



CONTACT INFORMATION

Mining Records Curator
Arizona Geological Survey
1520 West Adams St.
Phoenix, AZ 85007
602-771-1601
<http://www.azgs.az.gov>
inquiries@azgs.az.gov

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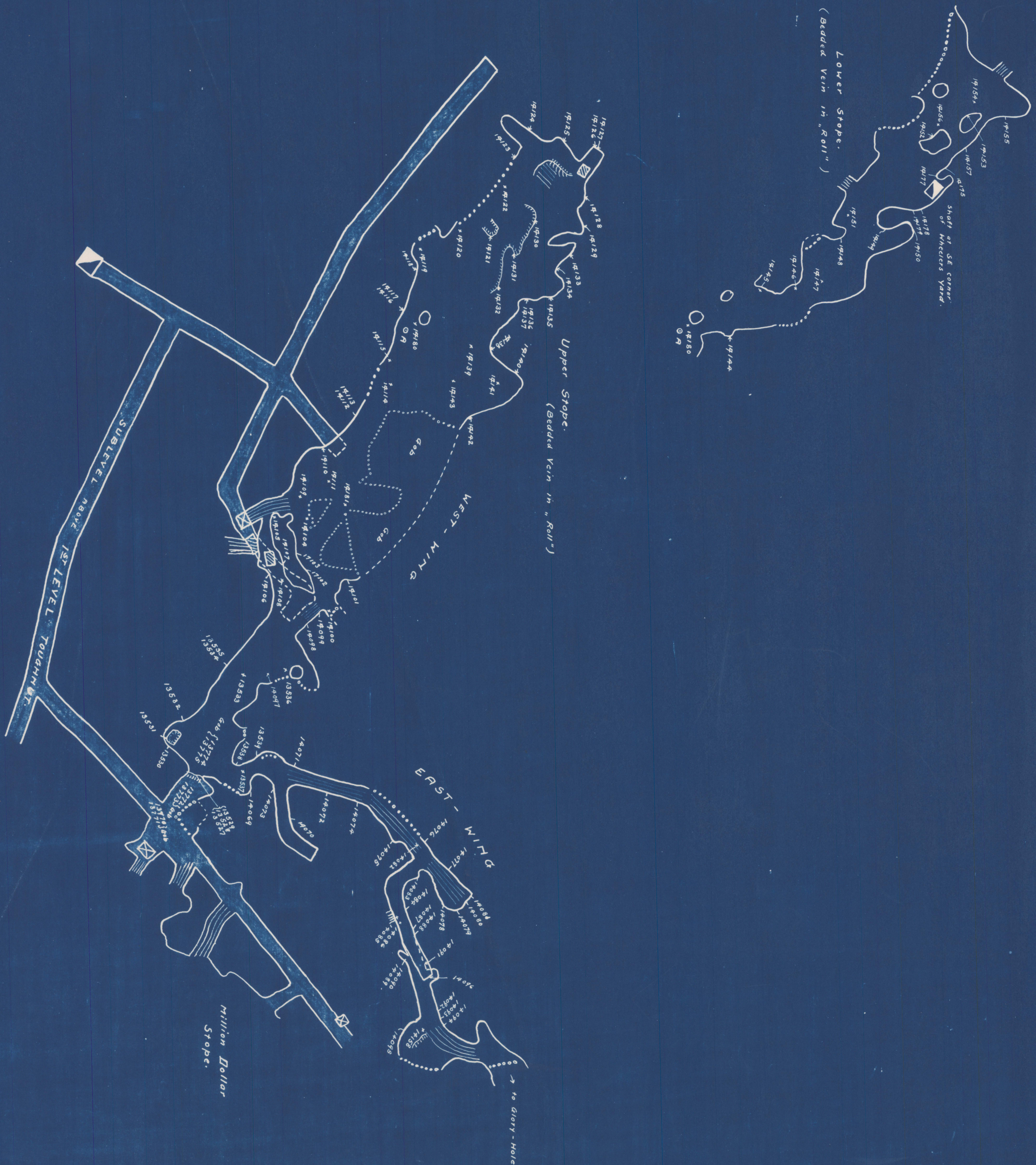
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Sample	Width	Pu. wt	Pg. wt	Pb. %	Cu. %	Mo. %	Wt. %	Description of Sample	Character of Ore
14 069	1"	.42	16.58					Roofing of slope. E. wall	Probably mostly Fe
14 070	10"	.01	1.28					" " " "	" " "
14 071	2"	.18	4.48					" " " "	" " "
14 072	2"	.18	4.48					" " " "	" " "
14 073	1"	.08	3.88					" " " "	" " "
14 074	1"	.20	5.44					" " " "	" " "
14 075	10"	.54	6.64					" " " "	" " "
14 076	5"	.16	4.56					" " " "	" " "
14 077	1"	.06	.06					" " " "	" " "
14 078	1"	.06	.06					" " " "	" " "
14 079	7"	.06	.06					" " " "	" " "
14 080	4"	.06	.06					" " " "	" " "
14 081	6"	.32	.32					" " " "	" " "
14 082	1"	.02	3.24					" " " "	" " "
14 083	1"	.06	8.32					" " " "	" " "
14 084	1"	.06	8.32					" " " "	" " "
14 085	1"	.06	8.32					" " " "	" " "
14 086	1"	.06	8.32					" " " "	" " "
14 087	2"	.10	1.00					" " " "	" " "
14 088	1"	.25	1.07					" " " "	" " "
14 089	5"	.28	2.40					" " " "	" " "
14 090	1"	.88	.88					" " " "	" " "
14 091	3"	.04	1.44					" " " "	" " "
14 092	1"	.01	8.04					" " " "	" " "
14 093	3"	.01	8.04					" " " "	" " "
14 094	10"	.01	8.04					" " " "	" " "
14 095	1"	.01	8.04					" " " "	" " "
14 096	1"	.01	8.04					" " " "	" " "
14 097	1"	.01	8.04					" " " "	" " "
14 098	1"	.01	8.04					" " " "	" " "
14 099	1"	.01	8.04					" " " "	" " "
14 100	5"	.01	1.72					" " " "	" " "
14 101	6"	.01	1.72					" " " "	" " "
14 102	1"	.09	12.80					" " " "	" " "
14 103	6"	.01	6.88					" " " "	" " "
14 104	10"	.06	16.64					" " " "	" " "
14 105	1"	.30	16.50					" " " "	" " "
14 106	1"	.45	5.32					" " " "	" " "
14 107	1"	.46	4.56					" " " "	" " "
14 108	1"	.46	4.56					" " " "	" " "
14 109	8"	.64	.64					" " " "	" " "
14 110	10"	.01	6.00					" " " "	" " "
14 111	1"	.10	3.76					" " " "	" " "
14 112	5"	.01	5.72					" " " "	" " "
14 113	1"	.01	7.00					" " " "	" " "
14 114	6"	.08	22.08					" " " "	" " "
14 115	10"	.07	8.16					" " " "	" " "
14 116	10"	.07	8.16					" " " "	" " "
14 117	10"	.07	8.16					" " " "	" " "
14 118	1"	.01	8.16					" " " "	" " "
14 119	1"	.01	8.16					" " " "	" " "
14 120	7"	.12	18.80					" " " "	" " "
14 121	7"	.12	18.80					" " " "	" " "
14 122	2"	.07	5.20					" " " "	" " "
14 123	5"	.01	2.08					" " " "	" " "
14 124	3"	.14	2.48					" " " "	" " "
14 125	6"	.22	2.64					" " " "	" " "
14 126	6"	.22	2.64					" " " "	" " "
14 127	2"	.01	2.76					" " " "	" " "
14 128	7"	.20	13.36					" " " "	" " "
14 129	3"	.47	16.12					" " " "	" " "
14 130	2"	.11	4.72					" " " "	" " "
14 131	10"	.11	11.72					" " " "	" " "
14 132	2"	.11	11.72					" " " "	" " "
14 133	7"	.14	8.96					" " " "	" " "
14 134	5"	.46	22.84					" " " "	" " "
14 135	3"	.26	2.68					" " " "	" " "
14 136	5"	.184	1.84					" " " "	" " "
14 137	1"	.12	2.84					" " " "	" " "
14 138	1"	.12	53.08					" " " "	" " "
14 139	10"	.06	1.36					" " " "	" " "
14 140	6"	.06	5.64					" " " "	" " "
14 141	10"	.07	8.16					" " " "	" " "
14 142	5"	.07	22.40					" " " "	" " "
14 143	6"	.17	18.00					" " " "	" " "
14 144	1"	.17	18.00					" " " "	" " "
14 145	1"	.17	18.00					" " " "	" " "
14 146	3"	.02	2.72					" " " "	" " "
14 147	3"	.02	2.72					" " " "	" " "
14 148	4"	.62	22.38					" " " "	" " "
14 149	10"	.58	113.30					" " " "	" " "
14 150	1"	.07	2.72					" " " "	" " "
14 151	3"	.12	2.72					" " " "	" " "
14 152	1"	.03	2.72					" " " "	" " "
14 153	2"	.07	22.40					" " " "	" " "
14 154	1"	.04	2.48					" " " "	" " "
14 155	2"	.06	40.78					" " " "	" " "
14 156	5"	.03	4.80					" " " "	" " "
14 157	1"	.03	4.80					" " " "	" " "
14 158	1"	.01	1.44					" " " "	" " "
14 159	10"	.02	3.84					" " " "	" " "
14 160	10"	.02	3.84					" " " "	" " "
14 161	10"	.02	3.84					" " " "	" " "
14 162	10"	.02	3.84					" " " "	" " "
14 163	10"	.02	3.84					" " " "	" " "
14 164	10"	.02	3.84					" " " "	" " "
14 165	10"	.02	3.84					" " " "	" " "
14 166	10"	.02	3.84					" " " "	" " "
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14 169	10"	.02	3.84					" " " "	" " "
14 170	10"	.02	3.84					" " " "	" " "
14 171	10"	.02	3.84					" " " "	" " "
14 172	10"	.02	3.84					" " " "	" " "
14 173	10"	.02	3.84					" " " "	" " "
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14 178	10"	.02	3.84					" " " "	" " "
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14 182	10"	.02	3.84					" " " "	" " "
14 183	10"	.02	3.84					" " " "	" " "
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14 185	10"	.02	3.84					" " " "	" " "
14 186	10"	.02	3.84					" " " "	" " "
14 187	10"	.02	3.84					" " " "	" " "
14 188	10"	.02	3.84					" " " "	" " "
14 189	10"	.02	3.84					" " " "	" " "
14 190	10"	.02	3.84					" " " "	" " "
14 191	10"	.02	3.84					" " " "	" " "
14 192	10"	.02	3.84					" " " "	" " "
14 193	10"	.02	3.84					" " " "	" " "
14 194	10"	.02	3.84					" " " "	" " "
14 195	10"	.02	3.84					" " " "	" " "
14 196	10"	.02	3.84					" " " "	" " "
14 197	10"	.02	3.84					" " " "	" " "
14 198	10"	.02	3.84					" " " "	" " "
14 199	10"	.02	3.84					" " " "	" " "
14 200	10"	.02	3.84					" " " "	" " "



ASSAY-MAP
TOUGHNUT MINE
STOPE UNDER WHEELER'S HOUSE =
NORTH - WEST-END OF MILLION-DOLLAR-STOPE.
SCALE: 1"=25'

ASME 0148-095

№ of sample	width	Ru g	Ag g	Pb %	Cu %	Total Wnd	Description of Sample	Character of Ore
16 276	—	5"	0.08	28.44		15.50	Northwall of Stope	Base-(Somehow)-ore
16 277	1' 6"	0.16	30.60			18.50	" " " top	Irony, possibly, sulphur
16 278	2' 5"	0.06	11.76			18.50	" " " bottom	Irony, possibly, sulphur
16 279	2' 8"	0.01	1.72			17.55	Roof " "	to Cyanide - Treatment
16 280	3' —	0.10	31.12				Roof " "	
16 281	1' —	0.08	12.30				Westwall of Pillar	
16 282	1' 3"	0.02	4.66				" "	
16 283	1' 6"	0.03	17.68				Roof of Stope	
16 284	2' 8"	0.08	17.68			9.45	Southwall Drift East	
16 285	1' 6"	0.01	1.04				" "	
16 286	—	0.03	3.80				Northwall " "	
16 287	1' 4"	0.07	12.72				Roof " "	
16 288	1' 1"	0.01	0.72				Southwall " "	
16 289	2' 10"	0.02	3.18				Roof " "	
16 290	3' 4"	0.01	1.16				Northwall of Stope at end	
16 291	1' 2"	0.02	2.48				Southwall Drift East	
16 292	1' 3"	0.02	35.86			24.00	Roof " "	
16 293	2' 8"	0.05	12.24			7.10	Southwall " "	
16 294	2' 4"	0.18	13.02			64.00	Northwall " "	
16 295	2' 10"	0.03	1.16				Southwall " "	
16 296	3' 4"	0.01	2.20				Roof " "	
16 297	2' —	0.01	2.20				Northwall " "	
16 298	1' 6"	0.01	1.52				Roof " "	
16 299	2' 6"	0.10	31.84			17.90	SW corner of Pillar	
16 300	2' 9"	0.05	4.80			6.75	Southwall " "	
16 301	8"	0.06	11.16			17.80	Eastwall of Stope	
16 302	1' —	0.09	32.04				" "	
16 303	1' —	0.05	6.88				" "	
16 304	3' 10"	0.01	0.84				Northwall of Pillar	
16 305	1' 10"	0.04	0.52				" "	
16 306	1' 4"	0.03	2.22				Roof " "	
16 307	1' 4"	0.02	25.83			14.35	Eastwall of Stope	
16 308	1' 6"	0.06	32.12			17.25	" "	
16 309	1' 6"	0.06	11.96			7.20	" "	
16 310	1' 8"	0.16	30.80			18.60	Southside of Pillar	
16 311	—	0.04	2.16			9.25	" "	
16 312	3' 6"	0.12	17.20			11.00	" "	
16 313	2' 4"	0.09	40.20			54.00	" "	
16 314	1' 3"	0.01	0.68			22.00	" "	
16 315	2' 6"	0.04	9.76				Roof of Pillar	
16 316	3' 5"	0.08	4.72				Eastwall of Stope	
16 317	2' 6"	0.10	13.20			12.55	" "	
16 318	2' 6"	0.04	2.12			7.50	" "	
16 319	1' 4"	0.07	22.32			12.70	" "	
16 320	1' 4"	0.08	11.84				" "	
16 321	1' 4"	0.08	22.20				" "	
16 322	1' 4"	0.08	3.46				" "	
16 323	1' 4"	0.08	0.52				" "	
16 324	1' 4"	0.08	11.00				" "	
16 325	1' 4"	0.08	13.84				" "	
16 326	1' 4"	0.08	13.84				" "	
16 327	1' 4"	0.08	13.84				" "	
16 328	1' 4"	0.08	13.84				" "	
16 329	1' 4"	0.08	13.84				" "	
16 330	1' 4"	0.08	13.84				" "	
16 331	1' 4"	0.08	13.84				" "	
16 332	1' 4"	0.08	13.84				" "	
16 333	1' 4"	0.08	13.84				" "	
16 334	1' 4"	0.08	13.84				" "	
16 335	1' 4"	0.08	13.84				" "	
16 336	1' 4"	0.08	13.84				" "	
16 337	1' 4"	0.08	13.84				" "	
16 338	1' 4"	0.08	13.84				" "	
16 339	1' 4"	0.08	13.84				" "	
16 340	1' 4"	0.08	13.84				" "	
16 341	1' 4"	0.08	13.84				" "	
16 342	1' 4"	0.08	13.84				" "	
16 343	1' 4"	0.08	13.84				" "	
16 344	1' 4"	0.08	13.84				" "	
16 345	1' 4"	0.08	13.84				" "	
16 346	1' 4"	0.08	13.84				" "	
16 347	1' 4"	0.08	13.84				" "	
16 348	1' 4"	0.08	13.84				" "	
16 349	1' 4"	0.08	13.84				" "	
16 350	1' 4"	0.08	13.84				" "	
16 351	1' 4"	0.08	13.84				" "	
16 352	1' 4"	0.08	13.84				" "	
16 353	1' 4"	0.08	13.84				" "	
16 354	1' 4"	0.08	13.84				" "	
16 355	1' 4"	0.08	13.84				" "	
16 356	1' 4"	0.08	13.84				" "	
16 357	1' 4"	0.08	13.84				" "	
16 358	1' 4"	0.08	13.84				" "	
16 359	1' 4"	0.08	13.84				" "	
16 360	1' 4"	0.08	13.84				" "	
16 361	1' 4"	0.08	13.84				" "	
16 362	1' 4"	0.08	13.84				" "	
16 363	1' 4"	0.08	13.84				" "	
16 364	1' 4"	0.08	13.84				" "	
16 365	1' 4"	0.08	13.84				" "	
16 366	1' 4"	0.08	13.84				" "	
16 367	1' 4"	0.08	13.84				" "	
16 368	1' 4"	0.08	13.84				" "	
16 369	1' 4"	0.08	13.84				" "	
16 370	1' 4"	0.08	13.84				" "	
16 371	1' 4"	0.08	13.84				" "	
16 372	1' 4"	0.08	13.84				" "	
16 373	1' 4"	0.08	13.84				" "	
16 374	1' 4"	0.08	13.84				" "	
16 375	1' 4"	0.08	13.84				" "	
16 376	1' 4"	0.08	13.84				" "	
16 377	1' 4"	0.08	13.84				" "	
16 378	1' 4"	0.08	13.84				" "	
16 379	1' 4"	0.08	13.84				" "	
16 380	1' 4"	0.08	13.84				" "	
16 381	1' 4"	0.08	13.84				" "	
16 382	1' 4"	0.08	13.84				" "	
16 383	1' 4"	0.08	13.84				" "	
16 384	1' 4"	0.08	13.84				" "	
16 385	1' 4"	0.08	13.84				" "	
16 386	1' 4"	0.08	13.84				" "	
16 387	1' 4"	0.08	13.84				" "	
16 388	1' 4"	0.08	13.84				" "	
16 389	1' 4"	0.08	13.84				" "	
16 390	1' 4"	0.08	13.84				" "	
16 391	1' 4"	0.08	13.84				" "	
16 392	1' 4"	0.08	13.84				" "	
16 393	1' 4"	0.08	13.84				" "	
16 394	1' 4"	0.08	13.84				" "	
16 395	1' 4"	0.08	13.84				" "	
16 396	1' 4"	0.08	13.84				" "	
16 397	1' 4"	0.08	13.84				" "	
16 398	1' 4"	0.08	13.84				" "	
16 399	1' 4"	0.08	13.84				" "	
16 400	1' 4"	0.08	13.84				" "	



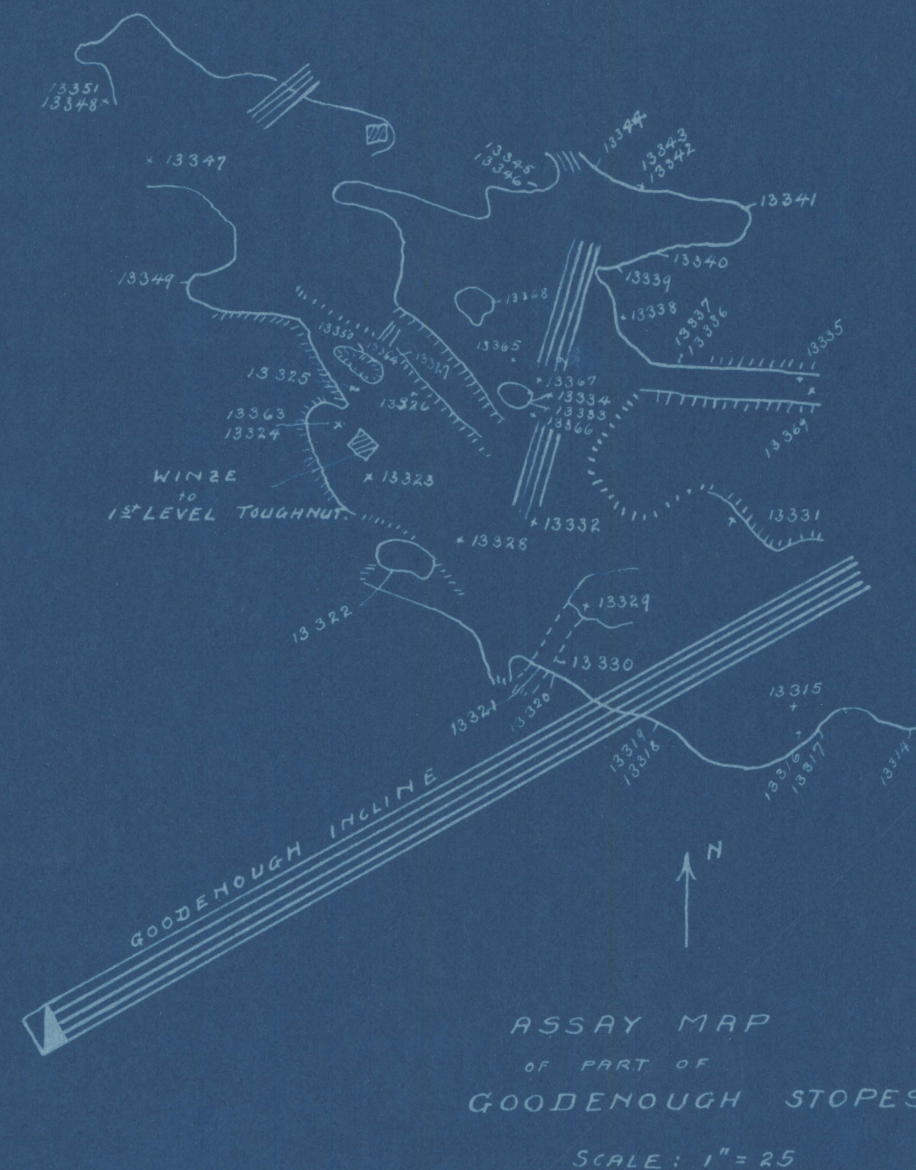
ASSAY - MAP
 OF PART OF
 NORTH-WEST STOPES
 OF
 TOUGHNUT MINE
 BETWEEN
 1ST LEVEL & SURFACE
 SCALE: 1" = 25'

ADMP 2148-0816

Sample No.	Wt. %	Au. %	Ag. %	Pb. %	Cu. %	Vol. %	Description of Sample	Character of Ore
17791	3	1.8	2.84	1.84	5.02	5.02	Million Dollar Sp. Roof	Mt. Roph + Lime
17792	—	8	3.05	3.4	1.74	1.74	"	"
17793	—	8	3.05	3.4	20.62	20.62	"	"
17794	2	6	1.04	80	1.20	1.20	"	"
17795	2	2	1.04	114.04	2.32	2.32	"	"
17796	1	10	.02	17.98	2.30	2.30	"	"
17797	1	9	.08	17.98	10.34	10.34	"	"
17798	1	3	.08	9.60	6.40	6.40	"	"
17799	—	—	1.08	9.60	5.40	5.40	"	"
17800	3	—	.08	9.60	6.40	6.40	"	"
17801	"	"	.03	4.76	5.40	5.40	Screenings 691, 713	"
17802	"	"	.03	4.76	5.40	5.40	Screenings 691, 713	"
17803	"	"	.01	10.08	5.24	5.24	Screenings 691, 713	"
17804	"	"	.04	9.00	5.30	5.30	Screenings 691, 713	"
17805	"	"	.17	19.64	3.22	3.22	Screenings 691, 713	"
17806	"	"	1.70	3.40	1.70	1.70	Screenings 691, 713	"
17807	"	"	9.48	7.64	5.24	5.24	Mt. Bull. St. bul. #1778	Mt. Roph + Lime
17808	"	"	1.04	7.64	2.90	2.90	Screenings 1778	"
17809	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17810	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17811	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17812	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17813	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17814	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17815	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17816	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17817	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17818	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17819	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17820	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17821	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17822	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17823	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17824	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17825	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17826	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17827	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17828	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17829	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17830	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17831	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17832	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17833	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17834	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17835	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17836	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17837	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17838	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17839	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17840	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17841	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17842	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17843	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17844	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17845	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17846	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17847	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17848	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17849	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17850	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17851	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17852	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17853	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17854	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17855	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17856	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17857	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17858	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17859	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17860	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17861	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17862	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17863	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17864	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17865	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17866	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17867	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17868	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17869	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17870	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17871	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17872	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17873	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17874	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17875	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17876	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17877	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17878	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17879	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17880	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17881	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17882	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17883	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17884	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17885	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17886	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17887	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17888	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17889	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17890	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17891	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17892	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17893	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17894	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17895	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17896	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17897	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17898	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17899	"	"	.01	5.40	2.90	2.90	Screenings 1778	"
17900	"	"	.01	5.40	2.90	2.90	Screenings 1778	"

No. Sample	Width "	Alt. Oz	Ag. Oz	Pb %	Cu %	Value	Description of Sample
17 657	11	6	—	—	—	40	Back near pillar
17 658	11	10	—	—	—	30	Walled back near pillar
17 659	11	3	—	—	—	30	Back of Sub drift
17 660	11	5	—	—	—	30	Back of Sub drift
17 661	11	10	—	—	—	30	Back of Sub drift
17 662	11	6	—	—	—	30	Back of Sub drift
17 663	11	10	—	—	—	30	Back of Sub drift
17 664	11	10	—	—	—	30	Back of Sub drift
17 665	11	10	—	—	—	30	Back of Sub drift
17 666	11	10	—	—	—	30	Back of Sub drift
17 667	11	10	—	—	—	30	Back of Sub drift
17 668	11	10	—	—	—	30	Back of Sub drift
17 669	11	10	—	—	—	30	Back of Sub drift
17 670	11	10	—	—	—	30	Back of Sub drift
17 671	11	10	—	—	—	30	Back of Sub drift
17 672	11	10	—	—	—	30	Back of Sub drift
17 673	11	10	—	—	—	30	Back of Sub drift
17 674	11	10	—	—	—	30	Back of Sub drift
17 675	11	10	—	—	—	30	Back of Sub drift
17 676	11	10	—	—	—	30	Back of Sub drift
17 677	11	10	—	—	—	30	Back of Sub drift
17 678	11	10	—	—	—	30	Back of Sub drift
17 679	11	10	—	—	—	30	Back of Sub drift
17 680	11	10	—	—	—	30	Back of Sub drift
17 681	11	10	—	—	—	30	Back of Sub drift
17 682	11	10	—	—	—	30	Back of Sub drift
17 683	11	10	—	—	—	30	Back of Sub drift
17 684	11	10	—	—	—	30	Back of Sub drift
17 685	11	10	—	—	—	30	Back of Sub drift
17 686	11	10	—	—	—	30	Back of Sub drift
17 687	11	10	—	—	—	30	Back of Sub drift
17 688	11	10	—	—	—	30	Back of Sub drift
17 689	11	10	—	—	—	30	Back of Sub drift
17 690	11	10	—	—	—	30	Back of Sub drift
17 691	11	10	—	—	—	30	Back of Sub drift
17 692	11	10	—	—	—	30	Back of Sub drift
17 693	11	10	—	—	—	30	Back of Sub drift
17 694	11	10	—	—	—	30	Back of Sub drift
17 695	11	10	—	—	—	30	Back of Sub drift
17 696	11	10	—	—	—	30	Back of Sub drift
17 697	11	10	—	—	—	30	Back of Sub drift
17 698	11	10	—	—	—	30	Back of Sub drift
17 699	11	10	—	—	—	30	Back of Sub drift
17 700	11	10	—	—	—	30	Back of Sub drift
17 701	11	10	—	—	—	30	Back of Sub drift
17 702	11	10	—	—	—	30	Back of Sub drift
17 703	11	10	—	—	—	30	Back of Sub drift
17 704	11	10	—	—	—	30	Back of Sub drift
17 705	11	10	—	—	—	30	Back of Sub drift
17 706	11	10	—	—	—	30	Back of Sub drift
17 707	11	10	—	—	—	30	Back of Sub drift
17 708	11	10	—	—	—	30	Back of Sub drift
17 709	11	10	—	—	—	30	Back of Sub drift
17 710	11	10	—	—	—	30	Back of Sub drift
17 711	11	10	—	—	—	30	Back of Sub drift
17 712	11	10	—	—	—	30	Back of Sub drift
17 713	11	10	—	—	—	30	Back of Sub drift
17 714	11	10	—	—	—	30	Back of Sub drift
17 715	11	10	—	—	—	30	Back of Sub drift
17 716	11	10	—	—	—	30	Back of Sub drift
17 717	11	10	—	—	—	30	Back of Sub drift
17 718	11	10	—	—	—	30	Back of Sub drift
17 719	11	10	—	—	—	30	

N ^o of Sample	Width	Au. oz.	Ag. oz.	Pb. %	Cu. %	Total Value	Description of Sample	Character of Ore
13 314	1' —	0.04	13.00			7.30	South Wall of Stope	Smelting - Ore
13 315	1' 3"	0.04	9.40			5.50	Roof "	perhaps amenable
13 316	— 6"	0.04	3.40				South Wall top "	to Cyanidization
13 317	— 7"	0.04	18.12			9.85	" bottom "	
13 318	— 10"	0.02	39.04			19.90	" top "	
13 319	— 9"	0.04	9.72			5.65	" bottom "	
13 320	— 8"	0.01	2.76				" top "	
13 321	— 6"	0.02	21.48			11.15	" bottom "	
13 322	— 10"	0.01	60.12			30.25	Pillar in "	
13 323	— 5"	0.02	9.20			5.00	Roof of "	
13 324	2' 6"	0.04	10.20			5.90	South Wall "	
13 325	— 2"	0.04	26.40			14.00	Roof "	
13 326	— 3"	0.01	2.00				" "	
13 327	— 11"	0.01	0.40				North Wall "	
13 328	1' 4"	0.01	4.56				Floor "	
13 329	2' 9"	0.01	0.88				Roof of Pit	
13 330	1' 1"	0.01	2.08				East Wall Drift below Stope	
13 331	2' —	0.01	12.36			6.40	North Wall of Stope	
13 332	— 4"	0.02	7.04			3.90	Roof "	
13 333	1' 1"	0.01	0.94				Pillar top	
13 334	1' —	0.01	1.44				" bottom	
13 335	1' 1"	0.01	1.06				Roof of Drift	
13 336	— 6"	0.01	7.28			3.85	North Wall top of Drift	
13 337	2' 7"	0.01	2.00				" bottom "	
13 338	— 9"	0.37	2.39			8.60	East Wall of Stope	
13 339	1' 4"	0.01	1.16				" "	
13 340	2' 10"	0.01	1.80				" "	
13 341	2' 1"	0.02	4.20				North Wall "	
13 342	1' —	0.01	0.44				" top "	
13 343	2' 10"	0.01	0.50				" bottom "	
13 344	3' 6"	0.01	1.04				" "	
13 345	2' 8"	0.02	1.36				" bottom "	
13 346	2' 2"	0.02	1.72				" top "	
13 347	— 10"	0.02	4.32				South Wall "	
13 348	1' 8"	0.01	0.40				" "	
13 349	— 11"	0.04	8.50			5.05	" "	
13 350	2' 9"	0.02	13.08			6.95	Wall of Raise	
13 351	1' 6"	0.01	1.04				South Wall at 13 348	
13 363	— 6"	0.02	21.64			11.20	Roof of Stope	
13 364	— 5"	0.01	8.40			4.40	Hall below * 13350	
13 365	— 2"	0.03	50.96			26.10	Roof of Stope	
13 366	1' —	0.01	0.32				Wall above * 13333	
13 367	1' 8"						" " 13 366	
13 368	2' —	0.01	3.00				Pillar in Stope	
13 369	1' —	0.01	1.40				Roof of Drift at 13335	



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No Sample	Width "	Au oz	Ag oz	Pb %	Cu %	Ten %	Description of Sample	Character of Ore
16.513	1' 5"	0.02	2.76				Northwell Hole #122	Copper-strewn
16.514	1' 6"	0.04	4.84				Southwell "	Smelting Ore
16.515	3' -	0.03	4.12				Roof Intermediate Drift	perhaps partly lime
16.516	2' 4"	0.04	15.60			8.60	Northwell "	pyrite
16.517	1' 8"	0.05	6.30				Roof "	Cyanidation
16.518	3' 4"	0.07	18.76			10.40	" "	"
16.519	4' 12"	0.09	13.72			8.15	Northwell "	"
16.520	3' -	0.06	14.40			3.40	Southwell "	"
16.521	1' 6"	0.13	30.36			17.80	Northwell "	"
16.522	2' 10"	-					Southwell "	"
16.523	1' 6"	0.08	28.68			16.00	" "	"
16.524	1' 6"	0.08	28.68				East end small slope	"
16.525	- 7"	0.48	72.68			42.00	Roof Intermediate Drift	"
16.526	1' 4"	0.04	21.12			11.40	Northwell bottom below 3th	"
16.527	1' 6"	0.04	6.70				" "	"
16.528	1' 2"	0.01	2.40				" Intermediate Drift	"
16.529	- 6"	0.06	7.36				" "	"
16.530	-	0.02	13.60				N.W. cross corner 2nd L.	Cu
16.531	1' 8"	0.02	13.60				Roof Intermediate Drift	Cu
16.532	3' 9"	0.02	4.24				" Small Drift	Cu
16.533	1' 8"	0.02	2.64				Southwell "	Cu
16.534	- 4"	0.02	60.72			32.00	Roof "	Cu
16.535	1' 10"	0.02	31.40				Southwell Intermediate drift	Cu
16.536	- 10"	0.03	38.72			21.00	" "	Cu
16.537	1' 6"	0.03	12.40				Roof "	Cu
16.538	1' 1"	-	16.24				Southwell "	Cu
16.539	1' 10"	0.03	27.20			9.70	East end small incline	Cu
16.540	2' 4"	0.06	4.24			14.80	Roof 2nd level drift	Cu
16.541	1' -	0.02	4.24				Roof 2nd level drift	Cu
16.542	1' 8"	0.08	42.76			23.00	Southwell bottom below 3th	Cu
16.543	- 10"	0.06	42.80			22.20	Northwell small incline	Cu
16.544	1' 2"	0.04	16.76			9.20	Roof "	Cu
16.545	- 10"	0.04	74.24			40.40	Roof "	Cu
16.546	1' 4"	0.05	14.48			8.85	Roof "	Cu
16.547	1' 4"	0.03	6.52			10.40	Northwell bottom below 3th	Cu
16.548	2' 6"	0.07	43.08			3.85	Roof "	Cu
16.549	1' 6"	0.03	12.40			23.30	Roof "	Cu
16.550	- 10"	0.03	12.40				Roof "	Cu
16.551	1' 6"	0.03	12.40				Roof "	Cu
16.552	1' 6"	0.03	12.40				Roof "	Cu
16.553	1' 6"	0.03	12.40				Roof "	Cu
16.554	1' 1"	-	16.24				Roof "	Cu
16.555	1' 10"	0.03	27.20				Roof "	Cu
16.556	2' 4"	0.06	4.24				Roof "	Cu
16.557	1' -	0.02	4.24				Roof "	Cu
16.558	1' 8"	0.08	42.76				Roof "	Cu
16.559	- 10"	0.06	42.80				Roof "	Cu
16.560	1' 2"	0.04	16.76				Roof "	Cu
16.561	- 10"	0.04	74.24				Roof "	Cu
16.562	1' 4"	0.05	14.48				Roof "	Cu
16.563	1' 4"	0.03	6.52				Roof "	Cu
16.564	2' 6"	0.07	43.08				Roof "	Cu
16.565	1' 6"	0.03	12.40				Roof "	Cu
16.566	1' 6"	0.03	12.40				Roof "	Cu
16.567	- 10"	0.03	12.40				Roof "	Cu
16.568	1' 7"	0.04	2.24				Roof "	Cu
16.569	2' 1"	0.02	4.24				Roof "	Cu
16.570	2' -	0.02	4.24				Roof "	Cu
16.571	2' 3"	0.02	1.6				Roof "	Cu
16.572	3' 3"	0.02	2.36				Roof "	Cu
16.573	4' 5"	0.01	0.60				Roof "	Cu
16.574	1' 5"	0.01	1.04				Roof "	Cu
16.575	3' 4"	0.01	0.24				Roof "	Cu
16.576	3' 4"	-	0.12				Roof "	Cu
16.577	3' 4"	-	0.12				Roof "	Cu
16.578	2' 6"	0.01	1.80				Roof "	Cu
16.579	3' 8"	0.01	1.96				Roof "	Cu
16.580	4' 3"	0.02	14.20				Roof "	Cu
16.581	1' -	0.02	2.40				Roof "	Cu
16.582	5' 5"	0.01	1.40				Roof "	Cu
16.583	1' 6"	0.05	7.52				Roof "	Cu
16.584	2' -	0.02	6.20				Roof "	Cu
16.585	2' -	0.03	8.40				Roof "	Cu
16.586	2' -	0.03	8.40				Roof "	Cu



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