33
					12.5	30.0	2.30
	30.0	END OF HOLE.					

CARLOTTA MINE

COMPARISON LPF vs. SEGREGATION - DIRECT OPERATING COSTS - SAME ORE

WASTE 7000 TONS AND TREAT 2000 TONS PER DAY

<u>OPERATIONAL STEP</u>	<u>2/10/69 BY LPF</u>	<u>4/1/69 BY SEGREGATION</u>
1) Waste to Dump	78.8	78.8
2) Ore mined & delivered	30.0	30.0
3) Grinding & flotation	78.0	78.0
4) Acid	56.0	-
5) Iron	73.6	-
6) Heat (Gas @ 40¢ MM)	-	82.0
7) Salt	-	15.0
8) Coke	-	7.50
9) Maintenance	Included	15.00
10) Labor	<u>Included</u>	<u>12.00</u>
<u>TOTAL LPF</u>	<u>316.40¢</u>	<u>TOTAL SEGREGATION</u>
		<u>318.30¢</u>

SOURCE OF COST DATA

<u>ITEM</u>	<u>SOURCE</u>	<u>COMMENT</u>
1,2,3	Bagdad Copper	See 1/10/69 report
4,5	Bagdad Est. adjusted to Carlotta	" " "
6	El Paso Natural Gas	Actual at 750 TPD
7,8	" " " "	Adj. Carlotta BM Test
9	Freeman, Bechtel, Runke	per memo to RST 3/28/69
10	El Paso Natural Gas	Adjusted to tonnage

PLACER MINING IN NEVADA

Start Page 113

From time to time the thought of placer mining the sands along the Carson River for the values lost in mill tailings is revived. These tailings were derived from the early-day mills used for the treatment of the Comstock ores. At one time it is reported there were 150 mills in the District, many of them along the Carson River. Virtually all of these mills were operated on a custom basis, and many of them never produced anything except litigation and assessments. These early-day mills employed the Washoe process (amalgamation in pans heated by steam, using quicksilver, salt, and copper sulphate for reagents), the Frieberg process (chloridizing roasting with subsequent amalgamation in barrels), Veatch process (same as Frieberg process, except that steam tubs were used instead of the barrels), and the Patio process (amalgamation on an open floor with the aid of salt and copper sulphate). These early-day processes were crude as compared with present metallurgical practice, and recovery was from 60 to 65 percent. The values lost in the tailings were deemed of minor importance. Although some of the tailings were impounded and subsequently re-treated, a vast amount was diverted into the Carson River. It is reported that some \$60,000,000 of values left in the old tailings were sluiced down the canyons or deposited directly into the Carson River.

In the early nineties a company, backed by Boston capitalists, was organized to recover the values in these old tailings. Seventeen miles of "tailings" were located along the course of the Carson River from Empire towards Dayton. Floured quicksilver could be panned or washed out along the banks, bed, and flats of the river, and assays showed from a few cents to a dollar or more per ton. Three dredges were constructed to work these tailings, two of which were of the clam-shell type, the third being a suction dredge, all powered by steam. Reported cost of the equipment was about \$300,000. Attempts to work the tailings persisted over a period of eight years, when finally the rich conundrum was abandoned. This venture demonstrated that no dredging process could profitably overcome the expense of washing the vast amount of sand, mud, and gravel to recover the values lost in the tailings.

ORE FROM MINE → COARSE ORE STORAGE

125 T.P.H. PORTABLE CRUSHER 101

SURGE BIN
24" X 36" JAW CRUSHER 100 H.P.

+ 2" SCREEN
+ 1/2" SCREEN

4' SYMON'S CONE CRUSHER 100 H.P.

2000 TON LIVE STORAGE

WEIGHTOMETER AND AUTOMATIC FEEDER 103

104 DRAW TUNNEL

KREBS CYCLONE 106

+ 20 MESH

6' X 12' ROD MILL 200 H.P. 105

6" X 6" SAND PUMP 10 H.P. 107

- 20 MESH

108 A

108 B

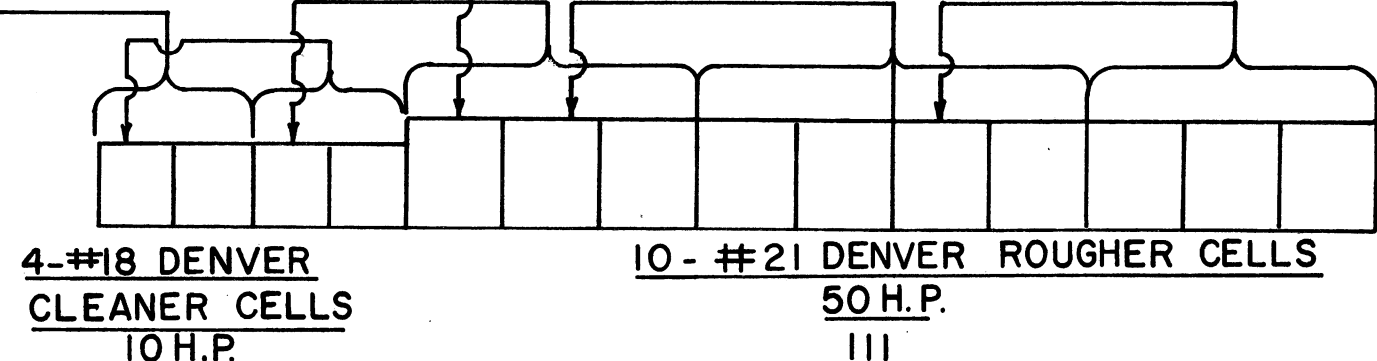
108 C

AIR AGITATION

3 - 9' X 10' AGITATION LEACHING VATS (1.5 HOURS RETENTION AT 30% SOLIDS)

6' X 50' PRECIPITATION TUBE (RUBBER LINED) 25 H.P. 109

MAGNETIC SEPARATOR AND SCREEN 110



TO TAILINGS POND

2- 6" X 6" SAND PUMPS (1 as standby) 114A 114B

NOT SHOWN

- ACID STORAGE TANK 115
- WATER STORAGE TANK 116
- BUTLER TYPE BLDG. 117
- FENCE 118
- SCALE 119

NO

- 115
- 116
- 117
- 118
- 119

EIMCO 2 LEAF 6' FILTER 4 H.P. 113

COPPER CEMENT TO MARKET

DIAGRAMATIC FLOW SHEET

LEACHING, PRECIPITATION, FLOTATION PLANT CARLOTTA PROJECT

G. A. FREEMAN
D. K. PICKENS

HOME-STAKE PRODUCTION COMPANY

TULSA, OKLA.

ORE IN- 700 T.P.D.
5 DAYS/WEEK, 8 HR. DAY

WATER BALANCE - PER 24 HR. PERIOD

TOTAL REQD.	360,000
LESS RETURN	108,000
NET MAKE UP	252,000 G.P.D. (175 G.P.M.)

RECOVERY

85% AS 80% CU CONTAINED IN CEMENT

CONCENTRATION RATIO

46.9 TO 1

LEACHING RETENTION TIME

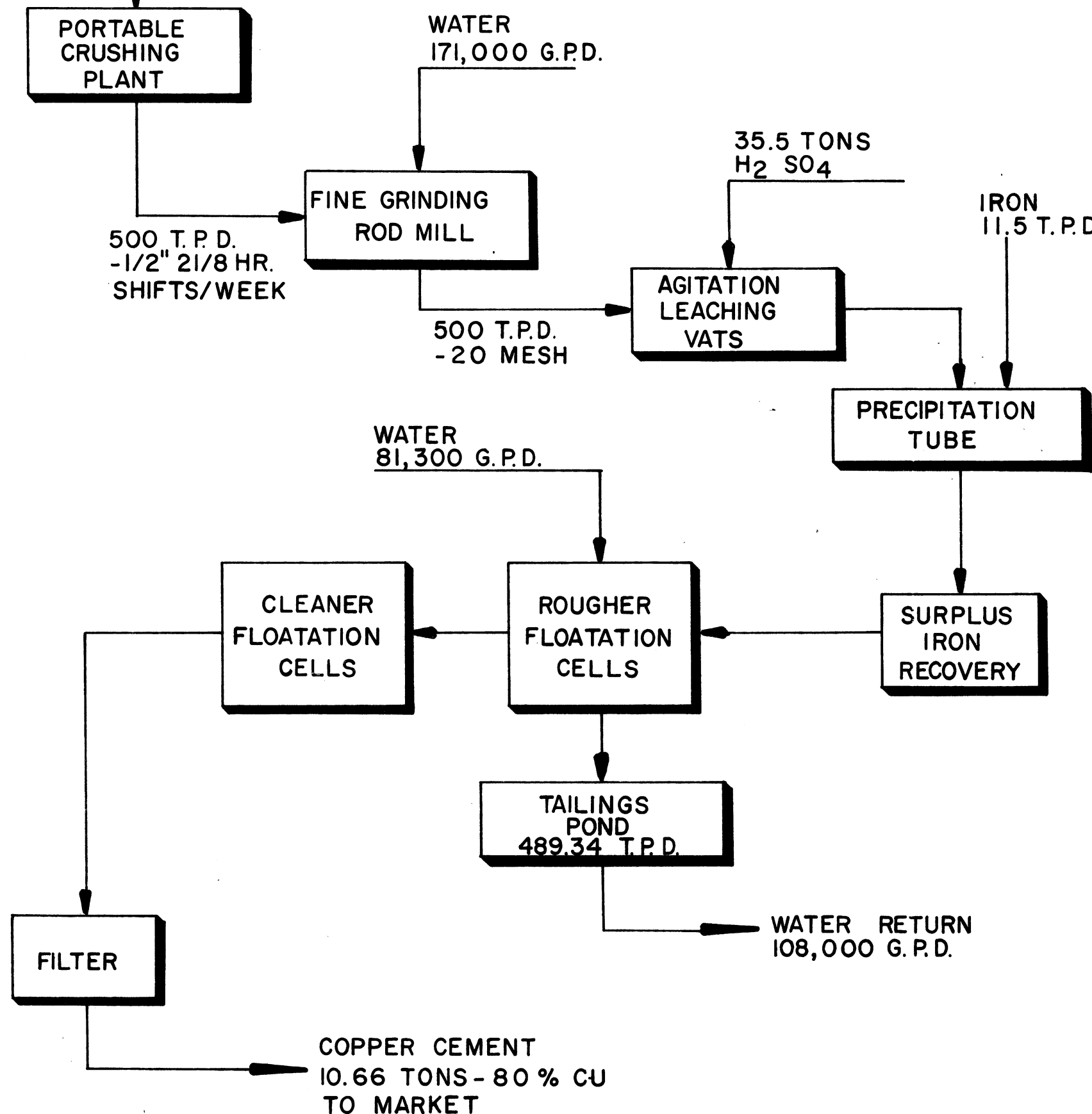
1.5 HOURS

ACID CONSUMPTION

3 LBS. ACID / LB. CU

IRON (CLEAN) CONSUMPTION

1.3 LBS. IRON / LB. CU



BLOCK FLOW DIAGRAM
AND
MATERIAL BALANCE
LEACHING, PRECIPITATION, FLOATATION PLANT
CARLOTTA PROJECT
G.A. FREEMAN
D.K. PICKENS
HOME-STAKE PRODUCTION COMPANY
TULSA, OKLA.

SCHEDULE II

CARLOTTA MINE - OPERATING COSTS

TO TREAT 500 TPD 2% Cu ORE PRODUCING 17,000# Cu/DAY AS PRECIPITATES

DIRECT COSTS

	<u>Day</u>	<u>¢/#/Cu</u>
1) <u>Labor</u>		
3 Mill Operators @ \$32/day	\$ 96.00	
3 Helpers @ \$24/day	72.00	
2 Pit Operators @ \$36/day	72.00	
1 Master Mechanic - Electrician @ \$32/day	32.00	
1 Mechanic Welder @ \$24/day	24.00	
1 Motor Patrol & Pond Operator @ \$32/day	32.00	
1 Crushing Plant Operator @ \$28/day	28.00	
	<hr/>	<hr/>
	\$ 356.00	2.094
2) <u>Supervision</u>		
Plant Manager	\$ 50.00	
Plant Superintendent	35.00	
Chemist	30.00	
Clerk Typist	30.00	
	<hr/>	<hr/>
	\$ 145.00	0.852
3) <u>Reagents & Utilities</u>		
Precipitation Iron 11.5 TPD @ \$50/ton	\$ 575.00	
Acid 25.5 TPD @ \$25/ton	637.50	
Flotation & Miscellaneous Chemicals	175.00	
Power 678 HP connected (over consump)		
9600 KWHR (day) 1¢/KWHR	96.00	
Fuel & Lubricants	30.00	
	<hr/>	<hr/>
	\$1,513.50	8.905
4) <u>Equipment Rentals</u>	\$ 250.00	1.470
5) <u>Miscellaneous Maintenance Parts,</u> <u>Repair Material & Operating Supplies</u>	<hr/>	<hr/>
	\$ 75.00	0.441
	<hr/>	<hr/>
<u>TOTAL DIRECT COSTS</u>	\$2,339.50	13.762

INDIRECT COSTS

6) <u>Royalties - In Lieu Acquisition Costs -</u> \$400,000 @ 10% - first 566 days (approx. 18 months) of Smelter Returns	<hr/>	<hr/>
	\$ 700.00	4.117
7) <u>Arizona "Sales" Tax 1½% Gross</u>	<hr/>	<hr/>
	104.50	0.617
8) <u>Local Taxes and Insurance</u>	<hr/>	<hr/>
	50.00	0.294
9) <u>General Administrative & Sales (tel & tel)</u> Travel, Accounting, Payroll Taxes, etc.	<hr/>	<hr/>
	100.00	0.588
10) <u>Depreciation</u> (7½ yr/straight line) on \$331,450	<hr/>	<hr/>
	135.00	0.794
	<hr/>	<hr/>
<u>TOTAL INDIRECT COSTS</u>	\$1,089.50	6.410
	<hr/>	<hr/>
<u>TOTAL ALL COSTS</u>	\$3,429.00	20.172

PROCESS DESCRIPTION - CARLOTTA PROJECT

After careful study, it has been decided that the most desirable system to be installed at Carlotta will be a combination leaching, precipitation, flotation plant (LPF). The plant will be very similar, but somewhat smaller than the Emerald Isle operation of El Paso Natural Gas near Kingman, Arizona. (See Plates A and B following)

A contractor's type portable crushing plant will take mine run ore and crush it to minus one-half inch at the rate of at least 700 tons per day, 5 days per week. This ore will be fed to a live storage pile which will be able to store 2,000 tons ahead. The draw tunnel from the live storage will feed through an automatic weighing and sampling device to a 6' x 12' rod mill which in turn will grind the material to minus 20 mesh, in closed circuit with a Krebs Cyclone.

The fine ground material will be fed, together with proper amount of acid, to a three stage (Denver Equipment Company) agitation leaching system equipped with both air and mechanical agitation. Tests have shown that 88% of the copper will readily go into solution in one hour with three pounds of acid per pound of copper or less. A 50% over-capacity for retention time has been allowed.

The leached copper and solids are then passed to a precipitation tube made of used kiln equipment, which tube will be 6' x 50' long and will receive iron in proper proportion with the slurry. An excess of iron will be used so as to be certain that all possible copper in solution is precipitated. A magnetic pulley and screen arrangement will recover any excess iron and return it to the circuit. Final separation will be by flotation in two stages. The copper precipitate (cement copper) will be partially dried in an Eimco two-leaf filter, final drying on pads in air.

The principal reason for the choice of the LPF system (rather than acid leaching, clarification and cementation) has been dictated primarily by the tendency of Carlotta ores to be very "slimey", giving trouble in settling basins and extraction. The LPF system eliminates this difficulty and gives a slightly higher grade product. It also uses less water and is easier to control, and gives better recovery.

In future, if sulphide ores are mined (or combination oxide-sulphide ores) the plant can be quickly adapted at low additional capital cost.

SCHEDULE III (cont'd)

<u>Item No.</u>		<u>Amount</u>	<u>Connected H. P.</u>
121	Tailings Pond Pump & Piping-contract	\$ 7,500	25
122	Reinforced Concrete Floors & Foundations - 300 cu. yd. @ \$30 cu. yd. in place	9,000	
123	Rental Equipment during Construction	20,000	
124	Instrumentation, Piping & Wiring - Subcontracts	37,500	
125	Engineering, Drafting Equipment Inspection, Travel & Misc.	12,500	
126	Advance to Arizona Public Service for Power line to Transformers	30,000 (1)	
127	Offsite - Preparation of Steel Scrap (Shredding & Handling Equipment)	30,000 (2)	
	TOTAL	<u>\$331,450</u>	<u>678</u>

(1) APS advance recovered over 5 years - assumes maximum 5 miles new line - alternate lease rental butane engine generator should be studied.

(2) Based on completed studies shredding Pittsburgh Steel copper clad (6%) waste steel.

SCHEDULE III

CAPITAL COST - CARLOTTA MINE

PLANT TO TREAT 500 TONS PER DAY

2% COPPER OXIDE TO PRODUCE 17,000# COPPER IN PRECIPITATES

A. Basic Equipment delivered and set on Foundations

<u>Item No.</u>		<u>Amount</u>	<u>Connected H. P.</u>
101	Contractors Portable Crushing Plant - 125 TPH - <u>(Used)</u>	\$35,000	200
102	Conveyor 24" x 100'	3,000	10
103	Feeder & Automatic Weighing Device	6,500	5
104	Conveyor 18" x 50'	2,000	5
105	6' x 12' Rod Mill <u>(Used)</u>	10,000	200
106	Krebs Cyclone	2,000	
107	6" x 6" Denver Sand Pump	1,800	10
108 abc	Agitated Leaching Vats (Standard Denver Equipment Co.)	10,050	30
109	Precipitation Tube (Iron Addition) <u>Used</u>	25,000	25
110	Magnetic Separator & Screen	6,000	3
111	10 - #21 Denver Float Cells (Roughers)	9,000	50
112	4 - #18 Denver " " (Cleaners)	4,000	10
113	Eimco 6' - 4 leaf vacuum filter	15,000	35
114 a&b	2 - 6" x 6" Denver Sand Pumps	3,600	20
115	Acid Storage Tank <u>(Used)</u>	4,000	
116	60,000 gallon Water Storage - 2 tanks - Fiberglass	10,000	
117	Prefabricated & Erected Bulter Type Building with Lighting	20,000	
118	Fence	3,000	
119	Scale <u>(Used)</u>	5,000	

B. Other Items of Construction Cost not included above:

120	Water Well, Pump & Pipe Installed - contract	10,000	50
-----	--	--------	----

CARLOTTA OPEN PIT MINE DESIGN

The classification of material as ore or waste in an open pit mine depends upon the grade of the material, the location, and the economic conditions. The table on the next page gives the value per ton of material at specified copper grades for the economic assumptions shown at the top of the page. This value per ton does not include the cost of mining the waste material which may overlay the ore. The column headed ALLOWABLE STRIPPING RATIO gives the number of waste tons which may be mined to remove one ton of ore. This table indicates that only material with an average grade greater than 0.70% copper is economic under the economic assumptions.

It is somewhat unlikely that an economic pit can be designed for the Carlotta deposit on the above basis with the current data that is available. Therefore, a pit was designed with a 50 degree slope to include as much of the +1.0% copper material as possible without sending the stripping ratio too high. A transparency has been prepared and is included in the geologic matrix section that shows the limits of the pit design on selected benches.

A second transparency has been prepared and included that shows the maximum size of several benches if the pit is limited to be within the property lines. A pit slope of 50 degrees was used to project down from the boundaries. This transparency shows the fact that no economic pit can be obtained with this limitation.

RESERVES FOR CARLOTTA PIT DESIGN

A summary of the reserves computed for each bench within the pit design is shown on a following page. These reserves are based on a tonnage factor of 12.0 cubic feet per ton, which is the factor used by Mieritz. This tonnage factor may be a little optimistic considering that a tonnage factor of 12.5 cubic feet per ton is normally used in this area. The reserves for all 25-foot bench accompanies this report. Two sets of the reserves were made to show the (1) +0.9%, +0.7%, +0.5% and 0.0 to 0.49% material and (2) +0.9%, 0.7 to 0.89%, 0.5 to 0.69% and 0.0 to 0.49% material.

ECONOMIC ASSUMPTIONS

PRICE \$/LB	=	.5000
MINING COST \$/TON	=	.4000
MILLING COST \$/TON	=	3.7000
INDIRECT COST \$/TON	=	.0000
MILL RECOVERY (XX.01)	=	.7700
SMLT, REF, MRKT \$/LB	=	.1000

these assumptions were used as guidelines in the pit design

they are assumptions only and a more detailed analysis should be made

GRADE	VALUE/TON	ALLOWABLE STRIPPING RATIO
.1000	-3.4840	.0000
.2000	-2.8680	.0000
.3001	-2.2520	.0000
.4001	-1.6360	.0000
.5001	-1.0200	.0000
.6001	-.4040	.0000
.7001	.2120	.5300
.8001	.8280	2.0700
.9001	1.4440	3.6100
1.0000	2.0600	5.1500
1.1000	2.6760	6.6900
1.2000	3.2920	8.2300
1.3000	3.9080	9.7700
1.4000	4.5240	11.3099
1.5000	5.1400	12.8499
1.6000	5.7560	14.3899
1.7000	6.3720	15.9299
1.8000	6.9880	17.4699
1.9000	7.6040	19.0099
2.0000	8.2200	20.5499

material with a copper grade of .70 will pay for itself

material with a copper grade of 1.1 would have a breakeven stripping ratio of 6.7:1

SEPT 1971

** GEOLOGIC RESERVES ** SANTA RITA MINING COMPANY **

CUT-OFF GRADE % CU	KELLY ZONE		CARLOTTA ZONE		BOTH ZONES	
	TONS X1000	% CU	TONS X1000	% CU	TONS X1000	% CU
0.10	4,286	1.283	6,000	0.508	10,286	0.831
0.20	4,286	1.283	5,172	0.564	9,458	0.890
0.30	4,286	1.283	4,271	0.629	8,557	0.957
0.40	4,068	1.333	2,828	0.774	6,896	1.104
0.50	3,740	1.410	2,266	0.855	6,006	1.200
0.60	3,505	1.467	1,594	0.985	5,099	1.317
0.70	3,224	1.540	1,135	1.122	4,359	1.431
0.80	3,125	1.566	812	1.270	3,932	1.505
0.90	3,052	1.583	656	1.371	3,708	1.545
1.00	2,870	1.624	536	1.465	3,406	1.599
1.10	1,307	2.367	427	1.566	1,734	2.169
1.20	1,250	2.424	349	1.666	1,599	2.259
1.30	1,146	2.532	312	1.713	1,458	2.356
1.40	1,047	2.642	292	1.739	1,339	2.445
1.50	927	2.800	260	1.775	1,187	2.575

TONNAGE FACTOR = 12.0 CUBIC FT/TON

MINTEC, INC.

GEOLOGY MATRIX

THE FOLLOWING MAPS SHOW THE GEOLOGY CODES FOR THE CARLOTTA:

1 = KELLY FAULT

2 = CARLOTTA

3 = UNKNOWN

The matrix origin is: XMIN (WEST) = -1500, mine grid
YMIN (SOUTH) = -200, mine grid

MAXIMUM PIT OUTLINES WITHIN PROPERTY BOUNDARIES

01 02 03 04 05

30

25

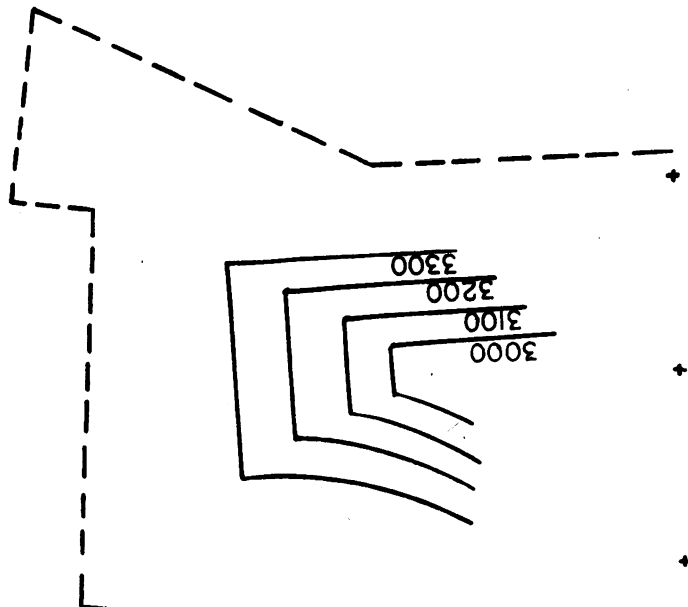
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15

10

5

1



TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL. LEVEL 4 3700.0 TO 3725.0

	10	20	30	40	50
ROW	+.....+	+.....+	+.....+	+.....+	+.....+
30	133333	333333	333333	333333	333333
29	133333	333333	333333	333333	333333
28	133333	333333	333333	333333	333333
27	133333	333333	333333	333333	333333
26	133333	333333	333333	333333	333333
25	133333	333333	333333	333333	333333
24	133333	333333	333333	333333	333333
23	133333	333333	333333	333333	333333
22	133333	333333	333333	333333	333333
21	133333	333333	333333	333333	333333
20	133333	333333	333333	333333	333333
19	133333	333333	333333	333333	333333
18	133333	333333	333333	333333	333333
17	133333	333333	333333	333333	333333
16	133333	333333	333333	333333	333333
15	133333	333333	333333	333333	333333
14	133333	333333	333333	333333	333333
13	133333	333333	333333	333333	333333
12	133333	333333	333333	333333	333333
11	133333	333333	333333	333333	333333
10	133333	333333	333333	333333	333333
9	133333	333333	333333	333333	333333
8	133333	333333	333333	333333	333333
7	133333	333333	333333	333333	333333
6	133333	333333	333333	333333	333333
5	133333	333333	333333	333333	333333
4	133333	333333	11111	333333	333333
3	133333	333333	333333	333333	333333
2	133333	333333	333333	333333	333333
1	133333	333333	333333	333333	333333
ROW	+.....+	+.....+	+.....+	+.....+	+.....+
	10	20	30	40	50

TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL, LEVEL 8 3600.0 TO 3625.0

	10	20	30	40	50
ROW +	+	+	+	+	+
30	1	3	3	3	3
29	1	3	3	3	3
28	1	3	3	3	3
27	1	3	3	3	3
26	1	3	3	3	3
25	1	3	3	3	3
24	1	3	3	3	3
23	1	3	3	3	3
22	1	3	3	3	3
21	1	3	3	3	3
20	1	3	3	3	3
19	1	3	3	3	3
18	1	3	3	3	3
17	1	3	3	3	3
16	1	3	3	3	3
15	1	3	3	3	3
14	1	3	3	3	3
13	1	3	3	3	3
12	1	3	3	3	3
11	1	3	3	3	3
10	1	3	3	3	3
9	1	3	3	3	3
8	1	3	3	3	3
7	1	3	3	3	3
6	1	3	3	3	3
5	1	3	3	3	3
4	1	3	3	3	3
3	1	3	3	3	3
2	1	3	3	3	3
1	1	3	3	3	3
ROW +	+	+	+	+	+

TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL. LEVEL 9 3575.0 TO 3600.0

	10	20	30	40	50
ROW	+	+	+	+	+
30	1	3	3	3	3
29	1	3	3	3	3
28	1	3	3	3	3
27	1	3	3	3	3
26	1	3	3	3	3
25	1	3	3	3	3
24	1	3	3	3	3
23	1	3	3	3	3
22	1	3	3	3	3
21	1	3	3	3	3
20	1	3	3	3	3
19	1	3	3	3	3
18	1	3	3	3	3
17	1	3	3	3	3
16	1	3	3	3	3
15	1	3	3	3	3
14	1	3	3	3	3
13	1	3	3	3	3
12	1	3	3	3	3
11	1	3	3	3	3
10	1	3	3	3	3
9	1	3	3	3	3
8	1	3	3	3	3
7	1	3	3	3	3
6	1	3	3	3	3
5	1	3	3	3	3
4	1	3	3	3	3
3	1	3	3	3	3
2	1	3	3	3	3
1	1	3	3	3	3
ROW	+	+	+	+	+

TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL, LEVEL 10 3550.0 TO 3575.0

	10	20	30	40	50
ROW	+	+	+	+	+
30	1	3	3	3	3
29	1	3	3	3	3
28	1	3	3	3	3
27	1	3	3	3	3
26	1	3	3	3	3
25	1	3	3	3	3
24	1	3	3	3	3
23	1	3	3	3	3
22	1	3	3	3	3
21	1	3	3	3	3
20	1	3	3	3	3
19	1	3	3	3	3
18	1	3	3	3	3
17	1	3	3	3	3
16	1	3	3	3	3
15	1	3	3	3	3
14	1	3	3	3	3
13	1	3	3	3	3
12	1	3	3	3	3
11	1	3	3	3	3
10	1	3	3	3	3
9	1	3	3	3	3
8	1	3	3	3	3
7	1	3	3	3	3
6	1	3	3	3	3
5	1	3	3	3	3
4	1	3	3	3	3
3	1	3	3	3	3
2	1	3	3	3	3
1	1	3	3	3	3
ROW	+	+	+	+	+

TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL, LEVEL 13 3475.0 TO 3500.0

	10	20	30	40	50
ROW	+.....+	+.....+	+.....+	+.....+	+.....+
30	133333	333333	333333	333333	333333
29	133333	333333	333333	333333	333333
28	133333	333333	333333	333333	333333
27	133333	333333	333333	333333	333333
26	133333	333333	333333	333333	333333
25	133333	333333	333333	333333	333333
24	133333	333333	333333	333333	333333
23	133333	333333	333333	333333	333333
22	133333	333333	333333	333333	333333
21	133333	333333	333333	333333	333333
20	133333	333333	333333	333333	333333
19	133333	333333	333333	333333	333333
18	133333	333333	333333	333333	333333
17	133333	333333	333333	333333	333333
16	133333	333333	333333	333333	333333
15	133333	333333	333333	333333	333333
14	133333	333333	333333	333333	333333
13	133333	333333	333333	333333	333333
12	133333	333333	333333	333333	333333
11	133333	333333	333333	333333	333333
10	133333	333333	333333	333333	333333
9	133333	333333	333333	333333	333333
8	133333	333333	1111	333333	333333
7	133333	333333	111111	333333	333333
6	133333	333333	111	333333	333333
5	133333	333333	333333	333333	333333
4	133333	333333	333333	333333	333333
3	133333	333333	333333	333333	333333
2	133333	333333	333333	333333	333333
1	133333	333333	333333	333333	333333
ROW	+.....+	+.....+	+.....+	+.....+	+.....+
	10	20	30	40	50

TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL. LEVEL 14 3450.0 TO 3475.0

	10	20	30	40	50
ROW	+	+	+	+	+
30	1	3	3	3	3
29	1	3	3	3	3
28	1	3	3	3	3
27	1	3	3	3	3
26	1	3	3	3	3
25	1	3	3	3	3
24	1	3	3	3	3
23	1	3	3	3	3
22	1	3	3	3	3
21	1	3	3	3	3
20	1	3	3	3	3
19	1	3	3	3	3
18	1	3	3	3	3
17	1	3	3	3	3
16	1	3	3	3	3
15	1	3	3	3	3
14	1	3	3	3	3
13	1	3	3	3	3
12	1	3	3	3	3
11	1	3	3	3	3
10	1	3	3	3	3
9	1	3	3	3	3
8	1	3	3	3	3
7	1	3	3	3	3
6	1	3	3	3	3
5	1	3	3	3	3
4	1	3	3	3	3
3	1	3	3	3	3
2	1	3	3	3	3
1	1	3	3	3	3
ROW	+	+	+	+	+

TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
SANTA PITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL, LEVEL 16 3400.0 TO 3425.0

	10	20	30	40	50
ROW	+.....+	+.....+	+.....+	+.....+	+.....+
30	133333	333333	333333	333333	333333
29	133333	333333	333333	333333	333333
28	133333	333333	333333	333333	333333
27	133333	333333	333333	333333	333333
26	133333	333333	333333	333333	333333
25	133333	333333	333333	333333	333333
24	133333	333333	333333	333333	333333
23	133333	333333	333333	333333	333333
22	133333	333333	333333	333333	333333
21	133333	333333	333333	333333	333333
20	133333	333333	333333	333333	333333
19	133333	333333	333333	333333	333333
18	133333	333333	333333	333333	333333
17	133333	333333	333333	333333	333333
16	133333	333333	333333	333333	333333
15	133333	333333	333333	333333	333333
14	133333	333333	333333	333333	333333
13	133333	333333	333333	333333	333333
12	133333	333333	333333	333333	333333
11	133333	333333	333333	333333	333333
10	133333	333333	333333	333333	333333
9	133333	333333	111	333333	333333
8	133333	333333	333	111	333333
7	133333	333333	333	333	111
6	133333	333333	333333	333333	333333
5	133333	333333	333333	333333	333333
4	133333	333333	333333	333333	333333
3	133333	333333	333333	333333	333333
2	133333	333333	333333	333333	333333
1	133333	333333	333333	333333	333333
ROW	+.....+	+.....+	+.....+	+.....+	+.....+
	10	20	30	40	50

TEST RUN AUGUST 19, 1971. GEOLOGIC ZONE
SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL. LEVEL 20 3300.0 TO 3325.0

	10	20	30	40	50
ROW	+.....+	+.....+	+.....+	+.....+	+.....+
30	133333	333333	333333	333333	333333
29	133333	333333	333333	333333	333333
28	133333	333333	333333	333333	333333
27	133333	333333	333333	333333	333333
26	133333	333333	333333	333333	333333
25	133333	333333	333333	333333	333333
24	133333	333333	333333	333333	333333
23	133333	333333	333333	333333	333333
22	133333	333333	333333	333333	333333
21	133333	333333	333333	333333	333333
20	133333	333333	333333	333333	333333
19	133333	333333	333333	333333	2223333333333333
18	133333	333333	333333	333333	222222333333333333
17	133333	333333	22233333333333	222222333333333333	3333333333333333
16	133333	333333	22222233333333	222333333333333333	3333333333333333
15	133333	333333	22222233333333	222333333333333333	3333333333333333
14	133333	333333	22233333333333	222333333333333333	3333333333333333
13	133333	333333	22233322222222	222333333333333333	3333333333333333
12	133333	333333	22233322222222	222333333333333333	3333333333333333
11	133333	333333	22233322222222	222333333333333333	3333333333333333
10	133333	333333	11133322222222	222333333333333333	3333333333333333
9	133333	333333	1111111111113333	333333333333333333	3333333333333333
8	133333	333333	1113333333333333	333333333333333333	3333333333333333
7	133333	333333	3333333333333333	333333333333333333	3333333333333333
6	133333	333333	3333333333333333	333333333333333333	3333333333333333
5	133333	333333	3333333333333333	333333333333333333	3333333333333333
4	133333	333333	3333333333333333	333333333333333333	3333333333333333
3	133333	333333	3333333333333333	333333333333333333	3333333333333333
2	133333	333333	3333333333333333	333333333333333333	3333333333333333
1	133333	333333	3333333333333333	333333333333333333	3333333333333333
ROW	+.....+	+.....+	+.....+	+.....+	+.....+
	10	20	30	40	50

TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL. LEVEL 21 3275.0 TO 3300.0

	10	20	30	40	50
ROW	+	+	+	+	+
30	1	3	3	3	3
29	1	3	3	3	3
28	1	3	3	3	3
27	1	3	3	3	3
26	1	3	3	3	3
25	1	3	3	3	3
24	1	3	3	3	3
23	1	3	3	3	3
22	1	3	3	3	3
21	1	3	3	3	3
20	1	3	3	3	3
19	1	3	3	3	3
18	1	3	3	3	3
17	1	3	3	3	3
16	1	3	3	3	3
15	1	3	3	3	3
14	1	3	3	3	3
13	1	3	3	3	3
12	1	3	3	3	3
11	1	3	3	3	3
10	1	3	3	3	3
9	1	3	3	3	3
8	1	3	3	3	3
7	1	3	3	3	3
6	1	3	3	3	3
5	1	3	3	3	3
4	1	3	3	3	3
3	1	3	3	3	3
2	1	3	3	3	3
1	1	3	3	3	3
ROW	+	+	+	+	+

TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
 SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL, LEVEL 22 3250.0 TO 3275.0

	10	20	30	40	50
ROW	+.....+	+.....+	+.....+	+.....+	+.....+
30	133333	333333	333333	333333	333333
29	133333	333333	333333	333333	333333
28	133333	333333	333333	333333	333333
27	133333	333333	333333	333333	333333
26	133333	333333	333333	333333	333333
25	133333	333333	333333	333333	333333
24	133333	333333	333333	333333	333333
23	133333	333333	333333	333333	333333
22	133333	333333	333333	333333	333333
21	133333	333333	333333	333333	333333
20	133333	333333	333333	333333	333333
19	133333	333333	333333	333333	2223333333333333
18	133333	333333	333333	333333	2222223333333333
17	133333	333333	333333	333333	2222223333333333
16	133333	333333	333333	333333	2222223333333333
15	133333	333333	333333	333333	2222223333333333
14	133333	333333	333333	333333	2222223333333333
13	133333	333333	333333	333333	2222223333333333
12	133333	333333	333333	333333	2222223333333333
11	133333	333333	333333	333333	2222223333333333
10	133333	333333	333333	111111222222	3333333333333333
9	133333	333333	333333	1113333333333333	3333333333333333
8	133333	333333	333333	333333	3333333333333333
7	133333	333333	333333	333333	3333333333333333
6	133333	333333	333333	333333	3333333333333333
5	133333	333333	333333	333333	3333333333333333
4	133333	333333	333333	333333	3333333333333333
3	133333	333333	333333	333333	3333333333333333
2	133333	333333	333333	333333	3333333333333333
1	133333	333333	333333	333333	3333333333333333
ROW	+.....+	+.....+	+.....+	+.....+	+.....+
	10	20	30	40	50

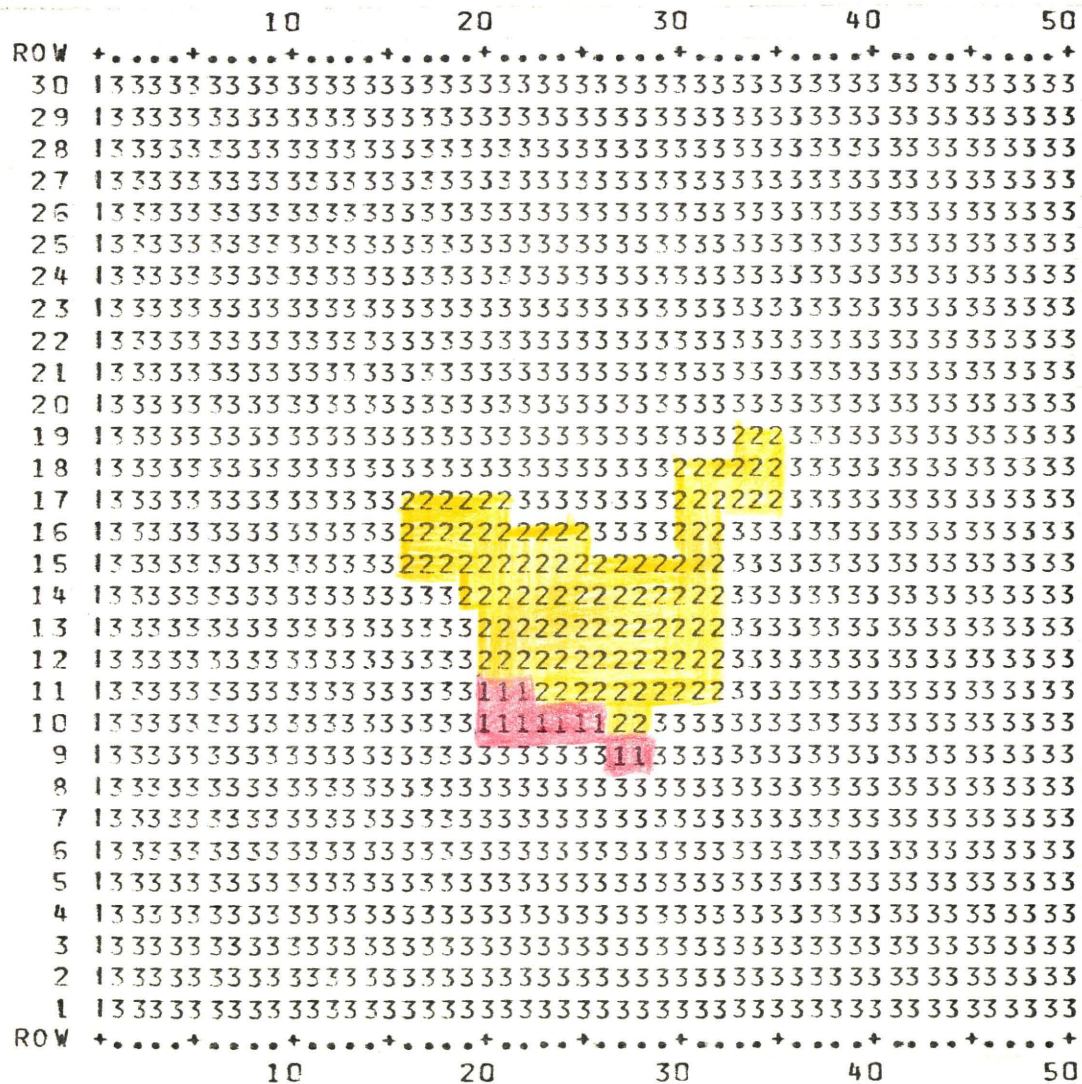
TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL, LEVEL 23 3225.0 TO 3250.0

	10	20	30	40	50
ROW	+.....+	+.....+	+.....+	+.....+	+.....+
30	1333333333	3333333333	3333333333	3333333333	3333333333
29	1333333333	3333333333	3333333333	3333333333	3333333333
28	1333333333	3333333333	3333333333	3333333333	3333333333
27	1333333333	3333333333	3333333333	3333333333	3333333333
26	1333333333	3333333333	3333333333	3333333333	3333333333
25	1333333333	3333333333	3333333333	3333333333	3333333333
24	1333333333	3333333333	3333333333	3333333333	3333333333
23	1333333333	3333333333	3333333333	3333333333	3333333333
22	1333333333	3333333333	3333333333	3333333333	3333333333
21	1333333333	3333333333	3333333333	3333333333	3333333333
20	1333333333	3333333333	3333333333	3333333333	3333333333
19	1333333333	3333333333	3333333333	2223333333	3333333333
18	1333333333	3333333333	3333333333	2222233333	3333333333
17	1333333333	3333332222	3333333333	2222233333	3333333333
16	1333333333	3333332222	2222233333	2223333333	3333333333
15	1333333333	3333332222	2222222222	3333333333	3333333333
14	1333333333	3333332222	2222222222	3333333333	3333333333
13	1333333333	3333332222	2222222222	3333333333	3333333333
12	1333333333	3333332222	2222222222	3333333333	3333333333
11	1333333333	3333331122	2222222222	3333333333	3333333333
10	1333333333	3333331111	2233333333	3333333333	3333333333
9	1333333333	3333333333	3333333311	3333333333	3333333333
8	1333333333	3333333333	3333333333	3333333333	3333333333
7	1333333333	3333333333	3333333333	3333333333	3333333333
6	1333333333	3333333333	3333333333	3333333333	3333333333
5	1333333333	3333333333	3333333333	3333333333	3333333333
4	1333333333	3333333333	3333333333	3333333333	3333333333
3	1333333333	3333333333	3333333333	3333333333	3333333333
2	1333333333	3333333333	3333333333	3333333333	3333333333
1	1333333333	3333333333	3333333333	3333333333	3333333333
ROW	+.....+	+.....+	+.....+	+.....+	+.....+
	10	20	30	40	50

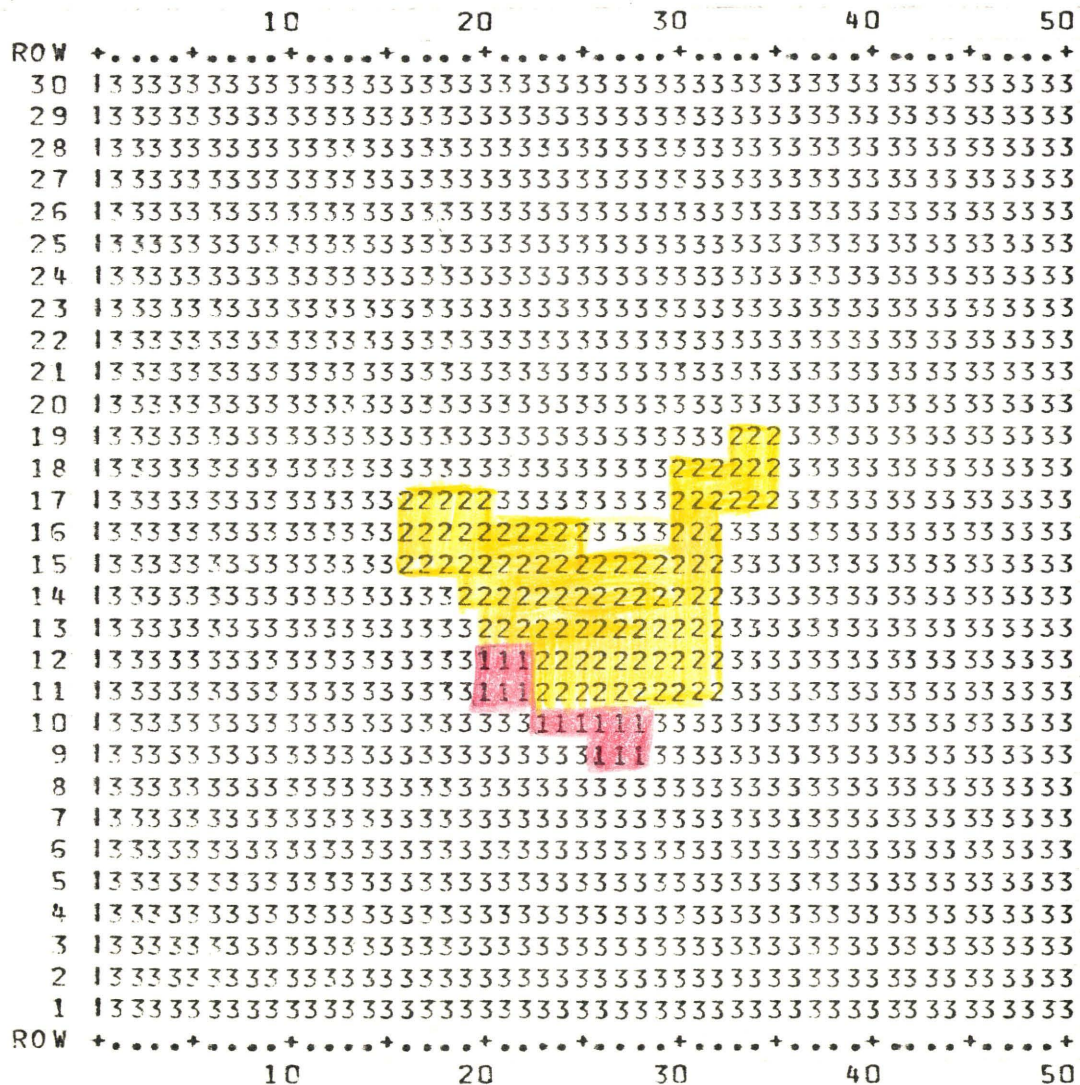
TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL. LEVEL 24 3200.0 TO 3225.0



TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL, LEVEL 25 3175.0 TO 3200.0



TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL. LEVEL 26 3150.0 TO 3175.0

	10	20	30	40	50
ROW	+.....+	+.....+	+.....+	+.....+	+.....+
30	1333333333	3333333333	3333333333	3333333333	3333333333
29	1333333333	3333333333	3333333333	3333333333	3333333333
28	1333333333	3333333333	3333333333	3333333333	3333333333
27	1333333333	3333333333	3333333333	3333333333	3333333333
26	1333333333	3333333333	3333333333	3333333333	3333333333
25	1333333333	3333333333	3333333333	3333333333	3333333333
24	1333333333	3333333333	3333333333	3333333333	3333333333
23	1333333333	3333333333	3333333333	3333333333	3333333333
22	1333333333	3333333333	3333333333	3333333333	3333333333
21	1333333333	3333333333	3333333333	3333333333	3333333333
20	1333333333	3333333333	3333333333	3333333333	3333333333
19	1333333333	3333333333	3333333333	3333333333	3333333333
18	1333333333	3333333333	3333333333	3333333333	3333333333
17	1333333333	3333333333	3333333333	3333333333	3333333333
16	1333333333	3333333333	3333333333	3333333333	3333333333
15	1333333333	3333333333	3333333333	3333333333	3333333333
14	1333333333	3333333333	3333333333	3333333333	3333333333
13	1333333333	3333333333	3333333333	3333333333	3333333333
12	1333333333	3333333333	3333333333	3333333333	3333333333
11	1333333333	3333333333	3333333333	3333333333	3333333333
10	1333333333	3333333333	3333333333	3333333333	3333333333
9	1333333333	3333333333	3333333333	3333333333	3333333333
8	1333333333	3333333333	3333333333	3333333333	3333333333
7	1333333333	3333333333	3333333333	3333333333	3333333333
6	1333333333	3333333333	3333333333	3333333333	3333333333
5	1333333333	3333333333	3333333333	3333333333	3333333333
4	1333333333	3333333333	3333333333	3333333333	3333333333
3	1333333333	3333333333	3333333333	3333333333	3333333333
2	1333333333	3333333333	3333333333	3333333333	3333333333
1	1333333333	3333333333	3333333333	3333333333	3333333333
ROW	+.....+	+.....+	+.....+	+.....+	+.....+

TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL, LEVEL 27 3125.0 TO 3150.0

	10	20	30	40	50
ROW	+.....+	+.....+	+.....+	+.....+	+.....+
30	133333	333333	333333	333333	333333
29	133333	333333	333333	333333	333333
28	133333	333333	333333	333333	333333
27	133333	333333	333333	333333	333333
26	133333	333333	333333	333333	333333
25	133333	333333	333333	333333	333333
24	133333	333333	333333	333333	333333
23	133333	333333	333333	333333	333333
22	133333	333333	333333	333333	333333
21	133333	333333	333333	333333	333333
20	133333	333333	333333	333333	333333
19	133333	333333	333333	333333	2223333333333333
18	133333	333333	333333	333333	22222233333333333333
17	133333	333333	222222	333333	22222233333333333333
16	133333	333333	222222	222222	33322233333333333333
15	133333	333333	222222	222222	22222233333333333333
14	133333	333333	222222	222222	22222233333333333333
13	133333	333333	222222	111222	22222233333333333333
12	133333	333333	333333	111222	22222233333333333333
11	133333	333333	333333	111111	22233333333333333333
10	133333	333333	333333	333333	11133333333333333333
9	133333	333333	333333	333333	33333333333333333333
8	133333	333333	333333	333333	33333333333333333333
7	133333	333333	333333	333333	33333333333333333333
6	133333	333333	333333	333333	33333333333333333333
5	133333	333333	333333	333333	33333333333333333333
4	133333	333333	333333	333333	33333333333333333333
3	133333	333333	333333	333333	33333333333333333333
2	133333	333333	333333	333333	33333333333333333333
1	133333	333333	333333	333333	33333333333333333333
ROW	+.....+	+.....+	+.....+	+.....+	+.....+

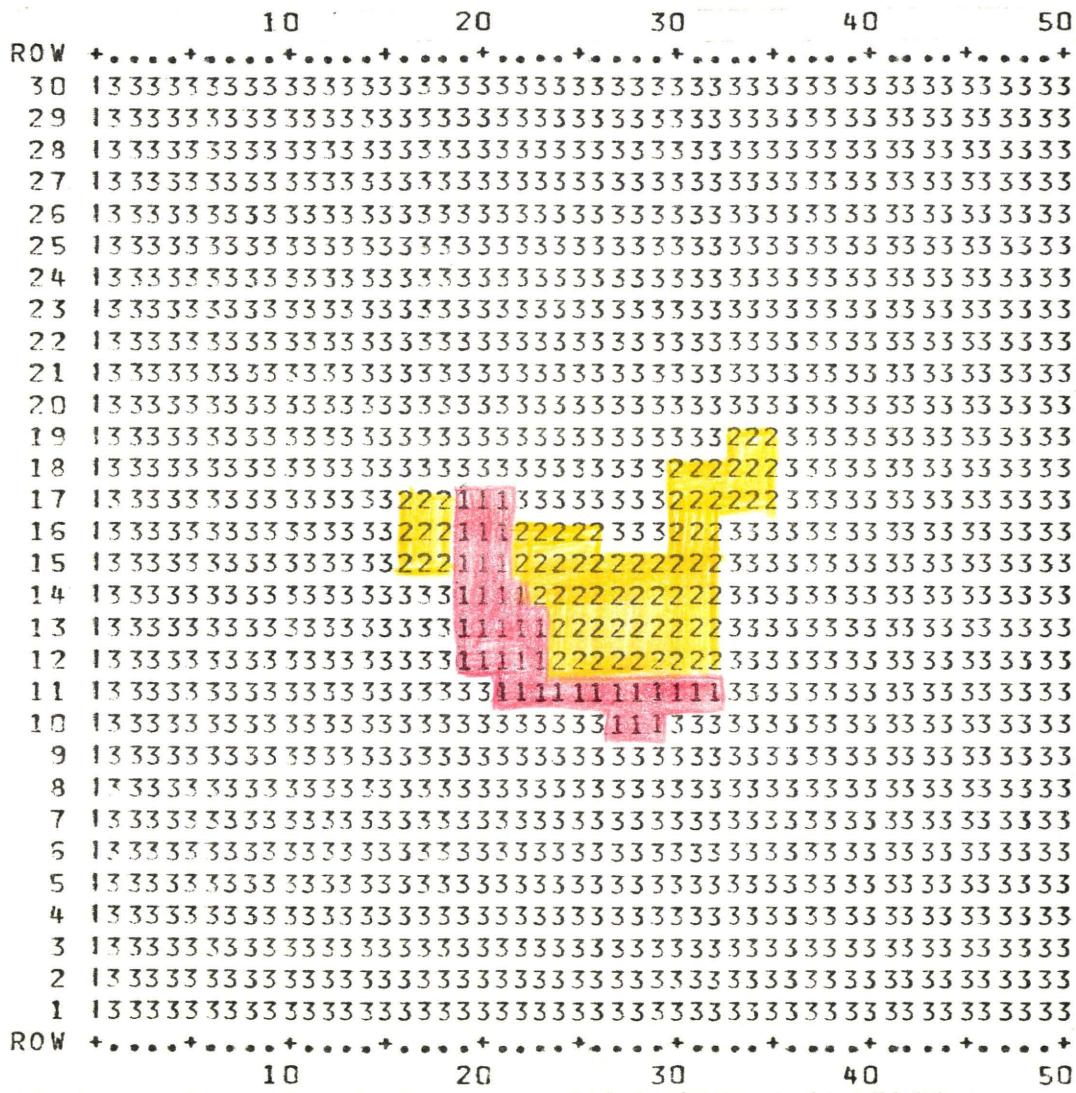
TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL, LEVEL 28 3100.0 TO 3125.0

	10	20	30	40	50
ROW	+.....+	+.....+	+.....+	+.....+	+.....+
30	133333	333333	333333	333333	333333
29	133333	333333	333333	333333	333333
28	133333	333333	333333	333333	333333
27	133333	333333	333333	333333	333333
26	133333	333333	333333	333333	333333
25	133333	333333	333333	333333	333333
24	133333	333333	333333	333333	333333
23	133333	333333	333333	333333	333333
22	133333	333333	333333	333333	333333
21	133333	333333	333333	333333	333333
20	133333	333333	333333	333333	333333
19	133333	333333	333333	333333	333333
18	133333	333333	333333	333333	333333
17	133333	333333	333333	333333	333333
16	133333	333333	333333	333333	333333
15	133333	333333	333333	333333	333333
14	133333	333333	333333	333333	333333
13	133333	333333	333333	333333	333333
12	133333	333333	333333	333333	333333
11	133333	333333	333333	333333	333333
10	133333	333333	333333	333333	333333
9	133333	333333	333333	333333	333333
8	133333	333333	333333	333333	333333
7	133333	333333	333333	333333	333333
6	133333	333333	333333	333333	333333
5	133333	333333	333333	333333	333333
4	133333	333333	333333	333333	333333
3	133333	333333	333333	333333	333333
2	133333	333333	333333	333333	333333
1	133333	333333	333333	333333	333333
ROW	+.....+	+.....+	+.....+	+.....+	+.....+

TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL, LEVEL 29 3075.0 TO 3100.0



TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL, LEVEL 38 2850.0 TO 2875.0

	10	20	30	40	50
ROW	+	+	+	+	+
30	1	3	3	3	3
29	1	3	3	3	3
28	1	3	3	3	3
27	1	3	3	3	3
26	1	3	3	3	3
25	1	3	3	3	3
24	1	3	3	3	3
23	1	3	3	3	3
22	1	3	3	3	3
21	1	3	3	3	3
20	1	3	3	3	3
19	1	3	3	3	3
18	1	3	3	3	3
17	1	3	3	3	3
16	1	3	3	3	3
15	1	3	3	3	3
14	1	3	3	3	3
13	1	3	3	3	3
12	1	3	3	3	3
11	1	3	3	3	3
10	1	3	3	3	3
9	1	3	3	3	3
8	1	3	3	3	3
7	1	3	3	3	3
6	1	3	3	3	3
5	1	3	3	3	3
4	1	3	3	3	3
3	1	3	3	3	3
2	1	3	3	3	3
1	1	3	3	3	3
ROW	+	+	+	+	+

TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL, LEVEL 39 2825.0 TO 2850.0

	10	20	30	40	50
ROW	+	+	+	+	+
30	1	3	3	3	3
29	1	3	3	3	3
28	1	3	3	3	3
27	1	3	3	3	3
26	1	3	3	3	3
25	1	3	3	3	3
24	1	3	3	3	3
23	1	3	3	3	3
22	1	3	3	3	3
21	1	3	3	3	3
20	1	3	3	3	3
19	1	3	3	3	3
18	1	3	3	3	3
17	1	3	3	3	3
16	1	3	3	3	3
15	1	3	3	3	3
14	1	3	3	3	3
13	1	3	3	3	3
12	1	3	3	3	3
11	1	3	3	3	3
10	1	3	3	3	3
9	1	3	3	3	3
8	1	3	3	3	3
7	1	3	3	3	3
6	1	3	3	3	3
5	1	3	3	3	3
4	1	3	3	3	3
3	1	3	3	3	3
2	1	3	3	3	3
1	1	3	3	3	3
ROW	+	+	+	+	+

TEST RUN AUGUST 19, 1971, GEOLOGIC ZONE
 SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF GEOL, LEVEL 40 2800.0 TO 2825.0

	10	20	30	40	50
ROW	+ . . . + . . . + . . . + . . . + . . . + . . . + . . . + . . . + . . . + . . . + . . . + . . . + . . . + . . . +				
30	133333	333333	333333	333333	333333
29	133333	333333	333333	333333	333333
28	133333	333333	333333	333333	333333
27	133333	333333	333333	333333	333333
26	133333	333333	333333	333333	333333
25	133333	333333	333333	333333	333333
24	133333	333333	333333	333333	333333
23	133333	333333	333333	333333	333333
22	133333	333333	333333	333333	333333
21	133333	333333	333333	333333	333333
20	133333	333333	333333	333333	333333
19	133333	333333	333333	333333	333333
18	133333	333333	333333	111	333333
17	133333	111	333333	111	333333
16	133333	111	333333	111	333333
15	133333	111	333333	333333	333333
14	133333	333333	111	333333	333333
13	133333	333333	111	333333	333333
12	133333	333333	111	333333	333333
11	133333	333333	333333	333333	333333
10	133333	333333	333333	333333	333333
9	133333	333333	333333	333333	333333
8	133333	333333	333333	333333	333333
7	133333	333333	333333	333333	333333
6	133333	333333	333333	333333	333333
5	133333	333333	333333	333333	333333
4	133333	333333	333333	333333	333333
3	133333	333333	333333	333333	333333
2	133333	333333	333333	333333	333333
1	133333	333333	333333	333333	333333
ROW	+ . . . + . . . + . . . + . . . + . . . + . . . + . . . + . . . + . . . + . . . + . . . + . . . +				
	10	20	30	40	50

MINTEC, INC.

KELLY FAULT UPDATE

Not all matrix blocks could be assigned a copper grade because the drillhole data was sparse in some areas. Wherever the Kelly Fault was interpreted to be present (from Mieritz's report) but no grade was assigned, a grade of 1.0% copper was assumed. The following printout shows the blocks that were assumed to be 1.0%.

MTX ITEM =	1	*CU*	1	0	FFFF0000	65536
MTX ITEM =	2	TOPO	1	0	0000FF00	256
MTX ITEM =	3	PIT	1	0	000000FF	1
MTX ITEM =	4	GEOL	2	50	FF000000	16777216
MTX ITEM =	5	ORE	2	50	00FF0000	65536
MTX ITEM =	6	OWNR	2	50	0000FF00	256
MTX ITEM =	7	SECT	2	50	000000FF	1

*LEVEL 1

	Row	Col	CU	
IY, IX =	4	18	1000	300
IY, IX =	4	19	1000	300
IY, IX =	4	20	1000	300
IY, IX =	4	21	1000	300
IY, IX =	4	22	1000	300

*LEVEL 2

IY, IX =	4	18	1000	300
IY, IX =	4	19	1000	300
IY, IX =	4	20	1000	300
IY, IX =	4	21	1000	300
IY, IX =	4	22	1000	300

*LEVEL 3

*LEVEL 4

*LEVEL 5

IY, IX =	5	18	1000	400
IY, IX =	5	19	1000	400
IY, IX =	5	20	1000	400
IY, IX =	5	21	1000	400
IY, IX =	5	22	1000	400

*LEVEL 6

IY, IX =	5	18	1000	400
IY, IX =	5	19	1000	400
IY, IX =	5	20	1000	400
IY, IX =	5	21	1000	400
IY, IX =	5	22	1000	400

*LEVEL 7

IY, IX =	5	24	1000	400
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IY, IX =	5	27	1000	400
IY, IX =	5	28	1000	400
IY, IX =	6	18	1000	500
IY, IX =	6	19	1000	500
IY, IX =	6	20	1000	500
IY, IX =	6	21	1000	500
IY, IX =	6	22	1000	500
IY, IX =	6	23	1000	500

*LEVEL 8

IY, IX =	5	28	1000	400
IY, IX =	6	18	1000	500
IY, IX =	6	19	1000	500

*LEVEL 9

IY, IX =	5	30	1000	400
IY, IX =	6	20	1000	500
IY, IX =	6	21	1000	500
IY, IX =	6	31	1000	500
IY, IX =	6	32	1000	500

*LEVEL 10

IY, IX =	5	30	1000	400
IY, IX =	6	31	1000	500
IY, IX =	6	32	1000	500

*LEVEL 11

IY, IX =	6	26	1000	500
IY, IX =	6	27	1000	500
IY, IX =	6	28	1000	500
IY, IX =	7	20	1000	600
IY, IX =	7	21	1000	600
IY, IX =	7	22	1000	600
IY, IX =	7	23	1000	600
IY, IX =	7	24	1000	600
IY, IX =	7	25	1000	600

*LEVEL 12

IY, IX =	6	26	1000	500
IY, IX =	6	27	1000	500
IY, IX =	6	28	1000	500
IY, IX =	7	20	1000	600
IY, IX =	7	21	1000	600
IY, IX =	7	22	1000	600
IY, IX =	7	23	1000	600
IY, IX =	7	24	1000	600
IY, IX =	7	25	1000	600

*LEVEL 13

IY, IX =	6	27	1000	500
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IY.	=	6	29	1000	500
IY.	=	7	24	1000	600
IY.	=	7	25	1000	600
IY.	IY =	7	26	1000	500
IY.	IY =	7	27	1000	600
IY.	TX =	7	28	1000	500
IY.	IX =	7	29	1000	600
IY.	TX =	8	20	1000	700
IY.	TX =	8	21	1000	700
IY.	TX =	8	22	1000	700
IY.	IX =	8	23	1000	700

*LEVEL 14

IY.	TX =	6	27	1000	500
IY.	TX =	6	28	1000	500
IY.	IX =	6	29	1000	500
IY.	IX =	7	24	1000	600
IY.	TX =	7	25	1000	600
IY.	IX =	7	26	1000	600
IY.	IX =	7	27	1000	600
IY.	IX =	7	28	1000	600
IY.	IX =	7	29	1000	600
IY.	IX =	8	20	1000	700
IY.	IX =	8	21	1000	700
IY.	IX =	8	22	1000	700
IY.	IX =	8	23	1000	700

*LEVEL 15

IY.	IX =	7	25	1000	500
IY.	IX =	7	27	1000	600
IY.	IX =	7	28	1000	600
IY.	IX =	7	29	1000	600
IY.	TX =	8	23	1000	700
IY.	IX =	8	24	1000	700
IY.	TX =	8	25	1000	700
IY.	IX =	8	20	1000	800
IY.	IX =	8	21	1000	800
IY.	IX =	8	22	1000	800

EXIT

MING10 VERSION 1 COMPILED AUG. 18. 71

MTX ITEM =	1	*CU*	1	0	FFFF0000	65536
MTX ITEM =	2	TOP0	1	0	0000FF00	256
MTX ITEM =	3	PIT	1	0	000000FF	1
MTX ITEM =	4	GEOL	2	50	FF000000	16777216
MTX ITEM =	5	ORC	2	50	00FF0000	65536
MTX ITEM =	6	OWNER	2	50	0000FF00	256
MTX ITEM =	7	SECT	2	50	000000FF	1

*LEVEL 16

IY, IX =	7	26	1000	600
IY, IX =	7	27	1000	600
IY, IX =	7	28	1000	600
IY, IX =	7	29	1000	600
IY, IX =	8	23	1000	700
IY, IX =	8	24	1000	700
IY, IX =	8	25	1000	700
IY, IX =	9	20	1000	800
IY, IX =	9	21	1000	800
IY, IX =	9	22	1000	800

*LEVEL 17

IY, IX =	7	27	1000	600
IY, IX =	7	28	1000	600
IY, IX =	7	29	1000	600
IY, IX =	8	27	1000	700
IY, IX =	8	28	1000	700
IY, IX =	8	29	1000	700
IY, IX =	9	20	1000	800
IY, IX =	9	21	1000	800
IY, IX =	9	22	1000	800
IY, IX =	9	23	1000	800
IY, IX =	9	24	1000	800
IY, IX =	9	25	1000	800
IY, IX =	9	26	1000	800

*LEVEL 18

IY, IX =	7	27	1000	600
IY, IX =	7	28	1000	600
IY, IX =	7	29	1000	600
IY, IX =	8	27	1000	700
IY, IX =	8	28	1000	700
IY, IX =	8	29	1000	700
IY, IX =	9	20	1000	800
IY, IX =	9	21	1000	800
IY, IX =	9	22	1000	800
IY, IX =	9	23	1000	800
IY, IX =	9	24	1000	800
IY, IX =	9	25	1000	800
IY, IX =	9	26	1000	800

IY, IX =	9	22	1000	800
IY, IX =	9	23	1000	800
IY, IX =	9	24	1000	800
IY, IX =	9	25	1000	800
IY, IX =	9	26	1000	800

*LEVEL 19

IY, IX =	8	27	1000	700
IY, IX =	8	28	1000	700
IY, IX =	9	29	1000	700
IY, IX =	9	20	1000	800
IY, IX =	9	21	1000	800
IY, IX =	9	22	1000	800
IY, IX =	9	23	1000	800
IY, IX =	9	24	1000	800
IY, IX =	9	25	1000	800
IY, IX =	9	26	1000	800
IY, IX =	9	27	1000	800
IY, IX =	9	28	1000	800
IY, IX =	9	29	1000	800
IY, IX =	10	21	1000	900
IY, IX =	10	22	1000	900

*LEVEL 20

IY, IX =	8	27	1000	700
IY, IX =	8	28	1000	700
IY, IX =	8	29	1000	700
IY, IX =	9	20	1000	800
IY, IX =	9	21	1000	800
IY, IX =	9	22	1000	800
IY, IX =	9	23	1000	800
IY, IX =	9	24	1000	800
IY, IX =	9	25	1000	800
IY, IX =	9	26	1000	800
IY, IX =	9	27	1000	800
IY, IX =	9	28	1000	800
IY, IX =	9	29	1000	800
IY, IX =	10	20	1000	900
IY, IX =	10	21	1000	900
IY, IX =	10	22	1000	900

*LEVEL 21

IY, IX =	9	26	1000	800
IY, IX =	9	27	1000	800
IY, IX =	9	28	1000	800
IY, IX =	10	20	1000	900
IY, IX =	10	21	1000	900
IY, IX =	10	22	1000	900
IY, IX =	10	23	1000	900

IY, TX =	9	26	1000	800
IY, TX =	9	27	1000	900
IY, IX =	9	28	1000	800
IY, IX =	10	20	1000	900
IY, IX =	10	21	1000	900
IY, IX =	10	22	1000	900
IY, IX =	10	23	1000	900
IY, IX =	10	24	1000	900
IY, IX =	10	25	1000	900

*LEVEL 23

IY, IX =	9	27	1000	800
IY, IX =	9	28	1000	800
IY, IX =	10	20	1000	900
IY, IX =	10	21	1000	900
IY, IX =	10	22	1000	900
IY, IX =	10	23	1000	900
IY, IX =	10	24	1000	900
IY, IX =	10	25	1000	900
IY, IX =	10	26	1000	900
IY, IX =	11	20	1000	1000
IY, IX =	11	21	1000	1000
IY, IX =	11	22	1000	1000

*LEVEL 24

IY, IX =	9	27	1000	800
IY, IX =	9	28	1000	800
IY, IX =	10	20	1000	900
IY, IX =	10	21	1000	900
IY, IX =	10	22	1000	900
IY, IX =	10	23	1000	900
IY, IX =	10	24	1000	900
IY, IX =	10	25	1000	900
IY, IX =	10	26	1000	900
IY, IX =	11	20	1000	1000
IY, IX =	11	21	1000	1000
IY, IX =	11	22	1000	1000

*LEVEL 25

IY, IX =	9	26	1000	800
IY, IX =	9	27	1000	800
IY, IX =	9	28	1000	800
IY, IX =	10	25	1000	900
IY, IX =	10	26	1000	900
IY, IX =	10	27	1000	900
IY, IX =	10	28	1000	900

*LEVEL 26

IY, IX =	9	26	1000	800
IY, IX =	9	27	1000	800

IY, IX =	10	25	1000	900
IY, IX =	10	26	1000	900
IY, IX =	10	27	1000	900
IY, IX =	10	28	1000	900

*LEVEL 27

IY, IX =	10	27	1000	900
IY, IX =	10	28	1000	900
IY, IX =	10	29	1000	900
IY, IX =	11	25	1000	1000
IY, IX =	11	26	1000	1000

*LEVEL 28

IY, IX =	10	27	1000	900
IY, IX =	10	28	1000	900
IY, IX =	10	29	1000	900
IY, IX =	11	25	1000	1000
IY, IX =	11	26	1000	1000

*LEVEL 29

IY, IX =	10	27	1000	900
IY, IX =	10	28	1000	900
IY, IX =	10	29	1000	900
IY, IX =	11	25	1000	1000
IY, IX =	11	26	1000	1000
IY, IX =	11	27	1000	1000
IY, IX =	11	28	1000	1000
IY, IX =	11	29	1000	1000
IY, IX =	11	30	1000	1000
IY, IX =	11	31	1000	1000
IY, IX =	11	32	1000	1000

*LEVEL 30

IY, IX =	10	27	1000	900
IY, IX =	10	28	1000	900
IY, IX =	10	29	1000	900
IY, IX =	11	25	1000	1000
IY, IX =	11	26	1000	1000
IY, IX =	11	27	1000	1000
IY, IX =	11	28	1000	1000
IY, IX =	11	29	1000	1000
IY, IX =	11	30	1000	1000
IY, IX =	11	31	1000	1000
IY, IX =	11	32	1000	1000

EXIT

MTX ITEM =	1	*CU*	1	0	FFFF0000	65536
MTX ITEM =	2	TOPO	1	0	0000FF00	256
MTX ITEM =	3	PIT	1	0	000000FF	1
MTX ITEM =	4	GEOL	2	50	FF000000	16777216
MTX ITEM =	5	ORE	2	50	00FF0000	65536
MTX ITEM =	6	OWNR	2	50	0000FF00	256
MTX ITEM =	7	SECT	2	50	000000FF	1

*LEVEL 31

IY, IX =	11	27	1000	1000
IY, IX =	11	28	1000	1000
IY, IX =	11	29	1000	1000
IY, IX =	11	30	1000	1000
IY, IX =	11	31	1000	1000
IY, IX =	11	32	1000	1000
IY, IX =	12	25	1000	1100
IY, IX =	12	26	1000	1100
IY, IX =	12	30	1000	1100
IY, IX =	12	31	1000	1100
IY, IX =	12	32	1000	1100
IY, IX =	13	30	1000	1200
IY, IX =	13	31	1000	1200
IY, IX =	13	32	1000	1200
IY, IX =	14	30	1000	1300
IY, IX =	14	31	1000	1300
IY, IX =	14	32	1000	1300

*LEVEL 32

IY, IX =	11	27	1000	1000
IY, IX =	12	25	1000	1100
IY, IX =	12	26	1000	1100

*LEVEL 33

*LEVEL 34

*LEVEL 35

*LEVEL 36

*LEVEL 37

*LEVEL 38

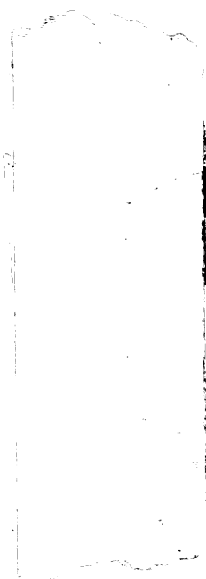
*LEVL 30

*LEVEL 40

IV. IX =	16	32	1000	1500
IV. IX =	17	32	1000	1600
IV. IX =	18	30	1000	1700
IV. IX =	18	31	1000	1700
IV. IX =	18	32	1000	1700

EXIT

TOPOGRAPHY
(Map in Folder)



TOPOGRAPHY

THE FOLLOWING MAPS SHOW THE PERCENTAGE OF THE BLOCKS ON EACH BENCH THAT ARE BELOW THE SURFACE TOPOGRAPHY. AN "*" INDICATES THAT THE BLOCK IS ENTIRELY BELOW THE SURFACE, A "0" INDICATES THAT THE BLOCK IS FROM 0 TO 10% BELOW THE SURFACE, A "1" INDICATES THAT THE BLOCK IS FROM 10 TO 20% BELOW THE SURFACE, ETC. A BLANK INDICATES THAT THE BLOCK IS ENTIRELY IN THIN AIR.

** RUN AUGUST 19, 1971 **
SANTA RITA MINING COMPANY

CARLOTTA MINE PROJECT

SYMBOL PLOT OF TOPO, LEVEL 5 3675.0 TO 3700.0

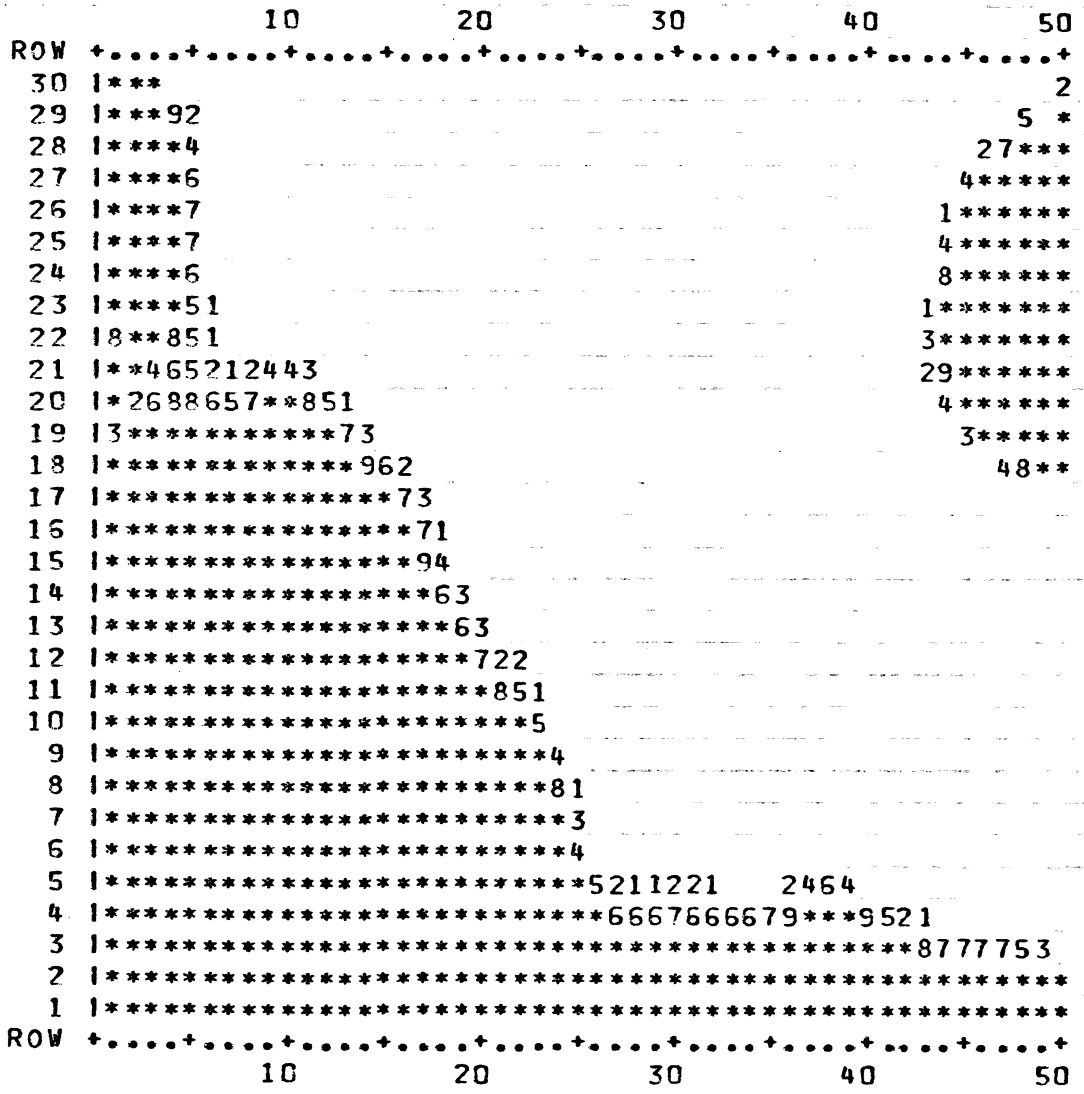
```

      10      20      30      40      50
ROW +.....+.....+.....+.....+.....+.....+.....+
30 |**7
29 |***
28 |***3
27 |***5
26 |***6
25 |***6
24 |***4
23 |9*91
22 | 2
21 |*
20 |
19 | 1233234553
18 |5789*****62
17 |*****751
16 |*****84
15 |*****852
14 |*****742
13 |*****6342
12 |*****78541
11 |*****62
10 |*****73
 9 |*****861
 8 |*****85
 7 |*****6
 6 |*****4
 5 |*****8
 4 |*****6
 3 |*****621 232 12357**963
 2 |*****742358*****75455432
 1 |*****8459*****9
ROW +.....+.....+.....+.....+.....+.....+
      10      20      30      40      50
```

** RUN AUGUST 19, 1971 **
SANTA RITA MINING COMPANY

CARLOTTA MINE PROJECT

SYMBOL PLOT OF TOPO, LEVEL 6 3650.0 TO 3675.0



** RUN AUGUST 19, 1971 **
SANTA RITA MINING COMPANY

CARLOTTA MINE PROJECT

SYMBOL PLOT OF TOPO, LEVEL 7 3625.0 TO 3650.0

ROW	10	20	30	40	50
30	1***1				642*
29	1*****3				16**9*
28	1*****6				16*****
27	1*****82				7*****
26	1*****93				3*****
25	1*****94				5*****
24	1*****62				8*****
23	1*****8642				2*****
22	1*****898641				4*****
21	1*****962				5*****
20	1*****7431				18*****
19	1*****852				6*****
18	1*****952				38*****
17	1*****842				2677
16	1*****63				
15	1*****952				
14	1*****963				
13	1*****984				
12	1*****82				
11	1*****6				
10	1*****4				
9	1*****83				
8	1*****741				
7	1*****864322				
6	1*****8776664445641				
5	1*****7432121				
4	1*****9742				
3	1*****				
2	1*****				
1	1*****				
ROW	10	20	30	40	50

** RUN AUGUST 19, 1971 **
SANTA RITA MINING COMPANY

CARLOTTA MINE PROJECT

SYMBOL PLOT OF TOPO, LEVEL 8 3600.0 TO 3625.0

ROW	10	20	30	40	50
30	*****3				6****
29	*****6				26*****
28	*****94				6*****
27	*****62				2*****
26	*****84				5*****
25	*****63				8*****
24	*****6432				3*****
23	*****86432				5*****
22	*****86543234431				6*****
21	*****8864589742				5*****
20	*****9789*8421				*****
19	*****9862				1*****
18	*****852				6*****
17	*****841				38****
16	*****62				2113
15	*****94				
14	*****82				
13	*****72				
12	*****61				
11	*****62				
10	*****642				
9	*****76432				
8	*****9876421				
7	*****98777642				
6	*****86533221				
5	*****74				
4	*****				
3	*****				
2	*****				
1	*****				

** RUN AUGUST 19, 1971 **
SANTA RITA MINING COMPANY

CARLOTTA MINE PROJECT

SYMBOL PLOT OF TOPO, LEVEL 9 3575.0 TO 3600.0

ROW	10	20	30	40	50
30	*****9				54 *****
29	*****62				5*****
28	*****52				9*****
27	*****8431				5*****
26	*****86431				18*****
25	*****986544332221				4*****
24	*****9877666542				6*****
23	*****9864				7*****
22	*****962				7*****
21	*****6				5*****
20	*****6				*****
19	*****72				2*****
18	*****62				9*****
17	*****851				6*****
16	*****952				8*****
15	*****63				
14	*****85				
13	*****73				
12	*****75442112				
11	*****8764431				
10	*****98642				
9	*****75421				
8	*****97642				1
7	*****865422345				
6	*****9				
5	*****				
4	*****				
3	*****				
2	*****				
1	*****				

** RUN AUGUST 19, 1971 **
SANTA RITA MINING COMPANY

CARLOTTA MINE PROJECT

SYMBOL PLOT OF TOPO, LEVEL 10 3550.0 TO 3575.0

ROW	10	20	30	40	50
3074
299432216
28864322233221
279876556655427
269999886415
2596318
24523
23622
2251
21828
2074
1954
18833
17732
16843
1595234889*
147543
1386574
123
1161
1074
98532115
88764468*
7
6
5
4
3
2
1
ROW1020304050

** RUN AUGUST 19, 1971 **
SANTA RITA MINING COMPANY

CARLOTTA MINE PROJECT

SYMBOL PLOT OF TOPO, LEVEL 11 3525.0 TO 3550.0

	10	20	30	40	50
ROW	+.....+	+.....+	+.....+	+.....+	+.....+
30	*****2784432	1*32			*****
29	*****857*89**86542			6*****	
28	*****8531			4*****	
27	*****9642			2*****	
26	*****852			7*****	
25	*****73			2*****	
24	*****941			4*****	
23	*****62			4*****	
22	*****72			4*****	
21	*****8			4*****	
20	*****71			8*****	
19	*****72			28*****	
18	*****72			6*****	
17	*****83			6*****	
16	*****952			5*****	
15	*****9642			49*****	
14	*****984			24677	
13	*****6				
12	*****6				
11	*****731				
10	*****86542222347				
9	*****98888**				
8	*****				
7	*****				
6	*****				
5	*****				
4	*****				
3	*****				
2	*****				
1	*****				
ROW	+.....+	+.....+	+.....+	+.....+	+.....+

** RUN AUGUST 19, 1971 **
SANTA RITA MINING COMPANY

CARLOTTA MINE PROJECT

SYMBOL PLOT OF TOPO. LEVEL 12 3500.0 TO 3525.0

	10	20	30	40	50
ROW	+	+	+	+	+
30	*****	23161****	29*2 5	4994*****	*****
29	*****	*****	9*72	169*****	*****
28	*****	*****	962	148*****	*****
27	*****	*****	952	37*****	*****
26	*****	*****	952	3*****	*****
25	*****	*****	72	3*****	*****
24	*****	*****	83	4*****	*****
23	*****	*****	74	16*****	*****
22	*****	*****	741	26*****	*****
21	*****	*****	741	6*****	*****
20	*****	*****	741	3*****	*****
19	*****	*****	842	26*****	*****
18	*****	*****	85311125	*****	*****
17	*****	*****	7422	25*****	*****
16	*****	*****	8531	248*****	*****
15	*****	*****	641	36*****	*****
14	*****	*****	9521	27*****	*****
13	*****	*****	96421224545898	*****	*****
12	*****	*****	864444323564	*****	*****
11	*****	*****	9877666788	*****	*****
10	*****	*****	*****	*****	*****
9	*****	*****	*****	*****	*****
8	*****	*****	*****	*****	*****
7	*****	*****	*****	*****	*****
6	*****	*****	*****	*****	*****
5	*****	*****	*****	*****	*****
4	*****	*****	*****	*****	*****
3	*****	*****	*****	*****	*****
2	*****	*****	*****	*****	*****
1	*****	*****	*****	*****	*****
ROW	+	+	+	+	+

** RUN AUGUST 19, 1971 **
SANTA RITA MINING COMPANY

CARLOTTA MINE PROJECT

SYMBOL PLOT OF TOPO, LEVEL 13 3475.0 TO 3500.0

ROW	10	20	30	40	50
30	+	+	+	+	+
29				334	
28				9998	
27				99	
26				879	
25				868	
24				978	
23				99	
22					
21				99	
20				99	
19					
18					
17					
16					
15					
14					
13					
12					
11					
10					
9					
8					
7					
6					
5					
4					
3					
2					
1					
ROW	+	+	+	+	+

** RUN AUGUST 19, 1971 **
SANTA RITA MINING COMPANY

CARLOTTA MINE PROJECT

SYMBOL PLOT OF TOPO, LEVEL 14 3450.0 TO 3475.0

ROW	10	20	30	40	50
30	+	+	+	+	+
29	+	+	+	+	+
28	+	+	+	+	+
27	+	+	+	+	+
26	+	+	+	+	+
25	+	+	+	+	+
24	+	+	+	+	+
23	+	+	+	+	+
22	+	+	+	+	+
21	+	+	+	+	+
20	+	+	+	+	+
19	+	+	+	+	+
18	+	+	+	+	+
17	+	+	+	+	+
16	+	+	+	+	+
15	+	+	+	+	+
14	+	+	+	+	+
13	+	+	+	+	+
12	+	+	+	+	+
11	+	+	+	+	+
10	+	+	+	+	+
9	+	+	+	+	+
8	+	+	+	+	+
7	+	+	+	+	+
6	+	+	+	+	+
5	+	+	+	+	+
4	+	+	+	+	+
3	+	+	+	+	+
2	+	+	+	+	+
1	+	+	+	+	+
ROW	+	+	+	+	+

** RUN AUGUST 19, 1971 **
SANTA RITA MINING COMPANY

CARLOTTA MINE PROJECT

SYMBOL PLOT OF TOPO, LEVEL 15 3425.0 TO 3450.0

ROW	10	20	30	40	50
30	+	+	+	+	+
29					
28					
27					
26					
25					
24					
23					
22					
21					
20					
19					
18					
17					
16					
15					
14					
13					
12					
11					
10					
9					
8					
7					
6					
5					
4					
3					
2					
1					
ROW	+	+	+	+	+

** RUN AUGUST 19, 1971 **
SANTA RITA MINING COMPANY

CARLOTTA MINE PROJECT

SYMBOL PLOT OF TOPO, LEVEL 16 3400.0 TO 3425.0

ROW	10	20	30	40	50
30	+	+	+	+	+
29					
28					
27					
26					
25					
24					
23					
22					
21					
20					
19					
18					
17					
16					
15					
14					
13					
12					
11					
10					
9					
8					
7					
6					
5					
4					
3					
2					
1					
ROW	+	+	+	+	+

** RUN AUGUST 19, 1971 **
SANTA RITA MINING COMPANY

CARLOTTA MINE PROJECT

SYMBOL PLOT OF TOPO, LEVEL 17 3375.0 TO 3400.0

ROW	10	20	30	40	50
30	+	+	+	+	+
29					
28					
27					
26					
25					
24					
23					
22					
21					
20					
19					
18					
17					
16					
15					
14					
13					
12					
11					
10					
9					
8					
7					
6					
5					
4					
3					
2					
1					
ROW	+	+	+	+	+

** RUN AUGUST 19, 1971 **
SANTA RITA MINING COMPANY

CARLOTTA MINE PROJECT

SYMBOL PLOT OF TOPO, LEVEL 18 3350.0 TO 3375.0

ROW	10	20	30	40	50
30	+	+	+	+	+
29					
28					
27					
26					
25					
24					
23					
22					
21					
20					
19					
18					
17					
16					
15					
14					
13					
12					
11					
10					
9					
8					
7					
6					
5					
4					
3					
2					
1					
ROW	+	+	+	+	+

MINTEC, INC.

PROPERTY TYPES

THE FOLLOWING MAPS SHOW THE PROPERTY TYPES FOR THE CARLOTTA:

1 = MATERIAL INSIDE PROPERTY LINES

2 = MATERIAL OUTSIDE PROPERTY LINES

THESE TYPES WERE ASSIGNED ON A FULL BLOCK BASIS WHEREIN THE
BLOCK WAS EITHER ENTIRELY INSIDE OR ENTIRELY OUTSIDE THE
PROPERTY LINES.

MINE LIMITS *

CARLOTTA MINE PROJECT

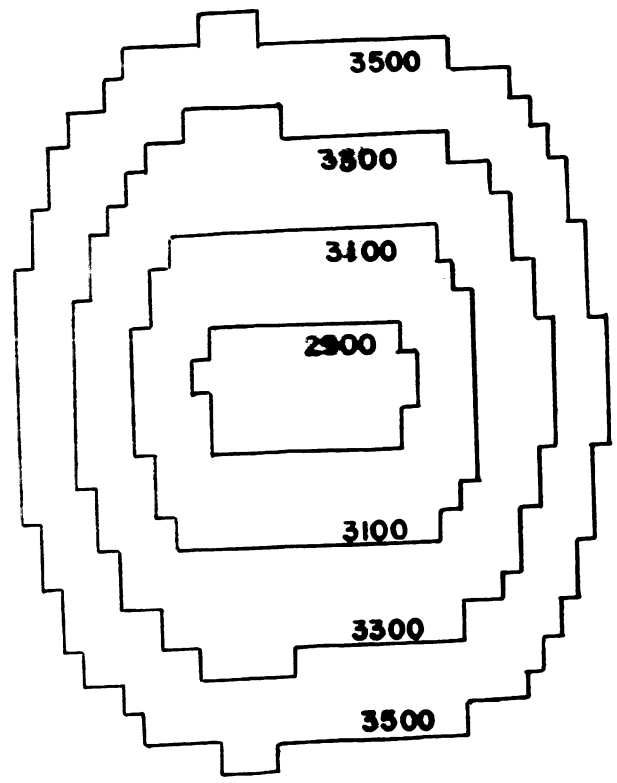
10
+

20
+

30
+

40
+

50
+



* **BLOCKS WITHIN MINE LIMITS
ARE WHOLLY OR PARTIALLY
MINED.**

PIT SLOPE = 50°

TEST RUN AUGUST 19, 1971. PROPERTY TYPES
SANTA RITA MINING COMPANY CARLOTTA MINE PROJECT

SYMBOL PLOT OF OWNER, LEVEL 1 3775.0 TO 3800.0

	10	20	30	40	50
ROW	+	+	+	+	+
75	1	2	2	2	2
29	1	2	2	2	2
28	1	2	2	2	2
27	1	2	2	2	2
26	1	2	2	2	2
25	1	2	2	2	2
24	1	2	2	2	2
23	1	2	2	2	2
22	1	2	2	2	2
21	1	2	2	2	2
20	1	2	2	2	2
19	1	2	2	2	2
18	1	2	2	2	2
17	1	2	2	2	2
16	1	2	2	2	2
15	1	2	2	2	2
14	1	2	2	2	2
13	1	2	2	2	2
12	1	2	2	2	2
11	1	2	2	2	2
10	1	2	2	2	2
9	1	2	2	2	2
8	1	2	2	2	2
7	1	2	2	2	2
6	1	2	2	2	2
5	1	2	2	2	2
4	1	2	2	2	2
3	1	2	2	2	2
2	1	2	2	2	2
1	1	2	2	2	2
ROW	+	+	+	+	+
	10	20	30	40	50

PROPERTY TYPES

DISPLAY OF MINE BLOCK MODEL DATA.

CU X.XXX.
 GEOL XXXX.

LEVEL 13 FROM 3475.0 TO 3500.0

	-650.	-550.	-450.	-350.	-250.	-150.	-50.	50.	150.	250.											
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
800.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	800.
20	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	20
750.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	750.
19	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	19
700.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	700.
18	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	18
650.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	650.
17	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	17
600.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	600.
16	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	16
550.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	550.
15	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	15
500.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	500.
14	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	14
450.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	450.
13	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	13
400.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	400.
12	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	12
350.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	350.
11	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	11
300.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	300.
10	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	10
250.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	250.
9	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	9
200.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	200.
8	3	3	3	3	1	1	1	1	3	3	3	3	3	3	3	3	3	3	3	3	8
150.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	150.
7	3	3	3	3	3	3	3	3	1	1	1	1	1	1	3	3	3	3	3	3	7
100.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	100.
6	3	3	3	3	3	3	3	3	3	3	3	1	1	1	3	3	3	3	3	3	6
50.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	50.
5	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	5
0.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0.
4	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4
-50.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-50.
3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
-100.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-100.
2	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2
-150.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-150.
1	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	1
-200.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-200.
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
	-650.		-550.		-450.		-350.		-250.		-150.		-50.		50.		150.		250.		

DISPLAY OF MINE BLOCK MODEL DATA.

CU X.XXX
 GEOL XXXX.

LEVEL 14 FROM 3450.0 TO 3475.0

	-650.		-550.		-450.		-350.		-250.		-150.		-50.		50.	150.	250.				
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
800.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	800.
20	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	20
750.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	750.
19	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	19
700.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	700.
18	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	18
650.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	650.
17	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	17
600.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	600.
16	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	16
550.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	550.
15	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	15
500.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	500.
14	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	14
450.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	450.
13	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	13
400.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	400.
12	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	12
350.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	350.
11	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	11
300.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	300.
10	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	10
250.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	250.
9	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	9
200.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	200.
8	3	3	3	3	1000	1000	1000	1000	3	3	3	3	3	3	3	3	3	3	3	3	8
150.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	150.
7	3	3	3	3	3	3	3	3	1000	1000	1000	1000	1000	1000	3	3	3	3	3	3	7
100.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	100.
6	3	3	3	3	3	3	3	3	3	3	3	1000	1000	1000	3	3	3	3	3	3	6
50.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	50.
5	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	5
0.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0.
4	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4
-50.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-50.
3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
-100.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-100.
2	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2
-150.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-150.
1	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	1
-200.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-200.
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
	-650.	-650.	-550.	-550.	-450.	-450.	-350.	-350.	-250.	-250.	-150.	-150.	-50.	-50.	50.	50.	150.	150.	250.	250.	

DISPLAY OF MINE BLOCK MODEL DATA.

		LEVEL 15 FROM 3425.0 TO 3450.0																				
		CU										X.XXX										
		GEOL										XXXX.										
		-650.		-550.		-450.		-350.		-250.		-150.		-50.		50.	150.		250.			
		16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
800.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	800.
20		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	20
750.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	750.
19		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	19
700.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	700.
18		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	18
650.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	650.
17		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	17
600.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	600.
16		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	16
550.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	550.
15		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	15
500.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	500.
14		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	14
450.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	450.
13		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	13
400.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	400.
12		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	12
350.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	350.
11		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	11
300.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	300.
10		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	10
250.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	250.
9		3	3	3	3	1000	1000	1000	3	3	3	3	3	3	3	3	3	3	3	3	3	9
200.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	200.
8		3	3	3	3	3	3	1000	1000	1000	3	3	3	3	3	3	3	3	3	3	3	8
150.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	150.
7		3	3	3	3	3	3	3	3	3	1000	1000	1000	1000	3	3	3	3	3	3	3	7
100.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	100.
6		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	6
50.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	50.
5		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	5
0.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0.
4		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4
-50.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-50.
3		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
-100.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-100.
2		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2
-150.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-150.
1		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	1
-200.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-200.
		16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
		-650.		-550.		-450.		-350.		-250.		-150.		-50.	50.		150.		250.			

DISPLAY OF MINE BLOCK MODEL DATA.

CU X.XXX
GEOL XXXX.

LEVEL 17 FROM 3375.0 TO 3400.0

	-650.		-550.		-450.		-350.		-250.		-150.		-50.		50.	150.	250.				
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
800.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	800.
20	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	20
750.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	750.
19	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2	2	2	19
700.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	700.
18	3	3	3	3	3	3	3	3	3	3	3	3	3	3	769	756	556	293	273	272	18
650.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	2	2	2	2	2	2	650.
17	2	2	2	3	3	3	3	3	3	3	3	3	3	3	780	780	631	304	274	272	17
600.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	2	2	2	2	2	2	600.
16	2	2	2	3	3	3	3	3	3	3	3	3	3	3	771	763	640				16
550.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	2	2	2	3	3	3	550.
15	2	2	2	3	3	3	3	3	3	3	3	3	3	3	738	713	616				15
500.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	2	2	2	3	3	3	500.
14	3	3	3	3	3	3	3	3	3	3	3	3	3	3	696	664	595				14
450.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	2	2	2	3	3	3	450.
13	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2	2	2	3	3	3	13
400.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	400.
12	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2	2	2	3	3	3	12
350.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	350.
11	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2	2	2	3	3	3	11
300.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	300.
10	3	3	3	3	26	26	26	3	3	3	3	3	3	3	2	2	2	3	3	3	10
250.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	250.
9	3	3	3	3	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	2	2	2	3	3	3	9
200.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	200.
8	3	3	3	3	3	3	3	3	3	3	3	3	3	3	1000	1000	1000				8
150.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	150.
7	3	3	3	3	3	3	3	3	3	3	3	3	3	3	1000	1000	1000				7
100.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	100.
6	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	6
50.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	50.
5	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	5
0.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0.
4	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4
-50.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-50.
3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
-100.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-100.
2	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2
-150.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-150.
1	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	1
-200.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-200.
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
	-650.		-550.		-450.		-350.		-250.		-150.		-50.		50.		150.		250.		

DISPLAY OF MINE BLOCK MODEL DATA.

+ *CU* X.XXX
 + GEOL XXXX.
 + +

LEVEL 19		FROM 3325.0 TO 3350.0																			
	-650.	-550.	-450.	-350.	-250.	-150.	-50.	50.	150.	250.											
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
800.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	800.
20	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	20
750.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	750.
19	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	350	328	315	19
700.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	700.
18	3	3	3	3	3	3	3	3	3	3	3	3	3	3	580	573	466	326	315	315	18
650.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	650.
17	326	326	326	3	3	3	3	3	3	3	3	3	3	3	2	2	2	2	2	2	17
600.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	600.
16	326	326	326	326	326	2	3	3	3	3	3	3	3	3	2	2	2	3	3	3	16
550.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	550.
15	326	326	326	326	326	2	3	3	3	3	3	3	3	3	2	2	2	3	3	3	15
500.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	500.
14	3	3	3	2	2	2	3	3	3	3	3	3	3	3	408	392	391	3	3	3	14
450.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	450.
13	3	3	3	3	2	2	2	3	3	3	2	2	2	2	368	368	368	368	368	3	13
400.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	400.
12	3	3	3	3	2	2	2	3	3	3	2	2	2	2	368	368	368	368	368	3	12
350.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	350.
11	3	3	3	3	2	2	2	3	3	3	2	2	2	2	368	368	368	368	368	3	11
300.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	300.
10	3	3	3	3	3	1	1	3	3	3	2	2	2	2	368	368	368	368	368	3	10
250.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	250.
9	3	3	3	3	1	1	1	1	1	1	1	1	1	1	1000	1000	1000	1000	1000	1000	9
200.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	200.
8	3	3	3	3	3	3	3	3	3	3	3	3	3	3	1000	1000	1000	3	3	3	8
150.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	150.
7	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	7
100.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	100.
6	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	6
50.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	50.
5	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	5
0.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0.
4	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4
-50.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-50.
3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
-100.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-100.
2	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2
-150.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-150.
1	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	1
-200.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-200.
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
	-650.	-550.	-450.	-350.	-250.	-150.	-50.	50.	150.	250.											

DISPLAY OF MINE BLOCK MODEL DATA.

CU X.XXX
 GEOL XXXX.

LEVEL 20 FROM 3300.0 TO 3325.0

	-650.	-550.	-450.	-350.	-250.	-150.	-50.	50.	150.	250.	350.	450.	550.	650.	750.	800.				
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35
800.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
750.+	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
700.+	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	113	104	98
650.+	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	207	204	160	103	99
600.+	504	505	508	3	3	3	3	3	3	3	3	3	3	3	3	211	210	177	106	99
550.+	504	504	504	516	527	525	3	3	3	3	3	3	3	3	3	230	222	207	3	3
500.+	504	503	502	516	529	527	3	3	3	3	3	3	3	3	3	362	337	309	3	3
450.+	3	3	3	487	497	474	3	3	3	3	3	3	3	3	3	521	523	495	3	3
400.+	3	3	3	3	355	339	351	3	3	3	641	641	641	624	581	573	573	3	3	3
350.+	3	3	3	3	337	330	335	3	3	3	641	641	636	612	578	573	573	3	3	3
300.+	3	3	3	3	330	330	330	3	3	3	641	641	625	604	583	576	573	3	3	3
250.+	3	3	3	3	1000	1000	1000	3	3	3	641	641	616	602	588	581	573	3	3	3
200.+	3	3	3	3	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	3	3	3	3	3
150.+	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
100.+	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
50.+	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
0.	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
-50.+	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
-100.+	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
-150.+	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
-200.+	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3

16 -650. 17 -550. 18 -450. 19 -350. 20 -250. 21 -150. 22 -50. 23 50. 24 150. 25 250. 26 350. 27 450. 28 550. 29 650. 30 750. 31 800. 32 850. 33 900. 34 950. 35 1000.

DISPLAY OF MINE BLOCK MODEL DATA.

CU X.XXX
 GEOL XXXX.

LEVEL 22 FROM 3250.0 TO 3275.0

	-650.	-550.	-450.	-350.	-250.	-150.	-50.	50.	150.											
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35
800.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
750.+	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	20
700.+	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	189	189	189
650.+	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2	2	2
600.+	340	351	398																	
550.+	2	2	2	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
500.+	340	340	379	581	672	676														
450.+	2	2	2	2	2	2	3	3	3	3	3	3	3	3	3	3	3	3	3	3
400.+	340	345	403	608	685	680	635	717	795	822	1116	1526	1454	996	472	308	173			
350.+	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	3	3	3
300.+	3	3	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
250.+	3	3	3	3	2	2	2	2	2	2	2	2	2	2	2	2	2	3	3	3
200.+	3	3	3	3	2	2	2	2	2	2	2	2	2	2	2	2	2	3	3	3
150.+	3	3	3	3	2	2	2	2	2	2	2	2	2	2	2	2	2	3	3	3
100.+	3	3	3	3	2	2	2	2	2	2	2	2	2	2	2	2	2	3	3	3
50.+	3	3	3	3	2	2	2	2	2	2	2	2	2	2	2	2	2	3	3	3
0.	3	3	3	3	2	2	2	2	2	2	2	2	2	2	2	2	2	3	3	3
-50.	3	3	3	3	2	2	2	2	2	2	2	2	2	2	2	2	2	3	3	3
-100.	3	3	3	3	2	2	2	2	2	2	2	2	2	2	2	2	2	3	3	3
-150.	3	3	3	3	2	2	2	2	2	2	2	2	2	2	2	2	2	3	3	3
-200.	3	3	3	3	2	2	2	2	2	2	2	2	2	2	2	2	2	3	3	3

DISPLAY OF MINE BLOCK MODEL DATA.

CU X.XXX
 GEOL XXXX.

LEVEL 25 FROM 3175.0 TO 3200.0

	-650.		-550.		-450.		-350.		-250.		-150.		-50.		50.	150.	250.				
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
800.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	800.
20	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	20
750.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	750.
19	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2	2	2	19
700.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	700.
18	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2	2	2	2	2	2	18
650.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	650.
17	334	334	337	343	347										115	113	248	546	573	575	17
600.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	600.
16	334	334	337	348	350	348	331	277	272	284					140	137	231				16
550.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	550.
15	334	335	340	350	350	349	331	257	230	237	395	628	618	444	254	204	209				15
500.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	500.
14	3	3	3	356	356	357	337	255	222	227	485	771	771	608	282	165	138				14
450.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	450.
13	3	3	3	386	390	374	295	261	299	621	794	792	624	182	106	103					13
400.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	400.
12	3	3	3	1408	1408	1408	341	346	428	642	763	730	503	156	105	103					12
350.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	350.
11	3	3	3	1408	1408	1408	354	403	498	624	710	603	422	199	131	103					11
300.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	300.
10	3	3	3	1408	1408	1000	1000	1000	1000												10
250.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	250.
9	3	3	3	3	3	3	3	3	3	3	1	1	1	3	3	3	3	3	3	3	9
200.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	200.
8	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	8
150.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	150.
7	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	7
100.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	100.
6	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	6
50.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	50.
5	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	5
0.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0.
4	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4
-50.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-50.
3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
-100.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-100.
2	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2
-150.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-150.
1	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	1
-200.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-200.
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
	-650.		-550.		-450.		-350.		-250.		-150.		-50.		50.		150.		250.		

DISPLAY OF MINE BLOCK MODEL DATA.

CU X.XXX
 GEOL XXXX.

LEVEL 28 FROM 3100.0 TO 3125.0

	-650.		-550.		-450.		-350.		-250.		-150.		-50.		50.	150.	250.				
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
800.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	800.
750.+	20	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	20
700.+	19	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	145	96	67	19
650.+	18	3	3	3	3	3	3	3	3	3	3	3	3	3	2	2	2	93	69	67	18
600.+	17	1074	1075	1081	1098	1110	1051								672	673	496	106	70	67	
550.+	16	2	2	2	2	2	2	2	2	2	2	3	3	3	2	2	2	3	3	3	16
500.+	15	1074	1074	1083	1109	1115	1110	949	477	336	324	297	278	297	417	533	552	477			
450.+	14	3	3	3	2	2	2	2	2	2	2	2	2	2	2	2	2	438	452		
400.+	13	3	3	3	2	2	1	1	1	2	2	2	2	2	2	2	2	229	229	229	13
350.+	12	3	3	3	3	1	1	1	1	2	2	2	2	2	2	2	2	229	229	229	12
300.+	11	3	3	3	3	1	1	1	1	1	1	1	2	2	2	3	3	3	3	3	11
250.+	10	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	10
200.+	9	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	9
150.+	8	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	8
100.+	7	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	7
50.+	6	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	6
0.	5	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	5
-50.	4	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4
-100.	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
-150.	2	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2
-200.	1	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	1
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
	-650.		-550.		-450.		-350.		-250.		-150.		-50.		50.		150.		250.		

DISPLAY OF MINE BLOCK MODEL DATA.

+ +
CU X.XXX
GEOL XXXX.
+ +

LEVEL 29 FROM 3075.0 TO 3100.0

	-650.		-550.		-450.		-350.		-250.		-150.		-50.		50.	150.	250.				
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
800.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	800.
20	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	20
750.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	750.
19	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2	2	2	19
700.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	189	118	78	700.
18	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2	2	2	2	2	2	18
650.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	650.
17	668	668	668	1205	1205	1205									936	937	686	133	82	78	
600.+	2	2	2	1	1	1	3	3	3	3	3	3	3	3	2	2	2	2	2	2	17
550.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	550.
16	668	668	668	1237	1213	1219	533	533	521	513	478				883	880	659				
500.+	2	2	2	1	1	1	2	2	2	2	2	3	3	3	2	2	2	3	3	3	16
450.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	450.
15	668	668	668	1243	1206	1213	533	533	531	528	478	427	425	525	609	590	481				
500.+	2	2	2	1	1	1	2	2	2	2	2	2	2	2	2	2	2	3	3	3	15
400.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	400.
14	3	3	3	1	1	1	1	2	2	2	2	2	2	2	2	2	2	3	3	3	14
350.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	350.
13	3	3	3	1	1	1	1	1	2	2	2	2	2	2	2	2	2	3	3	3	13
300.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	300.
12	3	3	3	1	1	1	1	1	2	2	2	2	2	2	2	2	2	3	3	3	12
250.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	250.
11	3	3	3	3	3	1	1	1	1	1	1	1	1	1	1	1	1	3	3	3	11
200.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	200.
10	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	10
100.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	100.
9	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	9
50.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	50.
8	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	8
0.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0.
7	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	7
-50.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-50.
6	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	6
-100.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-100.
5	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	5
-150.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-150.
4	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4
-200.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-200.
3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
2	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2
1	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	1
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
	-650.		-550.		-450.		-350.		-250.		-150.		-50.		50.		150.		250.		

DISPLAY OF MINE BLOCK MODEL DATA.

+ +
CU X.XXX
GEOL XXXX.
+ +

LEVEL 30 FROM 3050.0 TO 3075.0

	-650.		-550.		-450.		-350.		-250.		-150.		-50.		50.	150.	250.				
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
800.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	800.
20	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	20
750.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	750.
19	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	86	63	50	19
700.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	2	2	2	700.
18	3	3	3	3	3	3	3	3	3	3	3	3	3	3	320	313	204	62	51	50	18
650.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	2	2	2	2	2	2	650.
17	294	294	294	2097	2097	2097									326	326	245	68	51	50	17
600.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	2	2	2	2	2	2	600.
16	294	294	294	2078	2092	2088									329	321	259				16
550.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	2	2	2	3	3	3	550.
15	294	294	294	2075	2096	2092	304	304	307	311	379	482	490	444	364	335	285				15
500.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	2	2	2	3	3	3	500.
14	3	3	3	2011	2034	1992	1918	304	305	307	417	539	541	499	402	374	349				14
450.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	2	2	2	3	3	3	450.
13	3	3	3	1859	1780	1736	1758	1798	316	338	475	549	548	507	399	380	379				13
400.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	2	2	2	3	3	3	400.
12	3	3	3	1780	1730	1719	1728	1760	351	393	484	536	530	478	392	380	379				12
350.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	2	2	2	3	3	3	350.
11	3	3	3	1719	1719	1719	1719	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000				11
300.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	1	1	1	3	3	3	300.
10	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	10
250.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	1	1	1	3	3	3	250.
9	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	9
200.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	200.
8	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	8
150.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	150.
7	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	7
100.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	100.
6	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	6
50.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	50.
5	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	5
0.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0.
4	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4
-50.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-50.
3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
-100.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-100.
2	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2
-150.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-150.
1	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	1
-200.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-200.
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
	-650.		-550.		-450.		-350.		-250.		-150.		-50.		50.		150.		250.		

DISPLAY OF MINE BLOCK MODEL DATA.

		LEVEL 31 FROM 3025.0 TO 3050.0																		*CU* X.XXX GEOL XXXX.			
		-650.	-550.	-450.	-350.	-250.	-150.	-50.	50.	150.	250.												
		16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35		
800.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	800.	
20		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	20	
750.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	750.	
19		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2	2	2	19	
700.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	700.	
18		3	3	3	3	3	3	3	3	3	3	3	3	3	3	2	2	2	2	2	2	18	
650.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	650.	
17		1	1	1	1381	1381	1381	1381								21	20	30	52	54	54	17	
600.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	600.	
16		2	2	2	1	1	1	1	2	2	2	2	3	3	3	2	2	2	3	3	3	16	
550.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	550.	
15		1	1	1	1480	1384	1403	1625	291	292	294	318	337	314	220	121	97	82				15	
500.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	500.	
14		3	3	3	1763	1661	1850	2178	291	291	292	331	373	370	310	1000	1000	1000				14	
450.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	450.	
13		3	3	3	2444	2796	2995	2897	291	296	303	352	378	377	329	1000	1000	1000				13	
400.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	400.	
12		3	3	3	2798	3021	3070	3027	2885	2730	1000	1000	373	361	294	1000	1000	1000				12	
350.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	350.	
11		3	3	3												1000	1000	1000	1000	1000	1000	11	
300.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	300.	
10		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	10	
250.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	250.	
9		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	9	
200.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	200.	
8		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	8	
150.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	150.	
7		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	7	
100.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	100.	
6		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	6	
50.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	50.	
5		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	5	
0.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0.	
4		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4	
-50.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-50.	
3		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	
-100.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-100.	
2		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2	
-150.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-150.	
1		3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	1	
-200.+		+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-200.	
		16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35		
		-650.	-550.	-450.	-350.	-250.	-150.	-50.	50.	150.	250.												

DISPLAY OF MINE BLOCK MODEL DATA.

+ +
CU X.XXX
GEOL XXXX.
+ +

LEVEL 39 FROM 2825.0 TO 2850.0

	-650.		-550.		-450.		-350.		-250.		-150.		-50.		50.	150.	250.				
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
800.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	800.
20	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	20
750.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	750.
19	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	19
700.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	700.
18	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	18
650.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	650.
17	449	449	449	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	17
600.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	600.
16	449	449	449	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	16
550.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	550.
15	449	449	449	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	15
500.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	500.
14	3	3	3	3	3	3	3	3	3	3	40	42	44	3	3	3	3	3	3	3	14
450.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	450.
13	3	3	3	3	3	3	3	3	3	3	40	40	40	3	3	3	3	3	3	3	13
400.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	400.
12	3	3	3	3	3	3	3	3	3	3	40	40	40	3	3	3	3	3	3	3	12
350.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	350.
11	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	11
300.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	300.
10	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	10
250.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	250.
9	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	9
200.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	200.
8	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	8
150.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	150.
7	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	7
100.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	100.
6	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	6
50.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	50.
5	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	5
0.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0.
4	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4
-50.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-50.
3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
-100.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-100.
2	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2
-150.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-150.
1	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	1
-200.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-200.
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
	-650.	-650.	-550.	-550.	-450.	-450.	-350.	-350.	-250.	-250.	-150.	-150.	-50.	-50.	50.	150.	150.	250.	250.		

DISPLAY OF MINE BLOCK MODEL DATA.

CU X.XXX
 GEOL XXXX.

LEVEL 40 FROM 2800.0 TO 2825.0

	-650.		-550.		-450.		-350.		-250.		-150.		-50.		50.	150.		250.			
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
800.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	800.
20	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	20
750.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	750.
19	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	19
700.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	700.
18	3	3	3	3	3	3	3	3	3	3	3	3	3	3	1000	1000	1000				18
650.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	650.
17	1516	1516	1516												40	40	1000				17
600.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	600.
16	1516	1516	1516												40	40	1000				16
550.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	550.
15	1516	1516	1516																		15
500.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	500.
14	3	3	3	3	3	3	3	3	3	3	40	40	40								14
450.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	450.
13	3	3	3	3	3	3	3	3	3	3	40	40	40								13
400.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	400.
12	3	3	3	3	3	3	3	3	3	3	40	40	40								12
350.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	350.
11	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	11
300.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	300.
10	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	10
250.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	250.
9	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	9
200.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	200.
8	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	8
150.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	150.
7	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	7
100.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	100.
6	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	6
50.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	50.
5	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	5
0.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0.
4	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4
-50.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-50.
3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
-100.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-100.
2	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2
-150.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-150.
1	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	1
-200.+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	-200.
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	
	-650.	-650.	-650.	-550.	-550.	-550.	-450.	-450.	-350.	-350.	-250.	-250.	-150.	-150.	-50.	50.	150.	150.	250.	250.	

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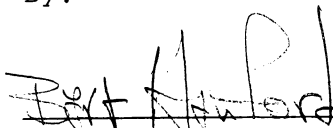
CAPITAL AND OPERATING COST ESTIMATES
FOR PROCESSING COPPER ORES

for

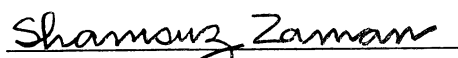
Home-Stake Production Company
4011 Silver Avenue, S.E.
Albuquerque, New Mexico

October 23, 1970

By:

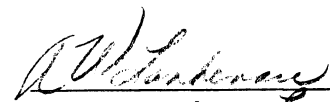


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INTRODUCTION

Hazen Research, Inc., was requested by Chapman, Wood, and Griswold acting in behalf of Home-Stake Production Company, to provide operating and capital cost estimates for processing the Kelly Fault and Carlotta ores. The estimates were to be based on reported metallurgical data from small scale batch tests, and the flowsheet was to consist of acid agitation leaching the Kelly Fault ore and acid baking the Carlotta ore followed by agitation leaching. It was assumed that the ores could be mixed in the agitation leach step for simplicity. The feed to the circuit was to consist of 2,500 tons per day of Kelly Fault ore and 500 tons per day of Carlotta ore.

During the course of obtaining grinding and settling data to size this equipment, confirming extraction tests were performed on the ores. The Kelly Fault ore responded as previously reported, but the extraction of copper from the Carlotta ore by acid baking varied considerably on two different samples. The previous information indicated that an extraction of 80% of the copper could be obtained by acid baking. A small sample from this previous testing gave copper extractions as high as 86%. However, the results obtained with a new sample, provided for grindability tests, gave an extraction of only 75% under the same test conditions.

As a result, several flowsheet variations were calculated using agitation leaching of the two ores.

Diluted ore grades were used in our estimates and were calculated from the following reported ore reserves:

	<u>Millions of Tons</u>	<u>% Cu</u>	<u>% Cu with 10% Dilution</u>
Kelly Fault	3.4	1.65	1.50
Carlotta	1.5	1.14	1.035
Carlotta low grade	3.3	0.337	

SUMMARY

Capital and operating costs were provided for the following flowsheets:

Flowsheet No. 1: Agitation leach of Kelly Fault ore (2,500 TPD) plus acid baking of Carlotta ore, (500 TPD) followed by countercurrent washing in thickeners and cementation of the copper.

Flowsheet No. 2: Agitation leach-CCD-cementation with 2,500 TPD of Kelly Fault Ore and 500 TPD of Carlotta ore.

Flowsheet No. 3: Same as Flowsheet No. 2 except that solvent extraction and electrowinning were substituted for cementation.

Flowsheet No. 4: Agitation leach-CCD-Cementation with 2,080 TPD of Kelly Fault ore and 920 TPD Carlotta ore. This is in the same ratio as the reported ore reserves.

The operating conditions and costs are shown in Table 1. No home office, mining, or royalty costs are included in these figures. No unusual costs were included for utilities, water, or tailings disposal. The mine and mill site has not been visited by the authors.

The preliminary capital costs are summarized in Table 2. Again, no unusual situations were provided for in the calculations.

RECOMMENDATIONS

It would be prudent to test numerous samples of each ore since the metallurgical data are based on small batch-scale tests from one sample of each ore. Additional efforts should be made to improve the extraction from the Carlotta ore, and tests should also be conducted on the Carlotta low grade to determine if it can be processed at a profit.

The preliminary processing cost studies appear to be favorable. However, it would be advisable to make a financial analysis of the cost data presented herein and include in any such study mining costs, head office expenses, pre-production costs, etc.

Table 1 (1 of 2 pages)

Operating Conditions and Costs

	Flowsheet 1			Flowsheet 2			Flowsheet 3			Flowsheet 4		
	Kelly Fault	Carlotta	Combined	Kelly Fault	Carlotta	Combined	Kelly Fault	Carlotta	Combined	Kelly Fault	Carlotta	Combined
Feed, tons/day	2,500	500	3,000	2,500	500	3,000	2,500	500	3,000	2,080	920	3,000
Feed, tons/month	68,750	13,750	82,500	68,750	13,750	82,500	68,750	13,750	82,500	57,200	25,300	82,500
Feed, tons/year	825,000	165,000	990,000	825,000	165,000	990,000	825,000	165,000	990,000	686,400	303,600	990,000
Feed grade, % Cu	1.50	1.035	1.42	1.50	1.035	1.42	1.50	1.035	1.42	1.50	1.035	1.357
Overall recovery, %			82.83			76.86			76.86			72.62
Lb Cu produced/ton			23.70			22.34			22.34			19.70
Lb Cu produced/month			1,955,250			1,843,050			1,843,050			1,625,250
Acid required, lb/ton	150	200	158.3	150	57	134.5	150	57	134.5	150	57	121.5
Acid added, tons/month			6,531			5,548			4,128			5,008
Extraction process	Agitation Leach	Bake		Agitation Leach	Agitation Leach		Agitation Leach	Agitation Leach		Agitation Leach	Agitation Leach	
Product			Cement Copper			Cement Copper			Cathode Copper			Cement Copper

Table 1 (2 of 2 pages)

Operating Costs

	Flowsheet 1 Combined Ore \$/Month	Flowsheet 2 Combined Ore \$/Month	Flowsheet 3 Combined Ore \$/Month	Flowsheet 4 Combined Ore \$/Month
Labor				
Supervisory and auxiliary	\$ 22,185	\$ 22,185	\$ 22,185	\$ 22,185
Hourly	35,180	25,880	57,825	25,880
Direct Materials				
Acid	130,615	110,960	82,560	100,155
Flocculant	14,850	14,850	14,850	14,850
Electricity	16,295	13,165	37,395	13,165
Iron	87,800	82,900		73,000
Electrowinning additives			1,845	
Solvent			48,000	
Anodes			2,000	
Maintenance Supplies	19,000	15,600	35,900	15,600
Property Taxes	8,570	6,855	15,750	6,855
Insurance	7,125	5,875	12,550	5,875
Office Expenses and Miscellaneous	8,500	7,900	12,000	7,900
Total Costs/Month	<u>\$350,120</u>	<u>\$306,170</u>	<u>\$342,800</u>	<u>\$281,965</u>
Cost/Ton	\$4.24	\$3.71	\$4.16	\$3.42
Cost/lb Cu	\$0.179	\$0.166	\$0.186	\$0.174

Table 2
Capital Cost Summary

	<u>Flowsheet 1</u>	<u>Flowsheet 2</u>	<u>Flowsheet 3</u>	<u>Flowsheet 4</u>
1. Crushing plant	\$ 800,000	\$ 800,000	\$ 800,000	\$ 800,000
2. Fine ore storage and feeding	325,000	325,000	325,000	325,000
3. Grinding circuit	725,000	360,000	360,000	360,000
4. Agitation leach	220,000	220,000	220,000	220,000
5. Acid bake	805,000			
6. CCD thickener circuit	1,035,000	1,035,000	1,035,000	1,035,000
7. Copper cementation	325,000	325,000		325,000
8. Solvent extraction			2,400,000	
9. Electrowinning			4,000,000	
10. Tailings disposal	100,000	100,000	100,000	100,000
11. Raffinate pond	30,000	30,000	30,000	30,000
12. Site preparation	50,000	50,000	50,000	50,000
13. Office, lab, ship, warehouse	150,000	150,000	150,000	150,000
14. Mobile equipment	240,000	240,000	240,000	240,000
15. Utilities	200,000	200,000	200,000	200,000
16. Engineering and construction supervision	475,000	300,000	300,000	300,000
17. Contingency	640,000	565,000	565,000	565,000
Total	<u>\$6,120,000</u>	<u>\$4,700,000</u>	<u>\$10,775,000</u>	<u>\$4,700,000</u>

METALLURGICAL INFORMATION

Hazen Research, Inc., was provided with copies of reports of laboratory tests conducted by the Galigher Company on the two ores.^{1]} Included in the report of April 24, 1970 was a letter report from Hazen Research, covering the examination of sulfuric acid leach residues of the Carlotta ore. Hazen's report concluded that the bulk of the copper occurs as exceedingly fine inclusions in jasper or chertlike particles and that there appears to be a relationship between copper and iron. It could not be ascertained with certainty whether the copper occurs as finely divided oxide, such as cuprite associated with hematite, or adsorbed on hematite and/or limonite. However, it is believed that the copper is adsorbed on the iron.

Extractions of 85 to 88% of the copper in the Kelly Fault ore sample were obtained in agitation leach tests ranging in duration from one to four hours with the addition of 146 pounds of H₂SO₄ per ton of ore. Extraction of about 90% of the copper were obtained with the addition of 221 pounds of H₂SO₄ per ton. However, with this addition of acid, the pH of the slurry at the end of the leach was 1.0 or less. Excessive consumption of iron would occur during cementation if this pH were not raised by the addition of an alkali.

Dilute sulfuric acid agitation leaching of the Carlotta ore resulted in a copper extraction of 57% when leaching for four hours at a pH of 1.5 to 1.6 due to the refractory nature of the ore. Varying the grind or extending the leaching time beyond one hour had little effect on the copper extraction.

In order to find an effective process for extracting the copper, a series of small scale, batch extraction tests utilizing various techniques were performed by Hazen Research on the residues from a mild acid leach of the Carlotta ore.^{2]}

^{1]} Home-Stake Production Company, Phoenix, Arizona
Laboratory Report covering the tests conducted on your two ore samples designated as our Lot No. 1889-A and 1889-B, January 22, 1970.
Home-Stake Production Company, Tulsa, Oklahoma
Laboratory Report on the additional testing of the Carlotta sample, our Lot No. 1889-A, April 24, 1970.

^{2]} Letter report to Mr. Frank E. Sims, Sr., Home-Stake Production Company, dated May 22, 1970.

The following conclusions were drawn from this test work:

1. Acid baking minus 20-mesh residues with 200 pounds of sulfuric acid per ton for four hours at 275°C resulted in the dissolution of 80% of the copper.

2. Roasting with 5% NaCl for one hour followed by sulfuric acid leaching at pH 2.0 produced an extraction of 76% of the copper.

3. Over 90% of the copper was volatilized from the leached residue by chlorination with CCl_4 or HCl at 700°C for 30 minutes.

4. High copper extractions were obtained by roasting the leach residue in a reducing atmosphere followed by leaching with an ammonia-ammonium carbonate solution.

Only a very small amount of Carlotta ore was left for any additional testing. Home-Stake Production Co. provided new samples of the Kelly Fault and Carlotta ores for grinding and settling tests. These samples were used to obtain additional information on copper extraction.

ACID AGITATION LEACHING OF KELLY FAULT ORE

Four leach tests were conducted on the minus 20-mesh ore from the grindability tests. This information confirmed the prior information with the following results:

Test No.	Leach Time Hr	H ₂ SO ₄ Added lb/ton	% Solids	Temp °C	First	Extn % Cu	lb H ₂ SO ₄ /lb Cu Extn
					Filtrate pH		
1	2	150	50	22	1.45	88.3	4.02
2	2	220	50	22	0.9	90.8	5.74
3	2	93(pH 1.8)	50	22	2.5	62.7	3.51
4	4	150	50	22	2.0	84.2	4.32

In all tests except No. 3, all of the acid was added at the beginning of the test. In test No. 3, a constant pH of 1.8 was maintained until almost the end of the test. The results show that adding all of the acid at once is the more effective method. Also, two hours retention time is adequate and 150 pounds of H₂SO₄ acid per ton not only gives a good extraction of the copper but results in a solution with a pH sufficiently high to be an acceptable feed to iron cementation.

The details of the leach tests are shown in the Appendix.

ACID AGITATION LEACHING OF CARLOTTA ORE

Two mild acid leaches of minus 20-mesh ore were performed with lower copper extractions than those reported from previous work. Two additional tests were then performed in which large quantities of acid, 500 and 1,000 pounds per ton of ore respectively, were added. It was hoped that this would give good copper extractions and contain sufficient free acid at the end of this strong leach so that the Kelly Fault ore could be added and effectively leached resulting in a final solution high enough in pH for acceptable operation of an iron cementation circuit.

The results of these tests are as follows:

Test No.	Leach Time Hr	H ₂ SO ₄ Added lb/ton	H ₂ SO ₄ Consumed lb/ton	% Solids	Temp °C	First Filtrate pH	Extn % Cu	lb H ₂ SO ₄ / lb Cu Extn
1	2	55		50	22	1.5	47.9	4.57
2	4	57		50	22	1.5	47.4	4.70
3	4	500	201	50	22	0	68.5	11.68
4	4	1,000	279	50	22	0	66.9	16.50

Copper extraction was not improved by increasing leaching time from two to four hours with the mild acid leach nor was it increased by the addition of more acid. In fact, the actual acid consumed varied from 28.7 to 44.2 pounds per pound of additional copper extracted. Details of these tests are given in the Appendix.

ACID BAKE OF CARLOTTA ORE

Tests were conducted on samples ground to 6, 10, and 20 mesh from the small sample remaining from the previous tests at Hazen Research to determine the effect of grind. Each sample was mixed with 200 pounds of sulfuric acid per ton of ore and 10% water to permit pugging, then baked at 275°C for four hours. The acid baked ore was then agitation leached in water at 50% solids for one hour.

Test No.	Ore Grind, Mesh	% Wt Gained in Roasting ^{1]}	% Wt Loss in Leaching ^{2]}	Residue % Cu	Extraction % Cu
1	-6	3.3	11.8	0.19	83.1
2	-10	3.9	12.1	0.18	83.6
3	-20	4.7	9.8	0.15	86.8

Heads -- 1.02% Cu.

^{1]} Based on ore weight.

^{2]} Based on calcine weight.

All copper extractions obtained in these tests were better than those obtained in the previous tests and showed an advantage for the minus 20-mesh grind over the coarser grinds.

When the minus 20 mesh sample from the grindability tests became available, tests were run at various bake times to obtain more information on this variable.

Test No.	Bake Time, Hr	Leach Residue % Cu	Extracted % Cu	lb Acid/lb Cu Extn
39	1	0.32	74.8	11.4
40	2	0.32	75.7	11.5
31	3	0.33	74.4	12.0
1	4	0.32	75.3	10.5

Extraction of copper was essentially the same for bake times of one to four hours. Even more significant is the fact that the extraction of copper is about 75%, whereas extractions of 80% and higher had been obtained in previous tests. The reason for this variance is not known. Details of the tests are in the Appendix.

SALT ROASTING-ACID LEACHING OF CARLOTTA ORE

Two tests were conducted on the minus 20 mesh ore by salt roasting for one and two hours, respectively, followed by acid leaching at pH 1.5. The results of these tests are as follows:

Heads % Cu	Roast Time Hr	Roast Temp °C	Leach Time Hr	Leach pH	% Solids in Leach	Acid Added lb/ton	Residue % Cu	Extn % Cu
1.26	1	850	4	1.5	50	62.5	0.61	50.9
1.26	2	850	2	1.5	50	36.8	0.44	66.9

Details of the better of these two tests are shown in the Appendix, and the results failed to confirm those previously reported. However, the tests show promise of improving copper extraction with less acid consumed than when leaching with mild acid.

THICKENING DATA

In order to provide data for sizing thickeners, settling tests were conducted on minus 20 mesh Kelly Fault and Carlotta ore samples. All tests were conducted in 1,000-milliliter graduates using a rake device rotating at six rpm. Leach pulps were diluted with water acidified with sulfuric acid to a pH of 1.50 to simulate the feed to a washing circuit. The data are summarized in Table 3 and the details are presented in the Appendix.

If it is assumed that the plant will operate with mild acid leaching of the Kelly Fault ore and either mild acid leaching or acid baking of the Carlotta ore, and that these two ores will be combined in a thickener circuit, then the thickener size would have to be based on 3,000 tons per day of Kelly Fault ore with a required settling area of 2.48 square feet/ton of solids/24 hours using 0.05 lb/ton of Separan NP-20. The flocculant is essential to the operation of this circuit. With a safety factor of 30%, a 110-foot diameter thickener would be required. A wood thickener tank with a stainless steel mechanism supported by a bridge truss would probably be the logical choice.

Table 3
Results of Settling Tests

Ore	Ratio	Treatment Method	% Solids		Separan NP-20, lb/ton	Settling Area ¹⁾ sq ft/ton/24 hr
			Feed	Underflow		
Kelly Fault		Mild acid leach	16.2	56.3	0	26.01
Kelly Fault		Mild acid leach	17.8	47.7	0.05	2.48
Carlotta		Mild acid leach	16.9		0	No clear overflow in 2 hr
Carlotta		Mild acid leach	16.9	59.4	0.05	1.60
Carlotta		Mild acid leach	16.9	59.4	0.10	3.30
Carlotta		Acid bake	15.7		0	Discarded - slimy overflow
Carlotta		Acid bake	15.7	53.8	0.05	0.14
Kelly Fault	5	Mild acid leach			0	30.25
Carlotta	1	Acid bake	17.5			
Kelly Fault	5	Mild acid leach			0.05	1.20
Carlotta	1	Acid bake	17.5	55.8		

¹⁾ No safety factor added.

GRINDABILITY TESTS

Rod mill grindability tests were run on the ores to assist in sizing the grinding mills. These tests were run by the Bond procedure to produce minus 20 mesh grinds to produce the following results:

<u>Ore</u>	<u>Bond Work Index</u>
Kelly Fault	14.43
Carlotta	9.56

These data indicate that the Kelly Fault ore is much harder than the Carlotta ore. The test details are presented in the Appendix.

PROCESS FLOWSHEETS

In all of the flowsheets studied in this report, only the minimum plant expenditures necessary to do an adequate job were estimated. For example, housing was considered necessary only for the secondary and tertiary crushers and screens, and for the grinding circuit. The fine ore bin is a covered pile with feeders under it. Some storage is provided for the ground ore prior to acid baking. The leaching and thickener circuits are not housed. The electrowinning circuit, of course, would be housed. Solution storage of pregnant solution and raffinate would be provided by ponds sealed with plastic sheeting or by other means.

Separation of solution and solids in all flowsheets is accomplished in a 3-thickener countercurrent decantation washing system. High washing efficiencies are achieved. Some variation in washing efficiencies between the various flowsheets is due to differences in the percent solids of the thickened solids as determined in the settling tests. Thickener underflow densities used in the calculations were a few percent lower than that determined in the tests.

CRUSHING PLANT

The crushing plant is the same for all flowsheets and consists of 3-stage crushing utilizing a 40" x 48" jaw crusher, 4-1/4' Symons standard cone crusher, and a 4-1/4' Symons short head cone crusher. All of the crushers are preceded by screens and the short head cone crusher is in closed circuit with a screen to insure a minus 3/4-inch or minus 5/8 inch product. Three-stage crushing is recommended in order to accommodate large size rock from open pit mining operations. A large gyratory crusher would be equally as satisfactory as a jaw crusher, but the cost of a new gyratory is considerably higher than that of a new jaw crusher. Dust collection must be provided at the secondary and tertiary crushers and screens.

It is proposed that the crushing plant operate 16 hours per day. The Kelly Fault and Carlotta ore would be stockpiled separately near the crushing plant feed hopper. The ore would be fed from the stockpiles to the feed hopper by a rubber-tired, front end loader with a 10-yard bucket. The proper number of loads from each stockpile would be taken to produce the desired ratio of the two ores in the feed.

A flowsheet of the crushing plant is shown in Figure 1.

Crushing Plant Flowsheet

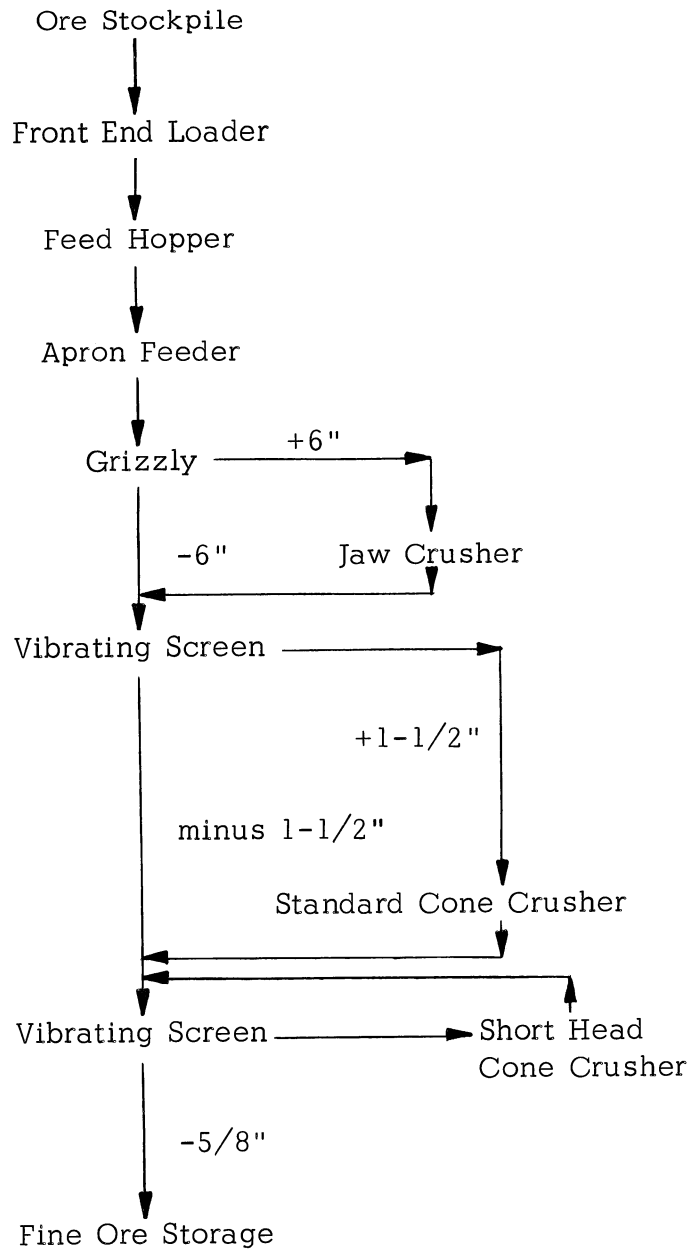


Figure 1

GRINDING CIRCUIT

In all of the flowsheets the water lost to the tailings pond was greater than that required to wet grind the ore. This made it possible to use wet grinding in all cases except for the ore which would be fed to the acid bake system.

A minus 20-mesh grind is required to achieve satisfactory metallurgy and proper operation of the thickener circuit. Finer grinding might increase the thickener area requirements. Open circuit grinding with rod mills of sufficient length to insure a minus 20 mesh grind is desirable. Cyclones are not very effective in making separations at this mesh. DSM screens are not recommended because of rapid wear and possible downtime. It is recognized that open circuit grinding with a limited top size does require additional horsepower over closed circuit grinding.

Since the Kelly Fault ore is harder, we have sized the grinding mills to treat 3,000 TPD of this ore. In normal operations the rod charge would be slightly reduced.

Consultation with two different mill manufacturers resulted in recommendations of 11'6" I.D. mills by 16'0" to 18' with connected motors of 1,000 to 1,150 horsepower. For dry grinding of the Carlotta ore, rod mills of 5'0" x 12'0" and 6' x 12' with 150 and 200 horsepower motors, respectively, were recommended. Air flow would have to be provided through the dry grinding mill for dust control.

LEACHING CIRCUIT

The leaching circuit would consist of three agitated leach tanks in series with the pulp flowing by gravity between the tanks. An average residence time of three hours should be provided to take care of the short circuiting of some of the ore. Three 20-foot diameter by 20-foot high wood tanks with brick lining should be used. Bypass arrangements should be such that any tank can be easily bypassed with the slurry while operating.

FLWSHEET NO. 1

Agitation Leaching Kelly Fault-Acid Bake of Carlotta Ore

A simplified flowsheet showing solid and solution flows is shown in Figure 2. The washing efficiency of this circuit is 99.4% with an overall extraction of 82.83%. The solution going to cementation contained 3.95 grams/liter of copper.

A 9' diameter x 180' long kiln with a 9" thickness of brick was calculated using a retention time in the kiln of three hours. Kiln slope was 3/8-inch per foot and the speed was 0.83 rpm. Kiln loading was 10.2%.

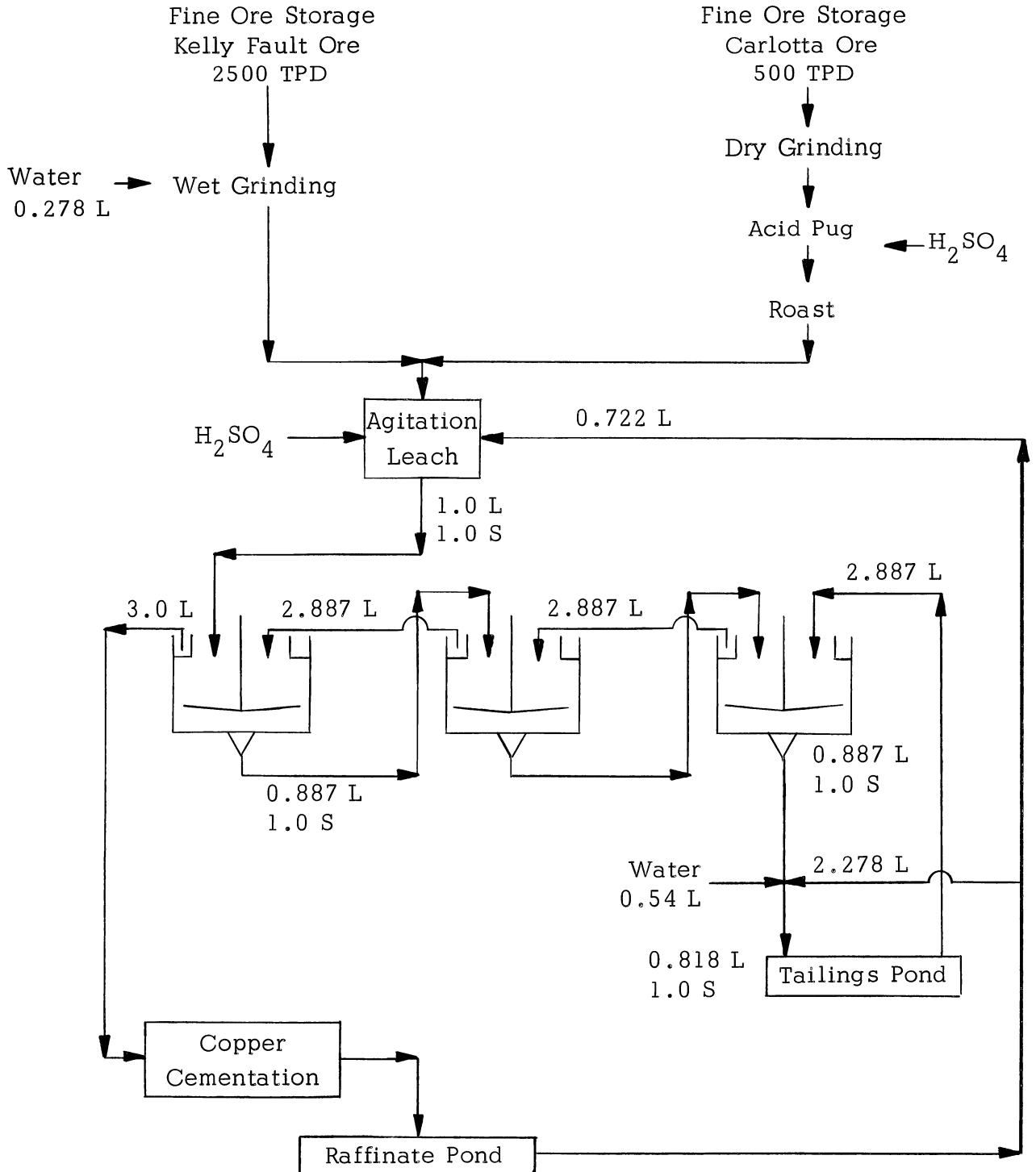
If the acid bake process is used, it should be piloted to verify the metallurgical data and to provide data for engineering.

FLWSHEET NO. 2

Agitation Leach-CCD-Cementation

In this flowsheet a washing efficiency of 97.7% was obtained because of the relatively low (47%) density of the thickener underflow solids. Overall recovery of copper is 76.86% and the grade of the solution going to precipitation is 3.72 grams/liter of copper.

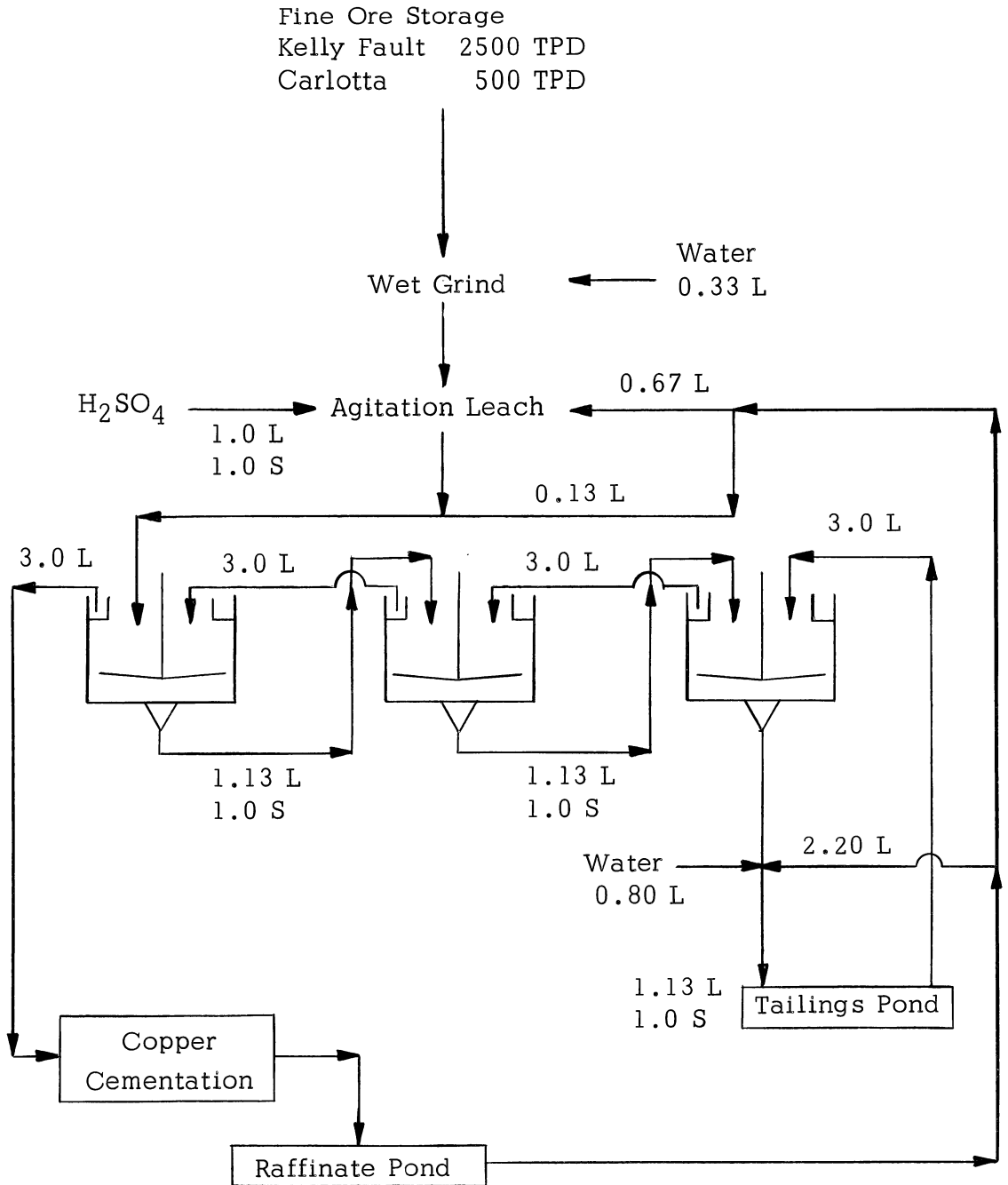
Flowsheet No. 1



Note: All flows of liquor and solids are based on 1.0 ton of solids feed.
Example: 1.0 L means 1.0 tons liquor
1.0 S means 1.0 tons solids

Figure 2
hri

Flowsheet No. 2



Note: All flows of liquor and solids are based on 1.0 ton of solids feed.

Figure 3

FLWSHEET NO. 3

Agitation Leach-CCD-SX-Electrowinning

This flowsheet is similar to No. 2 except that solvent extraction and electrowinning have been substituted for the cementation step.

In the solvent extraction loading step, one mole of sulfuric acid is exchanged to the solution for each mole of copper loaded. This results in an acid saving of 1,420 tons per month over Flowsheet No. 2. In the electrowinning step, one mole of acid is generated for each mole of copper plated.

In the solvent extraction circuit, three loading and three stripping stages would be required. Aqueous flow to solvent extraction would be 1,500 gallons per minute containing 3.72 grams/liter copper. Organic flow would be about 1,100 gpm.

For electrowinning, 62 cells each containing sixty 3' x 3' cathodes were calculated. Four of the cells would be used for producing starting sheets.

FLWSHEET NO. 4

Agitation Leach-CCD-Cementation

This flowsheet is similar to No. 2 except that the ratio of the Kelly Fault and Carlotta ore feeds is the same as the reported ore reserves.

FLWSHEET DISCUSSION

For each additional pound of copper extracted from the Carlotta ore using the acid bake process (FS1) the acid consumption was 17.5 pounds of sulfuric acid per pound of copper. With this acid consumption and this increased capital investment of an acid bake process (FS1) compared to a mild acid leaching process (FS2), FS1 does not appear to be economically attractive for the existing Carlotta ore reserves.

Since the capital cost of a solvent extraction-electrowinning plant (FS3) is so high, it is doubtful that any overall economic advantage can be gained by installing such facilities.

Flowsheet No. 4

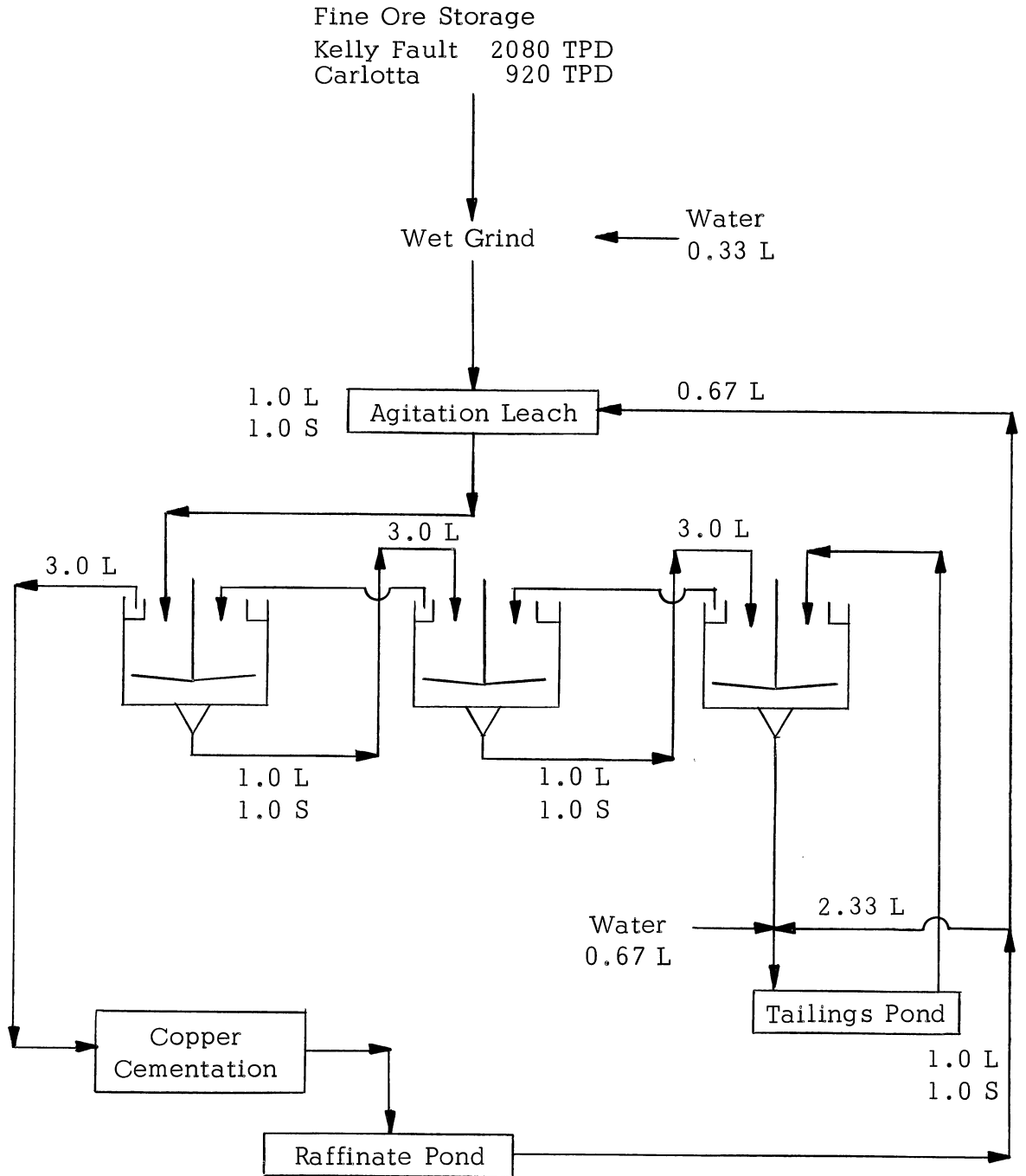


Figure 5

APPENDIX

Details of Laboratory Tests on
Carlotta and Kelly Fault Ores

Test 1 (1 of 2 pages)

Object: To observe the effect of acid baking time on the leach extraction of Carlotta copper ore.

Sample: Carlotta Ore, HRI 3094-2

Procedure: Four 200 g samples were split out from the minus 20 mesh blended rod mill grindability test (CSMRI). The four samples corresponding to sample No. 39, 40, 31, and 1 were moistened with 10% water, treated with 200 lb of H₂SO₄ per ton of ore, and baked at 275°C with time of baking ranging from one to four hours. The acid baked samples were then leached with water at 50% solids for one hour, further washed, and filtered.

Data:

<u>Bake Conditions</u>	<u>Sample #39</u>	<u>Sample #40</u>	<u>Sample #31</u>	<u>Sample #1</u>
Weight, g	200.0	200.0	200.0	200.0
Moisture, %	10.0	10.0	10.0	8.0
Acid, lb/ton	200.0	200.0	200.0	200.0
Time, hr	1.0	2.0	3.0	4.0
Temperature, °C	275	275	275	275
Weight change, %	+1.75		+2.05	1.6
Grind, mesh	-20	-20	-20	-20

Leach Conditions

Weight into leach, g	203.5	204.1	203.2	200.0
Time, hr	1.0	1.0	1.0	1.0
% solids	50	50	50	50
Temperature, °C	35	35	35	35
Volume filtrate, ml	180.0	216.0	188.0	600.0
Volume wash, ml*	510.0	500.0	480.0	-
Volume wash, ml	270.0	300.0	240.5	-
Weight residue, g	182.0	181.0	181.0	177.5
Weight leached, %	10.6	11.3	10.9	11.4
Filtrate, pH	1.7	1.85	1.9	1.5

* Washed and Repulped with pH 1.5 H₂O.

Test 1 (2 of 2 pages)Leach Conditions: (continued)

<u>Sample #39</u>			<u>Sample #40</u>			<u>Sample #31</u>			<u>Sample #1</u>		
Time min	pH	Temp °C	Time min	pH	Temp °C	Time min	pH	Temp °C	Time min	pH	Temp °C
0	1.35	28	0	1.3	28	0	1.3	28	0	1.55	35
15.0	1.40	32	15.0	1.4	32	15.0	1.4	30	20	1.55	35
30.0	1.40	40	30.0	1.4	43	30.0	1.4	35	40	1.55	35
45.0	1.40	42	45.0	1.4	48	45.0	1.4	38	60	1.55	35
60.0	1.40	42	60.0	1.4	46	60.0	1.4	38			

Results:

<u>Product</u>	<u>Assay % or g/l</u>	<u>% Distribution Cu</u>	<u>lb H₂SO₄/ lb Cu Extracted</u>
<u>Sample #39</u>			
Filtrate	6.48	49.2	
Wash #1	1.08	23.1	11.4
Wash #2	0.23	2.5	
Residue	0.32	25.2	
Calculated head	1.19	100.0	
<u>Sample #40</u>			
Filtrate	6.00	54.4	
Wash #1	0.92	19.2	
Wash #2	0.17	2.1	11.5
Residue	0.32	24.3	
Calculated head	1.19	100.0	
<u>Sample #31</u>			
Filtrate	6.24	49.2	
Wash #1	1.18	23.9	
Wash #2	0.14	1.3	12.0
Residue	0.33	25.6	
Calculated head	1.19	100.0	
<u>Sample #1</u>			
Filtrate	2.88	73.3	
Residue	0.32	24.7	10.5
Calculated head	1.15	100.0	

Test 2 (1 of 2 pages)

Object: To observe the effect of varying acid concentrations on the extraction of Kelly Fault ore.

Sample: Kelly Fault Ore, HRI 3094-1

Procedure: Approximately 600 g of minus 20 mesh sample from the rod mill grindability tests (CSMRI) were blended carefully and three 200 g samples were split. Each of the three samples were then leached with H₂SO₄ at 50% solids for two hours at ambient temperature ($\approx 22^{\circ}\text{C}$) with varying acid concentrations.

Data:

<u>Leach Conditions</u>	<u>Sample #1</u>	<u>Sample #2</u>	<u>Sample #3</u>
Time, hr	2	2	2
Acid, H ₂ SO ₄ , lb/ton	150	220	93 (pH 1.8)
% solids	50	50	50
Temperature, $^{\circ}\text{C}$	22	22	22
Mesh	-20	-20	-20
Weight % leached	6.0	6.0	4.5
Weight into leach, g	200.0	200.0	200.0
Weight leach residue, g	188.0	188.0	191.0
Filtrates, volume, ml	160.0	175.0	225.0
Wash, volume, ml	600.0	610.0	600.0
Filtrate, ph	1.45	0.92	2.50
Acid added, ml	8.5	12.8	5.7

Results:

<u>Product</u>	<u>Assay</u> % or g/l	<u>%</u> Distribution Cu	<u>lb H₂SO₄/</u> <u>lb Cu</u> <u>Extracted</u>
<u>Sample #1</u>			
Filtrate	15.7	63.9	
Wash #1	1.60	24.4	4.02
Residue	0.246	11.7	
Calculated head	1.97	100.0	
<u>Sample #2</u>			
Filtrate	17.6	69.2	
Wash #1	1.57	21.6	5.74
Residue	0.219	9.2	
Calculated head	2.22	100.0	(cont'd)

Test 2 (2 of 2 pages)

<u>Product</u>	<u>Assay</u> <u>% or g/l</u>	<u>%</u> <u>Distribution</u> <u>Cu</u>	<u>1b H₂SO₄/</u> <u>1b Cu</u> <u>Extracted</u>
<u>Sample #3</u>			
Filtrate	8.00	42.1	
Wash #1	1.46	20.6	
Residue	0.84	37.3	3.51
Calculated head	2.14	100.0	

Test 4

Object: To observe the effect of lengthening leach time at 150 lb/ton acid to obtain a high extraction on the Kelly Fault ore.

Sample: Kelly Fault Ore, HRI 3094-1

Procedure: This test was carried out in a similar way to that of Test 2; however, the leach was prolonged 2 hours, giving a total of 4 hours leach time.

Data:

<u>Leach Conditions</u>	<u>Sample #2</u>
Time, hr	4
Acid, lb/ton	150
% solids	50
Temperature, °C	22
Mesh	-20
Weight % leached	5.0
Weight into leach, g	198.0
Weight leach residue, g	188.0
Filtrate, volume, ml	650.0

Results:

<u>Product</u>	<u>Assay % or g/l</u>	<u>% Distribution Cu</u>
Filtrate	5.23	84.2
Weight leach residue 134		15.8
Calculated head	2.04	100.0
Assay	2.06	

Test 5 (1 of 2 pages)

Object: To observe the effect of agitation leaching on the extraction of Carlotta Cu ore.

Sample: Carlotta Ore, HRI 3094-2

Procedure: Four 200 g samples were split out from the -20 mesh blended rod mill grindability test (CSMRI). The four samples corresponding to sample No. 1, 2, 3 and 4 were agitation leached at 50% solids at 22°C. The time of leach varied from 2 to 4 hours. Two samples were leached at a pH of 1.5 and the remaining two samples were leached at 500 lb acid/ton and 1,000 lb acid/ton respectively. The agitation leached samples were filtered and further washed.

Data:

<u>Leach Conditions</u>	<u>Sample #1</u>	<u>Sample #2</u>	<u>Sample #3</u>	<u>Sample #4</u> ^{1/}
Time, hr	2.0	4.0	4.0	4.0
Acid (H ₂ SO ₄)	55 lb/ton	57 lb/ton	500 lb/ton	1000 lb/ton
Acid consumed	--	--	201 lb/ton	279 lb/ton
% solids	50	50	50	50
Mesh	-20	-20	-20	-20
Weight, % leached	3.5	3.6	4.2	4.2
Weight into leach, g	200.0	201.2	201.5	201.5
Weight leach residue, g	193.0	194.0	193.0	193.0
Filtrate, volume, ml	600.0	450.0	440.0	340.0
Wash volume, ml				
pH filtrate	1.5	1.5	0.0	0.0

^{1/} Frothing upon addition of 1000 lb/ton H₂SO₄.

Test 5 (2 of 2 pages)Leach Conditions: (continued)

<u>Sample #1</u>			<u>Sample #2</u>			<u>Sample #3</u>		<u>Sample #4</u>	
Time min	Acid ml	pH	Time min	Acid ml	pH	Time min	pH	Time min	pH
0	1.4	6.3	0	0	6.7	0	6.7	0	6.6
10	0.3	1.5	10	2.3	1.5	10	<0.0	10	<0.0
30	0.2	1.5	30	0.6	1.5	40	<0.0	40	<0.0
45	0.6	1.5	45	0.2	1.5	120	<0.0	120	<0.0
101	0.6	1.5	101	1.4	1.5	180	<0.0	180	<0.0
120	0	1.8	120	0	1.5	240	<0.0	240	<0.0
			159	0	1.5				
			240	0	1.5				

Results:

<u>Product</u>	<u>Assay Cu % or g/l</u>	<u>% Distribution Cu</u>	<u>lb H₂SO₄/ lb Cu Extracted</u>
<u>Sample #1</u>			
Filtrate	2.07	47.9	
Residue ^{1/}	6.7	52.1	4.57
Calc head	1.28	100.0	
Assay head	1.26		
<u>Sample #2</u>			
Filtrate	2.77	47.4	
Residue ^{1/}	0.68	52.6	4.78
Calc head	1.25	100.0	
Assay head	1.26		
<u>Sample #3</u>			
Filtrate	3.40	68.5	
Residue ^{1/}	0.48	31.5	11.68
Calc head	1.09	100.0	
Assay head	1.26		
<u>Sample #4</u>			
Filtrate	4.93	66.9	
Residue ^{1/}	0.43	33.1	16.50
Calc head	1.25	100.0	
Assay head	1.26		

^{1/} Washed with pH 1.5 H₂O -- H₂SO₄
hri

Test 6 (1 of 2 pages)

Object: To form soluble copper chlorides through salt roasting in order to obtain a high extraction during leaching.

Sample: Carlotta Ore, HRI 3094-2

Procedure: Approximately 100 grams of minus 20 mesh sample from the rod mill grindability tests (CSMRI) was blended carefully and one 100 gram sample was split. The minus 20 mesh sample was then combined with 7% NaCl and roasted @ 850°C for 2 hours. The salt roasted product was leached for 2 hours with sulfuric acid @ 50% solids maintaining a pH of 1.5. The pulp was filtered and washed thoroughly.

Data:

Roast Conditions:

	<u>Sample #1</u>
Weight sample, g	96.2
Weight after roast, g	103.5
NaCl, %	7.6
Grind, mesh	-20
Temperature, °C	850
Time roast, hr	2:00

Leach Conditions:

Time, hr	2
Acid, H ₂ SO ₄ , lb/ton	36.8
Solids, %	50.0
Temperature, °C	22.0
Mesh	-20
Weight leached, %	6.7
Weight into leach, g	103.5
Weight leach residue, g	97.0
Filtrate, volume, ml	270.0

Leach Conditions: (continued)

Time Min	Sample #1 -- Reading --		Acid	pH
	Initial	Final		
0	37.6	38.4	0.8	6.4
20	40.4	40.2	0.2	2.4
40	40.4	40.4	0.0	1.5
60	40.4	40.4	0.0	1.5
80	40.4	40.4	0.0	1.5
120	40.4	40.4	0.0	1.5

Results:

Product	Assay Cu % or g/l	% Distribution Cu
Filtrate	1.33	66.9 ^{1/}
Residue	0.44	33.1
Calc head	0.76	100.0
Assay head	1.26	

^{1/} Calculated on the basis of assay head and leach residue.

KYNCH PROCEDURE
THICKENING TEST DATA

Pulp 3094-1 Kelly Fault ore leached for 2 hours at 50% solids with 150 lb/ton H₂SO₄. The sample was brought to 20% solids with pH 1.5 H₂O and allowed to settle with 0.05 lb/ton Separan NP 20.

Project 798-2
Test #2
Date 9/21/70
By Bart Hanford

Settling Rate		Pulp Density Measurements			
Level (ml)	Time (min)		Feed Pulp	Thickened Solids	Decant Liquor
		Volume, ml	1000	290 ml	710
930	300.50	Gross wet wt, g	1782	1028	
850	1.00	Tare, g	636	636	
780	1.50	Net wet wt, g	1056	392	
705	2.00	Gross dry wt, g	201.4		
685	2.50	Tare, g	14.6		
580	3.00	Net dry wt, g	186.8	186.8	
540	4.60	Density, g/l			
515	4.00	% Solids	17.8	47.7	
450	6.00	Thickener rake rotation = 6 min/rev			
420	7.00	<u>Terminal Density Calculation</u>			
410	8.00	Clear liquor volume at ___ hr: _____ ml			
360	12.00	Clear liquor weight at ___ hr: _____ ml x _____ g/l = _____ g			
300	23.00	Thickened slurry wt: (_____) g - (_____) g = _____ g			
290	52.00	Dry solids weight: _____ 186.8 g			
290	60.00	Thickened pulp density: 47.7 % Solids			
		<u>Thickener Unit Area Requirement</u>			
		Initial height, Ho: 1.146 ft			
		Initial pulp density, Co = (30.3 x 10 ⁻⁶) (feed pulp density, g/l) = _____ ton/ft ³			
		Co = 31.3 · 10 ⁻⁶ x 186.8 = 0.00585 T/ft ³			
		Critical time, t _x = 24 min = 0.01667 days			
		Unit area, A = $\frac{t_x}{CoHo}$ = $\frac{0.01667}{(0.00585)(1.146)}$			
		A = 2.48 ft ² /ton/day			
	Terminal Level _____ hours				

Remarks A great deal of sand in bottom of cylinder. Addition of 0.05 lb flocculant/ton or ore (0.1 lb/ton total) yielded a very clear effluent at a much higher settling rate.

Clarity of Decant Liquor: Cloudy -- particles in suspension, gas being given off.

KYNCH PROCEDURE
THICKENING TEST DATA

Pulp Minus 20 mesh Carlotta ore, HRI 3094-2, agitation leached
at 1.5 pH and 50% solids for 2 hours, diluted with 1.5 pH
solution and settled with 0.05 lb/ton Separan NP 20.

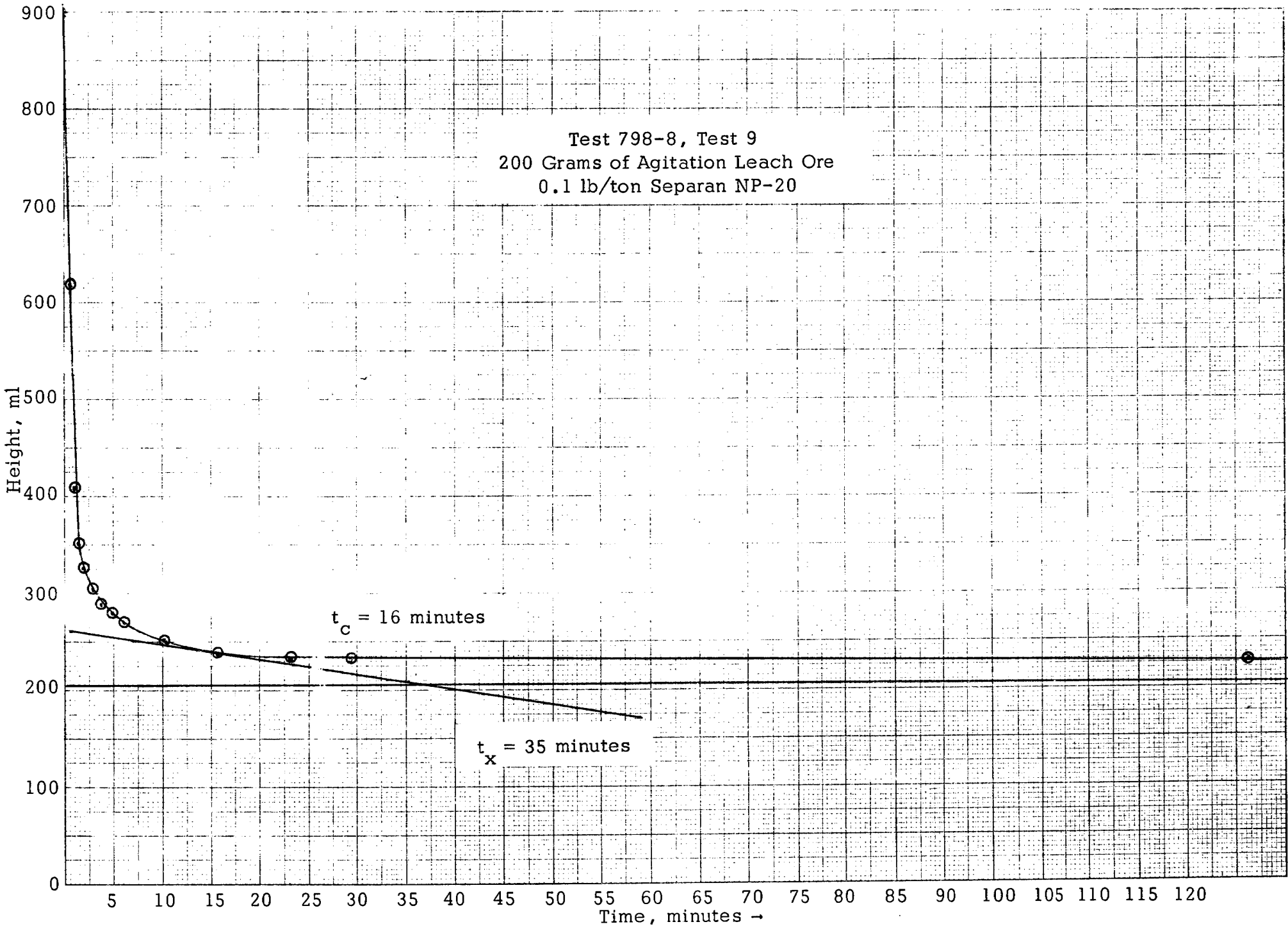
Project 798-8
Test #8
Date 10/7/70
By Bart Hanford

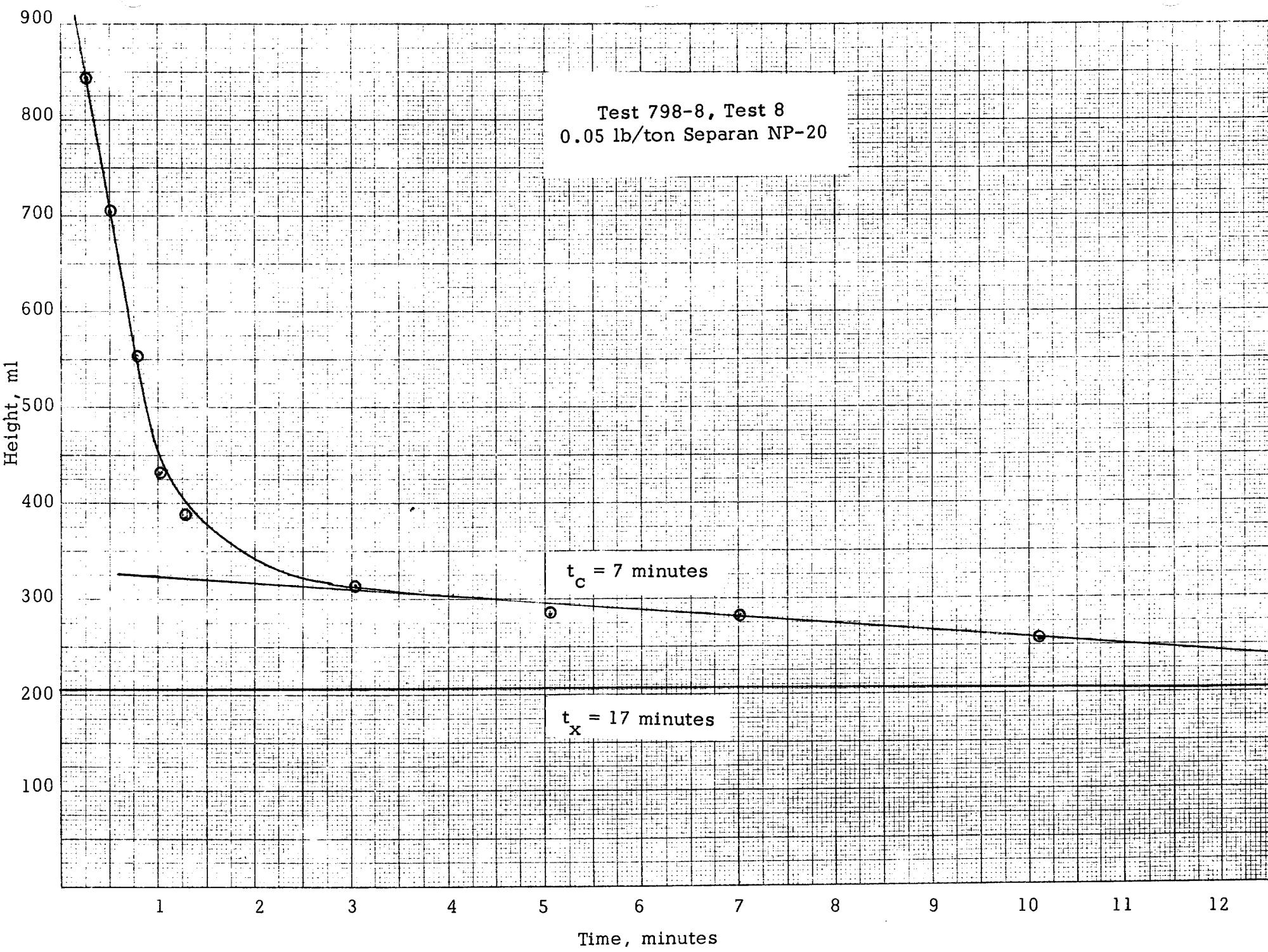
Settling Rate		Pulp Density Measurements			
Level (ml)	Time (min)		Feed Pulp	Thickened Solids	Decant Liquor
0		Volume, ml	1000	205	795
840	15 sec	Gross wet wt, g	1720.0	920.0	
700	30 "	Tare, g	600.0	600.0	
550	49 "	Net wet wt, g	1120.0	320.0	
430	60 "	Gross dry wt, g			
385	75 "	Tare, g			
360	90 "	Net dry wt, g			
310	3.0 min	Density, g/l		190.0	
300	4.0 "	% Solids	16.9	59.4	
285	5.0 "	Thickener rake rotation = _____ min/rev			
260	7.0 "	<u>Terminal Density Calculation</u>			
255	10.0 "	Clear liquor volume at ____ hr: _____ ml			
		Clear liquor weight at ____ hr: _____ ml x _____ g/l = _____ g			
		Thickened slurry wt: (_____) g - (_____) g = _____ g			
		Dry solids weight: _____ g			
		Thickened pulp density: _____ % Solids			
		<u>Thickener Unit Area Requirement</u>			
		Initial height, Ho: _____ 1.239 _____ ft			
		Initial pulp density, Co = (30.3 x 10 ⁻⁶) (feed pulp density, g/l) = _____ ton/ft ³			
		Co = 31.3 · 10 ⁻⁶ x 190.0 = 0.00595			
		Critical time, t _x = 17 min = 0.0118 _____ days			
		Unit area, A = $\frac{t_x}{CoHo}$ = _____ $\frac{0.0118}{0.00595 (1.239)}$			
		A = _____ 1.60 _____ ft ² /ton/day			
		Terminal Level _____ 19 _____ hours			

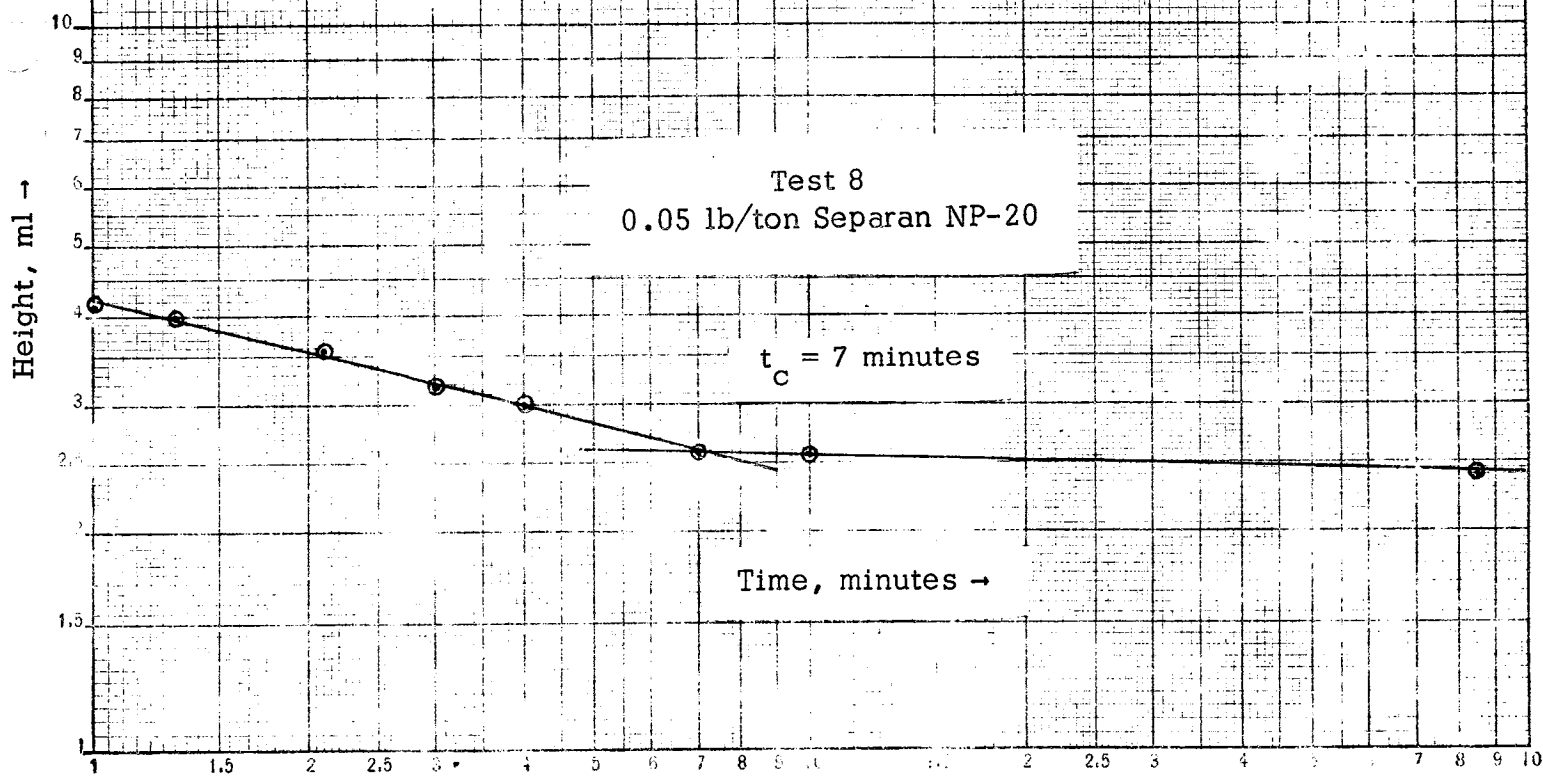
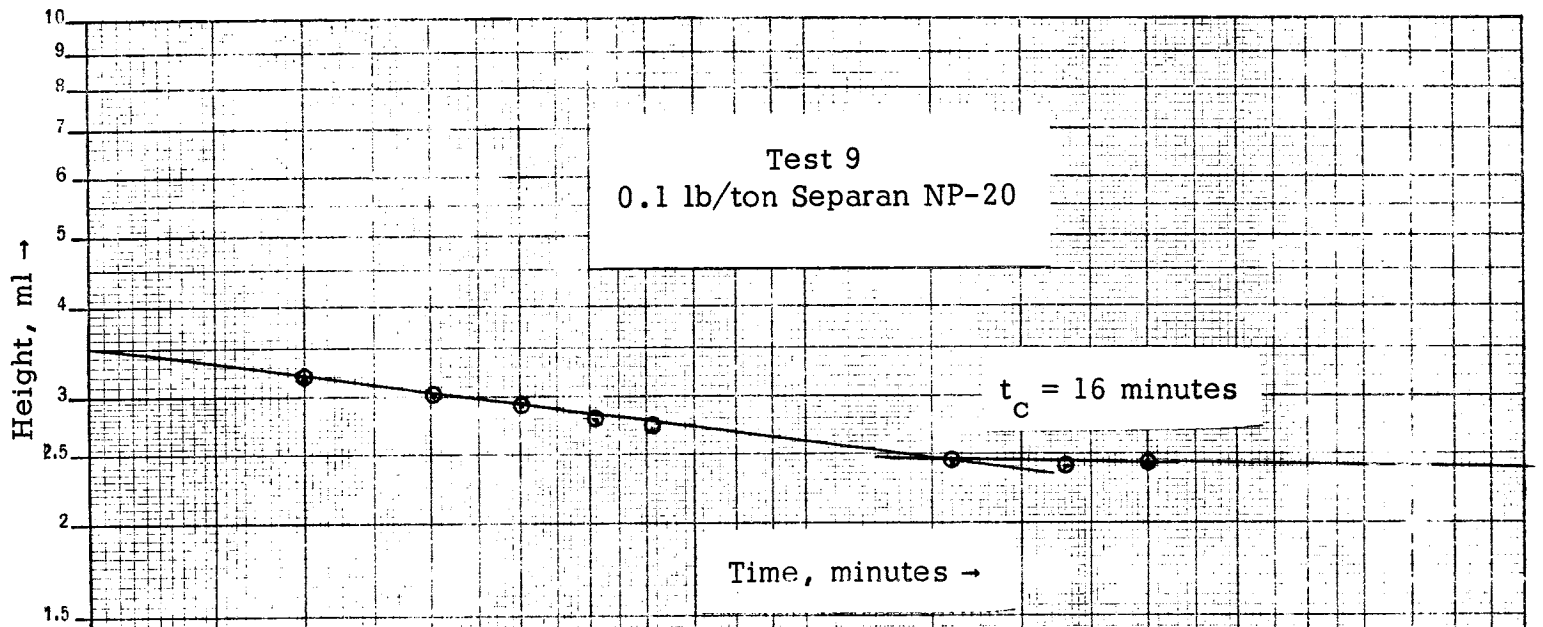
Remarks A great deal of solids in suspension with no distinct settling mud line
with no flocculant.

Clarity of Decant Liquor: Clear -- minor amounts of solids in suspension.

Test 798-8, Test 9
200 Grams of Agitation Leach Ore
0.1 lb/ton Separan NP-20







KYNCH PROCEDURE
THICKENING TEST DATA

Pulp 3094-2 200 grams Carlotta ore @20% solids after acid

 bake and water leach -- no flocculant

 Pour settling

Project 798-3

 Test #1

 Date 9/21/70

 By Bart Hanford

Settling Rate		Pulp Density Measurements		
Level (ml)	Time (min)	Feed Pulp	Thickened Solids	Decant Liquor
		Volume, ml		
		Gross wet wt, g		
1000	0	Tare, g		
985	2	Net wet wt, g		
970	18	Gross dry wt, g		
950	20	Tare, g	636	
170	51	Net dry wt, g		
		Density, g/l		
		% Solids	15.7	
		Thickener rake rotation = <u>6</u> min/rev		
		<u>Terminal Density Calculation</u>		
		Clear liquor volume at ___ hr: _____ ml		
		Clear liquor weight at ___ hr: _____ ml x _____ g/l = _____ g		
		Thickened slurry wt: (_____) g - (_____) g = _____ g		
		Dry solids weight: _____ g		
		Thickened pulp density: _____ % Solids		
		<u>Thickener Unit Area Requirement</u>		
		Initial height, Ho: <u>1.146</u> ft		
		Initial pulp density, Co = (30.3 x 10 ⁻⁶) (feed pulp density, g/l) = ton/ft ³		
		Co = 31.3 · 10 ⁻⁶ x _____ = _____		
		Critical time, t _x = _____ days		
		Unit area, A = $\frac{t_x}{CoHo}$ = _____		
		A = _____ ft ² /ton/day		
		Terminal Level _____ hours		

Remarks Effluent very slimy -- need flocculant -- unable to see mud line.

Clarity of Decant Liquor: _____

KYNCH PROCEDURE
THICKENING TEST DATA

Pulp 3094-2 200 grams Carlotta ore @20% solids after acid bake
and water leach -- 0.05 lb/ton Separan NP 20

Project 798-3
Test #2
Date 9/22/70
By Bart Hanford

Settling Rate Level (ml)	Time (min)	Pulp Density Measurements			
		Feed Pulp	Thickened Solids	Decant Liquor	
550	1/4	Volume, ml	1000	190	810
300	1/2	Gross wet wt, g	1747	961	
270	3/4	Tare, g	636	636	
260	1.0	Net wet wt, g	1111	325	
240	1.5	Gross dry wt, g	189.4		
225	2.0	Tare, g	14.6		
215	2.5	Net dry wt, g	174.8	174.8	
215	3.0	Density, g/l			
210	4.0	% Solids	15.7	53.8	
200	5.0	Thickener rake rotation = 6 min/rev			
190	6.0	<u>Terminal Density Calculation</u>			
190	12.0	Clear liquor volume at ___ hr: _____ ml			
190	20.0	Clear liquor weight at ___ hr: _____ ml x _____ g/l = _____ g			
190	32.0	Thickened slurry wt: (_____) g - (_____) g = _____ g			
190	43.0	Dry solids weight: _____ g			
		Thickened pulp density: _____ % Solids			
		<u>Thickener Unit Area Requirement</u>			
		Initial height, Ho: 1.146 ft			
		Initial pulp density, Co = (30.3 x 10 ⁻⁶) (feed pulp density, g/l) = ton/ft ³			
		Co = 31.3 · 10 ⁻⁶ x 174.8 = 0.00547			
		Critical time, t _x = 1.3 min = 0.0009027 days			
		Unit area, A = $\frac{t_x}{CoHo}$ = $\frac{0.0009027}{(0.00547)(1.146)}$			
		A = 0.144 ft ² /ton/day			
	Terminal Level _____ hours				

Remarks Addition of 0.05 lb/ton Separan NP 20, equivalent to 0.1 lb/ton total, eliminated the solids in suspension and yielded a very clear effluent with higher settling rate.

Clarity of Decant Liquor: Cloudy pea green

KYNCH PROCEDURE
THICKENING TEST DATA

Pulp 3094-1, 2. The leach pulps from the individual tests were combined @ 50% solids in a ratio of 5:1, Kelly to Carlotta, and then were diluted to 20% solids and allowed to settle. No flocculant

Project 798-4
Test #1
Date 9/22/70
By Bart Hanford

Settling Rate		Pulp Density Measurements			
Level (ml)	Time (min)		Feed Pulp	Thickened Solids	Decant Liquor
1000	0	Volume, ml	1000	210	790
960	3	Gross wet wt, g			
936	6	Tare, g			
850	14	Net wet wt, g			
775	22	Gross dry wt, g			
600	38	Tare, g			
540	53	Net dry wt, g		201.6	
480	63	Density, g/l			
445	74	% Solids	17.5		
420	84	Thickener rake rotation = 6 min/rev			
360	109	<u>Terminal Density Calculation</u>			
338	126	Clear liquor volume at ___ hr: _____ ml			
310	146	Clear liquor weight at ___ hr: _____ ml x _____ g/l = _____ g			
306	152	Thickened slurry wt: (_____) g - (_____) g = _____ g			
290	169	Dry solids weight: _____ g			
260	211	Thickened pulp density: _____ % Solids			
255	227	<u>Thickener Unit Area Requirement</u>			
255	234	Initial height, Ho: 1.146 ft			
250	245	Initial pulp density, Co = (30.3 x 10 ⁻⁶) (feed pulp density, g/l) = ton/ft ³			
250	260	$Co = 31.3 \cdot 10^{-6} \times 201.6 = 0.00631 \text{ T/ft}^3$			
250	273	Critical time, $t_x = 315.00 = 0.21875$ days			
		Unit area, $A = \frac{t_x}{CoHo} = \frac{0.21875}{(0.00631)(1.146)}$			
		Terminal Level _____ hours			
		A = 30.25 ft ² /ton/day			

Remarks _____

Clarity of Decant Liquor: _____

KYNCH PROCEDURE
THICKENING TEST DATA

Pulp 3094-1, 2. The leach pulps from the individual tests were combined @ 50% solids in the ratio of 5:1, Kelly to Carlotta, and the combined sample was allowed to settle with 0.05 lb/ton Separan NP 20

Project 798-4
Test #2
Date 9/22/70
By Bart Hanford

Settling Rate		Pulp Density Measurements			
Level (ml)	Time (min)		Feed Pulp	Thickened Solids	Decant Liquor
1000	0	Volume, ml	1000	210	790
950	1/4	Gross wet wt, g	1746	961	
900	1/2	Tare, g	600	600	
850	3/4	Net wet wt, g	1146	361	
810	1.0	Gross dry wt, g	216.2		
725	1.5	Tare, g	14.6		
650	2.0	Net dry wt, g	201.6	201.6	
580	2.5	Density, g/l			
535	3.0	% Solids	17.5	55.8	
510	3.5	Thickener rake rotation = 6 min/rev			
495	4.0	<u>Terminal Density Calculation</u>			
470	5.0	Clear liquor volume at ___ hr: _____ ml			
450	6.0	Clear liquor weight at ___ hr: _____ ml x _____ g/l = _____ g			
400	10.0	Thickened slurry wt: (_____) g - (_____) g = _____ g			
350	16.0	Dry solids weight: _____ g			
250	39.0	Thickened pulp density: 55.8 % Solids			
		<u>Thickener Unit Area Requirement</u>			
		Initial height, Ho: 1.146 ft			
		Initial pulp density, Co = (30.3×10^{-6}) (feed pulp density, g/l) = ton/ft ³			
		Co = $31.3 \cdot 10^{-6} \times 201.6 = 0.00631$ T/ft ³			
		Critical time, t _x = 12.55 = 0.00872 days			
		Unit area, A = $\frac{t_x}{CoHo} = \frac{0.00872}{(0.00631)(1.146)} =$			
		A = 1.206 ft ² /ton/day			
	Terminal Level _____ hours				

Remarks _____

Clarity of Decant Liquor: _____

ROD MILL GRINDABILITY TESTS

Rod Mill Grindability Test No. 1 -- Kelly Fault Ore

Purpose: To determine the rod mill grindability of the test sample in terms of a Bond work index number.

Sample: -1/2 in. ore from Sponsor's Sample No. HRI 3094-1.

Procedure: The equipment and procedure duplicate the Bond method for determining rod mill work indices.

Test

Conditions: Mesh of grind: 20
Weight of undersize product for 100% circulating load: 1050.2 gm
Weight % of undersize material in rod mill feed: 15.7

Results:

Stage No.	New Feed gm	Undersize		Revolutions	Undersize In Product gm	Undersize Produced	
		In Feed gm	To Be Ground gm			Total gm	Per Mill Revolution gm
1	2100.4	329.8	720.4	35	612.1	282.3	8.07
2	612.1	96.1	954.1	118	928.5	832.4	7.05
3	928.5	145.8	904.4	128	1056.7	910.9	7.12
4	1056.7	165.9	884.3	124	1093.8	927.9	7.48
5	1093.8	171.7	878.5	117	1065.7	894.0	7.64
6	1065.7	167.3	882.9	116	1096.8	929.5	8.01
7	1096.8	172.2	878.0	110	1019.5	847.3	7.70
8	1019.5	160.1	890.1	116	954.5	794.4	6.85
9	954.5	149.9	900.3	131	980.1	830.2	6.34
10	980.1	153.9	896.3	141	974.4	820.5	5.82
11	974.4	153.0	897.2	154	1089.4	936.4	6.08
12	1089.4	171.0	879.2	145	1010.5	839.5	5.79
13	1010.5	158.6	891.6	154	1074.6	916.0	5.95
14	1074.6	168.7	881.5	148	1047.7	879.0	5.94

Average last three = 5.89

Rod Mill Grindability Test No. 1 (continued)

Rod Mill Work Index Computations

$$Wi = \frac{62}{P_1^{0.23} \times Grp^{0.625} \times \left(\frac{10}{\sqrt{P}} - \frac{10}{\sqrt{F}} \right)}$$

Wherein: P_1 = 100% Passing Size of Product = 825 microns
Grp = Grams per Revolution = 5.89
P = 80% Passing Size of Product = 600 microns
F = 80% Passing Size of Feed = 8975 microns

$$Wi = 14.43$$

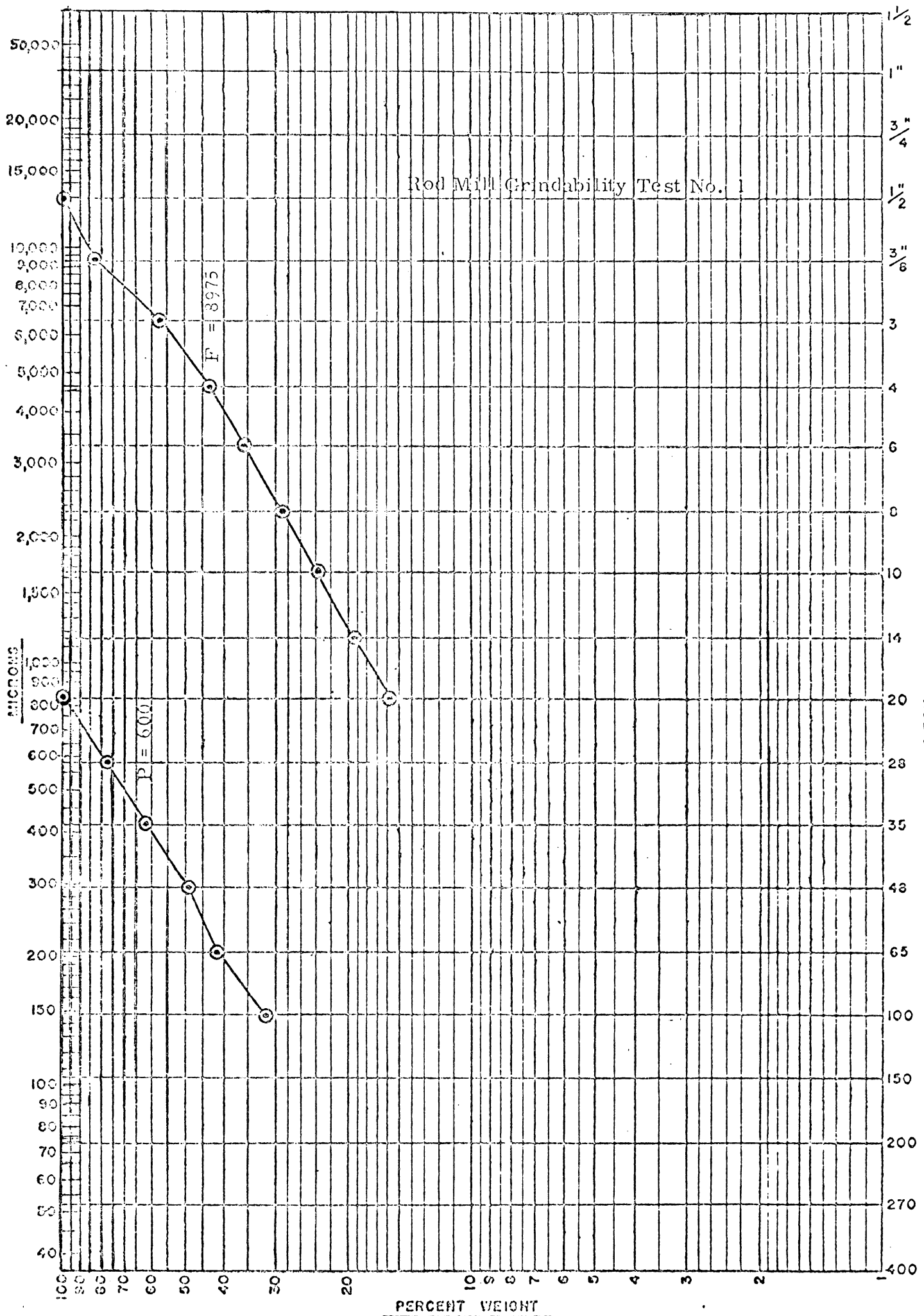
Rod Mill Grindability Test No. 1 (continued)

Screen Analysis of Test Feed

<u>Screen Product (Tyler) Mesh</u>	Weight %		
	<u>Direct</u>	<u>Cumulative Retained</u>	<u>Passing</u>
Head (computed)			
-1/2"+3/8"	17.2	17.2	100.0
-3/8"+3M	25.7	42.9	82.8
-3 +4	13.7	56.6	57.1
-4 +6	8.2	64.8	43.4
-6 +8	6.4	71.2	35.2
-8 +10	5.0	76.2	28.8
-10 +14	4.6	80.8	23.8
-14 +20	3.5	84.3	19.2
-20	15.7		15.7

Screen Analysis of Test Product

<u>Screen Product (Tyler) Mesh</u>	Weight %		
	<u>Direct</u>	<u>Cumulative Retained</u>	<u>Passing</u>
Head (computed)			
-20 +28	22.4	22.4	100.0
-28 +35	16.6	39.0	77.6
-35 +48	11.9	50.9	61.0
-48 +65	8.4	59.3	49.1
-65 +100	9.4	68.7	40.7
-100	31.3		31.3



Rod Mill Grindability Test No. 2 -- Carlotta Ore

Purpose: To determine the rod mill grindability of the test sample in terms of a Bond work index number.

Sample: -1/2 in. ore from Sponsor's Sample No. HRI 3094-2.

Procedure: The equipment and procedure duplicate the Bond method for determining rod mill work indices.

Test

Conditions: Mesh of grind: 20

Weight of undersize product for 100% circulating load: 1103.1 gm

Weight % of undersize material in rod mill feed: 25.2

Results:

Stage No.	New Feed gm	Undersize		Revolutions	Undersize In Product gm	Undersize Produced	
		In Feed gm	To Be Ground gm			Total gm	Per Mill Revolution gm
1	2206.2	556.0	547.1	35	890.1	334.1	9.55
2	890.1	224.3	878.8	92	1259.5	1035.2	11.25
3	1259.5	317.4	785.7	70	1197.8	880.4	12.58
4	1197.8	301.8	801.3	64	1063.0	761.2	11.89
5	1063.0	267.9	835.2	70	1120.3	852.4	12.18
6	1120.3	282.3	820.8	67	1139.1	856.8	12.79
7	1139.1	287.1	816.0	64	1096.3	809.2	12.64
8	1096.3	276.3	826.8	65	1098.3	822.0	12.65

Average last three = 12.69

Rod Mill Grindability Test No. 2 (continued)

Rod Mill Work Index Computations

$$Wi = \frac{62}{P_1^{0.23} \times Grp^{0.625} \times \left(\frac{10}{\sqrt{P}} - \frac{10}{\sqrt{F}} \right)}$$

Wherein: P_1 = 100% Passing Size of Product = 825 microns
Grp = Grams per Revolution = 12.69
P = 80% Passing Size of Product = 640 microns
F = 80% Passing Size of Feed = 7885 microns

$$Wi = 9.56$$

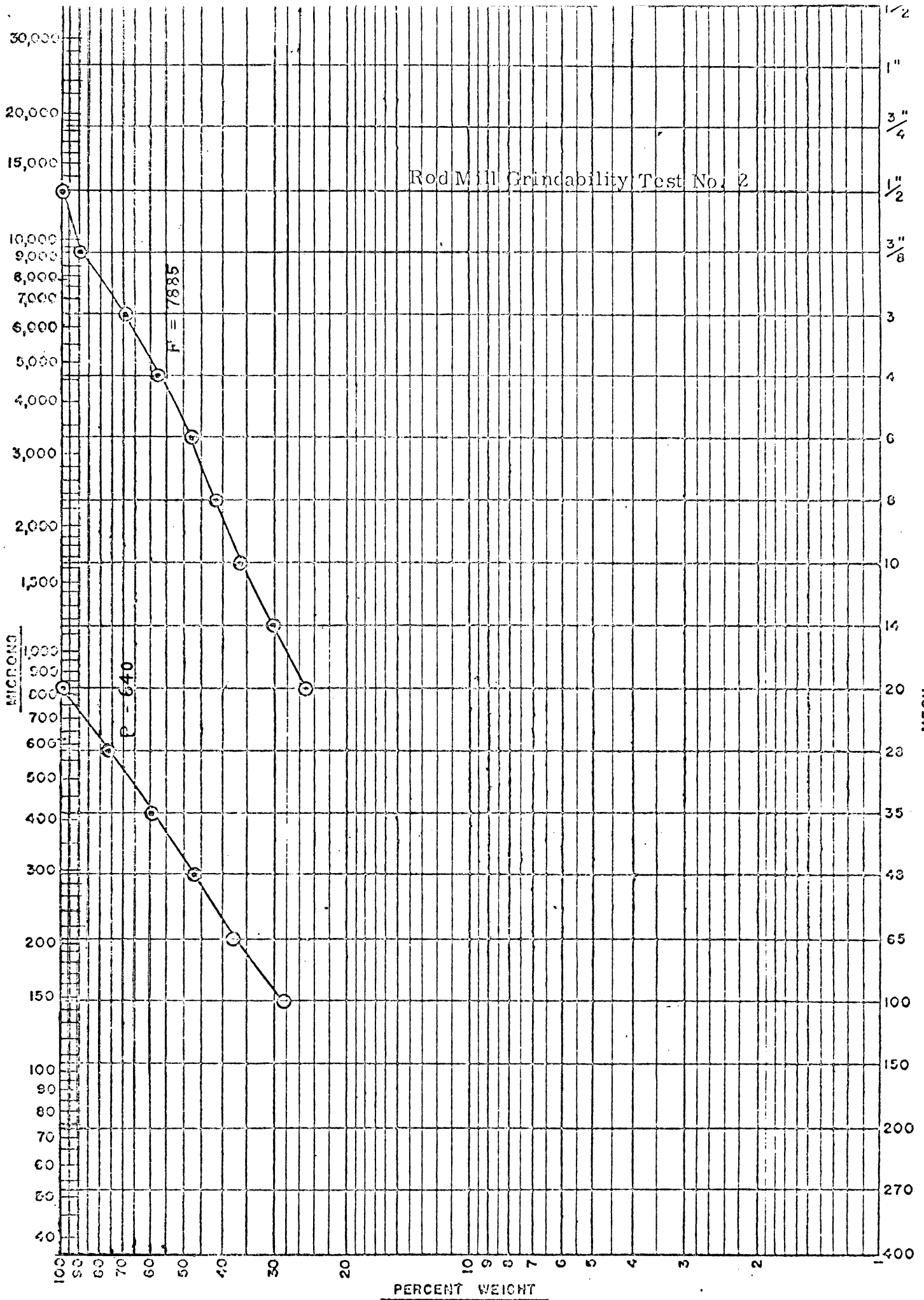
Rod Mill Grindability Test No. 2 (continued)

Screen Analysis of Test Feed

<u>Screen Product</u> <u>(Tyler) Mesh</u>	Weight %		
	<u>Direct</u>	<u>Cumulative</u> <u>Retained</u>	<u>Passing</u>
Head (computed)			
-1/2"+3/8"	10.4	10.4	100.0
-3/8"+3M	20.0	30.4	89.6
-3M +4	13.0	43.4	69.6
-4 +6	8.6	52.0	56.6
-6 +8	6.6	58.6	48.0
-8 +10	5.5	64.1	41.4
-10 +14	5.7	69.8	35.9
-14 +20	5.0	74.8	30.2
-20	25.2		25.2

Screen Analysis of Test Product

<u>Screen Product</u> <u>(Tyler) Mesh</u>	Weight %		
	<u>Direct</u>	<u>Cumulative</u> <u>Retained</u>	<u>Passing</u>
Head (computed)			
-20 +28	23.7	23.7	100.0
-28 +35	17.3	41.0	76.3
-35 +48	12.5	53.5	59.0
-48 +65	8.9	62.4	46.5
-65 +100	9.3	71.7	37.6
-100	28.3		28.3



From K

11/14/70

In summarizing the "report from Hazen Research, Inc., and using all of their cost figures where available, I come up with the following:

Kelly Fault Tons - 3.4 million of 1.65% Cu
Carlota Zone - 0.5 " " 1.035 " 1.42%

Milling 3000 Tons per day, 2500 of Kelly Fault and 500 Carlota, after a 10% Dilution Factor, the average grade would be 1.42% Cu.

Using their flowsheet #1 the overall recovery would be 82.83% or 23.7% recovered per ton of ore. Then the ^{operating} cost per pound of copper recovered would be \$0.179 plus mining. Using a mining cost figure of \$1.62/Ton, which includes stripping and waste cost, the cost/pound of copper recovered would be \$0.068. Total Operating Costs would then be \$0.247 per pound copper produced.

(2)

With a reserve of 5 million tons, including dilution, recovering 23.7 #/Ton produces 118,500,000 pounds of copper.

Total Value @ 48¢ Cu $(118,500,000 \times 0.48)$ \$ 56,880,000

Total Operating Costs $(118,500,000 \times 0.247)$ = 29,269,500

TOTAL OPERATING PROFIT = \$ 27,610,500

568800

Using Hazen's estimated plant cost (Flowsheet #1) of \$6,120,000 plus say 1 million for mining equipment and mine preparation, the present Reserves at Carlota, @ 48¢ copper price, would Net 20 million dollars plus after return of capital investment.

4282

Grizzly Mtn

4192

BLACK TUNNEL (Spring)

Spring

4109

Miller Spr

3439

3786

870000
FEET

PINALLA
COUNTY

Grizzly Bear
Spr

Creek

BM 3913

4083

3939

3931

CO

CO

4071

CARLOTA MINE

BM

Well

PINTO
SHAFT

HAMILTON
SHAFT

3642

Cottonwood

4011

COTTONWOOD

TAILINGS

POND

Powers

4101

T. 1 N.

T. 1 S.

Well

BLACK BESS
SHAFT

BOUNDARY
APPROXIMATE

3836

4301

Manitou Hill

4216

4044

4145

33° 22' 30"

YO TAMBIEN TUNNEL

740007