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DISTRICT: Crown King PRO PERTY: <u>Gladiator</u> 4 har Engle LOCATION: about $\frac{1}{2}$ mile below (N of) War Engle, q. v. OPERATOR: Fike & Starbird, lessees. VISITED: August 6, 1926, by D. M. Barringer, jr.

Property is opened by a single tunnel about 1900 feet long. This runs as a cross-cut for about 500', where it encountered the vein. A short drift runs N, the main tunnel turning to the right (S) and following the vein zone for 1400 feet.

Close to the intersection of tunnel with vein rather extensive stoping has been done. The stopes are inaccessible, but one is known to have holed surface by the air circulation. As the hill is very steep, this stope must be some 300' or more in height. Did not see where it came out on surface.

Between this stope and a smaller to the S is a pillar, whose height is indeterminate, whose length is 25 feet, and in which the vein is exposed between 18" and 24" thick, carrying, evidently rather heavy Pb, Zn, and Fe sulphides. A grab sample at the tunnel level ran:

Fike and Starbird propose mining this pillar, if sufficient equipment is forthcoming. The ore and walls are extremely hard, making hand mining practically impossible. They also propose milling some of the tailings from the old mill (the latter being entirely dismantled and, so far as I could see, worthless).

The 1400' of tunnel beyond the stope does not seem to have developed shything of interest. Although several small fissures were encountered, there has been no stoping on any of them, and I did not sample them.

AMASK

WAR EAGLE

spud

DISTRICT: Crown King LOCATION: 7000 feet by very rough road above Lincoln Mill, which in turn is four miles by rough road from Crown King.

OPERATOR: Fike and Starbird, Lessees.

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VISITED: August 6, 1926, by D. M. Barringer, Jr.

The vein is developed at two places, designated as the upper and lower shafts. The collar of the lower shaft is said to be 50' below the X-cut tunnel at the lower shaft, and the workings are some 800 feet apart. The X-cut tunnel, running N 80° W, encounters the upper shaft some 60 feet below the surface, and is rather badly caved at this point. A drift runs about 100' south and 150' north, developing a shoot 12" to 30" in width, 150' in length, and said to assay \$16 per ton in Au and Ag. No stoping has been done, unless fro some inaccessible level in the shaft. I was given to understand there had been none. About 50# of sorted ore taken from the dump for milling test.

The lower shaft, some 800' N of the upper, is caved. The only access to the workings was through a stope from the 100 level which had holed surface about 100' N of the shaft. Between it and the shaft is a pillar, containing some 200 tons (21' to 3' wide) which is claimed to run \$14.00. The ore is largely oxidized, though some galena and zinc blende were seen in it.

The shaft is accessible to the 200' level, below which water stands. On the 200 the same shoot as above is visible, tho reduced to 12" ave. thickness. The small amount of stoping seems to indicate that the values have decreased as well, and the ore is still pretty thoroughly oxidized.

Fike and Starbird propose milling the dumps at the two shafts, and the pillar in the lower shaft workings, also possibly some of the shoot in the upper shaft. Their haul to mill would average \$1.00; concs. to Crown King about \$2.00; and to Middleton about \$2.00 more. Freight to Humboldt \$1.00 on \$20.00 ore. They also propose milling some tailings and possibly ore from the Gladiator mine, report on which q. v. Samples from dumps at upper and lower shafts (about 50' each) sent to Tooele. Together they ran: Au, ; Ag, ; Pb, ; Cu, ; Fe, ; Zn, ; S, ; CaO, ; Insol, . D. M. Ballinger, Jr.

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(note by G. M. Colvocoresses - October 1937)

and

This property has turned out rather better than the reports would indicate for in 1936 it was reopened by E. M. Moore and Maguire and they have since been operating fairly steadily and shipping up to 100 tons per week of ore that has a gross value of better than \$20.00 per ton. The tonnage of such ore is probably limited but the operations so far appear to be moderately profitable.

On the occasion of my one visit to this mine, several years ago, I was impressed with the strength of the vein but the very inaccessible location and complex character of the ore deterred us from doing anything with it.

At present price of gold it may offer good possibilities for a small operation and I presume that Mooresewould be glad to talk business to other people.

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DISTRICT:Crown KingLOCATION:about $\frac{1}{2}$ mile below (N of) War Eagle, q.v.OPERATOR:Fike & Starbird, lessees.VISITED:August 6, 1926, by D. M. Barringer, jr.

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Re Gladiator Mine

9/28/38

Arthur Murphy tells me that contract is all ready to

be executed by Moores and Ross whereby Ross will furnish Moores with \$50,000 which will be put up by a very rich oil man from Fort Worth, Texas and Moores will have full control of spending it for development and operation of the mine and treatment of the ore in the Crown King Mill which Jones will lease to them for that purpose. Expected that this deal will go through very promptly and work start. Ross and his backer to get a large interest in the mine and may purchase it later. E. S. Clark is probably acting as attorney in this matter.

hits & S. h. C. 6/20:38

Some six miles from Crown King which in turn is about 53 miles (by road) south from Prescott. Road from Crown King is quite rough and steep, the 13 or more patented claims or fractions are at elevation of 6500 to 7500*, hence climate is cool and pleasant in summer but rather severe in winter. Country is Arebean Schist with granite intrusives and dykes of later volcanics, veins are mostly strong fissures with filling of quartz and apperite containing sulphides of iron with which gold and silver are associated and often lead, zinc and copper.

I visited this mine several years ago and was favorably impressed by the strength of the veins and the surface showings but all underground workings were inaccessible. In 1926 it was party reopened and one of my engineers from Humboldt made a brief inspection but could see little more than I had and the operators had no money and quit after making a few shipments from the dumps.

The first work here was done in the 1870's when a small but unrecorded production of high grade gold ore was made under very adverse conditions with shipments by burro. Mine was reopened in the 90's when the first road was built and a small stamp-mill hauled in and operated with limited water pumped from a local creek.

A poor recovery was made by emalgemetion and mine and mill shut down in about 1900.

About two years ago, Moores and Maguire took over the claims under bond and lease; the former is a man of considerable mining experience, the latter had some money and has invested about \$25,000 in reopening the property, rebuilding the road, and

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providing first class mining buildings and equipment including two compressors delivering 400 cu. ft. of air at that elevation.

They have shipped 5155 tons of ore with assay value shown on the print and are still shipping but with high working costs, excessive trucking expense, rail freight from Mayer to Hayden, Magma or El Paso and smelter charges they do little more than break even on \$20.00 ore and now realize that the only chance of profit lies in building a local mill and are therefore prepared to lease or sell to parties who can properly develop the mine and install this equipment.

They talk of a sale for \$200,000 on long terms but I pay very little attention to this figure and am satisfied that a long term royalty lease could be obtained with option to purchase at a much lower figure.

Flotation tests of their ore by the Minerals Separation Co. have shown that an iron-concentrate can be made with ratio of 4 to 1 and recovery of 93% of the values while tests by an independent metallurgist are said to have shown that most of the iron can be dropped with a ratio of 15 to 1 and recovery of slightly less than 90% of gold and silver. A composite sample of the December smelter shipments (1500 tons) analysed; Pb. 1%, Zn. 2.3%.

The copper content has usually been only 0.2 or 0.3% but at one point copper is coming in with depth and cut samples have given 2.5 to 3.5% at this location.

Local water in sufficient quantity for a 50 ton mill is lacking but Moores believes that by continuing to sink the winze (shown on print) for another 100 to 200° an ample flow would be obtained. The winze now has a depth of 250° below the main adit but the lower 70° has not been unwatered.

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From the adit to this depth (180°) the vein is said to have a width of 42" and average values from such samples as have been taken of \$12 to \$14 per ton. This work would therefore be a logical development in any event but should it fail to produce sufficient water the mill would probably have to be located about 2 miles from the mine at a much lower elevation. A gravity ropeway would furnish the best means of ore transportation.

The policy of the present operators has not included any substantial development or the blocking out of an ore reserve. As soon as they found pay-ore they mined and shipped it aiming to keep the average grade above \$20.00 per ton and sorting when necessary. Whenever the cost of sorting became too heavy they left that face or stope and mined at some other point and it is my information from Moores and others that they have a great many showings that will assay \$15.00 or better per ton both in surface pits and trenches and in underground workings. Moores believes that a thorough sampling with the cleaning out of some old workings would permit an engineer to estimate as proven or highly probable a minimum of 30,000 tons of \$15.00 ore or a larger tonnage of \$12.00 ore and with excellent chances that further development would greatly increase this tonnage.

Personally I cannot verify this opinion but I have known Moores for 10 years and consider him generally a reliable man and statements made to me by engineers who have recently visited the mine have been uniformly favorable as far as they could judge from appearances.

The question of additional tonnage is wholly problematical but the big chance lies with further development at depth for the contours are extremely steep and the breast of the 1900' long adit has a back of over 700' but the vein only shows near its ends and it is the theory of Moores and others that between these shoots the vein lies in the wall and would have to be

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explored by cross cuts. The showing in the winze is certainly encouraging, if correctly reported, but I think that Moores is inclined to exaggerate the average width which I would not put at over 3' but, - merely as a <u>possibility</u>, - if the ore should prove to be continuous from surface to adit and for a further depth of 200' as indicated in the winze it might amount to 250,000 tons with an average value of \$12.00, - perhaps \$15.00 per ton.

There are several other veins on the claims, some partly developed by surface pits and short adits and one which is supposed to be the extension of the original Crown King vein is particularly strong. Assays in the pits are generally not so good as from the mine but many run \$6.00 to \$12.00 and very few blanks are reported.

As a very rough estimate of operating costs, based on past records and my knowledge of local conditions, I should figure mining and current development at \$4.00 per ton, milling (at 50 tons per day) at \$1.50, transportation and treatment of concentrates, 10% royalty, smelter losses and penalties, selling expense and overhead at \$3.30 (with the higher ratio of concentration) with net returns of \$10.80 (if a \$12.00 head could be maintained leaving a profit of \$2.00 per ton on this basis or about \$4.50 per ton if the mill heads could be kept up to \$15.00.

The capital or preliminary expense may also be very roughly figured as follows:

Engineers examination, clearing old drifts & sampling to determine if further investigation is justified. \$1000.00 Check examination, - say 1000.00

Development of ore, including 3 cross cuts from main adit, deepening winze 200°, cleaning other openings in mine and work on or near surface

50 ton mill and accessories

Incidental

20,000.00

50,000.00

3,000.00

\$75,000.00

Total If insufficient water found in winze add for mill site, ropeway (to be secured 2nd hand locally) & water supply

25;000.00

Total

The above estimates do not include working capital but if your present clients should be interested in this venture the cost of the mill would be reduced to the expense of moving it from its present site and erecting it at or near the mine. The present mine equipment and camp accomodations should be nearly or quite sufficient to permit the production of 50 tons per day provided the mine were properly opened up in advance.

Obviously the parties who consider such an investment should not properly be called upon to pay for the preliminary engineering examination and report which should be furnished by the owners or operators but neither of them are in a position to do so. Moores and Maguire claim to have no spare cash whatever and the owner whom I know slightly is a lady in very moderate circumstances to whom this property came by inheritance..'I have every reason to believe that the titles are clear and valid.

The great danger in every mine in the Crown King or neighboring districts lies in the fact that the pay ore may be confined to comparatively short shoots spaced along the vein and with stretches of worthless material intervening; in which case the tonnage would be greatly reduced and mining expenses increased to a point where the property would not be attractive unless the average grade proved to be much richer than I have assumed.

This matter as well as some other points of importance could be determined by the preliminary examination which in my opinion is well justified by the present showings, and assuming that a favorable option to lease could be definitely secured. If the property were taken over the cost of this examination could quite certainly be deducted from subsequent royalty all of which would of course apply on any purchase price that might be agreed upon.

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The assays on the print, (which can only be read with a glass) are as per attached list,- if you are not interested in this mine kindly return the print as in that case I have promised to give it back to Moores.

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met 4 has blave Russell Panels (?)

raise .42 .38 11. 3' of 10' width, raise from 150' level .45 .20 12. Approximately 500' South of Gladiator Shaft. .28 3.60 13. 300' South from surface Gladiator Shaft. .28 3.60 13. 300' South from surface Gladiator Shaft. 2' 1.16 3.92 14. 30' West of No. 12 shaft, face 2'2" .20 2.88 15. 25' North of No. 12, surface 30" .80 3.36 16. War Eagle No. 1, 70' level up 20' 3' .32 4.65 17. War Eagle No. 3, Surface 2' .24 1.42 18. War Eagle No. 2, 30' shaft 2' .24 1.06 19. War Eagle No. 2, dump, 6 tons .72 8.80 20. War Eagle No. 1, 100' level, 160' NW Of No. 2 .24 .26 21. War Eagle No. 1, 100' level, North of No. 1 .60 2.00 22. War Eagle No. 1, 100' level, 50' North Of shaft. 2' .98 .02 23. <th></th> <th>LOCATION</th> <th>WIDTH</th> <th>AU.</th> <th>AG.</th>		LOCATION	WIDTH	AU.	AG.
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10. East of quartz 150' level, bottom of raise .42 .38 11. 3' of 10' width, raise from 150' level .45 .20 12. Approximately 500' South of Gladiator Shaft. .28 3.60 13. 300' South from surface Gladiator Shaft. .28 3.60 13. 300' South from surface Gladiator Shaft. 2' 1.16 3.92 14. 30' West of No. 12 shaft, face 2'2" .20 2.88 15. 25' North of No. 12, surface 30" .80 3.36 16. War Eagle No. 1, 70' level up 20' 3' .32 4.65 17. War Eagle No. 2, S0' shaft 2' .24 1.42 18. War Eagle No. 2, 30' shaft 2' .24 1.06 19. War Eagle No. 1, 100' level, North of No. 2 - .24 .26 20. War Eagle No. 1, 100' level, North of No. 1 - .60 2.00 22. War Eagle No. 1, 100' level, S0' North of Shaft. 2' .98 4.02 23. War Eagle No. 1, 100' level, S. drift 3' .5	8.	200' Level, 150' from South face	20"	.72	2.88
raise .42 .38 11. 3' of 10' width, raise from 150' level .45 .20 12. Approximately 500' South of Gladiator Shaft. .28 3.60 13. 300' South from surface Gladiator Shaft. .28 3.60 13. 300' South from surface Gladiator Shaft. 2' 1.16 3.92 14. 30' West of No. 12 shaft, face 2'2" .20 2.98 15. 25' North of No. 12, surface 30" .80 3.36 16. War Eagle No. 1, 70' level up 20' 3' .32 4.65 17. War Eagle No. 3, Surface 2' .24 1.42 18. War Eagle No. 2, 30' shaft 2' .24 1.42 19. War Eagle No. 2, 100' level, 160' NW of No. 2 .24 .26 21. War Eagle No. 1, 100' level, North of No. 1 .60 2.00 22. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 23. War Eagle No. 1, 100' level, 5.0' North of shaft. .98 .02 24. </td <td>9.</td> <td>180' North from raise, bottom of vein</td> <td>3*</td> <td>.32</td> <td>2.06</td>	9.	180' North from raise, bottom of vein	3*	.32	2.06
12. Approximately 500' South of Gladiator Shaft. .28 3.60 13. 300' South from surface Gladiator Shaft. 2' 1.16 3.92 14. 30' West of No. 12 shaft, face 2'2" .20 2.88 15. 25' North of No. 12, surface 30" .80 3.36 16. War Eagle No. 1, 70' level up 20' 3' .32 4.65 17. War Eagle No. 3, Surface 2' .24 1.42 18. War Eagle No. 2, 30' shaft 2' .24 1.42 19. War Eagle No. 2, 30' shaft 2' .24 1.42 19. War Eagle No. 2, 100' level, 160' NW of No. 2 .24 .26 20. War Eagle No. 1, 100' level, North of No. 1 .60 2.00 22. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 23. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 23. War Eagle No. 1, 100' level, S. drift 3' .52 3.14 24. War Eagle No. 1, 100' level, S. drift 3' .52 <td>LO.</td> <td></td> <td></td> <td>.42</td> <td>.38</td>	LO.			.42	.38
Shaft .28 3.60 13. 300' South from surface Gladiator Shaft. 2' 1.16 3.92 14. 30' West of No. 12 shaft, face 2'2" .20 2.88 15. 25' North of No. 12 shaft, face 30" .80 3.36 16. War Eagle No. 1, 70' level up 20' 3" .32 4.65 17. War Eagle No. 3, Surface 2' .24 1.42 18. War Eagle No. 2, 30' shaft 2' .24 1.42 18. War Eagle No. 2, dump, 8 tons .72 8.80 20. War Eagle No. 2, 100' level, 160' NW of No. 2 .24 .26 21. War Eagle No. 2, 100' level, North of No. 1 .60 2.00 22. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 23. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 23. War Eagle No. 1, 100' level, 5. drift 3' .52 3.14 24. War Eagle No. 1, 100' level , 5. drift 3' .52 3.14 24.	11.	3' of 10' width, raise from 150' level		.45	.20
Shaft. 2' 1.16 3.92 14. 30' West of No. 12 shaft, face 2'2" .20 2.88 15. 25' North of No. 12, surface 30" .80 3.36 16. War Eagle No. 1, 70' level up 20' 3' .32 4.65 17. War Eagle No. 3, Surface 2' .24 1.42 18. War Eagle No. 2, 30' shaft 2' .24 1.42 19. War Eagle No. 2, dump, 8 tons .72 8.80 20. War Eagle No. 1, 100' level, 160' NW of No. 2 .84 .26 21. War Eagle No. 2, 100' level, North of No. 1 .60 2.00 22. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 23. War Eagle No. 1, 100' level, 50' North of shaft. .98 4.02 23. War Eagle No. 1, 100' level, 5. drift .24 1.66 24. War Eagle No. 1, 100' level, 5. drift .24 1.66 25. War Eagle No. 1, 100' level, 5. drift .52 3.14	12.			.28	3.60
15. 25' North of No. 12, surface 30" .80 3.36 16. War Eagle No. 1, 70' level up 20' 3' .32 4.65 17. War Eagle No. 3, Surface 2' .24 1.42 18. War Eagle No. 2, 30' shaft 2' .24 1.42 18. War Eagle No. 2, 30' shaft 2' .24 1.42 19. War Eagle No. 2, dump, 8 tons .72 8.80 20. War Eagle No. 1, 100' level, 160' NW of No. 2 .24 .26 21. War Eagle No. 2, 100' level, North of No. 1 .60 2.00 22. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 23. War Eagle No. 1, 100' level, 50' North of shaft. .98 4.02 23. War Eagle No. 1, 100' level, S. drift 3' .52 3.14 24. War Eagle No. 1, 100' level , S. drift 3' .52 3.14 25. War Eagle No. 1, cut in North shaft, .24 1.66	L3.		21	1.16	3.92
16. War Eagle No. 1, 70' level up 20' 3' .32 4.65 17. War Eagle No. 3, Surface 2' .24 1.42 18. War Eagle No. 2, 30' shaft 2' .24 1.06 19. War Eagle No. 2, dump, 8 tons .72 8.80 20. War Eagle No. 1, 100' level, 160' NW of No. 2 .24 .26 21. War Eagle No. 2, 100' level, North of No. 1 .60 2.00 22. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 23. War Eagle - cut in shaft, 100' level 4' .24 1.66 24. War Eagle No. 1, 100' level, 50 ' North of shaft. .98 4.02 25. War Eagle No. 1, 100' level , S. drift .52 3.14	.4 .	30' West of No. 12 shaft, face	2*2*	.20	2.88
17. War Eagle No. 3, Surface 2' .24 1.42 18. War Eagle No. 2, 30' shaft 2' .24 1.06 19. War Eagle No. 2, dump, 8 tons .72 8.80 20. War Eagle No. 1, 100' level, 160' NW of No. 2 .24 .26 21. War Eagle No. 2, 100' level, North of No. 1 .60 2.00 22. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 23. War Eagle - cut in shaft, 100' level 4' .24 1.66 24. War Eagle No. 1, 100' level, S. drift 3' .52 3.14 25. War Eagle No. 1, cut in North shaft, 3' .52 3.14	15.	25' North of No. 12, surface	30*	.80	3.36
18. War Eagle No. 2, 30' shaft 2' .24 1.06 19. War Eagle No. 2, dump, 8 tons .72 8.80 20. War Eagle No. 1, 100' level, 160' NW of No. 2 .24 .26 21. War Eagle No. 2, 100' level, North of No. 1 .60 2.00 22. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 23. War Eagle - cut in shaft, 100' level 4' .24 1.66 24. War Eagle No. 1, 100' level, S. drift 3' .52 3.14 25. War Eagle No. 1, cut in North shaft, 3' .52 3.14	.6.	War Eagle No. 1, 70' level up 20'	3*	.32	4.65
19. War Eagle No. 2, dump, 8 tons .72 8.80 20. War Eagle No. 1, 100' level, 160' NW of No. 2 .24 .26 21. War Eagle No. 2, 100' level, North of No. 1 .60 2.00 22. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 23. War Eagle - cut in shaft, 100' level 4' .24 1.66 24. War Eagle No. 1, 100' level, S. drift 3' .52 3.14 25. War Eagle No. 1, cut in North shaft, 100' level, 51 100' level, 51 100' level, 52 1.14	.7.	War Eagle No. 3, Surface	2*	.24	1.42
20. War Eagle No. 1, 100' level, 160' NW of No. 2 .24 .26 21. War Eagle No. 2, 100' level, North of No. 1 .60 2.00 22. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 23. War Eagle - cut in shaft, 100' level 4' .24 1.66 24. War Eagle No. 1, 100' level , S. drift 3' .52 3.14 25. War Eagle No. 1, cut in North shaft, 100' level , S. drift 3' .52 3.14	18.	War Eagle No. 2, 30' shaft	2*	.24	1.06
of No. 224 .26 21. War Eagle No. 2, 100' level, North of No. 160 2.00 22. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 23. War Eagle - cut in shaft, 100' level 4' .24 1.66 24. War Eagle No. 1, 100' level , S. drift 3' .52 3.14 25. War Eagle No. 1, cut in North shaft,	.9.	War Eagle No. 2, dump, 8 tons		.72	8.80
No. 1 .60 2.00 22. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 23. War Eagle - cut in shaft, 100' level 4' .24 1.66 24. War Eagle No. 1, 100' level , S. drift 3' .52 3.14 25. War Eagle No. 1, cut in North shaft,	30.			.24	.26
of shaft. 2' .98 4.02 23. War Eagle - cut in shaft, 100' level 4' .24 1.66 24. War Eagle No. 1, 100' level , S. drift 3' .52 3.14 25. War Eagle No. 1, cut in North shaft,	81.			.60	2.00
24. War Eagle No. 1, 100° level , S. drift 3° .52 3.14 25. War Eagle No. 1, cut in North shaft,	82.		27	.98	4.02
25. War Eagle No. 1, cut in North shaft,	23.	War Eagle - cut in shaft, 100' level	4*	.24	1.66
	24.	War Eagle No. 1, 100' level , S. drift	3'	.52	3.14
	5.		21	.40	4.90

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	LOCATION	WIDTH	AU.	AG.
26.	War Eagle - discovery shaft	2*	.20	3.10
27.	War Eagle - South tunnel, cut in bottom.	2*	.40	2.64
28.	War Eagle - South tunnel, cut No. 8	2*	,38	2.88
29.	5 tons of ore		1,24	10.14
30 .	Grab of dump-War Eagle		.28	2.01
31.	Gladiator shaft dump		,24	1.76
32.	Glediator tunnel ore dump		.20	5.90

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I am not sure that the description of some of these samples has been correctly copied as the photostat is very hard to read; Also I know nothing of the methods by which they were taken.

Shipping right along them 19440 using Solden Turky mile which they have prochased. Has been quite GLADIATOR AND WAR BAGLE a good title produces Some six miles from Crown King which in turn is about 53 miles (by road) south from Prescott. Road from Crown King is quite rough and steep, the 13 or more patented claims or fractions are at elevation of 6500 to 7500', hence climate is cool and pleasant in summer but rather severe in winter. Country is Arenean Schist with granite intrusives and dykes of later volcanics, veins are mostly strong fissures with filling of quartz and apperite containing sulphides of iron with which gold and silver are associated and often lead, zinc and copper.

I visited this mine several years ago and was favorably impressed by the strength of the veins and the surface showings but all underground workings were inaccessible. In 1926 it was party reopened and one of my engineers from Humboldt made a brief inspection but could see little more than I had and the operators had no money and quit after making a few shipments from the dumps.

The first work here was done in the 1870's when a small but unrecorded production of high grade gold ore was made under very adverse conditions with shipments by burro. Mine was reopened in the 90's when the first road was built and a small stamp-mill hauled in and operated with limited water pumped from a local creek.

A poor recovery was made by amalgamation and mine and mill shut down in about 1900.

About two years ago, Moores and Maguire took over the claims under bond and lease; the former is a man of considerable mining experience, the latter had some money and has invested about \$25,000 in reopening the property, rebuilding the road, and

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providing first class mining buildings and equipment including two compressors delivering 400 cu. ft. of air at that elevation.

They have shipped 5155 tons of ore with assay value shown on the print and are still shipping but with high working costs, excessive trucking expense, rail freight from Mayer to Hayden, Magma or El Paso and smelter charges they do little more than break even on \$20.00 ore and now realize that the only chance of profit lies in building a local mill and are therefore prepared to lease or sell to parties who can properly develop the mine and install this equipment.

They talk of a sale for \$200,000 on long terms but I pay very little attention to this figure and am satisfied that a long term royalty lease could be obtained with option to purchase at a much lower figure.

Flotation tests of their ore by the Minerals Separation Co. have shown that an iron-concentrate can be made with ratio of 4 to 1 and recovery of 93% of the values while tests by an independent metallurgist are said to have shown that most of the iron can be dropped with a ratio of 15 to 1 and recovery of slightly less than 90% of gold and silver. A composite sample of the December smelter shipments (1500 tons) analysed; Pb. 1%, Zn. 2.3%.

The copper content has usually been only 0.2 or 0.3% but at one point copper is coming in with depth and cut samples have given 2.5 to 3.5% at this location.

Local water in sufficient quantity for a 50 ton mill is lacking but Moores believes that by continuing to sink the winze (shown on print) for another 100 to 200° an ample flow would be obtained. The winze now has a depth of 250° below the main adit but the lower 70° has not been unwatered.

From the adit to this depth (180°) the vein is said to have a width of 42" and average values from such samples as have been taken of \$12 to \$14 per ton. This work would therefore be a logical development in any event but should it fail to produce sufficient water the mill would probably have to be located about 2 miles from the mine at a much lower elevation. A/gravity ropeway would furnish the best means of ore transportation.

The policy of the present operators has not included any substantial development or the blocking out of an ore reserve. As soon as they found pay-ore they mined and shipped it aiming to keep the average grade above \$20.00 per ton and sorting when necessary. Whenever the cost of sorting became too heavy they left that face or stope and mined at some other point and it is my information from Moores and others that they have a great many showings that will assay \$15.00 or better per ton both in surface pits and trenches and in underground workings. Moores believes that a thorough sampling with the cleaning out of some old workings would permit an engineer to estimate as proven or highly probable a minimum of 30,000 tons of \$15.00 ore or a larger tonnage of \$12.00 ore and with excellent chances that further development would greatly increase this tonnage.

Personally I cannot verify this opinion but I have known Moores for 10 years and consider him generally a reliable man and statements made to me by engineers who have recently visited the mine have been uniformly favorable as far as they could judge from appearances.

The question of additional tonnage is wholly problematical but the big chance lies with further development at depth for the contours are extremely steep and the breast of the 1900' long adit has a back of over 700' but the vein only shows near its ends and it is the theory of Moores and others that between these shoots the vein lies in the wall and would have to be

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explored by cross cuts. The showing in the winze is certainly encouraging, if correctly reported, but I think that Moores is inclined to exaggerate the average width which I would not put at over 3' but, - merely as a <u>possibility</u>, - if the ore should prove to be continuous from surface to adit and for a further depth of 200' as indicated in the winze it might amount to 250,000 tons with an average value of \$12.00, - perhaps \$15.00 per ton.

There are several other veins on the claims, some partly developed by surface pits and short adits and one which is supposed to be the extension of the original Crown King vein is particularly strong. Assays in the pits are generally not so good as from the mine but many run \$6.00 to \$12.00 and very few blanks are reported.

As a very rough estimate of operating costs, based on past records and my knowledge of local conditions, I should figure mining and current development at \$4.00 per ton, milling (at 50 tons per day) at \$1.50, transportation and treatment of concentrates, 10% royalty, smelter losses and penalties, selling expense and overhead at \$3.30 (with the higher ratio of concentration) with net returns of \$10.80 (if a \$12.00 head could be maintained leaving a profit of \$2.00 per ton on this basis or about \$4.50 per ton if the mill heads could be kept up to \$15.00.

The capital or preliminary expense may also be very roughly figured as follows: Engineers examination, clearing old drifts & sampling to determine if further investigation is justified. \$1000.00

Check examination, - say

Development of ore, including 3 cross cuts from main adit, deepening winze 200', cleaning other openings in mine and work on or near surface 20,000.00

50 ton mill and accessories

Incidental

Total If insufficient water found in winze add for mill site, ropeway (to be secured 2nd hand locally) & water supply

25;000.00 \$100,000.00

1000.00

50,000.00

3,000.00

\$75,000.00

Total

The above estimates do not include working capital but if your present clients should be interested in this venture the cost of the mill would be reduced to the expense of moving it from its present site and erecting it at or near the mine. The present mine equipment and camp accomodations should be nearly or quite sufficient to permit the production of 50 tons per day provided the mine were properly opened up in advance.

Obviously the parties who consider such an investment should not properly be called upon to pay for the preliminary engineering examination and report which should be furnished by the owners or operators but neither of them are in a position to do so. Moores and Maguire claim to have no spare cash whatever and the owner whom I know slightly is a lady in very moderate circumstances to whom this property came by inheritance.. I have every reason to believe that the titles are clear and valid.

The great danger in every mine in the Crown King or neighboring districts lies in the fact that the pay ore may be confined to comparatively short shoots spaced along the vein and with stretches of worthless material intervening; in which case the tonnage would be greatly reduced and mining expenses increased to a point where the property would not be attractive unless the average grade proved to be much richer than I have assumed.

This matter as well as some other points of importance could be determined by the preliminary examination which in my opinion is well justified by the present showings, and assuming that a favorable option to lease could be definitely secured. If the property were taken over the cost of this examination could quite certainly be deducted from subsequent royalty all of which would of course apply on any purchase price that might be agreed upon.

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The assays on the print, (which can only be read with a glass) are as per attached list,- if you are not interested in this mine kindly return the print as in that case I have promised to give it back to Moores.

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upied

DISTRICT: Crown King

PROPERTY: War Eagle

LOCATION: 7000 feet by very rough road above Lincoln Mill, which in turn is four miles by rough road from Crown King. OPERATOR: Fike and Starbird, Lessees.

VISITED: August 6, 1926, by D. M. Barringer, Jr.

The vein is developed at two places, designated as the upper and lower shafts. The collar of the lower shaft is said to be 50' below the X-cut tunnel at the lower shaft, and the workings are somw 800 feet apart. The X-cut tunnel, running N 80°W, encounters the upper shaft some 60 feet below the surface, and is rather badly caved at this point. A drift runs about 100' south and 150' north, developing a shoot 12" to 30" in width, 150' in length, and said to assay \$16 per ton in Au and Ag. No stoping has been done, unless from some inaccessible level in the shaft. I was given to understand there had been none. About 50# of sorted ore taken from the dump for milling test.

The lower shaft, some 800' N of the upper, is caved. The only access to the workings was through a stope from the 100 level which had holed surface about 100' N of the shaft. Between it and the shaft is a pillar, containing some 200 tons ($2\frac{1}{2}$ ' to 3' wide) which is claimed to run \$14.00. The ore is largely oxidized, though some galena and zinc blende were seen in it.

The shaft is accessible to the 200' level, below which water stands. On the 200 the same shoot as above is visible, tho $\frac{1}{2}$ reduced to 12^{n} ave. thickness. The small amount of stoping seems to indicate that the values have decreased as well, and the ore is still pretty thoroughly oxidized.

Fike & Starbird propose milling the dumps at the two shafts, and the pillar in the lower shaft workings, also possibly some of the shoot in the upper shaft. Their haul to mill would average \$1.00; concs. to Crown King about \$2.00; and to Middleton about \$2.00 more. Freight to Humboldt \$1.00 on \$20.00 ore. They also propose milling some tailings and possibly ore from the Gladiator mine, report on which q. v.

Samples from dumps at upper and lower shafts (about50' each) sent to Tooele. Together they ran: Au, ; Ag, ; Pb, ; Cu, ; Fe, Zn; ; S, ; CaO, ; Insol, ;

AMB/r.

3. 200° level - South face of drift 16° .40 2.72 4. Top of 70° raise - 200° level north side 1.35 2.44 5. Top of 70° raise - 200° level south side .96 2.80 6. 200° Level, 40° winze and 10° North 3° .36 4.2 7. 200° Level, 40° winze, South side .72 3.40 8. 200° Level, 150° from South face 20° .72 2.88 9. 180° North from raise, bottom of vein 3° .33 2.06 8. 20° Level, 150° level, bottom of raise .42 .38 9. 180° North from sufface fixed level .42 .38 10. East of quartz 150° level, bottom of raise .42 .38 11. 3° of 10° width, raise from 150° level .42 .38 12. 3° of 10° width, raise from 150° level .42 .38 3. 300° South from surface Gladiator Shaft. 2° 1.16 5.92 2. 2.5 25° North of No. 12, surface 30°		LOCATION	WI DTH	AU.	AG.
3. 200' level - South face of drift 16" .40 2.72 4. Top of 70' raise - 200' level north side 1.35 2.44 5. Top of 70' raise - 200' level south side .96 2.80 6. 200' Level, 40' winze and 10' North 3' .35 4.2 7. 200' Level, 40' winze and 10' North 3' .35 4.2 8. 200' Level, 40' winze, South side .72 2.88 9. 180' North from raise, bottom of vein 3' .33 2.06 0. East of quartz 150' level, bottom of raise .42 .38 1. 3' of 10' width, raise from 150' level .42 .38 1. 3' of 10' width, raise from 150' level .42 .38 2. Approximately 500' South of Gladiator Shaft. 2' 1.16 3.92 3. 300' South from surface Cladiator Shaft. 2' 1.16 3.92 4. 30' West of No. 12, surface 30''''''''''''''''''''''''''''''''''''	1.		2*	0.12	1.04
4. Top of 70' raise - 200' level north side 1.36 2.44 5. Top of 70' raise - 200' level south side .96 2.30 6. 200' Level, 40' winze and 10' North 3' .36 4.2 7. 200' Level, 40' winze, South side .72 3.40 8. 200' Level, 150' from South face 20" .72 2.88 9. 180' North from raise, bottom of vein 3' .38 2.06 0. East of quartz 150' level, bottom of raise .42 .38 1. 5' of 10' width, raise from 150' level .42 .38 1. 5' of 10' width, raise from 150' level .45 .20 2. Approximately 500' South of Gladiator Shaft. .28 3.60 3. 300' South from surface Gladiator Shaft. 2' .20 2.88 5. 25' North of No. 12, surface 30" .32 4.65 5. 25' North of No. 12, surface 2' .24 1.42 6. War Eagle No. 2, 30' shaft 2' .24 1.42	2.	300' level- South face hanging wall	12"	.34	2.14
side 1.36 2.44 5. Top of 70' raise - 200' level south side96 2.80 6. 200' Level, 40' winze and 10' North 3' .36 4.2 7. 200' Level, 40' winze, South side72 3.40 8. 200' Level, 150' from South face 20" .72 2.88 9. 180' North from raise, bottom of vein 3' .32 2.06 1. 3' of 10' width, raise from 150' level42 .38 1. 3' of 10' width, raise from 150' level45 .20 8. Approximately 500' South of Gladiator Shaft28 3.60 5. 300' South from surface Gladiator Shaft. 2' 1.16 3.92 4. 30' West of No. 12 shaft, face 2'2" .20 2.88 5. 25' North of No. 12, surface 30" .80 3.36 6. War Eagle No. 1, 70' level up 20' 3' .32 4.65 7. War Eagle No. 2, 30' shaft 2' .24 1.06 9. War Eagle No. 2, 100' level, 160' NW 10. War Eagle No. 1, 100' level, 50' North 11. War Eagle No. 1, 100' level, 50' North 12. War Eagle No. 1, 100' level, 50' North 13. 352 4.05 14. War Eagle No. 1, 100' level, 50' North 14. War Eagle No. 1, 100' level, 50' North 15. War Eagle No. 1, 100' level, 50' North 16. War Eagle No. 1, 100' level, 50' North 17. War Eagle No. 1, 100' level, 50' North 18. War Eagle No. 1, 100' level, 50' North 18. War Eagle No. 1, 100' level, 50' North 19. War Eagle No. 1, 100' level, 50' North 10. War Eagle No. 1, 100' level, 50' North 10. War Eagle No. 1, 100' level, 50' North 10. War Eagle No. 1, 100' level, 50' North 18. War Eagle No. 1, 100' level, 50' North 18. War Eagle No. 1, 100' level, 50' North 19. 4.02 19. War Eagle No. 1, 100' level, 50' North 10. 4. War Eagle No. 1, 100' level, 50' North 10. 52 3.14 10. 52	3.	200' level - South face of drift	16"	.40	2.72
side96 2.80 6. 200' Level, 40' winze and 10' North 3' .36 4.2 7. 200' Level, 40' winze, South side72 3.40 8. 200' Level, 150' from South face 20" .72 2.88 9. 180' North from raise, bottom of vein 3' .32 2.06 1. 5' of lo' width, raise from 150' level42 .38 1. 5' of lo' width, raise from 150' level45 .20 8. Approximately 500' South of Gladiator Shaft28 3.60 3. 300' South from surface Gladiator Shaft. 2' 1.16 3.92 4. 30' West of No. 12 shaft, face 2'2" .20 2.88 5. 25' North of No. 12, surface 30" .80 3.36 6. War Eagle No. 1, 70' level up 20' 3' .32 4.65 7. War Eagle No. 2, 30' shaft 2' .24 1.42 8. War Eagle No. 2, 30' shaft 2' .24 1.42 8. War Eagle No. 2, 100' level, 160' NW of No. 160 2.00 War Eagle No. 2, 100' level, North of No. 160 2.00 2. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 3. War Eagle No. 1, 100' level, S. drift 3' .52 3.14 3. War Eagle No. 1, 100' level, S. drift 3' .52 3.14 3. War Eagle No. 1, 100' level, S. drift 3' .52 3.14 3. War Eagle No. 1, 100' level, S. drift 3' .52 3.14	4.			1.36	2.44
7. 200° Level, 40° winze, South side .72 3.40 8. 200° Level, 150° from South face 20° .72 2.88 9. 180° North from raise, bottom of vein 3° .32 2.06 0. East of quartz 150° level, bottom of raise .42 .38 1. 5° of 10° width, raise from 150° level .45 .20 2. Approximately 500° South of Gladiator Shaft. .28 3.60 3. 300° South from surface Gladiator Shaft. .28 3.60 3. 300° South from surface Gladiator Shaft. 2° 1.16 3.92 4. 30° West of No. 12 shaft, face 2°2* .20 2.88 5. 25° North of No. 12, surface 30° .32 4.65 6. War Eagle No. 1, 70° level up 20° 3° .32 4.65 7. War Eagle No. 2, 30° shaft 2° .24 1.42 8. War Eagle No. 2, 00° level, 160° NW of No. 2 .24 1.22 8. War Eagle No. 1, 100° level, North of No. 1 .26 .200 .	5.			.96	2.80
8. 200' Level, 150' from South face 20" .72 2.88 9. 180' North from raise, bottom of vein 3' .32 2.06 10. East of quartz 150' level, bottom of raise .42 .38 11. 3' of 10' width, raise from 150' level .42 .38 11. 3' of 10' width, raise from 150' level .45 .20 22. Approximately 500' South of Gladiator Shaft. .28 3.60 3. 300' South from surface Gladiator Shaft. 2' 1.16 3.92 4. 30' West of No. 12 shaft, face 2'2" .20 2.88 5. 25' North of No. 12, surface 30" .30 3.36 6. War Eagle No. 3, Surface 2' .24 1.42 7. War Eagle No. 2, 30' shaft 2' .24 1.42 9. War Eagle No. 2, 100' level, 160' NW of No. 2 .24 .26 10. War Eagle No. 1, 100' level, North of No. 1 .60 2.00 12. War Eagle No. 1, 100' level, 50' North of shaft. 2' <td< td=""><td>6.</td><td>200' Level, 40' winze and 10' North</td><td>3*</td><td>.36</td><td>4.2</td></td<>	6.	200' Level, 40' winze and 10' North	3*	.36	4.2
9. 180° North from raise, bottom of vein 3° .32 2.06 0. East of quartz 150° level, bottom of raise .42 .38 1. S' of 10° width, raise from 150° level .45 .20 2. Approximately 500° South of Gladiator Shaft. .28 3.60 3. 300° South from surface Gladiator Shaft. .28 3.60 3. 300° South from surface Gladiator Shaft. 2° .28 3.92 4. 30° West of No. 12 shaft, face 2°2° .20 2.88 5. 25° North of No. 12, surface 30° .30 3.36 6. War Eagle No. 1, 70° level up 20° 3° .32 4.65 7. War Eagle No. 2, 30° shaft 2° .24 1.42 8. War Eagle No. 2, dump, 8 tons .72 8.80 9. War Eagle No. 1, 100° level, 160° NW of No. 1 .60 2.00 8. War Eagle No. 1, 100° level, So' North of No. 1 .60 2.00 8. War Eagle No. 1, 100° level, So' North of Shaft. .98 4.02	7.	200' Level, 40' winze, South side	65.107	.72	3.40
0. East of quartz 150' level, bottom of raise .42 .38 1. 3' of 10' width, raise from 150' level .45 .20 2. Approximately 500' South of Gladiator Shaft. .28 3.60 3. 300' South from surface Gladiator Shaft. .28 3.60 3. 300' South from surface Gladiator Shaft. 2' 1.16 3.92 4. 30' West of No. 12 shaft, face 2'2" .20 2.88 5. 25' North of No. 12, surface 30" .80 3.36 6. War Eagle No. 1, 70' level up 20' 3' .32 4.65 7. War Eagle No. 2, 30' shaft 2' .24 1.42 8. War Eagle No. 2, 30' shaft 2' .24 1.42 9. War Eagle No. 2, dump, 8 tons .72 8.60 10. War Eagle No. 1, 100' level, 160' NW of No. 1 .26 .20 12. War Eagle No. 1, 100' level, So' North of No. 1 .60 2.00 12. War Eagle No. 1, 100' level, So' North of Shaft. .98 4.02	8.	200' Level, 150' from South face	80*	.72	2.88
raise .42 .38 1. 3' of 10' width, raise from 150' level .45 .20 2. Approximately 500' South of Gladiator Shaft. .28 3.60 3. 300' South from surface Gladiator Shaft. .28 3.60 3. 300' South from surface Gladiator Shaft. 2' 1.16 3.92 4. 30' West of No. 12 shaft, face 2'2" .20 2.88 5. 25' North of No. 12, surface 30" .80 3.36 6. War Eagle No. 1, 70' level up 20' 3' .32 4.65 7. War Eagle No. 2, Surface 2' .24 1.42 8. War Eagle No. 2, 30' shaft 2' .24 1.42 9. War Eagle No. 2, dump, 8 tons .72 8.80 10. War Eagle No. 1, 100' level, 160' NW of Ho. 2 .24 .26 21. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 23. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 23.	9.	180* North from raise, bottom of vein	3*	.32	2.06
2. Approximately 500' South of Gladiator Shaft. .28 3.60 3. 300' South from surface Gladiator Shaft. 2' 1.16 3.92 4. 30' West of No. 12 shaft, face 2'2" .20 2.88 5. 25' North of No. 12, surface 30" .80 3.36 5. 25' North of No. 12, surface 30" .80 3.36 6. War Eagle No. 1, 70' level up 20' 3' .32 4.65 7. War Eagle No. 3, Surface 2' .24 1.42 8. War Eagle No. 2, 30' shaft 2' .24 1.42 9. War Eagle No. 2, dump, 8 tons .72 8.80 9. War Eagle No. 1, 100' level, 160' NW of No. 2 .26 9. War Eagle No. 1, 100' level, North of No. 1 .60 2.00 9. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 9. War Eagle No. 1, 100' level, 50' North of shaft. .98 4.02 9. War Eagle No. 1, 100' level, 50' North of shaft. .98 4.02 9.	10.			.42	.38
Shaft. .28 3.60 3. 300' South from surface Gladiator Shaft. 2' 1.16 3.92 4. 30' West of No. 12 shaft, face 2'2" .20 2.38 5. 25' North of No. 12, surface 30" .80 3.36 5. 25' North of No. 12, surface 30" .80 3.36 5. 25' North of No. 12, surface 30" .80 3.36 5. 25' North of No. 12, surface 2'2" .24 1.65 5. 25' North of No. 3, Surface 2' .24 1.42 5. War Eagle No. 2, 30' shaft 2' .24 1.42 5. War Eagle No. 2, dump, 8 tons .72 8.80 50. War Eagle No. 1, 100' level, 160' NW of No. 2 .24 .26 61. War Eagle No. 2, 100' level, North of No. 1 .60 2.00 82. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 83. War Eagle No. 1, 100' level , S. drift 3' .52 3.14 84. War Eagle No. 1,	11.	3' of 10' width, raise from 150' level		.45	.20
Shaft. 2* 1.16 3.92 4. 30' West of No. 12 shaft, face 2'2" .20 2.88 5. 25' North of No. 12, surface 30" .80 3.36 5. 25' North of No. 12, surface 30" .80 3.36 5. 25' North of No. 12, surface 30" .80 3.36 5. 25' North of No. 1, 70' level up 20' 3" .32 4.65 5. War Eagle No. 1, 70' level up 20' 3" .32 4.65 7. War Eagle No. 3, Surface 2" .24 1.42 8. War Eagle No. 2, 30' shaft 2" .24 1.42 9. War Eagle No. 2, dump, 8 tons .72 8.80 8. War Eagle No. 1, 100' level, 160' NW of No. 2 .24 .26 8. War Eagle No. 2, 100' level, North of No. 1 .60 2.00 82. War Eagle No. 1, 100' level, 50' North of shaft. 2" .98 4.02 83. War Eagle No. 1, 100' level, 5. drift 3" .52 3.14 84. War Eagle No.	12.			.28	3.60
5. 25' North of No. 12, surface 30" .80 3.36 .6. War Eagle No. 1, 70' level up 20' 3' .32 4.65 .7. War Eagle No. 3, Surface 2' .24 1.42 .8. War Eagle No. 2, 30' shaft 2' .24 1.42 .8. War Eagle No. 2, 30' shaft 2' .24 1.06 .9. War Eagle No. 2, dump, 8 tons .72 8.80 80. War Eagle No. 1, 100' level, 160' NW of No. 2 .24 .26 81. War Eagle No. 2, 100' level, North of No. 1 .60 2.00 82. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 83. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 83. War Eagle - cut in shaft, 100' level 4' .24 1.66 84. War Eagle No. 1, 100' level , 5. drift 3' .52 3.14 85. War Eagle No. 1, cut in North shaft, 5' .52 3.14	13.		23	1.16	3.92
.6. War Eagle No. 1, 70° level up 20° 3° .32 4.65 .7. War Eagle No. 3, Surface 2° .24 1.42 .8. War Eagle No. 2, 30° shaft 2° .24 1.42 .8. War Eagle No. 2, 30° shaft 2° .24 1.42 .9. War Eagle No. 2, 30° shaft 2° .24 1.06 .9. War Eagle No. 2, dump, 8 tons .72 8.80 .0. War Eagle No. 1, 100° level, 160° NW of No. 2 .24 .26 .0. War Eagle No. 2, 100° level, North of No. 1 .60 2.00 .2. War Eagle No. 1, 100° level, 50° North of shaft. 2° .98 4.02 .3. War Eagle No. 1, 100° level, S. drift 3° .52 3.14 .8. War Eagle No. 1, 100° level , S. drift 3° .52 3.14	14 .	30' West of No. 12 shaft, face	2*2*	.20	2.88
.7. War Eagle No. 3, Surface 2' .24 1.42 .8. War Eagle No. 2, 30' shaft 2' .24 1.06 .9. War Eagle No. 2, dump, 8 tons .72 8.80 .0. War Eagle No. 1, 100' level, 160' NW of No. 2 .24 .26 .1. War Eagle No. 2, 100' level, North of No. 1 .60 2.00 .2. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 .23. War Eagle - cut in shaft, 100' level 4' .24 1.66 .4. War Eagle No. 1, 100' level , 5. drift 3' .52 3.14 .55. War Eagle No. 1, cut in North shaft, .52 3.14	15.	25' North of No. 12, surface	30"	.80	3.36
.8. War Eagle No. 2, 30' shaft 2' .24 1.06 .9. War Eagle No. 2, dump, 8 tons .72 8.80 80. War Eagle No. 1, 100' level, 160' NW of No. 2 .24 .26 81. War Eagle No. 2, 100' level, North of No. 1 .60 2.00 82. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 83. War Eagle - cut in shaft, 100' level 4' .24 1.66 94. War Eagle No. 1, 100' level , S. drift 3' .52 3.14 95. War Eagle No. 1, cut in North shaft, 1 1 1	L6.	War Eagle No. 1, 70' level up 20'	3*	•32	4.65
.9. War Eagle No. 2, dump, 8 tons .72 8.80 .0. War Eagle No. 1, 100' level, 160' NW of No. 2 .24 .26 .1. War Eagle No. 2, 100' level, North of No. 1 .60 2.00 .2. War Eagle No. 1, 100' level, 50' North of shaft. .60 2.00 .2. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 .3. War Eagle - cut in shaft, 100' level 4' .24 1.66 .4. War Eagle No. 1, 100' level, 5. drift 3' .52 3.14 .5. War Eagle No. 1, cut in North shaft,	L7.	War Eagle No. 3, Surface	2*	.24	1.42
20. War Eagle No. 1, 100' level, 160' NW of No. 2 .24 .26 21. War Eagle No. 2, 100' level, North of No. 1 .60 2.00 22. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 23. War Eagle - cut in shaft, 100' level 4' .24 1.66 24. War Eagle No. 1, 100' level , S. drift 3' .52 3.14 25. War Eagle No. 1, cut in North shaft, .93 .52 3.14	18.	War Eegle No. 2, 30' shaft	21	.24	1.06
of No. 224 .26 21. War Eagle No. 2, 100' level, North of No. 160 2.00 22. War Eagle No. 1, 100' level, 50' North of shaft. 2' .98 4.02 23. War Eagle - cut in shaft, 100' level 4' .24 1.66 24. War Eagle No. 1, 100' level , S. drift 3' .52 3.14 25. War Eagle No. 1, cut in North shaft,	19.	War Eagle No. 2, dump, 8 tons	***	.72	8.80
No. 1 .60 2.00 No. 1 .60 2.00 No. 1 .60 2.00 No. 1 .98 4.02 No. 1 .98 4.02 No. 1 .98 4.02 No. 1 .00' level 4' .24 No. 1 .00' level .52 3.14 No. 1 .00' level .52 3.14 No. 1 .00. 1 .00th shaft, .52	80.			.84	.26
of shaft. 2' .98 4.02 23. War Eagle - cut in shaft, 100' level 4' .24 1.66 24. War Eagle No. 1, 100' level , S. drift 3' .52 3.14 25. War Eagle No. 1, cut in North shaft,	81.			.60	2.00
4. War Eagle No. 1, 100' level, S. drift 3' .52 3.14 5. War Eagle No. 1, cut in North shaft,	82.		2"	.98	4.02
5. War Eagle No. 1, cut in North shaft,	23.	War Eagle - cut in shaft, 100' level	4°	.24	1.66
	24.	War Eagle No. 1, 100' level , S. drift	3°	.52	3.14
	25.		21	.40	4.90

	LOCATION	WIDTH	AU.	AG.
86 .	War Eagle - discovery shaft	2*	.20	3.10
27.	War Eagle - South tunnel, cut in bottom.	2*	•40	2.64
. 88	War Eagle - South tunnel, cut No. 8	21	.38	2.88
29.	5 tons of ore		1.24	10.14
30.	Grab of dump-War Eagle		.28	2.01
31.	Gladiator shaft dump		.24	1.76
32.	Gladiator tunnel ore dump	-	.20	5.90

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I am not sure that the description of some of these samples has been correctly copied as the photostat is very hard to read; Also I know nothing of the methods by which they were taken.